

SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA — RÉPUBLIQUE SOCIALISTE FÉDÉRATIVE DE YUGOSLAVIE  
HIDROMETEOROLŠKA SLUŽBA — SERVICE HYDRO-MÉTÉOROLOGIQUE

---

# METEOROLOŠKI GODIŠNjak I

## ANNUAIRE METEOROLOGIQUE I

GODINA 1974 ANNÉE

QC  
989  
.Y8  
M48  
1974



LIBRARY

APR 2000

Federal Meteorological  
Administration  
U.S. Dept. of Commerce

---

IZDANJE SAVEZNOG HIDROMETEOROLOŠKOG ZAVODA  
PUBLIÉ PAR L'INSTITUT HYDROMÉTÉOROLOGIQUE FÉDÉRAL  
B E O G R A D

**National Oceanic and Atmospheric Administration**

**Environmental Data Rescue Program**

**ERRATA NOTICE**

One or more conditions of the original document may affect the quality of the image, such as:

Discolored pages  
Faded or light ink  
Binding intrudes into the text

This document has been imaged through the NOAA Environmental Data Rescue Program. To view the original document, please contact the NOAA Central Library in Silver Spring, MD at (301) 713-2607 x124 or [www.reference@nodc.noaa.gov](mailto:www.reference@nodc.noaa.gov).

Information Manufacturing Corporation  
Imaging Subcontractor  
Rocket Center, West Virginia  
September 14, 1999

S A D R Ž A J

Strana

Objašnjenja

Azbučni spisak meteoroloških stanica .....	I
A) Dnevna osmatranja .....	1
B) Mesečni i godišnji pregled .....	99

TABLE DES MATIERES

	Pages
Notice explicative	
Liste alphabétique des stations météorologiques	I
A) Observations journalières .....	1
B) Revue mensuelle et annuelle .....	99

## O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljaju se podaci 8 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelashnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

$\varphi$  = geografska širina,  $\lambda$  = geografska dužina od Griniča,  $\Delta G$  vremenska razlika u odnosu na Grinič,  $H_s$  = nadmorska visina podnožja termometarskog zaklona,  $H_b$  = nadmorska visina rezervoara barometra,  $h_t$  = visina rezervoara termometra iznad tla,  $h_r$  = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebљene prema medjunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

$P$  = vazdušni pritisak u mm visine živinog stuba, reducirane na  $0^{\circ}\text{C}$ ;  $T$  = temperatura u  $^{\circ}\text{C}$ ;  $e$  = pritisak vodene pare u mm visine živinog stuba;  $U$  = relativna vlažnost u procentima;  $D$  = pravac vetra po ruži vetra od 16 ili 8 pravaca;  $F$  = jačina vetra po Boforovoj skali (0-12);  $v$  = brzina vetra u m/sek;  $V$  = vidljivost u km;  $N$  = oblačnost (0-10); insola - cija = trajanje osunčavanja u satima;  $R$  = padavine u mm;  $R_s$  = padavine u mm;  $h_s$  = snežni pokrivač u cm;  $W$  = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan medjunarodnim simbolima.

U rubrici "razvoj vremena" su potrebljene ove skraćenice:

$n$  = u toku noći;  $a$  = pre podne;  $p$  = posle podne;  $i$  = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente ( $P$ ,  $e$ ,  $U$ ,  $N$ ) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su čitavani i uredjivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebљene su oznake  $M_{\overline{ax}}$  i  $M_{\overline{in}}$ ; za rubrike broj dana sa • ili •, ✕ ili  $\Delta$ , i  $\not\Delta$  prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Ažbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1974. godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

## NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

$\varphi$  = latitude,  $\lambda$  = longitude E de Greenwich,  $\Delta G$  = différence entre l'heure locale et l'heure de Greenwich,  $h_s$  = altitude du pied de l'abri météorologique,  $h_b$  = altitude de la ouverte du baromètre,  $h_t$  = hauteur, au-dessus du sol, du réservoir du thermomètre,  $h_r$  = hauteur, au-dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

$P$  = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à  $0^{\circ}\text{C}$ );  $T$  = température en  $^{\circ}\text{C}$ ;  $e$  = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure;  $U$  = humidité relative en %;  $D$  = direction du vent en rose des vents de 8 ou de 16 directions;  $F$  = force du vent d'après l'échelle Beaufort (0-12);  $v$  = vitesse du vent en m/s;  $V$  = visibilité en km;  $N$  = nébulosité (0-10); insolation = durée d'insolation en heures;  $R$  = précipitations en mm;  $h_s$  = épaisseur de la couche de neige en cm;  $W$  = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Kazvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

$n$  = pendant la nuit;  $a$  = avant midi;  $p$  = après midi;  $i$  = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4},$$

et pour les autres éléments ( $F$ ,  $e$ ,  $U$ ,  $N$ ) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faits à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent  $F \geq 6$  (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications  $M_{\overline{ax}}$  et  $M_{\overline{in}}$  ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) • ou , , \* ou △, et × sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1974; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

A Z B U Č N I S P I S A K G T A N I C A  
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

I

A Z B U Ć N I S P I N J A K S T A N I C A  
PO SOČIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

II

S T A N I C A	Broj stanice 2	Nadmorska visina H, m. 3	Geografska širina φ, °N 4	Geografska dužina λ, °E Gr. 5	Pođ t e stanice	Vrednost prištak 7	Temperatura vazduha 8	Vlažnost vazduha 9	Vetar 10	Oblakost 11	Iznoslacija 12	Padavine 13	Broj karak- terističnih dodata 14
1													
Cres	76	10	44°59'	14°24'	ob		x	x	x	x	x	x	x
Crikvenica	49	2	45 10	14 42	ob		x	x	x	x	x	x	x
Čazma	62	144	45 45	16 38	ob		x	x	x	x	x	x	x
Beruvar	66	161	45 36	17 14	gl	x	x	x	x	x	x	x	x
Bonji Meljani	67	120	45 44	17 38	ob		x	x	x	x	x	x	x
Donji Miholjac	70	97	45 46	18 10	ob		x	x	x	x	x	x	x
Dubrovnik	100	49	42 39	18 06	ob		x	x	x	x	x	x	x
Djakovo	71	98	45 17	18 25	ob		x	x	x	x	x	x	x
Gospic	84	564	44 33	15 22	gl	x	x	x	x	x	x	x	x
Gračac	85	560	44 18	15 51	ob		x	x	x	x	x	x	x
Hvar	90	20	43 10	16 27	gl	x	x	x	x	x	x	x	x
Illok	74	133	45 14	19 23	ob		x	x	x	x	x	x	x
Karlovac	53	112	45 30	15 33	ob	x	x	x	x	x	x	x	x
Knin	86	234	44 02	16 12	ob	x	x	x	x	x	x	x	x
Komiža	88	6	43 03	16 05	ob		x	x	x	x	x	x	x
Koprivnica	43	141	46 11	16 49	ob		x	x	x	x	x	x	x
Korčula	97	15	42 58	17 09	ob		x	x	x	x	x	x	x
Kostel	40	270	46 11	15 45	ob		x	x	x	x	x	x	x
Križevci	42	155	46 02	16 33	ob	x	x	x	x	x	x	x	x
Lastovo	96	186	42 46	16 54	gl	x	x	x	x	x	x	x	x
Lidčko Lešće	83	463	44 48	15 19	ob		x	x	x	x	x	x	x
Lipik	65	154	45 25	17 10	ob		x	x	x	x	x	x	x
Makarska	92	2	43 18	17 01	ob		x	x	x	x	x	x	x
Mali Lošinj	77	53	44 32	14 28	gl	x	x	x	x	x	x	x	x
Ogulin	52	328	45 16	15 14	gl	x	x	x	x	x	x	x	x
Opuzen	93	2	43 01	17 34	ob		x	x	x	x	x	x	x
Orebic	98	6	42 58	17 10	ob		x	x	x	x	x	x	x
Osijek	73	89	45 32	18 44	gl	x	x	x	x	x	x	x	x
Pag	81	3	44 27	15 04	ob		x	x	x	x	x	x	x
Palagruž	94	98	42 24	16 16	ob	x	x	x	x	x	x	x	x
Parg	48	863	45 36	14 38	ob	x	x	x	x	x	x	x	x
Pazin	46	291	45 14	13 56	ob	x	x	x	x	x	x	x	x
Poreč	44	15	45 14	13 36	ob		x	x	x	x	x	x	x
Pula	75	30	44 52	13 51	ob		x	x	x	x	x	x	x
Puntijarka	55	988	45 55	15 58	gl	x	x	x	x	x	x	x	x
Rab	78	24	44 45	14 46	ob	x	x	x	x	x	x	x	x
Rijeka	47	104	45 20	14 27	ob	x	x	x	x	x	x	x	x
Rovinj	45	5	45 05	13 39	ob		x	x	x	x	x	x	x
Senj	79	26	44 59	14 54	gl	x	x	x	x	x	x	x	x
Sinj	91	308	43 43	16 40	ob		x	x	x	x	x	x	x
Sisak	61	93	45 30	16 23	ob	x	x	x	x	x	x	x	x
Škrad	51	675	45 26	14 59	ob		x	x	x	x	x	x	x
Sl. Požega	68	152	45 20	17 41	ob		x	x	x	x	x	x	x
Sl. kroc	69	88	45 10	18 00	gl	x	x	x	x	x	x	x	x
Slunji	54	258	45 07	15 35	ob		x	x	x	x	x	x	x

A Z B U Č N I S P I S A K S T A N I C A  
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteorooloških elemenata navedenih u kolonama 7-14.

III

AKTUVČNI SFIŠSAK STANICA  
PO SOCIJALISTIČKIM AC. UBLJEDAM

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A 1	Broj stanice 2	Nadmorska visina H.m 3	Geografska širina lat. 4	Geografska dužina lon. 5	Red stanice 6	Vrednost pritisak atmosfera 7	Temperatura vazduha 8	Vlažnost vazduha 9	Vetar 10	Oblačnost 11	Insolacija 12	Padavine 13	Broj karak- terističnih dani 14
Maoča	124	325	44°19'	18°59'	ob		x	x	x	x	x	x	x
Mlinište	110	1130	44 16	16 52	ob		x	x	x	x	x	x	x
Modriča	122	115	44 59	17 18	ob		x	x	x	x	x	x	x
Mostar	137	99	43 21	17 18	gl	x	x	x	x	x	x	x	x
Ponikve	125	970	44 11	18 22	ob		x	x	x	x	x	x	x
Potoci-Zeljuša	138	96	43 24	17 53	ob		x	x	x	x	x	x	x
Prijedor	109	135	44 59	16 45	ob		x	x	x	x	x	x	x
Prnjavor	118	150	44 52	17 42	ob		x	x	x	x	x	x	x
Prozor	133	800	43 50	17 38	ob		x	x	x	x	x	x	x
Rakitno	131	915	43 34	17 27	ob		x	x	x	x	x	x	x
Sanski Most	108	158	44 46	16 42	gl		x	x	x	x	x	x	x
Sarajevo-aerodrom	142	510	43 49	18 20	gl	x	x	x	x	x	x	x	x
Sarajevo	143	630	43 52	18 26	gl	x	x	x	x	x	x	x	x
Sokolac	147	872	43 57	18 49	ob		x	x	x	x	x	x	x
Srebrenica	129	550	44 02	19 19	ob		x	x	x	x	x	x	x
Teslić	119	225	44 36	17 54	ob		x	x	x	x	x	x	x
Travnik	117	581	44 14	17 40	ob		x	x	x	x	x	x	x
Tuzla	125	305	44 33	18 42	gl	x	x	x	x	x	x	x	x
Vlašenica	127	630	44 12	18 57	ob		x	x	x	x	x	x	x
Zenica	120	344	44 13	17 54	gl	x	x	x	x	x	x	x	x
S O C I J A L I S T I C K A R E P U B L I K A S R B I J A													
Al-Ksandrovac	202	360	43°27'	21°04'	ob		x		x	x	x	x	x
Babušnica	214	495	43 04	22 26	ob		x		x	x	x	x	x
Bačka Topola	156	100	41 41	19 39	ob		x	x	x	x	x	x	x
Bački Petrovac	155	89	41 22	19 34	ob		x	x	x	x	x	x	x
Bećej	161	78	45 38	20 02	ob		x	x	x	x	x	x	x
Bela Crkva	183	90	44 54	21 25	ob		x	x	x	x	x	x	x
Bele Vode-Golija	197	1500	43 25	20 17	ob		x	x	x	x	x	x	x
Beograd	173	132	44 48	20 28	gl	x	x	x	x	x	x	x	x
Bor	188	380	44 05	22 06	ob		x	x	x	x	x	x	x
Bosiljevac	235	830	42 30	22 28	ob		x	x	x	x	x	x	x
Bujanovac	228	400	42 27	21 47	ob		x	x	x	x	x	x	x
Bukovička Banja	176	265	44 18	20 33	ob		x	x	x	x	x	x	x
Čačak	198	250	43 53	20 19	ob		x	x	x	x	x	x	x
Čuprija	207	123	43 56	21 23	gl	x	x	x	x	x	x	x	x
Debeli Lug	187	290	44 22	21 55	ob		x	x	x	x	x	x	x
Dimitrovgrad	217	446	43 01	22 45	gl	x	x	x	x	x	x	x	x
Dragaš	222	1060	42 04	20 39	ob		x	x	x	x	x	x	x
Flamunda	181	160	44 56	21 05	ob		x	x	x	x	x	x	x
Gladnoš	160	185	45 08	20 00	ob		x	x	x	x	x	x	x
Gornji Milanovac	174	335	44 02	20 28	ob		x		x	x	x	x	x
Istok	220	465	42 47	20 30	ob		x		x	x	x	x	x
Ivanjica	196	465	43 35	20 14	ob		x	x	x	x	x	x	x
Jaša	165	80	41 27	20 51	ob		x	x	x	x	x	x	x

## AZBUČNI SPISAK STANICA

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

V

S T A N I C A	Broj stanice	Nadmorska visina H m	Geografska latituda 9°N	Geografska duljina 17°E Gr.	Rod stanice	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Imobilacija	Padavine	Broj karak- teristич- nih dani	
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Kikinda	164	81	45°51'	20°28'	gl		x	x	x	x	x	x	x
Klina	221	385	42 38	20 34	ob		x		x	x	x	x	x
Knjaževac	212	280	43 34	22 16	ob		x		x	x	x	x	x
Kos.Mitrovica	224	510	42 53	20 52	ob		x		x	x	x	x	x
Kragujevac	179	190	44 02	20 56	ob		x		x	x	x	x	x
Kraljevo	200	219	43 44	20 41	gl	x	x	x	x	x	x	x	x
Kruševac	206	166	43 34	21 21	gl		x		x	x	x	x	x
Kukavica	230	1250	42 45	21 59	ob		x		x	x	x	x	x
Kuršumlija	205	380	43 08	21 16	gl		x		x	x	x	x	x
Leskovac	211	224	43 01	21 57	gl	x	x	x	x	x	x	x	x
Loznica	167	121	44 33	19 14	gl	x	x	x	x	x	x	x	x
Ljubovija	168	170	44 11	19 23	ob		x		x	x	x	x	x
Mitrovac-Tara	191	1080	43 55	19 26	ob		x		x	x	x	x	x
Negotin	190	42	44 14	22 33	gl	x	x	x	x	x	x	x	x
Niš	210	202	43 20	21 54	gl	x	x	x	x	x	x	x	x
Novi Pazar	199	545	43 08	20 31	ob		x		x	x	x	x	x
Novi Sad-Petrovaradin	159	132	45 15	19 52	gl	x	x	x	x	x	x	x	x
Novi Sad-Rimske Šančevi	158	84	45 20	19 51	ob	x	x	x	x	x	x	x	x
Palić	152	102	46 06	19 46	gl	x	x	x	x	x	x	x	x
Pančevo	177	80	44 53	20 40	ob		x		x	x	x	x	x
Peć	218	498	42 40	20 18	gl	x	x	x	x	x	x	x	x
Petrovac	184	120	44 23	21 25	ob		x		x	x	x	x	x
Pirot	215	370	43 09	22 36	ob		x		x	x	x	x	x
Predejane	232	318	42 50	22 08	ob		x		x	x	x	x	x
Priština	225	573	42 39	21 09	gl	x	x	x	x	x	x	x	x
Prizren	223	402	42 13	20 44	gl		x		x	x	x	x	x
Prokuplje	208	265	43 14	21 36	ob		x		x	x	x	x	x
Rekovac	203	230	43 52	21 06	ob		x		x	x	x	x	x
Rudnik	175	700	44 08	20 31	ob		x		x	x	x	x	x
Senta	162	80	45 56	20 05	ob		x		x	x	x	x	x
Sijarinska Banja	227	455	42 47	21 36	ob		x		x	x	x	x	x
Sjenica	194	1015	43 16	20 01	gl	x	x	x	x	x	x	x	x
Skivjane-Djakovica	219	415	42 26	20 21	ob		x		x	x	x	x	x
Smederevo	178	120	44 39	20 55	ob		x		x	x	x	x	x
Smed.Palanka	180	121	44 22	20 57	gl	x	x	x	x	x	x	x	x
Sokobanja	209	300	43 39	21 51	ob		x		x	x	x	x	x
Sombor	153	88	45 47	19 05	gl		x		x	x	x	x	x
Sr.Mitrovica	169	81	44 58	19 38	gl		x		x	x	x	x	x
Surdulica	233	500	42 41	22 11	ob		x		x	x	x	x	x
Svetozarevo	204	115	43 59	21 14	ob		x		x	x	x	x	x
Šabac	170	80	44 46	19 41	ob		x		x	x	x	x	x
Šid	154	105	45 07	19 15	ob		x		x	x	x	x	x
Šušara	182	180	44 56	21 08	ob		x		x	x	x	x	x
Tekija	189	50	44 41	22 25	ob		x		x	x	x	x	x
Titovo Užice	193	440	43 52	19 51	ob		x		x	x	x	x	x

A Z B U Ć N I S P I S A K S T A N I C A  
PO SOCIJALISTIČKIM REPUBLIKAMA

VI Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadzemna visina H, m	Geografska širina φ, °N	Geografska dužina λ, °E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblakost	Insolencija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Topli Do	216	700	43°20'	22°41'	ob		x			x		x	x
Uroševac	226	580	42 23	21 10	ob		x	x	x	x	x	x	x
Už. Požega	195	311	43 51	20 02	gl	x	x	x	x	x	x	x	x
Valjevo	172	174	44 17	19 55	gl	x	x	x	x	x	x	x	x
Veliko Gradište	185	79	44 46	21 31	gl	x	x	x	x	x	x	x	x
Vladimirci	171	120	44 37	19 47	ob		x	x	x	x	x	x	x
Vlasina	234	1190	42 44	22 21	ob		x	x	x	x	x	x	x
Vlasotince	231	270	42 58	22 08	ob		x	x	x	x	x	x	x
Vranje	229	433	42 33	21 55	gl	x	x	x	x	x	x	x	x
Vrbas	157	87	45 34	19 39	ob		x	x	x	x	x	x	x
Vrnjačka Banja	201	235	43 37	20 54	ob		x	x	x	x	x	x	x
Vršac	166	83	45 09	21 19	gl	x	x	x	x	x	x	x	x
Zaječar	213	197	43 53	22 18	ob		x	x	x	x	x	x	x
Zlatibor	192	1029	43 44	19 43	gl	x	x	x	x	x	x	x	x
Zrenjanin	163	80	45 24	20 21	gl		x	x	x	x	x	x	x
Žagubica	186	314	44 12	21 47	ob		x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A C R N A G O R A													
Bar	247	1	42°06'	19°06'	gl	x	x	x	x	x	x	x	x
Bijelo Polje	238	560	43 02	19 45	ob		x	x	x	x	x	x	x
Budva	243	2	42 17	18 51	ob	x	x	x	x	x	x	x	x
Cetinje	244	655	42 24	18 56	ob		x	x	x	x	x	x	x
Građevno	241	710	42 39	18 41	ob		x	x	x	x	x	x	x
Herceg Novi - Igalo	240	40	42 28	18 30	gl	x	x	x	x	x	x	x	x
Ivangrad	250	670	42 50	19 52	ob	x	x	x	x	x	x	x	x
Kolašin	249	944	42 50	19 32	gl	x	x	x	x	x	x	x	x
Krtac	236	950	43 00	18 44	ob		x	x	x	x	x	x	x
Nikšić	245	647	42 46	18 57	gl	x	x	x	x	x	x	x	x
Pljevlja	239	784	43 21	19 21	gl	x	x	x	x	x	x	x	x
Titograd	248	49	42 26	19 17	ob	x	x	x	x	x	x	x	x
Tivat	242	5	42 26	18 42	ob	x	x	x	x	x	x	x	x
Ulcinj	251	97	41 55	19 13	gl	x	x	x	x	x	x	x	x
Virkapazar	246	14	42 14	19 05	ob		x	x	x	x	x	x	x
Žabljak	237	1450	43 09	19 08	gl	x	x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A M A K E D O N I J A													
Berovo	283	824	41°43'	22°51'	gl	x	x	x	x	x	x	x	x
Bitola	267	586	41 03	21 22	gl	x	x	x	x	x	x	x	x
Debar	257	675	41 31	20 32	ob		x	x	x	x	x	x	x
Delčevo	282	630	41 58	22 46	ob		x	x	x	x	x	x	x
Demir Kapija	275	125	41 25	22 15	gl	x	x	x	x	x	x	x	x
Erdišelija	272	253	41 50	22 02	ob		x	x	x	x	x	x	x
Gevgelija	278	59	41 09	22 30	ob		x	x	x	x	x	x	x
Gostivar	262	525	41 48	20 55	ob		x	x	x	x	x	x	x
Kavadarci	273	265	41 26	22 02	ob		x	x	x	x	x	x	x

**A Z B U T S I S P I C A K S T A N D A R T  
R E C O R D I N G S C O M P A N Y**

Znak x pokazuje da stanica raspolaže odgovarajućim poticima za dobitku slike slike navedenih u kolonama 7-14

VII

STANICA	BROJ stанице	Nadmorska visina h, m	Geografska dužina širina lat. N long. E Gr.	Red stанице	Vrednost pričvršćujućih geodetskih vježbi	Vlastnost vezaduna	Vetar	Oblačnost	Iznoslacija	PadaVine	Broj karak- teističnih dana		
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Kruševac	263	620	41° 51' 20" S	ob	x	x	x	x		x	x	x	
Kočani	276	345	41 55 22 25	ob	x	x	x	x		x	x	x	
Kratovo	255	640	42 05 22 09	ob	x	x	x	x		x	x	x	
Kriva Palanka	256	691	42 12 22 20	gl	x	x	x	x		x	x	x	
Kruševac	266	1230	41 20 21 15	ob	x	x	x	x		x	x	x	
Kumanovo	254	338	42 08 21 43	ob	x	x	x	x		x	x	x	
Lazaropole	259	1332	41 30 20 42	gl	x	x	x	x		x	x	x	
Makedonski Brod	265	545	41 31 21 13	ob	x	x	x	x		x	x	x	
Mavrovi Anovi	260	1240	41 42 20 15	ob	x	x	x	x		x	x	x	
Novi Dojran	281	180	41 13 22 43	ob	x	x	x	x		x	x	x	
Ohrid	261	760	41 07 20 48	gl	x	x	x	x		x	x	x	
Popova Šapka	252	1750	42 01 20 53	ob	x	x	x	x		x	x	x	
Prilep	270	673	41 20 21 34	gl	x	x	x	x		x	x	x	
Radoviš	277	380	41 38 22 27	ob	x	x	x	x		x	x	x	
Resen	264	881	41 05 21 01	ob	x	x	x	x		x	x	x	
Skopje-Petrovac	268	232	41 57 21 38	gl	x	x	x	x		x	x	x	
Struga	258	695	41 11 20 41	ob	x	x	x	x		x	x	x	
Strumica	280	224	41 26 22 39	ob	x	x	x	x		x	x	x	
Štip	274	326	41 45 22 11	gl	x	x	x	x		x	x	x	
Tetovo	253	462	42 00 20 58	ob	x	x	x	x		x	x	x	
Titov Veles	271	175	41 43 21 46	ob	x	x	x	x		x	x	x	
Trubarevo	269	233	41 59 21 31	ob	x	x	x	x		x	x	x	
Valandovo	279	100	41 19 22 34	ob	x	x	x	x		x	x	x	

**A) Dnevna osmafranja**

$\psi = 46^{\circ}04'$ ,  $N \lambda = 14^{\circ}31'$ , E Gr.  $\Delta G = +58$  min.

MK. St. 13

DG	Vzdušni pritisak P mm	Temperatura vzduha T °C										Napon vodené pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
		7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21		
1	742.4	742.0	742.3	00.0	00.7	00.0	00.2	01.6	-00.2	-01.1	04.1	04.3	04.0	89	90	88	89	NF	1	W	1	NE	1
2	741.4	740.3	740.0	00.0	00.9	00.4	00.4	01.6	-00.2	-01.2	04.2	04.4	04.6	91	90	98	93	NE	1	NE	1	-	0
3	739.7	739.1	739.4	00.3	01.6	01.0	01.0	02.2	00.2	-00.3	04.6	04.9	04.7	98	95	95	96	NNW	1	NNW	1	NW	1
4	741.9	741.0	743.4	00.9	02.5	00.8	01.5	02.9	00.5	-00.5	04.7	05.3	04.9	97	97	100	98	W	1	E	1	NE	1
5	741.0	742.0	741.2	00.4	01.4	01.1	01.1	01.8	00.0	00.0	04.6	04.9	05.0	98	97	98	98	NE	1	SW	4	NE	1
6	737.3	735.0	736.4	01.0	00.8	00.7	00.8	02.0	00.4	00.4	04.9	04.8	04.7	100	98	97	98	NNW	1	NE	1	NE	1
7	734.9	734.1	740.0	01.0	02.4	01.0	01.4	02.7	00.6	-00.4	04.8	04.8	04.7	98	97	95	93	E	1	NW	1	NNW	1
8	733.4	734.1	740.0	00.6	02.4	01.0	01.3	02.6	00.4	00.4	04.7	06.9	04.8	95	90	97	94	SE	1	W	1	NE	1
9	732.6	738.1	736.0	00.6	01.6	01.0	01.1	02.2	00.4	00.2	04.6	04.9	04.7	95	95	95	95	NW	1	NE	1	SE	1
10	736.2	738.1	740.9	01.0	02.3	01.3	01.6	02.7	00.6	-00.2	04.7	04.5	04.4	95	92	88	88	NF	1	SF	1	SE	2
11	742.2	742.6	743.8	00.4	00.9	00.9	00.8	02.7	00.1	00.0	04.2	04.2	04.5	89	86	91	89	SF	1	S	2	SE	1
12	744.8	744.9	745.6	00.0	01.0	01.0	00.8	01.7	-00.1	-00.1	04.5	04.8	04.7	98	98	95	97	E	1	W	1	E	1
13	743.8	743.5	744.8	-00.6	00.4	00.1	00.0	01.0	-00.7	-00.6	04.3	04.6	04.3	98	96	93	96	SSE	1	NW	1	SE	1
14	744.3	743.9	744.6	00.0	00.4	-00.2	00.0	00.7	-00.2	-00.8	03.8	03.7	03.5	84	79	81	81	SF	1	E	1	NE	1
15	743.7	742.5	742.2	-01.0	01.4	01.1	00.7	01.8	-01.0	-01.5	03.5	04.0	04.1	81	78	83	81	NW	1	NW	1	NE	1
16	741.2	741.7	739.0	00.7	05.4	00.6	01.8	05.9	00.2	-01.8	04.4	05.0	04.5	91	74	93	86	SE	1	-	0	NE	1
17	735.1	736.7	739.3	00.0	06.2	01.4	03.8	06.8	-00.3	-04.2	05.6	06.3	04.6	86	69	87	87	NW	1	NE	1	NW	1
18	739.9	738.3	739.2	-00.7	07.2	03.8	03.5	08.3	-01.7	-04.5	03.6	04.0	04.7	82	52	78	71	N	1	NE	1	N	1
19	740.1	740.1	740.3	01.4	05.9	02.0	03.2	07.1	01.2	-02.4	04.6	05.2	04.9	90	74	87	84	NF	1	SE	1	NW	1
20	740.3	739.1	741.5	-01.6	08.6	02.6	03.1	11.3	-02.0	-05.1	03.9	06.2	04.7	96	74	86	85	N	1	ESE	1	-	0
21	743.3	742.2	743.5	-02.2	06.4	-00.2	01.0	07.4	-02.4	-07.5	03.7	05.3	04.4	98	73	98	90	SF	1	SW	1	-	0
22	741.2	741.6	741.6	-01.4	00.2	-01.2	-00.9	00.4	-01.9	-06.9	04.1	04.5	04.2	100	96	101	99	-	0	ESE	1	ESE	1
23	744.2	743.3	741.9	-01.6	01.7	00.2	00.0	02.0	-01.9	-02.0	04.0	04.7	04.5	100	93	96	96	NF	1	NE	1	W	1
24	741.8	740.0	738.7	-01.8	00.1	-01.0	-00.9	00.7	-01.8	-01.7	03.8	04.1	04.2	96	90	98	95	SW	1	S	1	SW	1
25	739.0	738.9	739.0	-01.4	02.8	00.0	00.4	04.4	-01.6	-02.0	04.1	04.7	04.5	100	84	98	94	F	1	E	1	N	1
26	739.9	739.7	739.1	-00.6	00.7	-00.3	-00.1	00.8	-00.7	-00.5	04.4	04.7	04.5	100	98	100	99	SE	1	NE	1	NE	1
27	736.8	736.1	737.9	-00.7	02.1	00.7	00.7	04.6	-00.8	-00.8	04.3	05.0	04.6	98	94	95	96	ENE	1	-	0	NE	1
28	739.7	739.4	739.4	-00.2	03.4	01.5	01.6	04.0	-00.6	-01.9	04.5	05.4	05.0	100	92	98	97	-	0	S	1	NW	1
29	738.7	738.2	739.5	00.0	04.7	04.8	03.6	05.7	00.0	00.0	04.6	05.3	05.2	100	83	80	88	SW	1	SW	3	SW	3
30	741.8	741.9	741.9	01.1	04.7	04.0	03.5	05.6	00.2	-03.7	04.6	05.4	05.5	93	84	90	89	NE	1	NE	1	N	1
31	741.5	741.0	741.2	02.0	07.5	07.6	06.2	08.7	01.4	-03.2	05.3	05.4	06.4	100	82	82	88	NF	1	S	1	W	1
MES.	740.8	740.3	741.1	00.1	02.8	01.2	01.4	03.7	-00.4	-01.7	00.4	04.9	04.6	95	87	92	91	0.9	1.1	1.0	1.0	1.0	

## 1974 FEBRUAR

## LJUBLJANA BEŽIGRAD

1	739.3	738.7	738.7	05.4	07.6	05.6	06.1	09.0	05.4	04.7	06.3	06.8	07.8	93	87	85	88	N	1	-	G	1	
2	738.3	737.7	738.3	05.3	10.0	07.8	07.7	10.8	05.0	04.9	06.5	07.6	07.5	97	85	95	92	-	0	NF	1	NE	1
3	736.7	734.1	733.2	05.4	10.0	06.9	07.3	10.3	05.3	02.2	06.7	07.5	07.5	100	81	97	93	N	1	NW	1	1	0
4	730.6	729.5	730.3	05.8	07.1	03.4	04.9	08.7	03.3	04.8	06.5	06.1	05.5	94	81	94	90	SE	1	SE	2	-	0
5	730.3	727.8	726.2	02.3	08.1	06.2	05.7	04.7	02.2	02.6	05.3	06.2	06.0	98	76	84	86	-	0	NE	1	SW	2
6	720.5	712.5	707.6	04.7	08.1	08.5	08.0	09.7	05.4	04.1	06.0	06.9	07.2	82	85	87	85	SW	2	SW	4	SW	3
7	712.7	715.5	719.7	01.0	07.7	01.2	02.8	01.6	00.8	-00.4	04.8	04.4	04.4	97	56	88	80	SE	1	SW	3	NE	1
8	727.5	731.9	736.0	-02.4	09.1	01.9	02.6	09.4	-02.4	-06.5	03.7	02.7	03.2	98	31	60	63	NE	1	NW	3	N	1
9	736.8	736.6	737.6	-02.4	11.5	05.4	05.0	11.7	-02.8	-07.4	03.2	03.7	04.0	85	36	59	60	N	1	K	4	W	3
10	737.8	738.7	738.9	02.4	11.7	06.8	06.9	12.3	01.4	-01.2	04.7	05.1	05.2	86	50	70	69	NW	1	SW	3	SW	3
11	736.2	733.9	732.3	06.3	09.8	08.7	08.4	10.8	00.7	-04.0	05.3	06.4	06.2	73	70	73	72	NW	2	SW	3	SW	3
12	730.6	730.3	729.3	08.4	11.6	07.9	09.0	12.5	06.9	06.4	06.4	06.0	05.7	78	59	71	69	SW	3	SW	3	MSW	1
13	726.8	72																					

HK. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Veličina 0-9	Oblačnost N (0-10)					Intenziteta broj sati	Padavine R mm	Snežni pokrov h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	5	10	10	-	10*	10.0	00.0	27.5	03	* <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> i, 16 <sup>3</sup> -n; <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub> i
2	5	10*	10*	-	10	10.0	00.0	04.1	07	= <sup>+</sup> n-9, <sup>+</sup> n-4 <sup>1</sup> / <sub>2</sub> -20 <sup>1</sup> , <sup>+</sup>
3	6	10	10	-	10	10.0	00.0	01.6	08	= <sup>+</sup> n-5 <sup>1</sup> / <sub>2-8<sup>1</sup>/<sub>2</sub>; *<sup>+</sup>n-5<sup>3</sup>/<sub>4</sub>, 8<sup>4</sup>o, <sup>+</sup>n-16<sup>4</sup>-17<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-17<sup>1</sup>/<sub>2</sub>-19<sup>3</sup>/<sub>4</sub>, <sup>+</sup></sub>
4	3	10	10	-	10	10.0	00.0	01.0	05	= <sup>+</sup> n-17 <sup>3</sup> / <sub>4</sub> , 12 <sup>1</sup> / <sub>2</sub> -17 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-17 <sup>1</sup> / <sub>2</sub> -12 <sup>3</sup> / <sub>4</sub> , <sup>+</sup> n-17 <sup>3</sup> / <sub>4</sub> -18 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-18 <sup>1</sup> / <sub>2</sub> -16 <sup>3</sup> / <sub>4</sub>
5	4	10	10	-	10	10	00.0	00.0	02	= <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-12 <sup>3</sup> / <sub>4</sub> , 15 <sup>3</sup> / <sub>4</sub> , <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> -16 <sup>3</sup> / <sub>4</sub> , <sup>+</sup> n-16 <sup>1</sup> / <sub>2</sub> -18, <sup>+</sup>
6	3	10	10	*	10	10	00.0	00.6	*	* <sup>+</sup> n-10 <sup>1</sup> / <sub>2, <sup>+</sup>n-10<sup>1</sup>/<sub>2</sub>-11<sup>1</sup>/<sub>2</sub>, *<sup>+</sup>n-11<sup>1</sup>/<sub>2</sub>-18<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-5, <sup>+</sup>n-10<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-15-17<sup>3</sup>/<sub>4</sub>, 10<sup>1</sup>/<sub>2</sub>-n, <sup>+</sup></sub>
7	6	10	10	-	10	10	00.0	04.5	00	= <sup>+</sup> n-9, <sup>+</sup> n-17 <sup>1</sup> / <sub>2</sub> -17 <sup>3</sup> / <sub>4</sub> , * <sup>+</sup> n-17 <sup>1</sup> / <sub>2</sub> -8 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-9, <sup>+</sup>
8	5	10	10	-	10	10.0	00.0	00.1	00	= <sup>+</sup> n-20 <sup>1</sup> , <sup>+</sup> n-20 <sup>1</sup> , n
9	5	10	10	*	10	10	00.0	00.0	*	* <sup>+</sup> n-5, <sup>+</sup> n-n, <sup>+</sup> n-12 <sup>1</sup> / <sub>2, <sup>+</sup>n-15<sup>1</sup>/<sub>2</sub>-19<sup>1</sup>/<sub>2, <sup>+</sup>n-19<sup>1</sup>/<sub>2</sub>-n</sub></sub>
10	6	10	10	*	10	10	00.0	02.1	00	* <sup>+</sup> n-4 <sup>1</sup> / <sub>2, =<sup>+</sup>n-n, <sup>+</sup>n-4<sup>1</sup>/<sub>2-7<sup>1</sup>/<sub>2, <sup>+</sup>n-7<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2</sub></sub></sub></sub>
11	6	10	10	-	10	10	10.0	00.0	00	= <sup>+</sup> n-7
12	3	10	10	*	10	10	00.0	00.0	*	= <sup>+</sup> n-4 <sup>1</sup> / <sub>2, <sup>+</sup>n-4<sup>1</sup>/<sub>2</sub>-6, 12<sup>1</sup>/<sub>2</sub>-19<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>, 10<sup>1</sup>/<sub>2</sub>-n</sub>
13	4	10	10	*	10	10	10.0	00.0	*	= <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-7-8, <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> -n
14	6	10	10	-	10	10	10.0	00.0	*	= <sup>+</sup> n-n
15	6	10	10	-	10	10	10.0	00.0	*	= <sup>+</sup> n-n
16	5	10	06	0	00	05.3	01.4	*	= <sup>+</sup> n-20 <sup>1</sup> , <sup>+</sup> n-20 <sup>1</sup> , <sup>+</sup> n-20 <sup>1</sup> -n	
17	6	10	06	0	00	05.3	01.0	*	= <sup>+</sup> n-4 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-4 <sup>1</sup> / <sub>2</sub> -15, <sup>+</sup> n-17 <sup>1</sup> / <sub>2</sub> -10 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-18 <sup>1</sup> / <sub>2</sub> -n, <sup>+</sup> n-20 <sup>1</sup> -n	
18	6	01	08	0	01	03.3	05.6	01.6	*	= <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-8 <sup>1</sup> / <sub>2</sub> -9 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> -n
19	6	10	08	0	00	06.0	00.4	*	= <sup>+</sup> n-9, <sup>+</sup> n-14, 18-n, <sup>+</sup> n-14-18	
20	4	02	04	0	00	02.0	04.2	*	= <sup>+</sup> n-6, <sup>+</sup> n-10, <sup>+</sup> n-10, <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> -9 <sup>1</sup> / <sub>2</sub>	
21	5	10	00	0	10	06.7	04.0	*	= <sup>+</sup> n-4, 12 <sup>1</sup> / <sub>2-15<sup>1</sup>/<sub>2, 12<sup>1</sup>/<sub>2-19<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-7-11<sup>1</sup>/<sub>2</sub>, 19<sup>1</sup>/<sub>2</sub>-17<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>, 10<sup>1</sup>/<sub>2</sub>-n</sub></sub></sub>	
22	3	10	10	*	10	10.0	00.0	*	= <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-12 <sup>1</sup> / <sub>2-48, <sup>+</sup>n-20<sup>1</sup>-8<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-8<sup>1</sup>/<sub>2</sub>-11<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-13<sup>1</sup>/<sub>2</sub>-14<sup>1</sup>/<sub>2</sub>, =<sup>+</sup>n-14<sup>1</sup>/<sub>2</sub>-18</sub>	
23	3	10	10	*	10	10.0	00.0	*	= <sup>+</sup> n-4, 12 <sup>1</sup> / <sub>2-18<sup>1</sup>/<sub>2, <sup>+</sup>n-18<sup>1</sup>/<sub>2</sub>-11<sup>1</sup>/<sub>2, 16<sup>1</sup>/<sub>2</sub>-18<sup>1</sup>/<sub>2</sub>, =<sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-16<sup>1</sup>/<sub>2</sub></sub></sub></sub>	
24	5	10	09	0	10	09.7	00.0	*	= <sup>+</sup> n-4, 12 <sup>1</sup> / <sub>2-10<sup>1</sup>/<sub>2, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2</sub></sub></sub></sub>	
25	4	10	08	0	10	05.3	01.5	*	= <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> -7 <sup>1</sup> / <sub>2, <sup>+</sup>n-7<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2, =<sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-10<sup>1</sup>/<sub>2</sub></sub></sub>	
26	2	10	*	10	*	10	10.0	00.0	00.2	00
27	5	10	10	*	09	05.7	00.7	00.1	*	= <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> -17 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-7 <sup>1</sup> / <sub>2</sub> -10 <sup>1</sup> / <sub>2</sub>
28	3	10	*	09	05	10	05.0	00.5	00.1	= <sup>+</sup> n-2 <sup>1</sup> / <sub>2-12<sup>1</sup>/<sub>2, <sup>+</sup>n-13<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-13<sup>1</sup>/<sub>2</sub>-18<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-13<sup>1</sup>/<sub>2</sub>-18<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-14<sup>1</sup>/<sub>2</sub>-18<sup>1</sup>/<sub>2</sub></sub></sub>
29	6	10	*	10	08	04.3	00.0	*	= <sup>+</sup> n-12, <sup>+</sup> n-12-12 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> -17 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub> -n, <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub>	
30	6	10	*	10	10	10.0	00.0	*	= <sup>+</sup> n-n, <sup>+</sup> n-8 <sup>1</sup> / <sub>2</sub>	
31	5	10	*	09	09	09.3	00.1	*	= <sup>+</sup> n-n, <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> , 8 <sup>1</sup> / <sub>2</sub> -9, = <sup>+</sup> n-2 <sup>1</sup> / <sub>2-8<sup>1</sup>/<sub>2, =<sup>+</sup>n-9-17, <sup>+</sup>n-16<sup>1</sup>/<sub>2</sub>-17<sup>1</sup>/<sub>2</sub></sub></sub>	
MES. WRED.			09.4	08.9	09.3	08.9	19.3	44.6		

## LJUBLJANA BEŽIGRAD

1974 FEBRUAR

1	7	10	08	06	08.0	00.5	C3.7	*	* <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-13, <sup>+</sup> n-18 <sup>1</sup> / <sub>2</sub> -n
2	8	10	10	10	10.0	00.0	05.1	*	* <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-17 <sup>1</sup> / <sub>2</sub> -19 <sup>1</sup> / <sub>2</sub>
3	8	10	09	10	09.7	01.1	C3.4	*	= <sup>+</sup> n-4 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-6 <sup>1</sup> / <sub>2</sub> -9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> , 5 <sup>1</sup> / <sub>2</sub> , 9 <sup>1</sup> / <sub>2</sub> , 10, 14 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> , 17 <sup>1</sup> / <sub>2</sub> -n
4	6	10	09	07	08.7	00.7	07.7	*	* <sup>+</sup> n-6, <sup>+</sup> n-14 <sup>1</sup> / <sub>2</sub> -18 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-14 <sup>1</sup> / <sub>2</sub> -n, <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub> -n
5	6	10	08	10	09.3	01.6	*	*	= <sup>+</sup> n-4 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-8 <sup>1</sup> / <sub>2</sub> -10 <sup>1</sup> / <sub>2, =<sup>+</sup>n-14<sup>1</sup>/<sub>2</sub>-8<sup>1</sup>/<sub>2</sub>, <sup>+</sup>n-10<sup>1</sup>/<sub>2</sub>-n, <sup>+</sup>n-12<sup>1</sup>/<sub>2</sub>-19<sup>1</sup>/<sub>2</sub></sub>
6	7	10	10	10	10.0	00.0	00.2	*	= <sup>+</sup> n-6 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-15 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-16 <sup>1</sup> / <sub>2</sub> -n, <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub>
7	8	10	04	02	05.3	05.7	22.2	C2	* <sup>+</sup> n-16 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub>
8	8	10	03	02	05.0	06.1	*	*	= <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> , 5 <sup>1</sup> / <sub>2</sub> , 11 <sup>1</sup> / <sub>2</sub> -19 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-15 <sup>1</sup> / <sub>2</sub> , 10 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-25 <sup>1</sup> / <sub>2</sub>
9	8	02	05	10	05.7	06.3	*	*	= <sup>+</sup> n-10
10	8	08	04	00	04.0	06.2	*	*	*
11	7	10	09	09	09.3	01.0	*	*	<sup>+</sup> n-6
12	8	05	09	03	05.7	04.0	*	*	<sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub>
13	6	09	10	08	09.0	00.4	*	*	<sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , 19 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> -18 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-18 <sup>1</sup> / <sub>2</sub> -17 <sup>1</sup> / <sub>2</sub>
14	6	10	10	10	10.0	00.0	00.2	*	<sup>+</sup> n-12 <sup>1</sup> / <sub>2</sub> , 19 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> -14 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> -19 <sup>1</sup> / <sub>2</sub>
15	6	10	08	10	09.3	01.1	03.1	*	<sup>+</sup> n-9, 19-n, <sup>+</sup> n-8 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> -14 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-14 <sup>1</sup> / <sub>2</sub> -n
16	6	10	10	10	10.0	00.0	*	*	<sup>+</sup> n-15 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-15-18 <sup>1</sup> / <sub>2</sub>
17	7	10	10	09	09.7	00.1	CC.0	*	<sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-20 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-19 <sup>1</sup> / <sub>2</sub> -n
18	4	10	10	10	10	00.0	C1.0	*	= <sup>+</sup> n-5, 9, 17 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-3 <sup>1</sup> / <sub>2</sub> -6 <sup>2</sup> / <sub>1, <sup>+</sup>n-20<sup>1</sup>/<sub>2</sub>, =<sup>+</sup>n-9, 17<sup>1</sup>/<sub>2</sub>-n, <sup>+</sup>n-6<sup>2</sup>/<sub>1</sub></sub>
19	7	10	06	03	06.3	04.6	02.0	*	= <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> -11 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> -n, <sup>+</sup> n-25 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-2 <sup>1</sup> / <sub>2</sub> -6 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-8 <sup>1</sup> / <sub>2</sub> ui, <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> -13 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-13 <sup>1</sup> / <sub>2</sub> -19 <sup>1</sup> / <sub>2</sub>
20	7	01	10	10	07.0	03.4	*	*	<sup>+</sup> n-9, 19-n, <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> -6, <sup>+</sup> n-6-9-19 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9-19 <sup>1</sup> / <sub>2</sub>
21	7	10	09	08	09.0	01.2	CC.3	*	<sup>+</sup> n-9, 19-n, <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> -6, <sup>+</sup> n-6-9-19 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9-19 <sup>1</sup> / <sub>2</sub>
22	7	10	10	00	06.7	00.2	00.0	*	<sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , = <sup>+</sup> n-5 <sup>1</sup> / <sub>2</sub> -12
23	7	10	01	00	03.7	06.2	*	*	= <sup>+</sup> n-11 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-10 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-14 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-20 <sup>1</sup> / <sub>2</sub> -n
24	8	04	10	09	07.7	02.1	*	*	<sup>+</sup> n-7-9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> , <sup>+</sup> n-9 <sup>1</sup> / <sub>2</sub> -10 <sup>1</sup> / <sub>2</sub>
25	6	09	10	10	09.7	0			

1974 MART

LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

BR. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vozduha T C°								Napon vodene pare e mm			Relativna vlažnost U%			Pravac i jačina vetro D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	737.0	736.0	734.7	-00.6	05.3	00.7	01.6	06.2	-00.8	-06.6	02.7	02.9	04.7	62	42	58	67	ENE 1	E 2	N 1
2	732.3	732.3	734.2	00.3	01.2	00.4	00.6	01.8	-00.2	-00.6	04.5	04.7	04.5	96	93	95	95	NF 1	NE 1	W 1
3	736.0	736.5	737.9	00.2	05.4	01.7	02.3	05.9	00.1	-00.2	04.5	03.5	04.1	96	53	79	76	N 1	S 1	E 1
4	736.9	735.7	734.1	00.4	01.3	00.6	00.7	02.0	00.4	00.1	04.6	04.7	04.7	96	93	98	96	NE 1	W 1	NE 1
5	732.4	733.3	733.6	07.0	03.7	02.0	02.4	03.8	00.5	00.0	05.0	05.6	05.0	94	94	95	94	NE 1	K 1	S 1
6	733.2	734.9	737.1	00.4	02.6	01.9	01.7	04.4	00.3	00.0	04.6	05.0	04.7	97	91	90	93	W 1	S 2	SE 2
7	737.6	734.1	739.3	02.2	04.6	02.6	03.0	06.0	01.9	00.4	05.1	04.5	04.4	95	71	80	82	W 1	SE 2	SE 3
8	739.2	736.8	740.9	01.2	02.7	01.1	01.9	03.3	01.0	00.6	04.3	04.5	04.6	87	81	89	86	SE 2	E 2	SE 1
9	733.7	736.9	741.0	01.0	03.7	01.2	01.8	04.3	00.7	00.0	04.6	04.1	04.0	93	69	80	81	SE 1	SE 3	SE 3
10	740.1	737.8	741.1	00.7	05.1	02.0	02.4	05.6	00.4	-00.9	04.0	03.3	04.4	84	51	84	73	N 1	E 3	SE 2
11	742.1	742.8	744.2	-01.0	05.4	02.8	02.8	07.4	-01.0	-05.4	03.8	04.0	04.6	89	56	83	76	NE 1	NE 3	E 1
12	744.0	743.1	741.0	02.2	04.7	02.9	03.2	05.6	01.8	-02.0	04.8	04.3	04.2	90	67	74	77	SE 1	E 2	E 2
13	739.1	736.0	735.4	01.0	08.3	03.4	04.2	10.6	01.4	00.8	03.6	03.8	04.3	71	47	73	64	NE 1	SE 1	SE 1
14	733.8	730.5	730.3	-02.6	12.5	06.3	05.7	13.7	-02.8	-07.5	03.8	05.4	04.8	100	49	67	72	NF 1	W 1	SSE 1
15	729.0	730.4	730.2	-00.6	10.1	04.6	04.6	10.8	-00.8	-06.5	04.1	05.7	05.0	95	62	80	79	NW 1	NE 3	SW 1
16	729.0	727.8	728.9	02.4	13.8	08.4	08.3	14.3	02.4	-00.6	04.8	03.9	04.3	89	33	53	58	W 1	SW 2	S 3
17	730.0	731.1	733.0	-00.4	15.9	10.2	09.0	16.8	-00.4	-04.9	04.2	05.8	04.8	95	43	51	63	NE 1	SW 4	WSH 3
18	734.0	733.2	733.9	02.2	12.0	11.4	09.5	13.7	01.4	-03.2	04.9	07.1	07.9	90	64	78	77	NF 1	SW 3	W 3
19	735.0	736.0	737.6	11.0	15.4	11.8	12.5	16.6	10.2	05.2	08.1	08.5	08.2	82	65	79	75	SW 2	SW 4	SW 2
20	737.0	732.1	739.6	11.4	16.2	11.8	12.8	17.1	10.9	08.2	08.5	07.6	07.6	84	55	75	71	SW 3	NM 3	SW 2
21	740.0	738.0	740.2	05.0	21.7	14.4	14.0	24.0	03.9	00.0	06.4	07.1	07.5	94	36	60	65	SE 1	NE 2	NW 2
22	740.0	737.6	736.4	04.9	22.8	14.4	14.1	24.4	04.9	-01.4	06.3	05.6	06.2	97	27	50	58	NE 1	NE 1	NW 1
23	736.3	736.0	737.8	07.5	19.2	12.2	12.8	19.4	07.2	03.2	06.5	05.2	07.3	83	31	68	61	N 1	SW 4	SW 1
24	739.0	737.5	737.3	04.4	20.2	14.2	13.3	21.2	04.0	-01.0	06.1	04.8	06.5	97	27	54	59	E 1	NE 1	SE 1
25	737.1	736.6	737.8	08.3	17.4	11.7	12.3	17.8	07.6	02.6	06.5	06.1	08.4	79	54	61	71	SW 1	NE 1	NE 1
26	737.7	734.9	734.3	08.0	19.0	14.6	14.1	19.3	07.0	02.6	07.5	08.7	07.9	94	53	63	70	NE 1	NE 1	NE 1
27	733.0	732.0	733.4	08.5	17.4	13.4	13.2	18.4	08.1	03.5	08.1	07.8	08.2	96	52	71	73	SW 1	SW 3	NW 3
28	734.5	734.3	735.7	06.1	14.4	09.7	10.0	18.6	05.8	00.3	07.0	05.2	08.3	99	67	92	86	E 1	2	NF 1
29	737.2	736.3	737.1	04.6	17.0	14.6	12.9	19.3	04.6	00.6	06.4	06.3	08.1	100	41	65	69	S 1	WSW 1	E 1
30	738.6	738.3	739.5	07.6	16.0	18.4	11.1	16.6	07.4	03.4	07.2	07.6	05.8	92	56	62	70	E 1	SE 1	E 1
31	738.5	736.1	736.4	05.5	14.8	10.6	10.4	15.3	05.3	01.1	08.4	04.6	05.5	94	37	57	63	NE 1	E 3	SE 3
MES.	736.5	735.0	735.6	03.6	11.4	07.6	07.4	12.4	03.0	-00.3	05.4	05.6	05.6	91	57	75	74	1.1	2.1	1.4
VRFD.	736.5	735.0	735.6	03.6	11.4	07.6	07.4	12.4	03.0	-00.3	05.4	05.6	05.6	91	57	75	74	1.1	2.1	1.4

1974 APRIL

LJUBLJANA BEŽIGRAD

1	734.6	735.0	726.0	06.4	12.3	08.8	09.1	12.6	05.7	-0C.4	06.3	05.3	05.4	88	50	63	67	SE 1	SE 2	SE 2
2	736.5	736.3	739.4	07.2	11.2	09.2	09.2	11.8	06.6	05.6	06.7	06.1	06.2	88	61	71	73	SE 1	NE 3	E 1
3	740.4	739.1	739.3	02.2	16.1	09.0	09.1	16.1	01.5	-03.6	05.3	05.4	04.6	99	39	53	63	NF 1	SF 2	NE 1
4	738.7	735.7	735.2	01.6	16.6	09.4	09.3	17.1	00.8	-04.9	04.5	03.9	04.8	87	27	54	56	NF 1	SW 1	NF 1
5	735.2	734.5	736.5	01.6	16.2	10.4	09.7	17.1	00.2	-02.4	04.6	04.2	04.4	88	30	46	55	NE 1	E 3	N 2
6	737.5	736.4	737.6	03.6	16.1	09.6	09.7	17.0	02.5	-03.2	04.8	04.5	04.9	80	33	54	56	-	0	E 2
7	739.3	736.8	736.7	03.6	15.7	11.8	10.7	16.2	02.0	-03.3	05.0	05.6	05.6	85	42	54	60	E 1	NE 1	N 1
8	737.0	735.3	737.0	07.6	18.3	10.6	11.8	19.1	05.4	-01.2	04.8	04.4	04.7	97	28	49	55	NE 1	E 2	E 1
9	738.4	735.8	735.2	03.4	19.0	13.1	12.2	20.3	01.6	-04.1	04.8	03.7	06.6	82	23	58	54	E 1	N 1	SW 3
10	734.7	731.5	731.0	04.6	19.0	12.0	20.2	12.1	02.6	-01.7	05.6	04.7	04.2	88	27	40	52	N 1	SW 3	SW 3
11	728.8	727.2	726.7	05.7	12.7	08.9	09.1	14.0	04.0	-01.0	05.5	08.0	08.4	80	73	99	84	E 1	SE 2	NW 1
12	725.6	724.7	726.9	07.3	16.4	05.8	10.8	17.1	06.7	01.0	07.5	08.2	08.1	97	58	89	81	SW 1	SSW 3	St 1
13	728.2	729.6	730.7	09.4	12.8	10.6	10.9	13.5	08.4	07.0	08.6	09.0	08.8	98	81	92	90	SE 1	SW 1	SE 1
14	730.6	728.7	729.7	05.6	08.5	03.6	05.4	11.0	03.6	04.4	03.7	03.4	05.2	55	41	89	61	SE 4	SE 3	SE 1
15	728.8	725.9	727.9	03.2	13.5	09.2	08.8	13.7	01.6	-03.0	05.2	03.2	03.0	91	28	34	51	NE 1	E 3	SF 2
16	729.7	729.																		

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_f = 1.5 \text{ m}$ 

Dan	Veličina 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	03	070	10*	06.7	05.7	.	.	.		
2	3	10*	10*	10*	10.0	00.0	06.0	06.0	06		
3	7	10	060	10	09.7	02.8	09.5	11			
4	3	10*	10*	10*	10.0	00.0	01.5	01			
5	3	10	10*	10*	10.0	00.0	17.4	03			
6	5	10*	10	10*	10.0	00.0	14.5	03			
7	6	09	050	10	09.3	02.1	06.1	01			
8	6	10	10*	10*	10.0	00.0	00.2	*			
9	6	10*	10	10	10.0	00.0	00.3	00			
10	8	09	100	10	09.7	02.8	00.0	00			
11	7	02	09	09	06.7	03.5	00.0	00			
12	7	10	10	10	10.0	00.1	.	.			
13	7	09	020	00	03.7	07.6	.	.			
14	7	10*	000	00	03.3	07.6	.	.			
15	7	010	060	02	03.0	04.4	.	.			
16	7	08	080	06	07.3	05.9	.	.			
17	7	030	010	06	03.3	08.0	.	.			
18	7	050	10	10*	08.3	00.4	.	.			
19	7	09	040	01	04.7	04.6	00.0	.	.		
20	8	10	080	07	08.3	05.6	00.0	.	.		
21	8	00*	000	00	00.0	09.9	.	.			
22	8	000	000	00	00.0	08.6	.	.			
23	8	10	050	06	08.0	01.5	.	.			
24	8	020	070	03	02.3	09.7	.	.			
25	7	09	060	08	07.7	03.9	.	.			
26	7	10*	030	10	07.7	06.0	04.0	.			
27	6	050	100	05	06.7	06.9	.	.			
28	6	11*	100*	00	03.7	05.7	00.0	.			
29	7	10*	09	08	08.0	03.2	06.4	.			
30	7	10	10	10	10.0	00.0	.	.			
31	8	090	090	10	09.3	03.2	.	.			
32	8	070	070	06	06.8	11.7	00.5	.			
33	8	070	070	06	06.8	11.7	00.0	.			
34	8	000	010	00	00.2	11.7	.	.			
35	8	000	030	04	02.3	06.2	.	.			
36	7	10	10	10	10.0	00.0	.	.			
37	8	10	08	10*	08.3	04.0	03.3	.			
38	7	10*	10*	10	10.0	00.0	01.1	.			
39	8	10	10	10	10.0	00.1	01.2	.			
40	8	080	070	10	08.3	06.7	00.4	.			
41	7	060	09	03	06.0	09.4	00.0	.			
42	8	10	10	10	10.0	01.2	00.0	.			
43	8	070	10	04	07.0	02.0	.	.			
44	8	030	080	03	04.7	10.0	.	.			
45	8	000	010	00	00.3	12.4	.	.			
46	7	070	10	10*	05.0	02.6	.	.			
47	7	10*	050	06	07.0	02.2	00.0	.			
48	8	010	070	00	02.7	10.6	00.0	.			
49	6	080	090	09	08.7	02.4	.	.			
50	6	100	10	08	09.3	00.0	08.5	.			
51	7	070	10	10*	05.0	02.6	.	.			
52	7	10*	050	06	07.0	02.2	00.0	.			
53	8	010	070	00	02.7	10.6	00.0	.			
54	6	080	090	09	08.7	02.4	.	.			
55	6	100	10	08	09.3	00.0	08.5	.			
56	8	100	080	04	07.3	04.4	14.7	.			
57	7	030	10	10*	07.7	06.1	00.4	.			
58	6	10	10*	10*	10.0	00.0	02.8	.			
59	6	10*	090	08	09.3	00.9	18.9	.			
60	8	080	10	10	09.3	01.2	04.1	.			
MES.	MES.	06.1	07.5	06.1	06.5	161.6	55.5				

1	7	07	050	10	09.7	03.7	.	.			
2	7	10	10	07	06.0	00.4	00.1	.			
3	8	01*	050	01	02.0	08.1	00.0	.			
4	8	000	010	00	00.3	11.1	.	.			
5	7	000	060	06	04.0	10.2	.	.			
6	8	09	040	00	04.3	07.9	.	.			
7	8	030	10	09	07.3	01.3	.	.			
8	8	010	040	00	01.7	11.2	00.0	.			
9	8	000	010	00	00.2	11.7	.	.			
10	8	000	030	04	02.3	06.2	.	.			
11	7	10	10	10	10.0	00.0	.	.			
12	8	10	08	10*	08.3	04.0	03.3	.			
13	7	10*	10*	10	10.0	00.0	01.1	.			
14	8	10	10	10	10.0	00.1	01.2	.			
15	8	080	070	10	08.3	06.7	00.4	.			
16	7	060	09	03	06.0	09.4	00.0	.			
17	8	10	10	10	10.0	01.2	00.0	.			
18	8	070	10	04	07.0	02.0	.	.			
19	8	030	080	03	04.7	10.0	.	.			
20	8	000	010	00	00.3	12.4	.	.			
21	7	070	10	10*	05.0	02.6	.	.			
22	7	10*	050	06	07.0	02.2	00.0	.			
23	8	010	070	00	02.7	10.6	00.0	.			
24	6	080	090	09	08.7	02.4	.	.			
25	6	100	10	08	09.3	00.0	08.5	.			
26	8	100	080	04	07.3	04.4	14.7	.			
27	7	030	10	10*	07.7	06.1	00.4	.			
28	6	10	10*	10*	10.0	00.0	02.8	.			
29	6	10*	090	08	09.3	00.9	18.9	.			
30	8	080	10	10	09.3	01.2	04.1	.			
MES.	MES.	06.1	07.5	06.1	06.5	161.6	55.5				

1974 MAJ

LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

BR. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parov e mm			Relativna vlažnost v %				Pravac i jačina vetrova D, f (0—12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	718.3	719.0	722.3	11.4	18.8	13.7	14.4	19.1	10.9	08.9	05.3	06.8	05.6	92	42	48	61	SW	1	N	2	NW	1
2	724.7	726.8	727.9	10.8	13.4	10.6	11.4	16.4	07.8	02.6	07.3	08.2	09.1	75	71	95	80	SW	2	N	1	S	1
3	729.2	728.5	728.8	09.8	13.6	11.6	11.7	16.8	09.5	06.5	08.8	07.5	06.7	96	64	66	75	NE	1	W	2	SW	3
4	726.5	724.8	725.2	09.0	11.0	09.1	09.6	11.8	09.0	05.7	08.3	09.1	07.9	96	92	91	93	E	1	W	2	SW	1
5	724.6	725.3	726.5	08.6	12.2	10.8	10.6	13.4	08.0	07.0	08.0	07.5	07.9	95	70	81	82	E	1	W	2	SW	2
6	726.8	728.3	731.6	11.6	16.7	09.8	12.0	17.0	09.0	05.6	08.1	07.7	08.8	79	54	96	76	SW	1	SW	4	NE	1
7	733.6	734.6	735.8	09.4	10.1	10.5	10.1	12.0	09.0	08.1	08.6	08.6	09.0	98	93	94	95	NW	1	NW	1	SW	1
8	737.2	737.0	736.0	09.3	12.2	11.2	11.0	14.0	08.7	03.6	08.4	07.0	07.1	95	66	71	77	NE	1	NE	2	E	1
9	736.0	734.1	734.5	09.4	16.8	10.4	11.8	17.7	08.1	03.4	07.7	04.8	06.0	87	34	63	61	NE	1	SE	2	E	1
10	734.9	733.1	733.1	07.2	16.8	12.7	12.4	18.0	04.0	-00.2	06.3	07.3	06.4	83	51	58	64	NE	1	SW	4	W	1
11	733.8	734.3	735.3	09.0	16.0	13.0	12.8	18.0	07.9	02.5	07.6	06.8	07.0	88	50	62	67	N	1	SW	3	NW	2
12	736.2	735.8	738.8	12.4	21.7	15.0	16.0	22.0	10.6	08.2	08.0	05.7	08.8	74	29	69	57	NNW	2	NNW	3	SE	1
13	740.7	738.8	739.5	11.2	23.1	16.8	17.0	23.7	07.7	02.1	08.4	06.8	07.9	84	32	55	57	SW	1	W	2	SW	1
14	738.0	735.8	738.6	11.6	22.0	10.6	13.7	22.5	07.9	02.5	08.5	08.6	09.3	83	43	96	74	NE	1	SW	5	NW	2
15	737.9	734.5	734.2	09.1	18.2	11.7	12.7	19.0	07.6	03.9	07.8	06.1	07.7	90	39	75	68	ENE	1	NE	2	E	1
16	733.9	732.0	733.4	09.7	18.7	12.7	13.5	19.4	08.0	02.6	08.1	06.5	08.1	89	40	74	68	E	1	SW	2	SW	1
17	734.4	735.2	739.2	12.4	21.3	14.0	15.4	21.9	08.9	04.6	08.6	07.3	07.5	80	38	62	60	NNE	1	E	2	E	1
18	740.8	739.3	740.4	10.0	22.1	17.4	16.7	22.7	06.7	00.9	07.7	07.5	07.6	84	38	51	58	ENE	1	NE	2	NE	2
19	740.5	738.5	738.8	11.6	22.9	16.4	16.8	23.1	08.7	02.5	08.4	07.4	07.8	82	35	56	58	NE	1	ENE	3	NE	1
20	738.9	736.1	737.0	12.2	26.1	17.0	18.1	26.1	08.0	02.0	08.2	07.4	11.7	77	29	80	62	NE	1	SW	2	E	1
21	738.2	737.0	737.0	13.7	24.4	18.0	18.5	25.3	12.6	07.7	10.4	08.5	10.3	88	37	66	64	SE	1	NE	1	SE	1
22	734.9	727.9	729.0	13.2	24.2	14.2	16.5	24.5	12.5	07.6	10.4	09.7	09.2	91	43	76	70	SW	1	SW	4	ENE	2
23	730.2	728.8	728.8	10.3	14.2	11.0	11.6	17.9	07.5	00.9	08.3	07.3	07.4	88	60	76	75	NE	1	W	2	SW	1
24	729.1	729.3	730.4	07.9	09.4	07.0	07.8	11.2	06.2	00.3	07.9	08.4	07.2	87	95	96	93	N	1	NW	1	NW	2
25	732.1	734.9	736.8	07.1	14.6	10.9	10.9	16.9	06.2	05.5	07.1	07.8	08.1	93	62	83	79	W	2	SE	1	-	0
MES.	WRFED	733.7	732.7	733.6	10.7	18.5	13.4	14.0	19.7	08.7	04.5	08.4	07.8	08.3	87	51	72	70	1.2	2.2	1.4		

1974 JUN

LJUBLJANA BEŽIGRAD

1	733.9	736.8	738.5	15.0	15.6	14.4	14.9	18.2	14.4	13.3	12.4	11.5	11.4	97	86	93	92	NW	1	SW	2	S	1
2	740.8	740.7	742.4	14.4	22.2	17.0	17.7	23.6	12.5	08.4	10.9	07.5	09.6	89	37	68	64	-	0	SE	2	ESE	1
3	743.4	740.8	740.2	12.2	23.9	17.8	17.9	25.1	08.4	03.7	08.9	07.9	09.4	84	36	61	60	-	0	ESE	1	ESE	1
4	740.2	738.4	738.3	15.1	27.8	19.8	20.6	28.6	10.6	05.9	09.8	09.7	08.2	76	35	47	53	SE	1	W	3	SE	2
5	738.7	736.2	735.2	15.4	25.2	20.6	20.5	26.6	12.4	07.6	09.9	13.6	10.3	76	57	57	63	SW	1	NE	1	SF	1
6	734.1	734.1	734.7	16.0	18.8	15.4	16.4	23.0	13.4	07.4	10.5	12.3	12.1	77	75	92	81	S	1	SW	2	S	1
7	735.9	735.2	739.1	11.3	24.0	15.8	16.7	24.3	07.2	01.6	08.1	08.0	07.6	81	36	57	58	ENE	1	SE	1	SW	1
8	740.0	738.9	736.7	10.3	15.3	10.4	11.6	16.0	09.0	07.5	08.4	07.7	08.5	89	59	90	79	NE	1	SW	3	NW	1
9	733.2	731.3	730.9	08.2	17.3	12.7	12.7	18.3	06.9	02.2	07.9	08.5	10.8	97	58	98	84	SE	1	W	3	E	1
10	732.1	730.4	729.3	06.4	07.8	08.0	07.6	13.2	06.3	05.2	06.6	07.1	07.8	92	90	97	93	N	1	N	3	S	2
11	730.4	731.8	734.0	09.3	19.7	12.5	13.5	20.6	08.0	04.8	07.9	05.1	07.7	90	29	71	63	S	1	NW	3	SW	1
12	733.3	731.5	731.3	07.3	18.2	12.9	12.8	19.3	04.8	-00.4	06.6	04.6	04.4	86	29	39	51	N	1	N	2	NNW	2
13	728.5	728.8	729.2	07.8	16.3	13.5	12.8	18.7	05.7	04.6	06.4	06.4	07.5	81	46	65	64	NF	1	SW	4	SW	1
14	730.7	730.7	733.1	11.0	22.4	16.8	16.8	22.6	10.6	07.7	09.3	09.2	08.4	94	45	59	66	NE	1	S	4	SW	1
15	735.1	733.2	734.7	12.0	22.1	14.3	15.7	23.2	09.6	05.0	09.5	10.0	10.2	90	50	84	75	NE	1	SW	3	SW	2
16	734.3	732.8	733.9	12.0	23.7	16.2	17.0	24.6	09.9	04.5	09.6	08.6	10.7	91	39	77	69	NW	1	Nh	2	E	3
17	733.3	731.6	732.4	14.8	21.7	18.0	18.1	23.3	12.6	09.2	10.9	09.7	12.1	86	50	78	71	S	1	SW	2	SW	1
18	733.4	733.3	735.0	15.6	18.2	15.8	16.4	22.1	11.2	08.4	11.3	10.8	12.5	85	69	93	82	E	1	SE	2	S	1
19	737.2	737.6	738.3	14.6																			

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vidljivost 0.9	Oblačnost N (0-10)					Insolacija broj sati	Podzemne R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	10	09.0	07	08.7	00.0	10.4	.	.	= n 4.2, tr-o-n 0.4	
2	8	04.0	02.0	01	03.7	10.9	10.9	02.0	.	= n 8.2, tr-o-5.4, 0.4, tr-o-M.4, -18.4	
3	7	10.0	09.0	10	09.7	05.0	02.3	.	.	= n 10.2, tr-o-5.4, 0.4, 13.0, 14.5, 0.4, tr-o-15.4	
4	7	10.0	10.0	10.0	10.0	00.0	01.3	.	.	= 2.5.4, n.4, = 3.4, n.4, tr-o-18.4, -10.2	
5	7	10	10.0	10.0	10.0	00.0	13.4	.	.	= tr-o-18.4, 17.4, -n.4, = n.4	
6	8	10	06.0	10.	08.7	01.0	00.4	.	.	= 2.16.0, 17.4, 19.4, -n.4, = 3.4, 6.4, 8.4, 12.4, 15.4, 19.4, 17.4, 18.4, 15.4	
7	6	10.0	10.0	09	09.7	00.0	2.6	.	.	= n 10.2, 20.0, n.4, tr-o-n.4, 13.4	
8	7	10	10	10	10.0	01.0	13.4	14.4	.	= n 4.2, 12.4, n.4	
9	8	07.0	06.0	00	04.3	10.4	.	.	.	= n 8.0	
10	7	01.0	08.0	04	04.3	09.5	.	.	.	= 2.2.0, 4.4, = 4.4, 8.4, 00.4, 12.4, 14.4, 0.4	
11	8	10	05	04	04.3	02.4	00.0	.	.	= n 12.2, tr-o-8.4, 12.4, -n.4, 00.4, 12.4	
12	8	08.0	07.0	08	07.7	10.4	00.0	.	.	= 2.12.4	
13	8	01.0	01.0	01	01.0	12.5	.	.	.	= n 12.4, 12.4, 12.4	
14	8	00.0	08.0	10.	06.0	10.2	.	.	.	= n 8.0, 12.4, 20.0, n	
15	8	00	06.0	10.0	08.3	06.4	00.0	.	.	= n 8.0, 12.4, 17.4, 20.0	
16	8	05.0	05.0	10	03.3	10.5	00.0	.	.	= 2.12.4, 12.4, 20.0	
17	8	04.0	03.0	04	03.7	10.9	.	.	.	= 2.19.0, -n.4, = n.4, 00.4, 12.4, 14.4, 16.4, 18.4	
18	7	00.0	03.0	09	05.7	12.6	00.0	.	.	= 2.10.4, -n.4, = n.4, 00.4, 12.4, n	
19	7	01.0	03.0	00	01.3	12.9	.	.	.	= 2.12.4, = n.4, 00.4, 12.4, 14.4, 16.4	
20	7	00.0	08.0	04	05.7	11.8	.	.	.	= 2.10.4, 00.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
21	7	05	03.0	00	04.0	04.5	01.4	.	.	= n 10.0, 8.4, tr-o-3.4, 00.4, 2.4, n	
22	7	05	03.0	04	05.3	05.5	00.4	.	.	= n 8.2, = n.4, 7.4, 5.4, 10.4, 12.4, 14.4, 16.4, 18.4	
23	8	03.0	06.0	10	04.3	05.4	00.2	.	.	= 2.10.4, = n.4, 00.4, 12.4, 14.4, 16.4	
24	6	10	10.0	10	10.0	00.0	00.1	.	.	= n 10.0, 10.0, 10.0, 10.0, 10.0	
25	8	10.0	03.0	07	04.3	07.1	21.0	.	.	= 2.10.4, 10.0, 10.0, 10.0, 10.0	
26	8	10	03.0	00	04.2	10.9	01.0	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
27	7	00.0	03.0	07	03.2	12.2	.	.	.	= 2.10.4, -n.4, 12.4, 14.4	
28	8	05.0	09	10	08.0	04.2	.	.	.	= n 12.4, 12.4, 12.4	
29	7	10.0	04.0	00	04.7	07.9	04.6	.	.	= 2.10.4, = n.4, 8.4, 10.4, 12.4, 14.4, 16.4, 18.4	
30	7	10	09.0	05	09.3	08.5	00.0	.	.	= 2.10.4, 00.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
MES. VR.ED.		01.5	06.7	06.5	06.6	207.4	169.0				

1	6	10	10	07	08.0	00.0	10.7	.	.	= 2.12.5, 5.2, = 5.4, 15.4	
2	8	08.0	02.0	01	03.7	10.9	16.9	.	.	= n.4, 12.4, 12.4	
3	7	00.0	01.0	00	00.3	13.0	.	.	.	= n.4, 12.4, 12.4	
4	8	00.0	02.0	01	01.0	13.7	.	.	.	= 2.10.4, = n.4, 00.4, 12.4	
5	7	04.0	02.0	05	03.7	08.6	.	.	.	= 2.10.4, = n.4, 00.4, 12.4	
6	7	05.0	10	10.	08.7	01.2	00.0	.	.	= 2.10.4, 10.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
7	8	07.0	04.0	07	04.7	12.2	25.6	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
8	8	09	04.0	04	07.3	01.0	01.3	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
9	7	10.0	04	10.	08.7	01.8	00.2	.	.	= 2.10.4, = n.4, 12.4, 14.4, 16.4, 18.4	
10	6	10.0	10.0	10.	10.0	00.0	32.9	.	.	= 2.10.4, 00.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
11	8	09.0	04.0	01	04.7	11.8	40.1	.	.	= n.4, = n.4, 8.4	
12	9	09.0	08.0	01	06.0	05.0	.	.	.	= 2.10.4, = 5.4	
13	8	09.0	10	C5	08.0	05.1	.	.	.	= 2.10.4, 8.4, 12.4, 14.4, 16.4, 18.4	
14	8	10.0	04.0	01	05.0	07.0	00.0	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
15	7	07.0	06.0	07	04.7	04.4	00.0	.	.	= 2.10.4, = n.4, 8.4, 10.4, 12.4, T.15.4, 16.4, 17.4, 18.4	
16	7	00.0	04.0	07	03.7	10.8	00.0	.	.	= 2.10.4, = n.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
17	7	02.0	06.0	03	03.7	07.9	11.1	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
18	7	02.0	10.0	10.	07.3	02.8	.	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
19	8	10.0	07.0	01	06.0	02.8	05.1	.	.	= n.4, = n.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
20	7	01.0	06.0	09	04.2	04.9	00.2	.	.	= 2.10.4, = n.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
21	8	10.	05.0	03	06.0	07.0	06.2	.	.	= n.4, = n.4, 12.4, 14.4, 16.4, 18.4	
22	7	10	05.0	02	05.7	09.1	02.8	.	.	= n.4, = n.4, 12.4, 14.4, 16.4, 18.4	
23	7	04.0	02.0	10	05.3	09.3	.	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
24	7	09.0	10	C9	05.3	00.2	05.0	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
25	8	06.0	04.0	05	05.0	08.7	20.4	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
26	8	09.0	05.0	04	06.0	07.7	.	.	.	= 2.10.4, = n.4, 12.4, 14.4, 16.4, 18.4, 20.0, 22.4	
27	7	09.0	09.0	07	08.3	04.5	00.0	.	.	= 2.10.4, = n.4, 12.4, 14.4, 16.4, 18.4	
28	7	10.0	05	10.	05.7	01.4	01.5	.	.	= 2.10.4, 12.4, 14.4, 16.4, 18.4	
29	6	10.0	10.0	10.	10.0	00.0	11.7	.	.	= n.4, = n.4, 12.4, 14.4, 16.4, 18.4	
30	8	02.0	04.0	08	04.7	11.8	49.0	.	.	= 4.6	
MES. VR.ED.		06.8	06.2	05.7	06.2	189.1	245.2				

1974 JUL

## LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$ , N  $\lambda = 14^{\circ}31'$ , E Gr.  $\Delta G = + 58$  min.

BP. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T °C°							Napon vodenih pare e mm			Relativna vlažnost U %			Pravac i jačina vetrova D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	736.1	735.0	735.7	16.5	26.7	21.4	21.5	27.4	12.5	08.1	11.4	11.5	10.9	81	44	57	61	ESE	1	SW	4	SW	2
2	738.9	738.6	739.3	16.9	24.5	20.0	20.4	26.1	14.0	09.2	11.1	12.0	12.6	77	52	72	67	E	1	E	2	NE	1
3	738.9	733.7	733.4	17.4	26.2	17.6	19.7	27.8	12.9	07.7	10.3	11.9	13.7	69	47	91	69	SF	1	S	2	SW	1
4	735.5	735.2	736.2	14.9	22.5	18.4	18.6	24.0	13.3	09.3	11.6	11.3	11.4	91	55	72	73	NF	1	SE	3	E	1
5	738.0	736.9	736.2	16.8	24.6	20.8	20.8	25.6	15.4	11.9	10.9	11.3	13.2	76	48	72	65	NE	1	SE	2	SE	2
6	736.0	734.0	733.3	16.6	27.2	20.0	21.0	28.0	13.5	09.4	12.4	12.3	14.7	88	46	84	73	E	2	SW	3	N	1
7	733.8	736.4	737.5	17.2	30.1	15.8	17.2	21.0	15.8	15.0	13.5	10.6	09.9	91	60	73	75	NE	1	SE	4	E	1
8	739.5	737.2	738.3	11.4	22.6	17.7	17.4	23.3	10.2	05.3	09.0	07.0	09.2	97	34	69	64	NE	1	SW	3	NE	1
9	740.0	737.7	736.3	13.6	24.4	19.0	19.0	24.6	09.9	04.6	06.8	10.5	07.3	75	46	45	55	N	1	SW	3	SW	3
10	736.7	736.8	737.8	15.0	25.0	20.2	20.1	26.0	12.5	07.0	11.1	11.3	10.5	97	46	59	65	NW	2	S	2	E	1
11	733.5	736.6	737.4	16.9	27.3	22.0	22.1	27.7	16.0	11.5	11.6	12.4	13.1	80	46	66	64	E	1	SW	3	SW	3
12	736.6	736.2	736.6	21.1	27.5	22.8	23.6	28.5	14.2	11.2	11.6	14.2	13.0	62	52	62	59	W	2	SW	3	SW	2
13	736.4	734.9	734.2	19.4	29.0	24.0	24.1	30.0	17.0	12.7	14.1	15.3	12.1	83	51	54	63	S	1	SW	3	SW	3
14	734.4	733.5	734.2	18.6	29.1	22.8	23.3	29.8	15.7	10.7	12.0	13.4	11.7	74	44	56	58	NE	1	SW	3	W	2
15	737.1	739.1	739.3	10.4	19.0	17.2	18.2	22.9	17.0	12.9	12.7	11.8	12.9	75	71	48	78	SE	1	NE	2	N	1
16	737.2	735.0	733.8	15.9	26.4	21.7	21.9	30.6	14.0	09.6	12.7	13.3	17.7	94	46	65	68	NE	1	SW	2	-	0
17	732.5	730.0	729.8	18.7	29.4	24.0	24.0	30.6	14.8	09.7	12.1	13.0	13.2	75	42	59	59	SW	1	SW	3	SW	1
18	729.3	730.1	732.9	18.0	18.9	14.5	16.5	24.1	14.5	13.6	13.9	13.3	11.7	90	81	95	89	N	2	NE	1	NE	1
19	733.7	734.2	735.1	12.8	15.2	14.5	14.3	15.9	12.6	12.2	10.7	11.2	09.7	97	86	78	87	NW	1	S	1	-	0
20	735.6	734.6	734.6	13.0	19.2	15.0	15.6	20.0	09.4	11.9	08.0	07.5	06.4	71	45	65	60	SF	2	NE	3	SE	2
21	733.8	732.3	735.2	12.0	19.9	15.4	15.7	22.3	10.6	06.2	09.4	10.2	11.3	89	59	86	78	S	1	NW	3	SW	1
22	737.2	735.8	736.4	11.9	22.8	15.8	16.6	23.6	11.2	07.7	09.4	07.2	09.6	90	35	71	65	SW	1	NE	2	S	1
23	735.0	735.0	735.9	13.6	25.8	20.0	19.9	27.0	10.4	06.7	09.0	09.0	12.8	77	36	73	62	NE	2	NW	1	SK	3
24	736.6	735.1	734.2	15.4	25.5	20.4	20.4	26.3	12.9	08.7	11.4	08.9	15.0	87	36	72	65	NE	1	SW	4	K	1
25	732.8	737.1	739.9	17.9	12.6	13.4	14.3	20.6	12.4	05.8	14.6	10.2	10.3	95	92	89	92	NE	1	E	3	NE	1
26	740.1	738.7	738.6	12.1	22.2	17.7	17.4	23.1	09.8	07.5	09.7	08.2	10.1	91	41	66	66	NF	1	E	2	SF	1
27	739.1	737.1	737.4	11.2	25.5	18.9	18.6	26.0	10.0	07.1	09.9	11.1	12.5	99	45	76	73	-	0	FNE	1	-	0
28	739.2	738.9	740.0	13.3	27.0	20.4	20.4	28.1	12.0	07.5	11.1	12.0	15.9	97	45	87	76	E	1	E	2	-	0
29	741.7	740.0	739.5	15.4	28.6	22.0	22.0	30.0	14.3	10.4	12.9	14.0	15.2	90	48	76	74	NE	1	SF	2	NE	1
30	739.2	736.3	735.4	17.6	30.1	24.0	23.9	31.7	14.4	10.5	12.0	15.4	14.4	85	42	64	64	NF	1	NE	1	SW	1
31	736.1	735.0	735.0	19.2	30.2	22.4	23.7	30.7	16.1	11.7	13.5	15.8	14.0	81	49	68	66	E	1	NE	1	-	0
MES.	VRID.			15.8	24.4	19.4	19.7	25.9	13.2	09.4	11.4	11.4	12.0	84	51	71	65	1.2	2.4	1.7			

1974 AVGUST

## LJUBLJANA BEŽIGRAD

1	736.2	734.6	734.9	18.5	20.0	24.4	24.2	30.8	17.4	11.8	15.5	15.9	19.4	97	50	84	77	ESE	1	NE	1	NE	1
2	735.0	734.8	735.2	20.2	21.6	24.2	25.1	31.7	18.9	14.4	16.8	16.4	20.0	95	47	88	77	NF	1	SE	2	SE	1
3	735.7	735.6	737.1	19.8	30.0	24.2	24.6	31.2	18.3	13.9	14.0	15.9	18.4	81	50	81	71	SF	1	NE	1	NE	1
4	737.5	735.4	735.6	20.1	32.4	25.0	25.6	32.1	18.6	14.1	15.8	13.8	13.4	89	38	63	61	NE	1	SE	3	SW	2
5	737.0	736.3	736.4	19.6	29.6	23.8	24.7	29.8	17.0	12.3	14.0	14.0	15.4	82	45	70	66	NE	1	SL	2	E	1
6	739.8	741.3	741.2	18.6	20.4	16.6	18.1	23.8	16.6	15.3	15.8	11.2	12.0	98	62	85	82	NE	2	NE	2	NE	1
7	739.5	736.6	735.4	17.3	24.0	19.4	18.8	24.9	12.1	07.4	10.5	10.4	10.9	98	47	65	70	NF	1	SE	1	SE	1
8	733.5	729.9	729.7	13.4	27.3	21.4	20.9	28.5	12.4	08.0	11.0	12.9	13.3	96	47	69	71	N	1	SW	2	SW	1
9	732.0	731.4	733.9	16.0	24.8	17.4	18.7	25.2	14.2	10.9	12.1	11.6	11.6	95	49	78	74	NW	1	SW	1	NW	1
10	735.4	732.7	732.0	15.2	23.7	17.5	18.5	24.0	12.2	09.1	11.0	11.9	14.2	85	54	94	78	SE	1	NE	2	NE	1
11	732.3	732.7	733.9	11.8	16.9	13.9	14.1	19.8	10.7	09.2	09.8	09.0	10.0	94	62	84	80	W	3	S	1	-	C
12	735.5	735.4	737.2	11.5	24.4	17.0	17.5	25.3	10.3	07.2	09.6	06.7	10.3	93	29	71	64	SW	1	SW	2	Nh	1
13	739.6	738.4	736.4	12.7	26.2	20.2	19.8	26.6	09.7	05.5	09.0	11.3	13.0	82	44	73	66	NE	1	SE	2	SW	1
14</td																							

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

1. JUHIS JÄRNE, BEŽIGRAD

1974 AUGUST

1	7	00≡0	C10	06	02.3	11.2	.	.	$\Delta^2 n - 9^2 4_2 = n - 4^2 4_2 \cdot 2^2 4_2 - 9^2 4_2 \equiv -4^2 4_2 - 7^2 4_2 = -4^2 4_2 - 6^2 4_2, \text{ or } 9^2 4_2 - n$
2	7	030	020	00	C1.7	11.3	.	.	$\Delta^2 n - 8^2 4_2 = n - 8^2 4_2 \cdot 2^2 4_2 - 8^2 4_2 \equiv -8^2 4_2 - 5^2 4_2, \text{ or } 8^2 4_2 - n$
3	7	050	030	C1	03.0	10.1	.	.	$\Delta^2 n - 9 = n - 9^2 4_2, 20^2 4_2 - n; \text{ or } 9^2 4_2 - 20^2 4_2$
4	7	010	010	C1	01.0	11.6	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, \text{ or } 9^2 4_2 - n$
5	7	050	020	01	02.7	11.5	.	.	$\Delta^2 n - 7^2 4_2 = 4^2 4_2 \cdot 8^2 4_2, \text{ or } 8^2 4_2 - n$
6	7	10●	090	00	04.3	C5.2	C1.2	.	$= n - 10^2 4_2, \bullet^{n-2} 4^2 8^2 4_2 - n$
7	7	10≡	070	CC	04.3	C1.5	C3.6	.	$\equiv n^2 4_2, \bullet^{n-2} 6^2 4_2 - 7^2 4_2, = 7^2 4_2 - 9^2 4_2, 20^2 4_2 - n$
8	7	020	080	05	05.0	C9.2	.	.	$\Delta^2 n - 9 = n - 4^2 4_2 - 9^2 4_2, \bullet^{n-2} 5^2 4_2 - 6^2 4_2, 20^2 4_2 - 17^2 4_2, + 20^2 4_2 - n$
9	8	090	050	01	05.0	07.0	C5.2	.	$\Delta^2 n - 9^2 4_2 = 5^2 4_2 - 8^2 4_2, 15^2 4_2 - 10^2 4_2$
10	8	040	050	CG	07.3	05.6	00.0	.	$T^2 14^2 4_2 - 15, \sqrt{14^2 4_2 - 15} - 16^2 4_2, 15^2 4_2 - 15^2 4_2, \bullet^{n-2} 15^2 4_2 - 15^2 4_2$
11	8	10●R	C30	C1	04.7	04.8	28.7	.	$= n - 4^2 4_2, T^2 n, 8^2 4_2 - 9, \bullet^{n-2} n - 9, 18 - 19^2 4_2, \bullet^{n-2} 3^2 4_2 - 8^2 4_2, \bullet^{n-2} 9 - 12^2 4_2$
12	8	10	C30	0C	04.3	10.3	11.9	.	$\equiv n^2 4_2, \bullet^{n-2} 4^2 4_2 - 10^2 4_2$
13	8	090	050	01	05.0	12.1	.	.	$\equiv n - 4^2 4_2, \bullet^{n-2} 10^2 4_2$
14	8	000	020	C1	01.0	11.7	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, \bullet^{n-2} 14^2 4_2 - 6^2 4_2$
15	7	030≡	030	00	02.0	11.5	.	.	$\Delta^2 n - 9 = n - 10^2 4_2, \bullet^{n-2} 8^2 4_2 - 9, 20^2 4_2 - n$
16	7	00≡0	000	00	00.0	11.2	.	.	$\Delta^2 n - 9, \equiv 0^2 4^2 n - 8^2 4_2, \equiv 1^2 4^2 6^2 4_2, = 6^2 4_2 - 9^2 4_2, 20^2 4_2 - n$
17	7	00≡0	010	00	00.3	11.3	.	.	$\Delta^2 n - 9 = n - 4^2 4_2, 8^2 4_2 - 10^2 4_2, \bullet^{n-2} 4^2 4_2 - 8^2 4_2, \equiv 2^2 4^2 6^2 4_2 - 6^2 4_2, = 6^2 4_2 - 10^2 4_2, 20^2 4_2 - n$
18	7	000	000	CC	00.0	11.6	.	.	$\Delta^2 n - 9^2 4_2, \bullet^{n-2} 5^2 4_2 - 8^2 4_2, \equiv 5^2 4_2 - 8^2 4_2, 15^2 4_2 - 10^2 4_2$
19	7	10≡	020	00	04.0	09.9	.	.	$\Delta^2 n - 9^2 4_2, 20^2 4_2 - n, \equiv 2^2 4^2 6^2 4_2 - 4^2 4^2 8^2 4_2, \equiv 2^2 4^2 6^2 4_2 - 8^2 4_2 - 9^2 4_2, 20^2 4_2 - 14^2 4_2$
20	7	00≡0	040	CC	01.3	11.0	.	.	$\Delta^2 n - 9, 20^2 4_2 - n, = n - 9^2 4_2, 19^2 4_2 - n, \equiv 2^2 4^2 6^2 4_2 - 8^2 4_2, 10^2 4_2 - 9^2 4_2, 20^2 4_2 - n$
21	7	090	-070	10R	08.7	09.1	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, 6^2 4_2 - 4, 20^2 4_2 - 20^2 4_2, \bullet^{n-2} 6^2 4_2 - 7^2 4_2, T^2 20^2 4_2 - n$
22	7	C9	09	C9	C9.0	02.6	C0.1	.	$\equiv n - 10^2 4_2, T^2 n - 5^2 4_2, 3^2 4_2 - 4^2 4_2, 20^2 4_2 - n$
23	8	10●R	060	09	C6.3	04.8	33.4	.	$\bullet^{n-2} 10^2 4_2, 17^2 4_2, \bullet^{n-2} 10^2 4_2, 17^2 4_2, 17^2 4_2, \bullet^{n-2} 10^2 4_2, 17^2 4_2, = n - 6^2 4_2, \bullet^{n-2} 4^2 8^2 4_2 - 10^2 4_2, \bullet^{n-2} 7^2 4_2, \equiv 5^2 4_2 - 6^2 4_2, 9^2 4_2 - 10^2 4_2, \bullet^{n-2} 6^2 4_2, 15^2 4_2 - 10^2 4_2$
24	7	10	10	03	C7.7	00.9	07.5	.	$\equiv n - 7^2 4_2, \bullet^{n-2} 5^2 4_2 - 6^2 4_2, \bullet^{n-2} 5^2 4_2 - 7^2 4_2, \bullet^{n-2} 5^2 4_2 - 8^2 4_2, 14^2 4_2 - n$
25	6	10●	10●	0?	C7.7	00.7	C1.5	.	$\equiv n - 7^2 4_2, \bullet^{n-2} 5^2 4_2 - 6^2 4_2, \bullet^{n-2} 5^2 4_2 - 7^2 4_2, \bullet^{n-2} 5^2 4_2 - 8^2 4_2, 14^2 4_2 - n$
26	7	10●	090	09	09.3	02.5	C6.5	.	$\Delta^2 n - 9^2 4_2, \bullet^{n-2} 4^2 4_2 - 11^2 4_2, \bullet^{n-2} 4^2 4_2 - 11^2 4_2, = 9^2 4_2 - 13$
27	6	10●	09R0	06	08.3	01.4	05.2	.	$\equiv n - 15^2 4_2, 6^2 4_2 - 7^2 4_2, 13^2 4_2, \bullet^{n-2} 14^2 4_2, 20^2 4_2 - n, \bullet^{n-2} 21^2 4_2 - n$
28	7	10●	10	10●R	10.0	00.0	15.2	.	$\bullet^{n-2} n - 10^2 4_2, T^2 n, \bullet^{n-2} 20^2 4_2 - n$
29	7	030	020	03	C2.7	11.2	37.4	.	$\Delta^2 n - 10, 20^2 4_2 - n, \equiv n - 4^2 4^2 7^2 4_2, \bullet^{n-2} 4^2 7^2 4_2, = 7^2 4_2 - 12^2 4_2, 20^2 4_2 - n, \bullet^{n-2} 14^2 4_2 - n$
30	7	10≡	050	01	05.3	07.9	.	.	$\Delta^2 n - 11, \equiv n - 2^2 n - 9^2 4_2, \bullet^{n-2} n - 9^2 4_2, \equiv 9^2 4_2 - 11^2 4_2$
31	7	10≡	040	1C	C8.0	06.2	00.0	.	

PES.  
WRED.

1974 SEPTEMBAR

LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

BR. ST. 13

SD	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parov e mm			Relativna vlažnost u %			Pravac i jačina vetrova D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	734.8	734.8	724.7	16.1	20.6	14.6	17.6	21.3	15.4	13.6	12.5	13.3	13.9	91	73	97	87	S	1	SE	1	NE	1
2	735.3	734.9	735.2	15.9	25.0	17.6	19.0	25.6	15.3	13.5	13.0	12.4	12.1	96	52	80	76	NE	1	S	3	SE	2
3	735.3	734.0	714.1	14.6	26.4	20.8	20.7	26.7	13.1	9.8.5	11.4	12.7	14.0	92	49	76	72	NE	1	SW	2	SW	3
4	733.8	733.6	734.5	15.8	20.6	13.1	15.7	22.7	13.1	10.6	12.5	14.6	11.1	93	79	98	90	NE	2	NE	2	NE	1
5	740.4	738.3	736.9	10.6	21.7	14.8	15.5	23.0	10.2	08.0	09.2	10.6	10.8	96	54	86	74	NE	1	NE	1	NE	1
6	714.1	729.7	728.4	11.4	25.7	16.2	17.4	25.7	10.6	06.3	10.0	10.5	13.0	99	44	94	76	NE	1	NE	1	SE	1
7	717.7	731.5	733.4	12.2	16.6	12.4	13.4	18.7	11.7	10.0	10.2	10.0	10.1	96	70	93	86	NW	3	SE	1	-	0
8	736.8	737.9	739.5	10.0	22.8	14.5	15.5	23.5	09.9	04.7	09.2	10.6	11.4	100	51	92	81	NE	1	SE	1	-	0
9	741.1	739.4	738.9	11.0	22.7	17.7	17.3	24.3	10.7	05.9	04.7	13.0	14.8	99	63	97	85	N	1	S	1	SE	1
10	740.1	740.6	745.1	13.8	25.4	14.9	17.3	25.4	13.0	08.0	11.8	12.3	11.2	100	51	88	80	-	0	E	2	SE	1
11	745.7	746.2	744.8	13.1	20.2	14.4	15.5	21.4	12.5	08.4	10.6	08.3	10.4	94	47	85	75	N	1	NE	2	NE	1
12	743.5	742.4	742.0	13.3	19.7	16.4	16.5	20.2	11.9	06.5	09.6	11.0	10.8	84	64	77	75	NE	1	SE	1	SE	1
13	741.6	740.4	741.0	11.4	23.4	16.2	16.9	24.7	10.7	05.2	10.0	11.5	12.2	90	53	87	80	NF	1	F	1	SS	3
14	741.4	740.1	740.1	13.0	26.0	18.1	18.8	26.7	12.5	07.2	11.1	14.1	14.0	99	56	95	83	SE	1	NE	1	NE	1
15	739.6	737.8	739.8	14.8	25.4	18.4	19.3	25.7	14.8	10.3	12.4	14.7	15.0	94	61	94	84	SE	1	N	2	NE	1
16	739.6	739.3	740.2	15.0	23.1	17.5	18.3	23.8	14.6	10.0	12.5	12.4	12.6	98	58	84	80	NE	1	SE	2	E	1
17	740.0	738.8	739.2	14.0	24.4	17.0	18.1	25.4	13.0	08.8	12.0	12.1	12.3	100	53	85	79	NE	1	NW	1	-	0
18	739.0	737.6	736.2	13.8	24.6	18.2	18.7	24.8	13.4	08.2	11.6	12.3	12.0	98	53	77	76	S	1	SW	3	SW	3
19	739.6	738.7	739.0	14.4	22.2	15.8	17.1	22.3	12.9	08.4	11.9	13.0	12.5	97	65	92	85	NE	1	NE	1	NE	1
20	734.7	733.6	733.4	14.0	16.4	14.8	15.0	17.4	13.8	10.0	11.7	12.8	12.1	98	91	96	95	NE	1	SE	1	N	1
21	733.6	734.1	733.0	13.8	13.7	12.4	13.1	15.1	12.4	11.9	10.5	09.7	09.4	89	82	87	86	SE	1	NE	1	SE	1
22	731.7	733.0	734.1	11.8	15.9	14.8	14.3	17.0	11.4	07.7	09.8	10.3	12.0	94	76	95	86	-	0	NE	1	-	0
23	736.4	736.4	733.9	10.0	11.8	11.0	11.0	15.3	09.5	08.0	08.7	08.3	08.8	94	80	90	86	NW	1	N	1	SW	1
24	729.2	726.0	725.5	05.2	15.4	13.2	12.5	16.7	08.6	04.6	08.6	11.6	11.1	99	82	98	95	-	0	NW	1	NW	1
25	726.7	725.4	722.7	08.4	10.7	09.0	09.3	13.4	08.3	06.7	07.9	07.8	08.2	95	81	95	90	SW	1	ENE	2	N	1
26	721.0	723.6	729.4	08.0	15.1	07.8	09.7	16.1	07.3	01.5	07.9	08.1	07.3	99	63	92	85	NW	1	SW	2	E	1
27	735.7	735.4	736.3	03.4	18.3	09.3	10.1	19.0	03.4	-01.4	05.8	04.1	06.0	100	26	91	72	NE	1	NE	1	NE	1
28	734.9	733.1	732.9	05.6	20.6	13.8	13.5	20.6	04.2	-00.5	06.3	07.9	08.1	92	43	65	68	NE	1	W	3	SW	2
29	729.0	731.3	732.9	11.0	19.6	12.1	13.7	20.0	09.8	03.9	09.6	12.6	09.3	98	74	88	87	NW	2	SW	1	NE	3
30	734.6	734.8	735.5	09.7	11.1	09.2	09.8	12.8	09.1	07.7	07.6	09.0	08.6	95	81	99	88	E	1	NE	3	NE	1
MES.	WRF.D.	736.0	735.4	735.0	12.0	20.2	14.6	15.4	21.2	11.2	07.5	10.2	11.0	11.3	96	63	89	82	1.0	1.6	1.1		

1974 OKTOBAR

LJUBLJANA BEŽIGRAD

1	735.7	735.3	736.2	07.2	13.2	07.4	08.8	13.3	06.5	05.0	07.4	07.5	07.3	97	66	95	86	SE	1	SE	2	NW	1
2	734.6	733.4	733.6	06.9	06.4	05.4	06.0	07.7	05.4	04.8	07.4	06.3	06.3	99	68	94	94	NE	1	NE	2	SW	1
3	736.4	736.2	735.7	04.0	10.4	08.0	07.6	11.7	03.1	-01.5	05.9	06.7	07.6	97	71	97	88	NE	1	SW	2	NE	1
4	733.8	735.7	737.4	10.6	11.4	06.7	08.9	12.0	06.7	05.6	09.0	09.9	07.2	94	98	97	96	N	2	ENE	1	SW	1
5	737.1	736.4	735.5	05.4	06.0	06.0	06.5	07.4	05.0	03.5	05.3	06.6	06.9	94	88	93	92	SE	1	S	2	N	1
6	734.8	735.6	736.4	06.3	09.2	04.0	05.5	10.0	04.0	03.4	06.8	05.8	05.9	95	67	97	86	SE	1	SE	2	NE	1
7	734.5	730.1	729.2	03.3	11.0	06.3	06.7	11.1	02.8	-03.1	05.8	06.1	06.8	100	62	95	86	NE	1	SE	1	N	1
8	725.7	728.3	731.1	06.6	07.2	06.0	06.5	07.6	05.4	-01.0	07.1	06.7	06.7	97	88	96	94	SW	2	N	2	NW	1
9	731.9	731.9	734.4	04.2	11.4	07.4	07.6	12.1	04.1	01.0	05.9	06.4	07.3	96	63	95	85	NW	1	SE	1	NW	2
10	737.0	736.6	737.4	04.0	10.9	04.8	06.1	12.2	02.8	-03.0	05.9	06.8	06.2	97	70	96	88	S	2	SE	1	-	0
11	737.0	736.5	737.3	04.2	09.9	08.1	07.6	10.1	03.6	00.5	06.0	07.5	07.9	97	82	97	92	N	1	N	1	SE	1
12	736.0	735.9	734.8	07.1	08.4	07.6	07.7	08.9	07.0	00.4	07.2	07.5	07.4	95	51	95	94	NE	1	N	1	N	1
13	734.9	736.0	736.6	07.1	07.9	06.6	07.1	08.3	06.6	05.5	07.3	08.8	06.9	96	85	95	92	NE	1	SSE	1	NF	1
14	735.5	735.3	736.2	06.0	08.9	05.5	06.5	09.0	05.4	03.5	06.6	05.7	06.1	94	68	90	84	N	1	SE	2	NE	1

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Insekcija broj sati	Podzemna voda mm	Snežni pokrovac h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7	05	10•	10	05.7	03.0	04.2	.		
2	7	10	040	05	06.2	08.4	11.0			
3	7	010	040	01	02.0	11.3	.			
4	7	070	08=	04	04.3	02.7	03.8	.		
5	6	050	010	01	02.3	10.3	03.4	.		
6	7	10=	020	02	04.7	05.7	00.0	.		
7	8	09•	050	06	06.0	01.2	42.2	.		
8	8	10=	020	00	04.0	09.8	00.1	.		
9	7	10=	080	02	01.7	06.4	.	.		
10	7	10=	040	10	08.7	06.8	00.1	.		
11	6	050	020	00	02.3	10.2	01.9	.		
12	7	10	10	09	04.7	00.4	.	.		
13	7	10=	000	00	03.3	07.9	.	.		
14	6	10=	010	00	02.7	08.9	.	.		
15	7	10=	010	00	03.7	07.2	.	.		
16	7	10=	080	06	08.0	04.7	.	.		
17	7	10=	030	04	05.7	06.6	.	.		
18	7	10=	040	00	04.7	06.2	.	.		
19	6	10=	09	02	07.0	01.2	00.0	.		
20	4	10=	10•	10•	10.0	00.0	03.8	.		
21	6	10•	10•	10	10.0	00.0	14.7	.		
22	6	10	10•	10	10.0	00.3	01.6	.		
23	8	10	10	10	10.0	00.0	35.4	.		
24	7	10=	10•	10•	10.0	00.0	01.8	.		
25	7	10	090	09	04.3	00.7	33.1	.		
26	8	09	050	01	05.0	04.3	06.2	.		
27	8	10=	030	00	04.2	09.1	.	.		
28	9	10	020	01	04.3	10.3	.	.		
29	7	10•	050	10	08.3	02.2	00.8	.		
30	8	10•	10	10•	10.0	00.0	05.3	.		
MES. VRKD.			09.2	05.0	04.0	06.5	145.8	165.4		

1	8	10•	070	09	08.7	01.9	11.3	.		
2	6	10•	10•	10	10.0	00.0	07.1	.		
3	7	10	090	10•	09.7	02.3	09.9	.		
4	4	10•	10•	10•	10.0	00.0	10.2	.		
5	7	10•	10	10•	10.0	00.0	05.8	.		
.										
6	8	10•	05	00	06.3	02.2	04.0	.		
7	6	080	03	07.0	02.2	00.0	.	.		
8	7	10•	10	00	06.7	00.3	24.3	.		
9	7	10•	050	10•	08.3	04.2	10.9	.		
10	7	10=	030	00	04.3	04.4	16.4	.		
.										
11	7	10=	09	10	09.7	01.0	00.2	.		
12	5	10	10•	10•	10.0	00.0	07.4	.		
13	7	10	10	10	10.0	00.0	12.1	.		
14	7	10	10	08	09.3	00.0	00.3	.		
15	7	10=	09	10•	09.7	00.0	.	.		
.										
16	6	10•	090	04	07.7	00.0	02.3	.		
17	8	10=	020	02	04.7	05.8	06.4	.		
18	8	020	040	09	05.0	08.3	.	.		
19	7	10	10	10	10.0	02.4	00.9	.		
20	4	10•	10•	10•	10.0	00.0	05.6	.		
.										
21	7	10•	10•	10	10.0	00.0	37.5	.		
22	8	10=	040	10	08.0	06.3	03.4	.		
23	8	10=	030	01	04.7	06.2	.	.		
24	8	070	09	08	08.3	02.7	.	.		
25	7	04=	020	02	02.7	08.1	.	.		
.										
26	6	10	080	06	08.0	00.0	.	.		
27	7	10=	040	10	08.0	05.6	00.2	.		
28	5	10•	10•	10•	10.0	00.0	01.7	.		
29	6	10=	060	00	05.3	04.0	10.6	.		
30	6	10=	000	04=	04.7	03.4	.	.		
31	6	09	070	07	07.7	00.4	01.3	.		
.										
MES. VRKD.		09.4	07.3	06.9	07.9	71.9	283.4			

1974 NOVEMBAR

## LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

BP. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, I (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	732.1	732.3	734.7	-00.4	10.2	02.8	04.1	10.9	-00.1	-04.4	04.3	03.1	03.1	91	33	56	60	NF	1	NW	2
2	735.2	733.7	736.2	-03.0	10.9	05.2	04.6	10.9	-03.0	-10.0	03.4	04.0	04.1	94	40	62	65	F	1	SW	4
3	737.0	737.1	737.5	-02.8	12.9	04.2	04.6	14.8	-02.8	-08.7	03.5	03.5	04.4	94	31	71	65	SE	1	NE	1
4	736.8	734.6	735.7	-01.1	09.9	04.2	05.3	10.3	-01.6	-07.3	04.0	04.7	06.3	95	52	89	79	NF	1	NE	1
5	737.1	738.6	741.3	04.4	06.2	04.7	05.0	06.6	04.4	02.6	06.0	05.9	05.8	96	82	90	89	N	3	NE	1
6	742.7	743.2	744.9	01.0	03.3	03.5	02.8	05.0	00.9	-01.5	04.7	05.4	05.7	95	94	97	95	NW	1	E	1
7	744.5	742.9	742.6	04.0	05.2	04.3	04.5	05.3	03.5	-01.2	05.6	05.6	05.7	92	84	91	89	N	1	S	1
8	741.4	740.5	742.0	03.3	07.2	01.7	03.2	08.3	01.2	-00.6	05.1	04.3	04.2	98	56	85	75	SW	1	SW	2
9	742.3	740.7	741.0	-02.2	08.7	01.0	01.9	09.2	-03.6	-09.5	03.5	04.2	04.3	100	46	88	79	SF	1	SE	1
10	740.1	738.2	738.7	-02.2	07.8	03.6	03.0	09.2	-03.6	-09.5	03.4	04.0	05.0	98	58	85	80	E	1	E	1
11	740.7	740.0	739.9	00.7	11.3	03.3	04.7	12.3	00.2	-05.5	04.6	04.4	05.0	95	44	86	75	E	1	SW	1
12	738.9	737.5	737.2	-00.9	10.7	04.0	04.5	11.4	-01.3	-06.5	04.1	05.4	06.3	96	56	79	77	NE	1	W	2
13	737.9	738.7	739.0	05.3	09.9	08.3	08.0	10.0	04.0	00.0	05.6	06.5	07.5	85	71	91	82	N	1	E	1
14	738.3	738.4	739.2	07.6	12.6	16.2	10.2	13.6	07.2	01.0	06.8	06.9	06.8	87	63	73	74	SW	1	WNW	2
15	738.5	738.9	738.7	11.0	11.6	12.7	12.0	13.0	09.6	05.0	08.4	09.6	08.3	85	93	76	85	WSW	3	W	3
16	737.6	736.8	738.0	12.7	14.4	12.8	13.2	15.3	12.5	10.3	07.9	07.0	08.2	72	57	74	64	SW	2	SW	3
17	740.2	740.4	740.5	10.8	15.0	06.7	10.4	16.0	09.5	09.9	03.7	09.4	07.6	90	74	90	85	SW	1	NW	3
18	739.7	739.4	738.0	10.2	14.4	12.9	12.6	14.8	05.8	00.0	06.9	07.4	08.0	74	60	72	69	W	3	SW	3
19	732.6	732.2	737.9	09.9	10.1	04.8	07.2	13.0	04.6	07.9	07.2	05.6	90	78	87	85	-	0	N	3	
20	740.1	739.6	739.9	03.1	05.9	04.5	04.5	06.4	03.0	-00.5	05.5	05.9	05.8	97	85	91	91	SE	1	NE	1
21	738.2	738.2	739.0	03.6	07.2	05.0	05.3	08.0	03.5	00.5	06.0	06.4	06.3	100	84	96	93	N	1	SW	1
22	739.6	738.4	738.4	03.8	08.5	06.0	07.1	08.7	03.6	03.4	05.7	06.4	06.5	95	77	81	84	N	1	SW	1
23	738.6	737.5	737.6	04.6	10.2	06.9	07.2	10.4	04.1	00.5	06.0	06.9	06.7	94	74	89	86	-	0	NW	1
24	737.5	737.2	737.5	05.4	08.4	07.4	07.2	08.8	05.1	04.9	06.4	07.0	07.3	96	85	95	92	NNE	1	-	0
25	735.0	731.7	731.2	07.2	09.4	06.4	07.4	10.2	06.2	05.6	07.4	07.1	06.5	97	80	91	89	SSW	2	NE	1
26	734.1	732.9	731.5	03.4	08.3	02.1	04.6	08.6	02.1	02.3	05.2	04.6	04.9	89	56	92	79	N	1	S	1
27	729.6	731.3	731.5	01.6	08.4	02.0	03.6	08.6	00.2	-04.2	04.7	04.9	04.5	92	59	86	75	NNE	1	SE	3
28	721.4	720.6	723.8	02.3	02.4	02.0	02.2	06.1	00.4	-00.2	05.1	05.1	05.0	94	94	94	94	SE	1	SE	2
29	725.1	726.0	729.1	-01.0	02.0	00.7	00.6	02.6	-01.4	-04.0	04.2	05.0	04.7	98	95	97	97	NF	1	ESE	1
30	733.5	735.6	735.9	-00.3	01.1	-00.2	00.1	01.3	-00.4	-00.5	04.3	04.3	04.3	96	87	95	93	NW	1	N	1
31	MES.	WRFD.	736.9	736.4	737.3	03.3	08.2	05.4	05.8	09.6	02.4	-00.4	00.4	92	68	85	82	1.2	1.8	1.2	

1974 DECEMBAR

## LJUBLJANA BEŽIGRAD

1	734.8	737.0	741.6	-00.7	07.4	02.2	02.8	08.0	-01.2	-01.5	04.1	05.0	05.0	94	65	94	84	N	1	-	U	SSW	1
2	741.6	732.2	745.3	01.4	05.0	01.2	02.2	06.6	00.2	-04.1	04.5	04.7	04.6	95	58	82	85	NE	1	NF	1		
3	745.9	746.1	746.3	-01.6	06.4	00.7	01.6	07.0	-01.6	-03.8	03.9	05.6	04.6	98	80	95	91	S	1	-	C	NE	1
4	745.3	742.6	740.0	-01.0	01.1	00.2	00.1	01.8	-01.3	-05.0	04.1	04.8	04.6	96	97	96	97	-	0	-	0	-	0
5	737.1	735.6	735.7	-01.5	-00.2	-00.3	-00.6	00.7	-01.7	-01.3	04.0	04.4	04.3	98	98	96	97	NE	1	SE	1	E	1
6	737.6	736.8	737.2	-01.3	00.4	00.0	00.2	00.6	-01.3	-01.3	04.0	04.6	04.6	98	96	97	97	SF	1	W	1	N	1
7	736.5	734.9	735.3	-01.6	-00.2	-00.8	-00.9	00.6	-01.7	-01.4	03.9	04.4	04.2	96	96	96	96	NE	1	NE	1	N	1
8	733.5	733.6	736.3	-01.6	07.5	02.0	02.9	08.4	-01.8	-04.4	03.8	05.9	05.3	94	75	94	88	NE	1	ENE	1	-	0
9	737.7	737.6	739.2	00.0	04.0	01.4	01.7	05.1	00.0	-05.1	04.4	05.7	04.9	96	94	97	96	-	0	N	1	-	0
10	738.9	738.6	739.7	00.0	01.4	02.6	01.7	02.7	-00.3	-00.2	04.5	05.0	05.3	98	93	95	97	ENE	1	E	1	NE	1
11	737.7	733.1	728.4	03.2	04.4	04.7	04.3	05.0	04.6	01.7	05.4	06.1	06.2	94	97	97	96	SE	1	N	1	NF	1
12	731.3	733.0	732.3	01.8	03.1	00.1	01.2	07.1	-00.6	-00.0	04.7	04.2	04.4	90	74	95	86	SE	2	SE	1	W	1
13	726.5	726.8	732.9	-00.9	03.7	02.3	01.9	04.1	-00.8	-05.4	04.2	04.3	02.3	96	72	42	70	SW	1	SW	2	ENE	1
14	729.0	738.9	740.2	-02.2	05.4	-00.6	00.4	05.6	-02.4	-03.2	02.5	02.6	02.9	98	39	68	58	W	1	SSW	1	S	1
15	739.5	737.8	737.5	-06.4	01.2	-01.7	-01.9	02.4	-06.7	-10.3	02.5	03.5	03.3	95	68	78	80	NE	1	N	1		
16	738.6	738.3	739.0	-04.6</td																			

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

MES. 68-3 97-5 86-5 67-5 72-4 106-5

I JUBI JANA BEŽIGRAD

1974 DECEMBER

PES.  
WRED. 07.4 06.4 06.7 06.8 56.9 30.7

1974 JANUAR

ZAGREB GRČ

 $\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	755.0	754.6	754.7	01.3	02.1	01.3	01.5	02.5	00.6	-	04.3	04.8	04.6	86	88	92	89	NN	2	NN	2	NE	1
2	753.8	752.8	752.5	01.5	02.4	01.7	01.8	02.7	01.0	-	04.8	05.0	05.0	93	93	97	94	NN	1	E	1	NE	1
3	751.1	750.7	752.0	01.8	02.2	01.9	02.0	02.3	01.4	-	05.0	05.3	04.8	95	98	91	95	NN	1	SSE	1	SSE	1
4	753.8	754.9	756.8	01.1	02.1	01.4	01.5	02.2	01.1	-	04.8	05.0	04.6	97	93	93	94	SSE	1	SSW	1	SSW	1
5	756.3	754.6	753.8	01.5	02.7	02.9	02.5	03.0	01.1	-	04.8	05.0	05.0	95	90	91	92	SSW	1	SSW	1	SSW	1
6	750.0	747.5	748.9	02.4	04.0	02.9	03.0	04.2	02.2	-	05.3	05.6	05.3	96	91	94	94	SSW	1	NE	2	SE	1
7	752.0	752.4	752.4	02.3	03.8	03.3	03.2	04.0	02.2	-	05.0	04.8	04.9	92	77	85	85	SSE	1	WNW	2	WSW	2
8	751.2	752.2	753.5	02.8	04.4	03.2	03.4	04.4	02.5	-	04.8	05.3	05.0	87	86	86	86	NE	1	ENE	1	SSE	1
9	752.0	751.1	750.0	02.5	03.0	01.8	02.3	03.2	01.8	-	05.0	05.0	04.7	92	87	90	90	ESF	2	SSE	2	FSE	2
10	749.0	751.1	753.8	00.5	01.1	06.7	00.8	01.8	-00.4	-	04.6	04.6	03.9	96	91	81	89	ENE	2	ENE	2	ENE	2
11	755.6	755.6	756.4	00.3	01.0	01.4	01.0	01.4	-00.5	-	03.9	04.0	04.1	84	82	82	83	S	2	SW	1	SSW	2
12	757.0	757.2	757.6	-00.4	04.8	02.4	02.3	05.3	-00.4	-	04.0	04.8	04.6	91	75	85	84	ENE	1	ENE	1	WNW	1
13	756.8	756.8	757.9	-00.4	-00.3	00.4	00.0	02.4	-01.4	-	04.4	04.1	04.3	100	95	92	96	SSW	1	ENE	2	NNE	2
14	757.8	757.7	756.6	00.1	00.8	-00.5	00.0	01.4	-00.6	-	03.8	03.4	03.2	82	71	73	75	ESE	2	ESE	2	WSW	1
15	756.1	755.8	755.5	-00.3	01.5	01.2	00.9	01.7	-00.5	-	03.4	03.6	04.4	75	71	88	78	WSW	2	SSW	2	ENE	1
16	754.6	754.3	752.1	00.7	03.1	02.3	02.1	03.5	00.5	-	04.3	05.0	04.9	89	86	91	89	NE	1	SW	1	SW	1
17	747.0	748.3	751.5	01.2	02.8	03.7	02.8	03.9	00.9	-	04.6	05.4	05.6	92	96	93	94	SW	1	NNW	2	W	2
18	752.1	751.3	752.0	01.7	04.4	03.5	03.5	04.4	00.7	-	04.2	04.6	04.6	80	75	76	77	W	2	ENE	1	NNE	1
19	752.5	752.2	751.6	03.3	06.2	07.0	05.9	07.2	03.2	-	05.1	05.8	06.6	88	81	87	85	W	2	W	2	W	2
20	750.5	751.2	754.4	06.8	14.4	07.3	09.0	14.8	06.4	-	05.9	07.4	06.4	80	60	84	75	EN	1	ESF	2	NW	2
21	755.6	755.1	756.2	02.0	07.5	02.5	04.3	07.9	01.7	-	05.0	06.2	05.2	93	79	86	86	E	1	SSF	2	NNE	1
22	755.3	753.6	753.7	-01.5	03.1	00.7	00.8	03.9	-02.1	-	04.0	05.0	04.6	98	86	96	93	SSF	1	SSF	1	NNW	1
23	755.6	754.7	753.3	00.3	03.2	00.8	01.3	03.8	-01.2	-	04.4	04.4	04.4	93	76	92	87	WSW	1	WSW	2	WSW	1
24	753.5	752.7	751.2	-01.0	00.0	-00.8	-00.5	00.8	-01.0	-	04.1	04.6	04.2	96	95	98	96	SW	1	SSE	1	SSE	1
25	751.1	750.7	752.1	-00.0	02.5	01.3	01.1	03.4	-01.4	-	04.2	05.0	04.8	96	92	95	94	SSF	1	SSE	1	SSE	1
26	752.5	752.0	751.7	-00.4	00.5	-00.5	-00.2	01.3	-00.9	-	04.3	04.6	04.3	96	95	98	96	SSW	1	SSW	1	S	1
27	749.3	748.2	749.7	-01.2	01.1	01.3	00.6	02.3	-02.0	-	04.0	04.7	05.0	96	94	99	96	SW	1	SSE	1	WSW	1
28	752.2	751.9	751.9	01.2	03.5	01.8	02.1	03.7	00.7	-	04.9	05.5	05.0	98	94	97	96	NNW	1	WSW	1	WSW	1
29	751.2	750.4	751.4	00.9	02.1	02.4	02.0	02.8	00.6	-	04.7	04.8	05.2	97	90	96	94	SSE	1	SSE	1	NNE	1
30	754.4	755.0	755.0	00.8	03.3	03.3	02.7	03.3	00.5	-	04.8	05.4	05.6	98	94	96	96	NE	1	SSE	1	ENE	1
31	754.4	753.5	753.2	02.0	06.7	07.1	05.7	07.1	01.7	-	05.2	05.9	06.3	98	80	82	87	SF	1	SE	1	NW	1
MES.	MRED.			753.2	752.9	753.3	01.1	03.2	02.3	02.2	03.8	00.6	-	04.6	05.0	04.9	92	86	90	89	1.2	1.4	1.2

1974 FEBRuar

ZAGREB GRČ

1	751.5	750.5	750.1	05.9	08.5	08.6	08.0	09.6	05.7	-	05.8	06.1	07.4	85	73	82	82	ENE	1	S	1	W	2
2	749.8	749.4	750.6	07.0	13.3	10.2	10.2	13.4	07.0	-	06.7	07.2	07.0	89	63	75	76	S	1	SW	3	WSW	2
3	749.5	746.8	745.0	06.7	11.3	09.0	09.0	11.3	06.7	-	05.7	05.8	07.2	77	57	84	73	ENE	2	ENE	2	NNE	2
4	742.4	741.2	742.2	06.8	07.4	05.7	06.4	09.0	05.7	-	06.7	07.4	06.1	91	96	88	92	W	1	S	1	ENE	2
5	742.3	740.5	739.1	04.6	07.8	06.3	06.2	07.9	04.5	-	05.8	06.6	06.0	90	84	85	86	SW	1	S	1	WSW	2
6	732.3	725.2	719.8	06.8	11.4	10.7	09.9	11.5	05.4	-	05.5	05.9	06.6	74	58	69	67	WSW	2	SSW	4	S	2
7	724.5	727.2	731.1	01.0	07.1	05.1	04.6	10.7	01.0	-	04.6	05.8	03.8	95	75	67	79	W	2	WSW	2	NW	2
8	739.2	744.0	748.1	02.9	09.4	04.7	05.4	09.4	02.6	-	03.5	03.0	02.4	63	35	37	45	NNW	2	WNW	2	N	2
9	748.0	747.6	748.9	02.9	11.1	07.4	07.2	11.8	02.6	-	03.1	03.1	04.4	55	31	58	48	WSW	2	W	3	WSW	3
10	749.0	749.9	749.8	08.5	13.4	05.8	10.4	13.5	05.7	-	05.2	05.8	05.7	63	50	63	59	WNW	3	WSW	2	W	3
11	747.6	744.4	742.9	04.3	14.9	10.0	05.6	14.9	04.1	-	05.2	06.0	05.6	84	47	61	64	WSW	2	WSW	5	SW	4
12	741.5	740.6	740.4	10.7	14.7	10.5	11.6	14.8	09.5	-	06.0	05.8	06.1	62	46	64	57	WSW	4	WSW	5	WSW	2
13	738.9	737.3	737.4	05.1	10.4	08.2	08.0	10.5	04.9	-	05.8	05.3	07.2	87	56	88	77	NNE	1	NE	2	S	1
14	738.0																						

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	5	10*	10*	10*	10*	10.0	00.0	05.1	.	=n-n, *tr-6° 13° 15°, *6° 13° 15° n; █	
2	4	10*	10*	10	10.0	00.0	15.6	.	=n-n, *tr-7° 17°, █		
3	1	10	10	10	10.0	00.0	00.5	.	=n-8, 16° 7°, *tr-7°, 16-17; =8-16°		
4	4	10	10	10	10.0	00.0	00.2	.	=n-n		
5	5	10	10	10	10.0	00.0	02.1	.	=n-ni, *tr-6°, =0 10° 12°		
6	5	10*	10*	10*	10.0	00.0	00.4	.	*n-n, =n-8°, =8° n		
7	6	10	10	10	10.0	00.0	09.5	.	=n-n		
8	3	10	10	10	10.0	00.0	00.0	.	=n-n, *tr-7°, 8° 10°, =12° 14°		
9	6	10	10	10	10.0	00.0	00.0	.	=n-n		
10	4	10*	10	10	10.0	00.0	00.0	.	=n-n, *tr-9°, =n-ni, =8° 9°, *tr-15°, 16°		
11	5	10	10	10	10.0	00.0	00.0	.	=n-n		
12	4	07	07	07	05.7	03.3	.	.	=n-n		
13	2	10	10	10	10.0	00.0	.	.	=n-14, *tr-9°, =14-n, *tr-19° n		
14	5	10	10	06	08.7	00.0	00.1	.	=n-n, *tr-14° 14°, *tr-0° 15° -n		
15	5	10	10	10	10.0	00.1	.	.	=n-n, *tr-14° 14°, *tr-0° 15° -n		
16	4	10*	10	10	10.0	00.0	02.5	.	=n-n, *tr-7°, 8°		
17	3	10	10	10	02	07.3	00.0	00.1	=n-7°, 14°, =14° n, *tr-0° 8° 14°		
18	4	09	09	03	07.0	01.0	06.6	.	=n-7°, 10°, =n-ni, =8° 10°		
19	5	10	10	10	10.0	00.0	00.5	.	=n-7°, 10°, =n-ni, =9° 11°		
20	6	10	01	00	03.7	05.6	02.0	.	=n-10°		
21	5	00	07	04	03.7	05.6	.	.	=0-1 n-12°, =12° n		
22	3	10	00	10	06.7	04.3	.	.	=2 n-9°, 16°, =19° n, =16°		
23	3	10	01	08	06.3	02.5	.	.	=n-7°, 13°, =17° 13°		
24	2	10	10	10	10.0	00.0	.	.	=0-1 n-12°, =13° n		
25	3	10	05	10	09.7	00.0	.	.	=0-2 n-13°, 16°, =13° 16°, *tr-9°, 11°		
26	1	10	10	10	10.0	00.0	00.0	.	=+2 n-n, *tr-7°, 9°		
27	4	10	08	10	09.3	00.1	00.0	.	=+2 n-14°, 17°, =11° 17°, *tr-0° 12° 13°		
28	3	10	10	10	10.0	00.0	00.1	.	=+2 n-n, *tr-7°, 14°, =0-1 n-14°, 20°		
29	3	10	10	10	10.0	00.0	00.0	.	=+2 n-n, *tr-7°, 14°, =14° 20°		
30	3	10	10	10	10.0	00.0	00.0	.	=+2 n-n, *tr-7°, 14°, =17° 14°		
31	4	10	09	09	09.3	01.2	.	.	=2 n-10°, *tr-8°, =10° 11°, 16° 18°, =11° 16°, 18°		
MES. VR.ED.		09.5	08.6	08.7	08.9	23.7	46.5				

1	3	09	10	10	09.7	00.3	.	.	=n-10°, 13°, *tr-8°, 11°, =0 10°, 13°		
2	7	03	09	06	06.0	01.1	00.0	.	=n-9°, 17°, n		
3	7	09	10	10	09.7	01.0	.	.	=n-7°, 15°, =0-1 n-16°, 20°		
4	3	10	10	10	10.0	00.0	01.5	.	=n-8°, 13°, =0 8°, 13°, *tr-10°, n		
5	5	10	05	04	06.3	02.5	05.5	.	=n-n		
6	8	10*	09	10	09.7	01.1	00.0	.	=+0-1-2 n-8°, 10°, =10°, *tr-0° 12° 13°		
7	9	10*	06	03	06.3	04.2	14.0	.	=+0-1 n-7°, 10°, =2 n-7°, 10°, =7° 10°, 11°, =7° 10°, 11°		
8	8	06	01	00	02.3	08.4	01.5	.	=n-11°, 11°, =17° 14°, 20°, =14° 20°		
9	8	09	08	01	06.0	04.4	.	.	=0-1 n-14°, 17°, =17° n		
10	6	05	04	00	03.0	07.0	.	.	=2 n-10°, *tr-8°, =10° 11°, 16° 18°, =11° 16°, 18°		
11	8	00	01	00	00.3	08.4	.	.	=n-7°, Fsw 13-17°		
12	8	00	01	00	00.3	09.0	.	.	Fsw 11-12		
13	6	02	10	10	07.3	01.6	.	.	=0-1 n-7°, 7°, 7°, n, *tr-0° 13°, 15°		
14	5	10*	10*	10	10.0	00.0	01.0	.	=tr-0° 12°, 12°, =0-1 n-12°, =12°		
15	5	10*	10	10	10.0	00.2	07.4	.	=0-1 n-10°, =10° n		
16	4	10	10	10	10.0	00.0	.	.	=n-n, *tr-17°		
17	6	10	07	04	07.0	01.6	00.0	.	=n-n		
18	3	10	10	10	10.0	00.1	00.1	.	=0-1 n-13°, =13° n		
19	7	10	05	00	06.3	01.3	00.0	.	=tr-0° 11°, 11°, =0-1 n-11°, =11° 11°		
20	6	04	09	10	07.7	03.0	01.3	.	=0-1 n-8°, =8° n		
21	6	10	05	09	09.3	00.2	.	.	=n-n		
22	5	10	05	09	09.3	02.5	.	.	=n-n		
23	5	10	10	10	10.0	00.0	.	.	=n-n		
24	5	10	10	10	10.0	00.0	00.0	.	=n-n, *tr-0° 6°, n, FNE 7°, 8°, 19°-n		
25	5	09	09	10	09.3	00.5	01.4	.	=n-n, FNE n-7°, n		
26	6	10	10	10	10.0	00.0	.	.	=n-n, *tr-0° 7°, 12°		
27	6	10*	05	10	09.7	01.1	00.1	.	=n-n, *tr-0° 6°, 9°		
28	8	02	03	10	05.0	07.0	00.0	.	=n-n		
MES. VR.ED.		07.9	07.8	07.0	07.5	66.5	33.8				

1974 MART

ZAGREB GRČ

 $\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost v%			Pravac i jačina vetro D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	750.3	748.6	747.3	00.5	05.2	02.6	02.8	05.3	00.5	-	03.0	03.2	03.2	64	48	58	57	ENE 1	SSE 2	NE 1	
2	744.8	744.3	745.1	01.7	03.4	05.1	03.8	05.1	01.4	-	03.6	04.0	04.6	69	68	69	69	ENE 2	NNE 2	NNE 3	
3	747.6	749.1	750.5	01.1	04.7	03.0	03.0	05.1	01.1	-	03.3	03.7	03.8	65	57	67	63	ENE 2	SE 3	NNE 1	
4	749.6	748.4	745.9	02.6	03.4	06.0	04.5	06.0	01.8	-	04.0	04.6	06.4	72	79	91	81	ENE 2	ENE 2	NE 3	
5	743.4	744.4	744.8	06.0	07.4	06.1	06.4	07.5	05.2	-	06.1	06.6	06.3	87	86	88	87	NNE 3	NE 2	ENE 2	
6	745.0	746.8	749.1	03.2	03.5	04.0	03.7	06.1	02.5	-	04.8	05.1	05.0	84	86	83	84	ENE 3	NNE 3	NNE 3	
7	750.2	751.1	752.0	03.1	04.9	02.9	03.4	04.9	02.9	-	04.4	04.6	04.8	75	71	85	77	NE 3	NE 2	ENE 2	
8	751.4	751.2	751.7	01.7	03.0	02.5	02.4	03.2	01.5	-	04.8	04.5	04.6	92	80	85	86	SSE 2	NNE 3	NNE 2	
9	751.4	752.0	753.6	01.3	02.5	01.9	01.9	03.2	01.3	-	04.5	04.2	04.2	90	75	81	82	NE 2	NE 2	NE 2	
10	752.9	753.0	754.0	01.2	03.0	02.5	02.3	03.1	01.2	-	04.6	04.6	04.4	92	81	79	84	ENE 1	ENE 2	NE 2	
11	754.6	755.8	757.1	02.4	04.6	03.7	03.6	04.9	02.2	-	04.6	04.8	04.5	85	74	75	78	NE 2	ESE 2	NE 1	
12	757.2	756.1	754.4	02.4	05.6	04.6	04.3	05.6	02.4	-	04.7	04.3	03.9	87	63	61	70	ENE 1	E 2	N 1	
13	751.4	749.0	748.0	03.4	08.1	05.2	05.5	08.7	03.4	-	04.9	04.4	04.2	82	54	64	67	NE 1	S 2	NNE 1	
14	745.8	743.4	742.1	00.4	11.0	08.2	07.0	11.0	00.4	-	04.2	05.3	05.1	89	54	62	68	N 1	ESE 2	NE 2	
15	741.6	741.6	742.3	07.2	10.8	08.0	08.5	10.8	06.7	-	04.4	06.1	05.1	57	63	63	61	NNE 2	ENE 1	ENE 1	
16	741.8	739.6	740.5	04.8	12.2	10.4	09.4	13.1	04.2	-	04.5	04.9	04.9	70	46	52	56	NE 1	WSW 2	WSW 1	
17	741.6	742.6	743.8	05.2	14.5	12.8	11.3	16.0	04.9	-	04.3	05.2	06.0	65	42	54	54	SSW 1	WSW 3	WSW 2	
18	744.8	743.8	744.2	11.2	18.3	13.7	14.2	18.3	07.4	-	05.1	06.0	06.6	51	38	56	48	NW 3	WSW 4	W 4	
19	745.8	746.3	748.4	13.8	20.1	14.2	15.6	20.1	12.9	-	07.0	07.0	06.8	59	40	56	52	W 4	W 4	W 3	
20	749.6	749.4	749.8	10.2	19.2	16.0	15.4	19.9	10.1	-	07.2	07.9	07.9	77	47	58	61	W 2	SSW 3	NW 2	
21	751.5	750.5	751.1	08.8	21.9	19.1	17.2	22.5	08.8	-	07.0	06.2	05.8	83	31	35	50	W 1	E 2	NE 2	
22	751.3	749.5	747.8	10.2	22.7	19.2	17.8	23.1	10.2	-	05.7	07.2	06.9	61	35	41	46	N 2	E 2	N 2	
23	747.2	747.5	748.9	13.6	19.9	15.6	16.2	20.2	11.7	-	05.7	06.6	06.5	49	38	49	45	N 1	WSW 2	W 2	
24	750.7	749.6	748.9	09.1	21.2	18.1	16.6	21.4	09.1	-	06.8	06.4	06.6	78	34	42	51	SSE 1	SSE 2	NNE 3	
25	749.0	749.3	749.7	13.1	15.9	13.1	13.8	18.1	13.1	-	07.2	08.3	07.2	65	61	64	63	NE 3	ENE 2	NNE 1	
26	749.7	747.3	746.1	08.0	17.7	15.4	14.1	18.6	07.7	-	06.7	07.5	07.4	83	50	57	63	NE 1	ESE 2	NNF 2	
27	744.8	744.3	744.8	11.0	19.4	14.0	14.6	19.8	10.3	-	05.6	08.5	07.6	77	50	67	65	E 1	SSW 1	WW 2	
28	746.2	746.0	747.1	10.3	19.5	13.2	14.0	19.5	10.0	-	07.7	07.4	09.0	82	44	79	68	ENE 1	ESE 2	NNE 2	
29	748.7	748.3	749.3	08.9	19.1	16.0	15.0	19.6	08.3	-	07.5	08.0	07.5	89	48	55	64	ENE 1	SE 2	NNE 2	
30	751.2	750.9	751.4	09.5	14.3	11.5	11.7	16.0	09.5	-	04.8	05.7	05.3	54	47	52	51	ENE 2	E 2	NNE 2	
31	750.9	749.3	749.0	07.3	12.6	09.8	09.9	14.0	06.9	-	05.2	04.9	05.1	68	45	56	56	E 1	F 1	ENE 2	
MES.	VRED.	748.4	748.0	748.3	06.2	11.9	09.6	09.4	12.6	05.8	-	05.3	05.7	05.7	74	56	64	65	1.7	2.2	2.0

1974 APRIL

ZAGREB GRČ

1	747.8	747.6	748.7	08.2	10.9	08.5	09.0	11.0	07.4	-	05.6	05.9	05.8	65	60	69	66	ENE 1	ENE 2	ENE 2
2	749.2	750.2	751.7	08.1	14.0	10.3	10.7	14.1	07.9	-	05.4	05.7	05.7	66	47	60	58	ENE 2	ESE 2	NNE 2
3	752.3	751.3	751.4	05.8	15.3	10.6	10.6	15.3	05.7	-	05.0	04.3	04.7	72	33	49	51	ESE 1	ESE 3	NNE 2
4	750.3	748.4	747.2	05.7	16.2	12.1	11.5	16.7	04.9	-	04.5	03.5	03.3	66	25	31	41	SE 1	ENE 2	NNE 2
5	746.8	746.8	748.1	06.4	16.8	13.4	12.5	17.1	06.2	-	04.6	04.0	03.9	64	28	34	42	NNE 1	E 2	NE 3
6	749.3	748.3	749.1	10.9	17.5	13.3	13.8	17.7	09.4	-	04.4	04.4	04.0	45	29	35	36	NE 2	ESE 3	NNE 2
7	749.3	748.3	748.2	07.9	15.7	14.1	13.0	17.0	07.5	-	05.2	05.2	05.7	64	39	47	50	- 0	NNE 2	N 2
8	748.6	747.3	749.4	11.4	16.1	12.6	13.2	17.0	10.3	-	04.9	04.1	03.9	48	30	36	38	NNE 2	NNE 3	NNE 2
9	749.5	748.1	747.3	09.1	17.9	14.0	13.8	18.6	08.2	-	04.6	04.8	05.0	53	31	42	42	NW 1	S 2	NF 1
10	746.2	742.9	742.1	08.0	20.2	14.4	14.2	20.8	06.7	-	05.4	04.3	05.3	67	24	43	45	NNW 1	SSW 3	WSW 2
11	740.3	738.9	730.2	09.1	14.5	09.5	10.8	14.7	08.7	-	06.0	06.5	07.7	69	52	85	69	W 1	S 2	NNE 2
12	737.2	737.0	736.1	09.7	16.2	12.0	12.5	16.5	09.2	-	08.2	09.6	09.9	90	66	94	84	SSE 1	SSE 2	WW 2
13	739.8	741.4	742.6	12.0	12.4	11.3	11.8	13.6	11.3	-	09.0	06.9	04.4	86	82	44	71	NNW 1	N 2	NE 3
14	743.4	741.7	741.1	04.0	06.8	04.3	04.8	11.3	03.1	-	04.8	05.0	05.2	78	67	84	76	ENE 2	N 1	WSW 2
15	740.7	738.5	740.4	07.8	12.2	08.4	09.2	12.8	04.3	-	02.6	02.5	03.1	32	23	37	31	NNE 2	NE 3	NE 1
16	741.5	741.5	743.7	06.6	11.3	08.1	08.5	11.5	06.2	-	03.5	02.7	03.1	46	27	38	37	NAT 3	NE 3	NNE 3
17	744.6	743.1	744.2	04.0	10.4	09.4	08.3	10.8	03.6	-	04.3	02.9	03.1	70	31	35	45	NNE 3	NE 4	NNF 4

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Intencija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6	05	040	05	07.3	C4.5	.	.	.	= n-n	
2	6	10	10*	10	10.0	CC.0	.	.	.	= n-n, * tr n-p, tr 17° 17° 17°	
3	6	10	05	10	09.7	C1.3	00.0	.	.	= n-n, * tr 19° 20°	
4	6	10	10**	10**	10.0	CC.0	00.0	.	.	= n-n, * 8° 10°, * 13° 13°	
5	6	10*	10*	10*	10.0	00.0	07.7	.	.	= n-n, * n-n	
6	5	10*	10*	10*	10.0	CC.0	11.7	.	.	= n-n, * tr 15° 18° 18° 18° 18°	
7	5	10**	10	10	10.0	00.0	09.3	.	.	= n-n, * tr 17° 17° 17° 17° 17°	
8	5	10**	10	10	10.0	CC.0	CC.6	.	.	= n-n, * tr n-j 8° 11° 13° 13° 13°	
9	6	10*	10	10	10.0	00.0	01.3	.	.	= n-n, * 8° 10°, 8° 10°, 8° 10°	
10	6	10*	10*	10*	10.0	CC.0	CC.3	.	.	= n-n, * tr 6° 17° 17° 17° 17°	
11	6	10	10	10	10.0	00.0	00.6	.	.	= n-n, * tr n-j, 8° 15° 9°	
12	5	10	10	10	10.0	CC.0	CC.0	.	.	= n-n	
13	6	09	030	00	04.0	05.6	.	.	.	= n-n	
14	5	00=	000	00	03.0	03.0	08.3	.	.	= n-n, * 10° = 10° n	
15	5	02=	09	04	05.0	CC.0	CC.0	.	.	= n-n, * 8° = 8° n	
16	6	000	010	08	C3.0	C7.1	.	.	.	= n-n	
17	6	C9	080	06	07.7	03.1	.	.	.	= n-n	
18	8	C30	10	C8	07.0	C4.2	.	.	.	= n-10°	
19	7	09	040	00	04.3	C5.4	.	.	.	= n-w 5-n	
20	7	10	C80	00	06.0	C7.2	.	.	.	= n-8°	
21	8	000	000	00	00.0	10.2	.	.	.	= n-9°	
22	7	000	000	00	00.0	10.2	.	.	.	= n-12° 17°	
23	6	10	10	10	10.0	CC.0	C2.5	.	.	= n-14°	
24	8	C70	080	C7	C7.3	C9.8	.	.	.	= n-r-j-8° = 7° 9°	
25	5	C9	090	00	06.0	CC.0	06.3	.	.	= n-n	
26	5	C5	040	C2	C3.7	C7.2	.	.	.	= n-n	
27	6	09=	040	00	06.0	04.1	.	.	.	= n-n, * tr 8° 10° n	
28	6	08	C30	10	07.0	05.0	.	.	.	= n-11° 17° 17°	
29	6	C20	070	07	05.3	09.0	CC.7	.	.	= n-14° 17°	
30	6	09	10	10	09.7	00.0	.	.	.	= n-n	
31	6	10	070	00	0F.7	C1.6	.	.	.	= n-n	
MES.	VRED.	07.4	07.2	06.7	07.1	11C.8	32.2				

1	5	10	10	10	10.0	00.0	.	.	.	= n-n	
2	6	10	C50	C1	C5.3	C2.5	.	.	.	= n-11°	
3	7	000	010	00	CC.3	10.1	.	.	.	= n-9° 18°	
4	7	000	000	00	00.0	11.0	.	.	.	= n-11° 18°	
5	8	010	080	C4	04.3	10.5	.	.	.	= n-11°	
6	8	070	040	C0	03.7	C5.1	.	.	.	= n-11° 18° n	
7	6	030	10	10	07.7	04.5	.	.	.	= n-p, * tr 19° 20°	
8	7	010	060	00	C2.3	11.0	00.0	.	.	= n-r-j	
9	7	000	000	00	CC.0	11.6	.	.	.	= n-8°	
10	7	000	060	04	03.3	09.5	.	.	.	= n-8°	
11	8	10	10	10	10.0	CC.0	.	.	.	= n-12° 13° 13° 13° n	
12	6	10*	C9	10*	05.7	00.6	01.7	.	.	= n-13° 13° 13° 13° n	
13	5	09	10	10	05.7	00.0	05.8	.	.	= n-n, * tr 8° 10°	
14	6	10*	10	10	10.0	CC.0	04.5	.	.	= n-n, * tr n-8°, * 6° 8°, * 8° 9°	
15	8	10	C30	C8	07.0	06.4	CC.4	.	.	.	
16	7	10	080	05	07.7	C5.7	.	.	.	= n-12°	
17	7	10*	10	10	10.0	C3.4	CC.0	.	.	= n-9° 12° 12° 12° 12°	
18	7	10	10	10	10.0	01.9	00.0	.	.	= n-9° 18° 18° 18° 18°	
19	7	10	050	09	09.3	07.6	.	.	.	= n-8° 10°	
20	8	000	080	06	04.7	10.0	.	.	.	.	
21	6	10	10	10	10.0	02.0	.	.	.	= n-n, * 19° 20°	
22	7	090	090	10	09.3	04.4	00.1	.	.	= n-12° 12° 12° 12° 12°	
23	6	010	060	03	03.3	C8.5	00.0	.	.	= n-9°	
24	7	000	10	10*	06.7	06.5	.	.	.	= n-7°	
25	5	10*	10*	10	10.0	CC.0	01.2	.	.	= n-n, * 6° 7°	
26	7	10*	080	09	09.0	02.4	12.9	.	.	= n-11°, * tr n-10°, * 0-15° 15° 15° 15°	
27	8	070	09	10	08.7	06.5	C2.5	.	.	= n-8°, * tr 13° 13°	
28	6	09	10*	10*	09.7	00.5	00.3	.	.	= n-n, * tr 13° 13°	
29	8	050	09	08	07.3	C5.7	C2.6	.	.	= n-n, * tr 14° 14° 14° 14°	
30	6	060	10	10*	08.7	01.2	CC.1	.	.	= r-j-13° i, 18-n-i, 17° 13° 13° 13° 13°	
MES.	VRED.	06.3	07.6	06.9	06.9	154.3	36.5				

1974 MAJ

## ZAGREB GRIC

 $\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1\text{h }04\text{ min.}$ 

BR. ST. 57

E D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare φ mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21
1	729.7	730.8	733.7	11.0	12.6	12.2	12.0	15.9	10.8	-	09.3	10.0	09.2	95	91	86	91	FSE 1	EKE 1	WW 1
2	735.9	737.5	739.6	12.8	18.3	13.4	14.5	19.0	12.0	-	06.6	07.3	08.9	59	46	77	61	NW 2	SSE 2	NNE 2
3	741.3	740.1	740.7	12.5	18.9	12.9	14.3	19.5	12.2	-	08.5	07.6	06.5	79	50	58	62	NW 1	SSW 3	SSW 1
4	738.7	736.3	737.0	10.8	12.1	10.7	11.1	12.9	09.6	-	08.5	09.9	08.3	88	93	86	89	ENE 1	NE 3	SW 1
5	736.5	737.0	738.1	09.2	12.9	11.7	11.4	13.2	09.1	-	08.4	09.5	08.7	96	85	91	91	WSW 2	WW 1	W 2
6	738.3	741.3	743.7	11.0	14.0	10.5	11.5	14.2	10.2	-	08.3	09.6	09.2	84	80	96	87	WW 2	SSW 2	NNW 1
7	746.0	746.6	747.5	10.5	12.8	12.2	11.9	13.4	10.0	-	08.9	09.2	09.2	93	83	86	87	ENE 1	SSW 2	WSW 1
8	750.0	749.2	747.9	08.7	13.4	11.6	11.3	14.2	08.2	-	07.5	07.5	08.3	88	68	78	78	ENE 2	SSE 2	N 2
9	747.2	746.2	746.1	12.1	15.2	10.9	12.3	16.4	10.2	-	04.3	04.7	05.7	51	41	56	49	N 2	N 2	N 2
10	746.2	744.1	744.2	08.9	19.4	14.7	14.4	19.7	07.3	-	08.0	05.1	05.7	75	39	58	57	WSW 1	SSW 2	WSW 2
11	745.5	745.6	745.7	11.3	18.9	16.0	15.6	20.0	10.2	-	05.5	07.4	07.1	64	44	56	55	SW 1	SW 3	WSW 1
12	747.8	748.3	751.0	12.8	19.2	14.4	15.2	20.5	11.9	-	07.6	07.0	09.5	75	43	70	63	WW 2	ESE 2	NNE 1
13	752.7	751.7	751.4	13.4	20.3	17.2	17.0	21.1	10.2	-	08.4	07.9	07.4	76	47	60	61	SW 1	SE 2	NNE 2
14	750.1	747.1	750.5	13.3	23.4	10.8	14.6	23.9	10.8	-	09.5	09.7	08.7	83	45	90	73	ENE 1	SSE 2	ESE 2
15	749.3	746.7	746.2	10.9	16.9	10.7	12.3	17.4	09.4	-	08.3	06.8	08.9	84	47	92	74	WW 2	NNW 1	SSE 2
16	745.3	744.2	745.4	11.7	16.9	13.8	14.0	17.6	09.6	-	08.4	06.8	08.0	81	47	68	65	WSW 1	ESE 2	NE 2
17	746.5	748.4	750.9	11.4	16.7	12.6	13.3	18.1	10.2	-	07.2	07.6	07.7	71	53	70	65	ENE 1	ESE 3	NNE 2
18	751.5	751.6	752.2	13.1	19.1	14.8	15.4	19.5	09.6	-	08.1	08.7	09.7	71	52	77	67	WW 2	NE 3	NNE 2
19	751.8	750.5	750.0	14.6	21.1	17.7	17.8	22.0	13.5	-	07.9	07.8	08.0	63	41	52	52	WSW 1	NNE 3	N 2
20	749.4	748.1	747.8	16.5	24.6	18.4	19.5	25.2	13.4	-	08.9	09.0	10.4	63	39	65	56	WSW 1	ESE 2	NNE 1
21	749.3	749.3	749.4	16.9	21.0	17.5	18.2	22.7	13.7	-	09.9	10.1	11.6	68	54	77	66	NW 2	ENE 1	NNE 2
22	746.0	739.0	740.7	16.0	24.6	13.0	16.6	25.6	13.0	-	10.5	11.6	10.5	77	50	93	73	SE 1	WSW 3	S 1
23	741.4	739.6	740.4	13.0	18.4	11.9	13.8	18.9	10.9	-	08.9	05.3	07.8	79	33	74	62	NW 2	NNW 3	NE 1
24	741.1	740.8	741.8	11.9	13.4	11.8	12.2	14.2	11.2	-	06.8	07.6	08.9	65	66	86	72	NE 2	NNE 1	NE 1
25	743.3	746.4	748.7	10.8	14.6	12.5	12.6	16.5	10.4	-	08.5	07.1	07.9	87	57	72	72	NW 1	NNW 2	NNW 1
MES.																				
MRED.	745.2	744.5	745.2	12.7	18.4	14.2	15.6	19.4	11.1	-	08.5	08.4	08.7	77	54	73	68	1.4	2.2	1.5

1974 JUN

## ZAGREB GRIC

1	745.6	747.5	750.0	18.4	19.2	16.1	17.4	19.3	16.1	-	11.4	11.4	11.2	72	68	83	74	WSW 2	SSW 1	NW 2
2	752.7	753.4	754.7	14.9	21.3	17.1	17.6	22.0	14.3	-	10.2	08.4	08.0	80	44	55	60	WSW 1	ENE 3	NNE 1
3	754.7	753.3	752.1	15.2	22.3	18.1	18.4	23.5	12.2	-	08.2	10.1	12.7	63	50	66	60	SSW 1	S 2	N 1
4	751.9	750.9	749.8	15.6	26.0	21.5	21.2	27.1	13.0	-	08.9	10.4	11.0	76	41	57	58	SSW 1	SSE 2	NE 2
5	750.0	748.5	747.2	18.9	25.1	21.5	21.8	25.7	15.5	-	12.1	12.9	13.5	74	54	70	66	E 1	ESE 2	NE 2
6	745.5	744.7	746.3	19.4	25.4	18.4	20.4	25.9	17.2	-	13.0	11.2	11.6	77	46	73	65	SE 1	WSW 3	S 2
7	747.6	748.4	751.5	14.6	18.0	11.4	13.8	19.2	11.4	-	08.1	09.8	09.2	65	63	91	73	SSW 2	SSW 3	E 2
8	752.3	750.6	748.3	13.8	17.2	14.5	15.0	18.9	10.0	-	09.1	06.4	07.2	77	43	58	59	SSW 1	SSE 2	N 1
9	744.8	742.1	743.1	12.4	21.5	16.2	16.6	23.3	9.0	-	07.8	10.4	11.5	72	54	83	70	WSW 1	WSW 3	NNW 2
10	743.7	742.1	740.8	11.0	11.8	12.1	11.8	16.3	10.1	-	08.5	09.0	09.7	86	87	91	88	NNW 2	SF 2	NE 1
11	742.2	743.4	745.5	09.7	17.9	14.5	14.2	19.7	05.1	-	08.3	07.5	07.1	91	49	47	62	NNW 1	NW 3	NNE 2
12	744.2	742.4	742.9	10.7	19.0	13.9	14.4	19.7	08.3	-	07.1	05.6	06.8	73	34	47	51	W 2	NNW 3	NNE 2
13	740.2	739.8	740.9	10.5	16.6	13.7	13.6	17.1	08.8	-	06.8	06.4	08.7	71	46	74	64	WSW 1	WSW 3	NNE 1
14	742.1	742.1	744.3	13.0	22.2	17.5	17.6	22.7	11.4	-	09.1	08.6	10.4	81	43	69	64	WNW 2	WNW 2	NNW 2
15	746.7	745.1	745.9	15.8	21.3	17.1	17.8	22.5	13.3	-	10.5	11.1	10.3	76	58	70	69	S 1	WSW 2	W 2
16	745.5	744.8	744.9	17.1	23.2	19.2	19.7	24.4	14.0	-	09.8	10.0	10.5	67	47	63	59	WNW 2	ESE 2	NNE 2
17	744.7	743.4	744.4	17.1	25.2	18.7	19.9	25.7	14.1	-	11.0	11.5	11.5	75	48	71	65	SE 1	S 2	E 1
18	744.8	743.9	745.7	16.5	24.6	18.2	19.4	25.0	14.8	-	11.0	11.4	12.5	78	49	80	69	E 1	SSE 3	NNW 3
19	748.9	749.2	750.3	15.2	21.6	18.3	18.4	22.2	14.9	-	11.9	10.3	09.5	92	53	60	68	SSW 1	NE 2	NNE 1
20	750.7	749.5	748.9	15.6	22.6	17.8	18.4	23.2	13.1	-	09.2	08.4	08.9	69	41	58	56	WSW 1	E 2	NNE 2
21	749.3	749.6	748.5	15.6	20.0	15.8	16.8	20.0	13.8	-	10.8	10.4	09.4	81	59	70	70	SSW 1	SSW 2	NNE 1
22	748.3	747.5	747.3	13.6	20.9	17.6	17.4	22.5												

BR. ST. 57

$$H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$$

Dan	Vlaknost 0-9	Oblačnost N (0-10)					Inzolačija broj soči	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	6	10•	10•	10•	10.0	00.0	41.5	.	.	$\bullet^{n-1} n-n = rj-n$
2	8	C9	09	10	09.3	02.6	31.0	.	.	$\bullet^{tr-0} 10^{25} 17^{00} i$
3	7	10	040	02	05.3	06.5	00.4	.	.	$= n-10 \bullet^{\nabla} n$
4	5	10•	10•	10	10.0	00.0	00.6	.	.	$= rj-6 \bullet^{tr-1} rj-15^{50} i \nabla 14^{40} 14^{50} R^{0-1} 14^{35} 15^{45} Fw 14^{40} 14^{50}$
5	6	10•	10•	10	10.0	00.0	36.5	.	.	$\bullet^{tr-2} n-22^{45} i = 930 h$
6	6	10	10•	10•	10.0	00.0	11.8	.	.	$\bullet^{tr-0} 9^{38} ni$
7	6	10	1C•	10•	10.0	00.1	10.8	.	.	$= n-15^{45} \bullet^{tr-0-1} n-rj, 8^{40} 16^{15} i, 20^{32} n$
8	6	10	10	10	10.0	02.3	03.5	.	.	$= n-n$
9	7	040	08	0C	C4.0	09.2	.	.	.	$= n-9^{45}$
10	8	010	060	06	02.3	09.4	.	.	.	$= n-9^{45}$
11	8	1C	050	08	05.0	C3.0	.	.	.	$= n-9^{20}, n$
12	8	060	08	07	07.0	06.1	00.4	.	.	$\bullet n$
13	8	000	08	0C	C2.7	C8.9	.	.	.	$= n-830 \bullet^{\nabla} n-a$
14	7	000	10	10•	06.7	07.4	.	.	.	$= n-10^{45} 19^{15} n-a \bullet^{\nabla} n-a \nabla' 17^{16} 18^{36} \bullet^{\nabla} 18^{35} n, F_{NE-NNE} 17^{06} 17^{35} 15^{0-1} K^{35}$
15	8	010	06	1C	06.7	C8.2	22.1	.	.	$\bullet^{tr-0-1} 13^{02}, 18^{32} \nabla 18^{30} 21^{20} n, 18^{0-1} 17^{30} 18^{30}, 26^{45} 63^{02} n$
16	7	060	08	09	07.7	06.8	C3.3	.	.	$= rj-7^{30}$
17	7	10	090	09	C5.3	C5.0	.	.	.	$= n-9^{30}$
18	6	09	10	1C	C5.7	03.5	.	.	.	$= n-7^{30} \bullet^{tr-0} 18^{36} 20^{07} i$
19	8	010	040	0C	C1.7	11.1	00.1	.	.	$= 7^{15} 10^{30}$
20	8	000	020	10	C4.0	12.3	.	.	.	$= n-9^{15} \bullet^{\nabla} n, R^2 n$
21	7	05	05	C5	C6.3	05.3	C4.0	.	.	$R n, \nabla n = n-10^{30} 19^{30}$
22	5	10	09	1C	0C.7	02.9	.	.	.	$= n-14^{50} \bullet^{tr-1} 16^{45} 19^{05} R^{+2} 16-19$
23	9	C10	09	1C	C6.7	07.8	07.0	.	.	$\nabla^{\nabla} n, 14^{34} 19^{30} i$
24	8	10	10•	10	10.0	0C.3	C0.1	.	.	$= n! 7^{30} 13^{45} n, \nabla 7^{02} \bullet^{tr-0} 13^{35} 15^{40}$
25	8	10•	060	00	05.3	06.7	02.7	.	.	$= n-10^{30} \bullet^{\nabla} rj-925 R^{+2} 709 730$
26	8	000	010	10	C3.7	13.3	C4.7	.	.	$= n-8^{45} \Delta' n-a$
27	8	000	010	01	0C.7	13.2	.	.	.	$= n-11^{30} \Delta' n-a$
28	7	C10	090	1C	C6.7	C7.5	.	.	.	$= n-9^{45} \bullet^{\nabla} 19-ni$
29	7	080	070	04	0C.3	C6.5	08.3	.	.	$= n-12^{15} \bullet^{\nabla} n-rj$
30	6	000	050	1C	C6.3	10.3	.	.	.	$= n-13^{45} 16-n$
31	7	060	10	C9	0P.0	05.4	.	.	.	$= n-12^{15} \bullet^{\nabla} 10^{32} 1145$
MES. VRFD.										
		05.9	07.7	07.2	06.9	181.0	1E9.2			

1	8	10	10	10	1C.0	0C.6	.	.	$= 8^{46} 10^{30} \pi^{+0-1733} pi$
2	6	10	07	00	05.7	04.8	C2.3	.	$= 10^{30} n$
3	6	0C.0	04.0	00	C1.2	11.1	.	.	$= n-7, \frac{1}{n} n-a$
4	6	00.0	01.0	00	CC.2	12.6	.	.	$= n-10^{30} \Delta n-a$
5	6	02.0	02.0	01	02.0	09.1	.	.	$= n-n$
6	8	09	09	10	09.3	03.7	.	.	$= n-9^{30} \pi^{+16-02} 16^{44} 19^{06} 19^{10}$
7	8	1C.	07.0	10.	05.0	C3.4	C4.8	.	$= n-10^{45} \pi^{+0-1733} 6^{32} 10^{15}, 18^{04} n$
8	8	08	10	10	C5.3	C2.3	C1.5	.	$= n-7^{15} \sqrt{\pi^{+14-02} 14^{17}}$
9	8	00.0	07	10.	05.7	C8.3	CC.0	.	$= n-10, \pi^{+1-2} 13^{15} 17^{30} n$
10	6	10.	10.	10.	1C.0	0C.1	14.9	.	$= n-n, \pi^{+0-1733} 13-n$
11	7	10.	06.0	01	05.3	08.1	26.4	.	$= n-8^{15} \pi^{+17-02} 12^{30} 13^{07} i$
12	8	09	03.0	C1	C4.3	07.5	CC.4	.	$\pi^{+0-8^{15}} 8^{30} \pi^{+0-12-02} 12^{52} 12^{52} 17^{22} 17^{31} 16^{32} n$
13	8	10	1C	10.	1C.0	00.2	00.2	.	$\pi^{+16-n, \pi^{+0-20-02} n}$
14	7	09	06.0	C4	C6.3	C5.3	CC.2	.	$\pi^{+0-15^{22}-15^{57}}$
15	7	09	08.0	10	09.0	02.6	.	.	
16	7	01.0	02.0	06	C3.0	09.6	0C.1	.	$\pi^{+19-02} 19^{30}$
17	7	01.0	06.0	C2	C3.0	C9.1	0C.1	.	$\pi^{+15^{10}} = 17-n$
18	6	01.0	1C	10	C7.0	C8.0	CC.2	.	$= n-n, \Delta n-a, 16^{02} M^{45} 16^{15}, \pi^{+2} 15^{36} 16^{35}, \pi^{+2} n$
19	8	1C.	09	05	07.7	01.2	12.2	.	$= n-11^{15} \pi^{+0-7^{15}} = 17-n$
20	6	00.0	04.0	10	04.7	11.7	CC.0	.	$= n-n$
21	5	10	06.0	06	07.3	03.9	0C.0	.	$= n-n, \pi^{+6^{30} 11^{45}}$
22	6	10	03.0	00	04.3	C5.1	CC.3	.	$= n-10^{40} \pi^{+0-1733} 9^{45} 17^{05} 18^{20} i$
23	6	00.0	04.0	10	04.7	10.0	03.5	.	$= n-14^{40} \pi^{+14-02} 14^{10} 14^{10} n$
24	7	09	1C	10	09.7	C1.6	C1.0	.	$= n-8, \pi^{+1-2} 10^{30} D, 18^{0-10} - 10^{15} 22^{10} n, \pi^{+10-05} 10^{30}$
25	7	05.0	01.0	05	C3.7	07.9	07.7	.	$= n-9^{45} \pi^{+0-6^{30}}$
26	7	06.0	05.0	10	C7.0	C7.5	.	.	$= n-9^{30}$
27	7	10	09	03	07.3	05.6	.	.	$= n-9^{30}$
28	7	06.0	08.0	10	08.0	C4.5	.	.	$\pi^{+0-17}$
29	7	10	10.	10.	1C.0	00.9	00.9	.	$\bullet \pi^{+2} M^{42} n, \pi^{+0-13^{34}} 16^{32} 16^{20}$
30	9	07	03	00	C2.3	12.2	<u>50.5</u>	.	

1974 JUL

## ZAGREB GRČ

 $\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1\text{h}04\text{min}$ .

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	747.5	746.6	746.4	18.2	26.5	22.5	22.5	28.4	15.0	-	10.9	13.1	13.9	65	49	68	62	WSW 1	SSW 2	WNW 1	
2	750.8	750.9	751.7	18.6	24.0	20.1	20.7	25.3	17.6	-	12.4	11.6	11.0	77	52	62	64	ESE 2	SE 1	NNE 2	
3	750.5	745.9	743.9	18.4	25.2	20.2	21.0	26.7	16.8	-	08.6	12.0	12.8	54	50	72	59	NE 1	SE 2	NNW 3	
4	747.4	748.0	748.6	17.8	22.2	19.8	19.9	22.6	16.4	-	12.7	11.8	09.9	83	59	57	66	WNW 1	ENE 3	ENE 3	
5	749.7	749.4	748.4	18.3	24.0	20.3	20.7	24.7	17.1	-	08.1	10.7	12.4	51	48	69	56	NE 2	S 2	NNE 2	
6	747.5	745.9	744.5	18.6	27.3	23.5	23.2	29.4	16.5	-	13.2	13.6	14.1	82	50	65	66	S 1	SSW 2	NW 2	
7	746.9	749.6	749.9	15.6	18.0	15.0	15.9	23.5	14.8	-	12.2	09.4	10.0	92	60	78	77	ENE 2	SE 3	NNE 2	
8	751.0	749.8	750.5	14.4	20.5	16.6	17.0	22.1	12.4	-	09.8	09.5	09.9	80	52	70	67	NW 1	SSE 2	NNW 1	
9	751.4	749.5	747.8	15.2	24.0	20.0	19.8	24.2	12.9	-	09.6	11.2	11.9	74	50	68	64	NW 1	WNW 2	NNE 2	
10	748.0	748.8	750.2	19.2	25.0	20.1	21.1	25.2	16.5	-	10.9	11.7	09.2	65	49	52	55	W 2	ENE 2	ENE 2	
11	750.5	748.9	748.5	18.6	26.5	22.2	22.4	27.3	17.4	-	10.2	13.0	14.4	63	50	71	61	NNE 1	SSE 2	N 1	
12	747.9	747.1	747.9	20.3	30.0	24.2	24.7	30.6	18.5	-	13.1	14.3	14.8	73	45	65	61	SW 2	WSW 3	WSW 1	
13	747.8	745.8	745.2	20.7	30.8	25.4	25.6	31.4	18.6	-	12.8	14.4	11.7	70	43	48	54	WSW 2	WSW 4	MNW 2	
14	745.8	744.9	745.7	21.0	31.5	24.1	25.2	32.0	16.7	-	12.7	11.8	12.4	68	34	55	52	SW 1	SW 4	W 2	
15	749.3	750.6	750.8	20.9	24.0	19.2	20.8	25.0	19.2	-	12.3	11.5	10.4	66	51	62	60	ENE 3	SM 3	SM 2	
16	749.3	747.1	745.1	17.5	27.4	24.3	23.4	28.9	15.7	-	11.7	14.8	16.2	78	54	71	68	E 1	SE 2	NNE 1	
17	743.5	741.9	741.3	21.3	31.5	24.0	25.2	32.6	19.2	-	14.1	13.7	12.3	74	39	55	56	ENE 1	S 2	W 2	
18	742.4	741.5	744.3	18.3	23.4	17.3	19.1	25.2	16.4	-	14.5	14.7	13.1	92	68	88	83	ESE 2	WNW 2	ENE 1	
19	745.7	746.0	747.0	15.2	17.9	17.3	16.9	20.0	14.6	-	11.4	09.6	08.3	88	62	56	69	N 2	E NE 2	E NE 2	
20	747.5	746.9	746.4	15.4	19.6	15.5	16.7	19.9	15.0	-	07.6	08.2	08.3	58	48	61	56	NNE 2	NNE 2	NNE 1	
21	745.5	745.3	746.8	13.8	19.4	17.3	17.0	20.9	13.0	-	09.7	08.4	08.7	83	50	59	64	W 1	NNE 2	N 1	
22	748.6	747.6	747.5	15.9	22.0	19.6	19.3	22.6	14.5	-	08.7	07.5	07.4	64	38	43	48	NW 2	NEE 3	N 2	
23	746.9	747.2	747.3	17.6	21.6	20.1	19.8	24.1	17.3	-	08.7	11.4	11.5	57	59	65	60	NW 3	WSW 2	NW 2	
24	747.3	745.9	744.4	20.9	28.0	21.6	23.0	28.8	15.7	-	10.6	11.7	11.2	57	41	58	52	WNW 2	SSW 3	WSW 3	
25	745.3	748.4	750.3	20.3	14.8	13.5	15.5	21.6	13.2	-	12.7	11.5	10.8	62	91	93	92	NNW 1	NW 2	NW 1	
MES.	WRED.	748.3	747.6	747.6	18.0	24.7	20.6	21.0	26.1	16.1	-	11.4	11.8	11.8	73	51	64	63	1.4	2.3	1.7

1974 AVGUST

## ZAGREB GRČ

1	747.3	746.6	746.5	21.9	29.6	25.2	25.5	30.2	15.8	-	15.6	10.4	16.6	79	51	67	66	ENE 1	WNW 1	NNE 2
2	747.4	747.0	746.7	21.9	29.7	25.7	25.8	30.1	20.6	-	15.8	17.2	16.9	82	55	68	68	ENE 1	ENE 1	NNE 2
3	747.7	748.2	748.6	23.1	30.4	26.4	26.6	31.2	21.4	-	17.0	17.6	18.6	80	54	72	69	WNW 1	E 2	NNE 2
4	748.5	747.4	746.8	23.2	32.6	26.3	27.1	33.2	21.8	-	17.1	17.3	14.9	80	47	58	62	- 0	SSW 2	NNW 2
5	748.7	748.2	747.9	22.4	29.2	24.7	25.2	30.0	19.5	-	13.4	14.3	14.0	66	47	60	58	ESE 1	ENE 2	NNE 2
6	752.8	753.6	752.7	18.7	18.6	17.0	17.8	24.7	17.0	-	11.0	10.9	10.5	68	54	72	69	ENE 2	ENF 1	- 0
7	751.2	749.0	747.4	16.1	24.3	19.4	19.8	24.3	13.9	-	11.0	10.1	10.5	80	44	62	62	NE 1	SSE 2	NNE 2
8	745.0	741.8	740.9	16.5	26.4	22.4	21.9	27.4	14.7	-	10.8	12.8	15.9	77	50	78	68	E 1	SE 2	NNE 1
9	743.4	743.7	746.2	17.7	22.6	19.3	19.7	24.1	16.7	-	13.2	12.1	11.8	87	59	71	72	ENE 1	SSE 2	NE 2
10	747.5	744.9	743.3	15.7	25.2	20.8	20.6	25.6	14.8	-	12.4	12.0	12.0	93	50	65	69	ESE 1	SE 2	NNE 2
11	742.5	744.0	745.6	14.7	14.2	13.4	13.9	20.8	12.1	-	11.5	10.3	09.6	92	85	83	87	ENE 2	NW 2	NNW 2
12	746.7	747.4	749.0	15.5	22.9	16.6	17.9	23.7	12.0	-	09.6	07.4	09.2	73	35	65	58	NW 2	NNW 2	WSW 1
13	751.1	750.7	751.0	14.4	24.0	19.5	19.4	25.2	11.3	-	09.4	10.3	10.3	77	46	68	64	E 1	S 2	NNE 1
14	751.7	752.1	752.4	15.5	27.4	22.4	21.9	28.0	14.2	-	11.8	14.5	15.4	89	53	76	73	E 1	SSE 2	NNE 1
15	752.9	753.2	753.4	19.0	30.2	25.5	25.0	30.4	17.6	-	14.5	17.4	17.1	88	54	70	71	SSE 1	SE 1	N 1
16	753.1	752.0	751.4	21.7	31.7	26.5	26.6	32.1	20.1	-	16.0	16.4	17.7	82	47	68	66	SE 1	SSW 2	NNE 2
17	751.0	750.0	749.5	22.3	31.5	24.7	25.8	31.7	21.1	-	17.4	17.3	15.6	86	50	67	68	SSE 1	SSE 2	NNE 1
18	749.5	748.4	747.5	20.9	30.2	26.1	25.8	30.5	19.8	-	15.4	16.8	16.2	83	52	64	66	- 0	SE 2	NNE 2
19	748.6	748.5	749.3	21.7	31.5	26.5	26.8	31.5	20.3	-	15.4	14.5	14.9	79	44	56	60	NNW 1	E 2	NNW 2
20	750.3	749.5	749.3	21.4	30.4	26.7	26.3	30.6	20.7	-	14.9	16.9	15.8	78	52	60	63	S 1	ENE 3	NNE 2
21	749.4	748.2	747.3	22.7	29.4	24.8	25.4	29.5	21.6	-	16.8	17.2	18.8	81	56	80	72	SSE 1	ESE 2	NNE 1
22	749.0	747.5	747.3	20.2	23.2	21.2	21.4	26.0	18.5	-	14.9	14.5	15.1	84	68	80	77	WNW 1	S 2	NNE 2
23	7																			

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblakost N (0-10)					Temperatura broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	070	020	CC	C2.0	14.3	.	.	=n-7 <sup>30</sup>	
2	7	10	090	01	C6.7	06.5	.	.		
3	7	000	010	1C	02.7	11.8	.	.	=n-20 <sup>30</sup> 21 <sup>30</sup> , 21 <sup>30</sup> 22, F=20 <sup>45</sup> 21 <sup>30</sup>	
4	8	040	07	08	C6.3	C6.4	01.6	.		
5	8	010	010	00	00.7	12.6	.	.	=n-8 <sup>15</sup>	
6	8	000	030	C7	C3.3	11.5	.	.	=n-9 <sup>45</sup> , n-a, 17 <sup>45</sup> 23 <sup>00</sup>	
7	6	10	1C	C3	C7.7	C4.7	18.4	.	=n-9 <sup>10</sup> , 18 <sup>30</sup> -n	
8	7	040	060	06	C5.3	C8.1	03.3	.	=n-10 <sup>30</sup>	
9	7	010	09	10	06.7	C7.0	.	.	=n-10 <sup>45</sup>	
10	8	09	09	10	C9.3	C3.8	.	.	=n-10 <sup>30</sup> , 14 <sup>20</sup> 14 <sup>30</sup>	
11	6	10	020	04	C5.3	06.2	00.0	.	=n-n, +6 <sup>30</sup> 6 <sup>45</sup>	
12	6	010	060	00	C2.3	12.3	.	.	=n-n, n-a	
13	8	000	000	00	00.0	13.6	.	.	=n-16 <sup>30</sup> , n-a	
14	8	000	000	00	CC.0	13.4	.	.	=n-8 <sup>30</sup> , n-a	
15	8	010	060	05	04.0	10.7	.	.		
16	7	000	000	04	C1.3	11.5	.	.	=n-8 <sup>30</sup> , n-a	
17	8	020	010	08	03.7	12.4	.	.	=n-10 <sup>45</sup> , n-a	
18	8	10	060	10	08.7	C3.5	C1.8	.	=n-13 <sup>15</sup> , +n-5 <sup>45</sup> , n; 17 <sup>45</sup> 17 <sup>45</sup> , 15 <sup>45</sup> 17 <sup>45</sup> , 17 <sup>45</sup> 17 <sup>45</sup> , 15 <sup>45</sup> 17 <sup>45</sup>	
19	8	10	10	10	10.0	00.2	15.3	.	=n-8 <sup>30</sup>	
20	6	09	07	06	07.3	05.0	00.2	.	=n-n	
21	6	10	09	10	05.7	03.8	00.2	.	+n, =7 <sup>30</sup> 18	
22	7	10	08	08	C5.0	C6.2	.	.		
23	7	10	08	04	07.3	02.0	.	.		
24	7	010	09	1C	C6.7	11.1	.	.	+n-19 <sup>55</sup> ni	
25	7	10	10	10	1C.0	00.0	.	.		
26	7	070	04	0C	C3.7	12.1	11.0	.	*n = n-8 <sup>30</sup>	
27	6	000	000	00	00.0	13.3	.	.	=n-n	
28	7	000	010	0C	CC.3	12.5	.	.	=n-10 <sup>30</sup>	
29	7	000	000	00	0C.0	13.2	.	.	=n-10 <sup>30</sup> , n-a	
30	7	000	000	0C	CC.0	12.7	.	.	=n-11 <sup>45</sup> , n-a	
31	7	010	040	0C	C1.7	11.6	.	.	=n-10 <sup>30</sup> , n-a	
MES.	VRED.	04.4	04.8	04.6	04.6	274.8	51.8			

1	6	000	050	02	C2.3	11.6	.	.	=n-n, n-a	
2	6	000	010	00	CC.3	11.5	.	.	=n-n, n-a	
3	6	000	020	00	CC.7	10.1	.	.	=n-15 <sup>30</sup> , n-a	
4	6	000	010	00	CC.2	12.1	.	.	=n-15 <sup>30</sup> , n-a	
5	7	010	010	00	00.7	12.2	.	.	=n-17 <sup>30</sup>	
6	7	10	10	00	06.7	01.0	.	.	=n-15 <sup>30</sup>	
7	5	000	050	00	01.7	11.6	.	.	=n-n	
8	6	000	05	09	C4.7	10.0	.	.	=n-10 <sup>45</sup> , +n-18 <sup>45</sup> , 3 <sup>27</sup>	
9	8	09	060	01	05.3	06.3	03.6	.	=n-11 <sup>45</sup> , 17 <sup>45</sup> , n, 22-n	
10	8	10	060	10	08.7	C7.9	.	.	=n-12 <sup>45</sup> , +n-17 <sup>45</sup> , 17 <sup>45</sup> 10 <sup>22</sup> , 16 <sup>45</sup> n	
11	7	10	10	01	07.0	C1.5	06.8	.	=n-12 <sup>45</sup> , +n-17 <sup>45</sup> , 17 <sup>45</sup> 10 <sup>22</sup> , 16 <sup>45</sup> n	
12	9	08	04	C1	C4.3	11.0	15.0	.	=n-17 <sup>30</sup>	
13	9	030	070	03	04.3	08.6	.	.	=n-17 <sup>30</sup>	
14	7	000	020	02	C1.3	12.8	.	.	=n-n	
15	6	020	020	01	C1.7	11.7	.	.	=n-n	
16	6	000	010	0C	CC.3	12.5	.	.	=n-13 <sup>45</sup>	
17	6	000	000	00	00.0	12.5	.	.	=n-14 <sup>30</sup> , 18 <sup>45</sup> n	
18	6	000	000	01	0C.3	12.2	.	.	=n-n	
19	5	000	010	00	0C.3	11.8	.	.	=n-n, n-a	
20	6	000	010	09	03.3	10.8	.	.	=n-n, n-a	
21	5	000	010	00	00.3	09.7	.	.	=n-n, n-a, 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 22 <sup>45</sup> 22 <sup>45</sup> , F <sub>NNE-ENE</sub> 22 <sup>30</sup> 23 <sup>35</sup>	
22	8	08	10	04	07.3	06.3	47.3	.	=n-17 <sup>45</sup> , 17 <sup>45</sup> n, 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 22 <sup>45</sup> 22 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup>	
23	7	070	050	10	07.3	08.4	09.2	.	=n-14 <sup>30</sup> , 17 <sup>45</sup> n, 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 22 <sup>45</sup> 22 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup>	
24	6	10	090	10	09.7	03.1	15.4	.	=n-n, 17 <sup>45</sup> n	
25	5	10	10	10	10.0	00.4	CC.0	.	=n-n, 17 <sup>45</sup> n, 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 22 <sup>45</sup> 22 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup>	
26	6	10	09	08	C5.0	C1.6	05.5	.	=n-n	
27	6	10	060	09	08.3	04.5	.	.	=n-n, n-a, 17 <sup>45</sup> 21 <sup>45</sup> , 17 <sup>45</sup> 21 <sup>45</sup> , 22 <sup>45</sup> 22 <sup>45</sup>	
28	5	10	10	08	09.3	00.2	09.7	.	=n-15 <sup>45</sup>	
29	5	000	020	01	01.0	10.4	04.0	.	=n-11 <sup>45</sup> , n-a	
30	7	010	020	00	01.0	10.6	.	.	=n-11 <sup>45</sup> , n-a	
31	7	000	010	07	02.7	11.6	.	.	=n-10 <sup>45</sup>	
MES.	VRED.	03.8	04.4	03.5	03.9	266.5	117.7			[24 <sup>45</sup> n]

1974. SEPTEMBAR

ZAGREB GRČ

 $\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina vetroa D, I (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	746.6	746.5	746.2	17.7	24.3	20.3	20.6	24.4	17.2	-	13.9	13.2	14.3	91	58	80	76	SSW 1	SSW 2	NNE 2			
2	745.5	746.5	746.6	17.2	26.1	20.8	21.2	26.4	16.2	-	13.2	13.5	12.4	90	55	67	71	WSW 1	SSW 2	NW 1			
3	745.5	746.5	745.7	17.7	27.3	21.5	22.0	27.3	16.6	-	11.9	14.7	14.1	78	54	73	68	WNW 1	SSW 4	W 2			
4	745.2	746.6	750.8	19.0	19.0	13.9	16.4	21.5	13.9	-	15.4	11.1	11.2	93	67	94	85	NNW 1	NE 3	NNW 1			
5	752.2	750.6	749.0	12.1	20.6	16.4	16.4	21.1	10.5	-	05.8	10.0	05.8	92	55	70	72	W 1	S 2	NNE 1			
6	745.8	742.3	740.0	13.3	23.3	20.1	19.2	23.9	12.4	-	09.9	12.9	13.1	88	60	74	74	NF 1	SSE 2	NNF 2			
7	741.8	743.1	745.2	14.4	16.9	15.4	15.5	20.1	14.2	-	11.2	05.9	10.1	91	68	77	79	ENE 2	WSW 1	NNW 1			
8	749.5	749.8	751.1	12.8	21.8	16.6	17.0	21.9	11.6	-	09.3	10.2	11.2	84	52	79	72	NW 1	WSW 2	NNE 1			
9	752.7	751.3	750.4	14.8	22.6	18.5	18.8	23.4	13.3	-	11.3	13.0	13.9	89	65	84	79	WNW 1	SSE 2	N 1			
10	751.0	752.7	757.1	14.9	24.8	17.0	18.4	25.1	14.0	-	12.1	13.0	08.6	95	55	59	70	W 1	ENF 3	NE 1			
11	757.5	757.0	756.7	15.2	19.7	17.3	17.4	19.7	14.8	-	08.8	08.8	10.4	68	51	70	63	ENE 1	ENE 2	NNE 2			
12	756.2	754.3	753.4	16.7	22.0	18.5	18.9	22.5	16.4	-	09.8	10.3	12.7	69	52	77	66	ENF 2	NNF 1	N 1			
13	752.0	752.3	752.5	17.4	22.7	17.2	18.6	22.8	16.8	-	13.0	11.4	12.1	85	55	82	74	- 0	SSE 2	NNF 1			
14	753.0	752.0	751.6	14.3	24.1	19.6	19.4	24.5	14.2	-	11.3	14.3	12.7	92	63	94	80	NNW 1	SSW 2	NNF 1			
15	750.9	750.0	750.0	16.6	24.9	20.7	20.7	24.9	15.7	-	13.0	15.4	17.0	92	65	71	76	- 0	ESE 1	NNE 2			
16	751.3	751.5	751.5	18.0	23.7	20.0	20.4	23.7	17.5	-	12.0	12.9	12.1	77	55	69	63	ENE 2	ESE 2	NNE 2			
17	751.2	750.9	750.4	15.4	22.8	18.4	18.8	22.8	15.0	-	11.7	13.1	12.1	89	63	76	76	- 0	SE 2	NNE 2			
18	750.3	749.6	749.7	14.8	23.1	15.4	19.2	23.5	14.7	-	12.3	13.2	14.2	97	62	84	81	ENE 1	SSE 1	NE 2			
19	750.0	750.6	749.4	17.0	22.6	18.8	19.3	23.1	15.2	-	13.1	11.3	10.0	90	55	61	69	ENE 1	ENL 2	NNE 2			
20	746.3	744.5	744.6	16.4	18.7	16.1	16.8	18.8	15.3	-	10.6	13.4	12.4	76	56	90	84	ENF 1	NE 2	NE 2			
21	744.5	745.3	744.4	14.3	13.6	13.2	13.6	16.2	13.2	-	10.5	11.1	11.3	86	95	89	90	NNE 4	SW 2	SSE 1			
22	743.5	744.9	746.4	13.0	16.9	15.5	15.2	17.4	12.5	-	10.8	11.6	11.9	96	81	90	85	WSW 1	SSW 1	NE 2			
23	748.5	748.3	746.1	11.9	12.9	12.4	12.4	15.5	11.6	-	09.7	06.6	05.5	93	79	88	87	NNE 1	E 1	SSE 2			
24	741.7	739.2	737.6	11.9	17.1	16.1	15.3	18.0	11.5	-	09.6	12.0	11.0	92	82	80	85	SSE 1	ESE 2	NNW 1			
25	737.8	736.9	734.9	09.0	11.5	09.7	10.2	16.2	09.7	-	08.5	08.1	08.1	93	79	90	87	WNW 2	W 2	SSW 1			
26	732.1	735.5	740.8	06.9	14.6	09.8	11.0	14.7	05.3	-	08.7	08.2	07.8	95	65	87	82	NNE 1	SSW 1	NNE 2			
27	747.5	747.9	748.2	06.3	16.8	12.1	11.8	16.8	06.3	-	06.6	05.6	06.7	93	39	63	65	WSW 1	WNW 2	W 1			
28	746.1	743.8	743.5	06.2	21.1	14.0	14.6	21.1	07.6	-	07.1	09.2	07.5	87	49	60	65	WSW 1	WSW 4	KSW 3			
29	741.6	743.0	745.3	14.7	17.9	11.1	13.7	18.4	11.1	-	07.2	11.6	09.0	69	73	91	78	NNE 1	SSE 1	KSW 3			
30	745.8	747.3	747.7	10.1	10.4	10.2	10.2	11.2	09.2	-	08.9	09.0	08.8	96	95	94	95	SSE 1	ESE 2	ENE 1			
MES.	MREFD.			747.6	747.3	747.6	14.2	20.1	16.4	16.8	20.9	13.2	-	10.7	11.4	11.1	88	65	78	77	1.1	1.9	1.6

1974. OKTOBAR

ZAGREB GRČ

1	747.2	749.0	749.7	09.5	10.1	08.1	09.0	11.3	08.1	-	08.5	06.9	07.1	95	75	87	86	WSW 1	WNW 1	N 1
2	747.1	744.9	744.3	07.7	07.6	05.8	06.7	08.8	05.6	-	07.2	07.0	05.9	91	84	88	89	NE 1	NE 2	W 1
3	740.3	748.6	747.8	04.6	12.4	09.8	09.2	13.5	04.6	-	06.1	06.6	07.2	96	61	79	74	WSW 2	SW 3	N 1
4	746.8	748.4	749.3	10.6	09.8	07.7	09.0	11.6	07.5	-	07.8	09.5	07.1	81	93	90	88	SSW 2	ENE 2	NE 2
5	748.7	748.2	747.3	07.6	08.4	07.6	07.8	08.5	07.5	-	07.5	07.0	07.2	95	84	92	90	WSW 1	ENF 2	NNW 1
6	746.6	748.1	748.4	06.6	06.7	06.2	06.4	08.6	06.2	-	06.9	07.0	06.4	95	95	91	94	SW 1	NNF 2	NNW 1
7	746.5	743.3	741.9	03.3	06.6	06.6	05.8	07.3	02.8	-	05.0	06.3	06.1	87	86	90	88	NNW 1	ESE 2	WSW 1
8	737.7	739.3	742.5	07.9	11.5	08.9	09.3	12.7	06.6	-	07.6	08.2	07.2	95	81	85	87	NNW 2	SW 2	N 2
9	743.5	744.3	745.9	06.9	09.0	08.1	08.0	10.0	05.5	-	07.2	07.7	07.6	96	91	94	94	ENE 1	WSW 1	ENE 1
10	748.5	748.5	749.2	06.4	13.9	09.4	09.8	14.0	06.4	-	07.0	06.4	07.1	97	54	79	77	W 2	SSW 2	NNW 2
11	748.8	748.7	749.2	07.2	10.4	08.9	08.8	10.4	05.8	-	07.2	08.1	07.9	95	86	93	91	ENE 1	SSW 1	NNW 1
12	748.4	747.8	745.5	07.2	09.6	05.7	05.0	09.9	06.9	-	07.1	08.7	08.7	92	96	96	95	ENE 1	FNF 1	NNW 1
13	746.9	748.0	748.9	08.3	08.6	07.5	08.0	09.7	07.4	-	07.1	07.6	07.3	87	91	94	91	NNE 2	S 2	WSW 1
14	747.6	747.9	743.6	07.3	07.3	05.9	06.4	07.5	10.1	-	07.1	06.2	04.1	97	69	82	82	W 1	NNE 2	NNW 1
15	749.0	746.8	745.1	04.9	06.3	06.3	06.0	07.3	04.3	-	05.9	06.4	06.5	90	89	90	90	SSE 1	WNW 1	NNW 1
16	744.7	746.8	748.1	06.2	06.7	04.5	05.7	06.7	04.9	-	06.5	06.8	06.0	93	93	94	93	NNW 1	WNW 1	NNW 2
17	749.6	749.7	750.1	02.1	11.0	07.5	07.0	11.6	01.7	-	05.2	07.1	05.9	97	72	76	82	SW 2	SW 2	WSW 2
18	7																			

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblakost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	09	060	03	C6.0	C6.1	00.3	.	= n-10 <sup>30</sup> • 0°5 <sup>30</sup> 6	
2	7	030	080	06	C5.7	C5.4	.	.	= n-10 <sup>6</sup> • 0°1n-a	
3	8	020	020	C6	C3.3	C8.9	.	.		
4	8	09	10	C6	C8.3	C2.4	00.3	.	= rj-12 <sup>15</sup> △ <sup>tr-2</sup> 6-10 <sup>24</sup> R <sup>70</sup> 10 <sup>15</sup> F <sub>NN</sub> 14 <sup>00</sup> 16 <sup>10</sup> , 0°-15 <sup>04</sup> 17 <sup>20</sup> , 15 <sup>20</sup> kV	
5	8	010	010	00	00.7	11.6	22.5	.	= 2n-a, = rj-6 <sup>30</sup> = 6 <sup>20</sup> 10 <sup>15</sup> 18-kV	
6	8	000	000	01	C6.2	11.1	.	.	= n-10 <sup>15</sup>	
7	8	100	10	09	C6.7	C6.6	22.7	.	= n-8 <sup>15</sup> • 0°-1n-915	
8	8	000	000	00	C6.0	11.5	C3.9	.	= △'n-930	
9	6	010	07	10	06.0	08.4	.	.	= n-n, △ <sup>2</sup> n-a	
10	6	000	020	10	C4.0	C7.9	.	.	= 2n-d, = n-930, = 930 10 <sup>15</sup>	
11	7	00	010	00	C3.3	08.9	.	.	= n-8 <sup>30</sup>	
12	6	10	020	10	C7.3	C2.1	.	.	= n-14 <sup>45</sup> , = 18 <sup>30</sup> n	
13	6	09	010	00	C3.3	06.1	.	.	= n-n	
14	5	000	000	00	C6.0	09.4	.	.	= n-n, △ <sup>2</sup> n-a	
15	6	08	040	00	C4.0	08.2	.	.	= △'n-a, = n-8 <sup>15</sup> , = 8 <sup>15</sup> n	
16	5	000	C10	00	06.3	07.9	.	.	= n-n, △ <sup>0</sup> n-a	
17	6	020	080	01	03.7	08.7	.	.	= △'n-d, = n-930, = 930 n	
18	6	10	020	00	04.0	C4.1	.	.	= n-n, △ <sup>0</sup> n-a	
19	6	04	070	07	C6.0	C2.2	.	.	= n-n, △ <sup>0</sup> n-a	
20	3	C6	100	10	08.7	00.0	.	.	= n-n, △ <sup>0</sup> n-14 <sup>45</sup> , = 18 <sup>30</sup> n	
21	4	100	100	10	10.0	00.0	16.8	.	= n-n, • tr-0 n-915 12 <sup>55</sup> 14 <sup>40</sup>	
22	5	10	10	10	10.0	00.1	C2.9	.	= n-n, • 0°-1n-12 <sup>30</sup> 12 <sup>40</sup> 15 <sup>45</sup> 16 <sup>30</sup>	
23	7	100	10	10	10.0	00.0	15.5	.	= n-8 <sup>45</sup> • tr-0 n-815 11 <sup>30</sup> 14 <sup>45</sup> R <sup>0-1340</sup> 5 <sup>06</sup>	
24	6	10	10	10	10.0	00.4	C0.7	.	= n-15 <sup>30</sup> • 0°13 <sup>30</sup> 15 <sup>45</sup> 16 <sup>30</sup>	
25	7	100	10	C2	C7.3	C0.0	18.6	.	= tr-0 n-13 <sup>02</sup> , = 8 <sup>30</sup> 10 <sup>45</sup>	
26	8	100	05	00	C6.3	C1.6	C7.7	.	= n-9 <sup>30</sup> • tr-0 n-815, 10 <sup>06</sup> 11 <sup>16</sup> 17 <sup>05</sup> 18 <sup>45</sup> R <sup>2</sup> 17 <sup>21</sup> 17 <sup>20</sup> , R <sup>11</sup> 17 <sup>08</sup> 17 <sup>23</sup>	
27	9	C10	010	00	C6.7	10.0	C6.9	.	= △ <sup>2</sup> n-a, = n-815	
28	8	000	010	00	C6.3	11.1	.	.	= rj-815	
29	7	10	10	10	10.0	00.7	C0.7	.	= tr-0 n-14 <sup>40</sup> ni, = 14 <sup>30</sup> n	
30	5	100	100	09	09.7	00.0	17.7	.	= n-h, • n-14 <sup>30</sup>	
MES.										
WRED.	05.8	05.4	04.7	05.3	159.7	141.5				

1	5	100	090	08	05.0	00.2	11.7	.	= n-10 <sup>15</sup> • 0°-1n-13 <sup>30</sup> R <sup>0-14<sup>30</sup>-15<sup>40</sup></sup>	
2	5	100	100	100	C6.0	C6.5	.	.	= n-n, • tr-0 n-n	
3	9	010	080	10	C6.3	06.2	30.2	.	= n-n, • 0°-1n-8 <sup>30</sup> 11 <sup>30</sup> R <sup>0</sup>	
4	4	100	100	10	10.0	00.0	00.5	.	= n-n, • 0°12 <sup>30</sup> 15 <sup>45</sup> R <sup>0</sup>	
5	6	100	10	100	C6.0	C6.5	.	.	= n-n, • 0°-1n-12 <sup>30</sup> , = tr-0 n-15 <sup>40</sup> n	
6	5	100	100	00	06.7	00.8	28.2	.	= n-15 <sup>15</sup> , • 0°-1n-14 <sup>50</sup>	
7	5	10	10	10	10.0	C0.1	C6.1	.	= △ <sup>2</sup> n-a, = 2n-10 <sup>30</sup> , = 10 <sup>30</sup> n	
8	5	100	06	10	C6.7	C2.8	C4.2	.	= n-n, • 0°-1n-8 <sup>30</sup> 11 <sup>30</sup> R <sup>0</sup>	
9	5	100	10	06	C6.7	C0.2	C4.8	.	= n-8 <sup>30</sup> , • 0°-1n-8 <sup>30</sup> = 8 <sup>30</sup> n	
10	8	010	010	01	01.0	09.7	02.7	.	= n-8 <sup>30</sup> , • 0°-1n-8 <sup>30</sup>	
11	4	10	10	07	05.0	C6.0	00.1	.	= tr-0 n-11 <sup>15</sup> , = 0°-1n-10 <sup>30</sup> 17 <sup>30</sup> n, = 10 <sup>30</sup> 17 <sup>30</sup>	
12	3	10	10	10	10.0	00.0	00.2	.	= n-n, • 0°-1n-12 <sup>30</sup> , = 16 <sup>25</sup> 20 <sup>45</sup>	
13	6	10	10	10	10.0	00.0	29.8	.	= n-15 <sup>15</sup> , 15 <sup>45</sup> n, = 16 <sup>25</sup> 20 <sup>45</sup>	
14	7	10	10	02	07.3	00.2	03.2	.	= n-n, = 8 <sup>15</sup> 9 <sup>15</sup> , • tr-0 n-8 <sup>30</sup> n	
15	5	10	100	10	10.0	C0.1	.	.	= n-n, = 8 <sup>15</sup> 9 <sup>15</sup> , • tr-0 n-8 <sup>30</sup> n	
16	5	10	100	02	C7.3	00.0	C6.4	.	= n-n, • tr-0 n-18 <sup>25</sup>	
17	8	000	010	00	C6.3	06.7	C3.2	.	= n-11 <sup>15</sup> , △ <sup>2</sup> n-a	
18	6	000	050	00	01.7	07.5	.	.	= △ <sup>2</sup> n-a, = 0°-1n-9 <sup>15</sup> = 9 <sup>15</sup> n	
19	4	000	000	09	C6.0	C2.6	.	.	= tr-0 n-11 <sup>15</sup> , = 11 <sup>20</sup> 12 <sup>30</sup> , = 0°-18 <sup>15</sup> 11 <sup>30</sup>	
20	8	09	10	100	05.7	C0.0	C0.6	.	= tr-0 n-14 <sup>30</sup> , = 14 <sup>15</sup> 15 <sup>45</sup> , = 17 <sup>05</sup> 17 <sup>30</sup> , = 11-14 <sup>15</sup> 11 <sup>30</sup>	
21	5	100	100	10	10.0	C6.0	24.5	.	= n-n, • 0°-1n-ni	
22	8	080	09	00	05.7	05.3	C5.4	.	= n-10 <sup>30</sup> , = n-n	
23	6	01	010	05	C2.3	C5.1	C0.1	.	= n-8 <sup>30</sup> , △ <sup>2</sup> n-a, = n	
24	8	08	09	04	C7.0	C1.1	.	.	= n-n	
25	5	08	000	08	05.3	C6.8	.	.		
26	5	10	05	05	08.0	00.0	.	.	= n-n, • tr-0 n-19 <sup>35</sup> , = 19 <sup>15</sup> 19 <sup>35</sup> R <sup>19</sup> n, = 19 <sup>30</sup>	
27	8	050	050	08	C6.0	C8.3	C6.5	.	= △ <sup>2</sup> n-d, = 7 <sup>15</sup> 9 <sup>30</sup>	
28	4	10	100	10	10.0	C6.0	C6.0	.	= n-n, • 0°-17 <sup>20</sup> n	
29	8	10	080	00	C6.0	00.5	23.7	.	= n-16 <sup>25</sup> , • tr-0 n-ni	
30	7	10	060	08	08.0	C4.7	.	.	= n-13 <sup>30</sup> , • tr-0 20 <sup>50</sup> n	
31	4	07	10	100	05.0	00.0	.	.	= n-n, • tr-0 20 <sup>50</sup> n	
MES.										
WRED.	07.7	07.6	06.5	07.3	74.9	224.0				

$\varphi = 45^{\circ}49'$  N  $\lambda = 15^{\circ}59'$  E Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0—12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	743.6	744.3	746.6	04.4	05.2	04.4	05.6	05.8	04.0	-	05.0	03.4	03.7	81	41	60	61	NNNE 1	NE 1	NW 1	
2	747.2	745.3	747.4	00.0	05.5	07.4	06.1	10.6	00.0	-	03.9	04.2	04.6	86	49	60	65	WSW 2	WSW 2	S 2	
3	749.3	749.5	749.9	05.2	12.7	05.2	09.1	12.8	02.6	-	03.8	02.9	04.1	56	28	47	44	NW 2	WNW 2	NE 1	
4	743.6	747.7	747.9	03.8	04.6	07.2	06.7	09.2	03.4	-	04.3	05.4	05.8	72	64	77	71	NNNE 1	SE 2	NF 2	
5	748.7	750.7	753.3	06.0	06.9	05.8	06.1	07.3	05.6	-	06.3	06.7	06.5	90	90	94	91	NNNE 1	WSW 1	WSW 1	
6	754.7	755.1	756.9	05.7	05.9	05.8	05.8	06.2	05.4	-	05.9	06.2	06.3	87	90	93	90	NNNE 1	SSW 1	SSS 1	
7	756.2	754.9	755.0	05.3	05.8	05.6	05.6	06.0	04.9	-	05.5	05.0	05.1	82	73	74	76	NNE 2	NNE 2	NNE 3	
8	753.5	753.4	754.2	05.0	06.8	06.6	06.2	07.0	04.8	-	04.7	04.4	03.8	72	60	55	62	WNW 1	ENE 2	NF 2	
9	753.8	753.0	753.1	03.3	05.8	04.9	04.9	08.9	03.2	-	04.5	04.4	04.6	80	53	57	56	WSW 1	SSF 2	WNW 1	
10	752.4	750.9	751.1	-00.2	08.3	04.0	08.4	-00.2	-	04.0	05.0	05.7	91	61	94	82	ENE 1	SE 2	ENF 2		
11	753.3	752.9	752.2	02.1	04.1	02.8	03.0	04.1	01.6	-	05.3	05.7	05.3	98	92	95	95	NNE 1	S 1	SSE 1	
12	750.6	749.1	749.8	01.7	11.1	10.6	08.5	11.8	00.8	-	05.1	06.9	06.8	98	69	71	79	WSW 2	SW 1	SW 2	
13	749.7	750.2	750.9	08.3	13.5	11.0	11.0	14.1	07.2	-	06.2	07.4	07.0	76	64	71	70	W 1	SSF 2	WNW 2	
14	750.1	749.8	750.1	10.1	14.7	11.6	12.0	14.7	06.5	-	07.0	07.0	07.3	75	56	67	65	WSW 2	SSW 4	WSW 2	
15	749.9	749.8	750.2	12.0	17.1	13.8	14.2	17.1	10.8	-	07.6	07.8	07.9	72	54	67	64	W 2	SW 5	WSW 2	
16	749.0	748.5	750.0	11.1	15.8	14.2	14.6	18.5	11.0	-	07.2	08.1	07.6	73	49	63	62	WNW 2	WSW 4	WNW 2	
17	752.4	752.5	752.2	11.2	14.2	13.0	13.4	16.2	11.2	-	07.3	08.2	08.5	73	55	76	69	SSW 2	SSW 2	WNW 2	
18	750.8	750.1	749.3	10.2	16.8	11.2	12.4	16.9	09.4	-	08.1	07.6	07.3	87	53	75	72	WNW 1	WSW 2	SSW 1	
19	745.2	744.4	740.3	08.7	11.4	07.1	08.6	13.6	06.9	-	07.1	07.8	07.0	85	77	93	85	ENE 2	SSW 3	SSW 2	
20	752.5	751.6	751.5	05.2	09.1	06.4	06.8	09.1	05.2	-	05.9	06.4	06.3	89	74	88	84	NNNE 1	S 1	N 1	
21	750.4	750.1	751.2	05.4	09.4	08.3	08.0	10.2	04.7	-	06.0	06.0	07.0	90	66	86	81	ENE 1	WNW 1	ENE 2	
22	752.1	750.5	750.1	05.6	06.8	06.2	06.2	08.3	05.4	-	06.2	06.5	06.7	90	88	94	91	E 2	SSE 1	SSW 2	
23	750.2	749.4	749.4	05.7	09.9	08.8	08.3	10.1	05.7	-	06.5	06.8	06.9	94	75	82	84	ENE 1	S 1	N 1	
24	749.4	749.6	749.9	07.7	09.6	06.8	03.7	09.7	07.7	-	06.8	06.7	06.9	87	75	83	82	ENE 1	E 1	ENE 1	
25	747.6	744.0	742.6	06.0	07.6	08.2	07.5	08.8	06.0	-	06.7	07.0	07.7	96	89	94	93	ENE 2	NNNE 1	ENE 1	
26	740.3	745.5	743.7	04.9	07.0	05.0	05.5	08.2	04.6	-	05.7	05.6	05.6	88	75	84	82	W 1	SW 2	W 1	
27	741.9	743.6	743.9	03.1	07.7	07.4	04.4	07.7	03.0	-	05.1	05.1	05.2	89	65	91	82	EKE 1	EKE 2	W 1	
28	733.3	732.7	735.9	02.0	04.6	00.9	02.0	06.2	00.6	-	05.0	05.5	04.8	73	86	99	93	WNW 2	NNE 2	WNW 1	
29	736.4	737.9	740.4	02.6	02.9	01.6	02.2	03.0	00.3	-	04.7	05.0	04.8	84	88	93	88	WSW 2	FNE 1	SW 1	
30	745.2	747.3	747.5	-00.1	05.0	03.3	02.9	05.0	-00.5	-	04.0	04.9	04.4	93	74	76	81	W 1	WSW 1	NW 1	
MES.	VRED.	748.8	748.5	749.2	05.4	05.5	07.2	07.3	10.0	04.8	-	05.7	06.0	06.0	R4	68	79	77	1.4	1.5	1.5

1	745.7	749.2	743.4	01.7	11.2	05.4	05.5	11.2	01.7	-	04.7	03.9	04.6	90	39	68	66	WSW 1	W 3	N 1
2	752.6	754.9	756.2	08.1	11.1	06.7	08.9	11.2	03.5	-	05.4	05.7	05.2	66	58	64	63	WNW 2	NNNE 1	WNW 2
3	757.4	757.6	757.8	06.6	12.4	04.2	09.4	12.4	05.9	-	06.1	06.0	07.0	84	56	73	73	ESE 1	SSE 1	WSW 1
4	756.5	754.4	751.3	04.5	10.2	06.6	07.0	10.2	04.3	-	05.5	06.4	06.2	67	69	87	81	ENE 1	SSE 1	NW 1
5	748.5	747.0	747.4	01.2	06.5	03.8	03.8	06.6	00.9	-	04.8	05.5	05.8	97	76	96	90	S 1	SE 1	ENE 1
6	749.4	748.7	749.1	03.6	05.8	03.6	04.2	05.8	03.3	-	04.9	05.8	05.3	85	83	88	85	ENE 1	SSE 2	NE 2
7	747.6	746.0	746.3	01.1	04.0	04.0	03.3	04.1	01.1	-	04.7	05.0	05.0	97	82	82	87	WSW 2	SSE 1	SSE 1
8	743.9	744.6	747.0	00.1	10.2	08.0	08.8	10.2	03.5	-	04.4	05.0	04.3	51	54	79	61	NW 3	NW 3	ENE 2
9	749.4	749.6	751.2	07.9	11.2	02.4	09.0	11.3	07.5	-	06.8	07.0	07.9	95	70	84	80	N 1	SSE 1	NNE 2
10	750.8	750.7	752.1	03.5	04.9	05.6	04.6	08.5	03.4	-	05.8	06.4	06.4	98	98	98	98	ENE 1	ENE 1	WSW 1
11	750.3	745.8	741.2	04.6	05.4	05.2	05.1	05.5	04.4	-	06.0	06.2	06.4	94	52	96	94	E 1	E 1	NE 2
12	744.9	745.5	744.4	01.4	02.6	02.6	02.3	06.4	01.2	-	04.8	04.8	04.7	95	87	89	89	ESE 2	WSW 2	WSW 1
13	733.9	733.7	734.1	-01.2	01.2	02.1	01.0	02.6	-01.2	-	04.2	04.3	03.0	98	86	57	80	WSW 2	WNW 2	NNE 2
14	751.5	751.7	752.6	02.3	04.2	-00.6	01.3	04.2	-00.6	-	03.1	03.4	03.0	57	55	69	60	N 3	NNE 2	WNW 1
15	751.1	749.9	749.7	-03.8	02.6	00.6	00.0	02.6	-03.8	-	02.9	02.9	03.0	84	52	67	67	WNW 1	WNW 2	SW 1
16	750.6	750.8	751.0	-02.2	02.6	01.8	01.0	02.8	-02.2	-	03.6	03.6	03.9	90	66	75	77	W 1	SSE 1	WNW 2
17	747.1	742.1	740.2	-01.4	02.7	08.5	04.6	08.8	-01.4	-	03.7	03.8	04.3	90	68	52	70	WSW 1	WSW 2	WSW 4
18	742.3	744.1	745.0	05.																

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Isotacija broj sani	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6	10	050	00	05.0	05.6	02.0	.	= n-12 <sup>46</sup>		
2	7	060	080	02	05.3	05.9	.	.	= n-10 <sup>30</sup> , △ <sup>0</sup> n-a		
3	6	010	030	10	04.7	08.9	.	.	= n-n, = 07 <sup>30</sup> 9 <sup>30</sup> , 0-19 <sup>40</sup> n		
4	4	05	09	100	08.0	00.8	.	.	= 0-11 <sup>00</sup> , 16 <sup>35</sup> n, = 0-11 <sup>30</sup> , = 11 <sup>30</sup> n		
5	4	100	10	100	10.0	00.0	03.6	.	• = 0-10 <sup>30</sup> , + r-0-17 <sup>25</sup> n, = 10 <sup>30</sup> n		
6	4	10	100	10	10.0	00.0	01.0	.	= n-n, △ <sup>0</sup> n		
7	4	10	10	10	10.0	00.0	05.8	.	= n-n, + r-0-17 <sup>25</sup> n		
8	5	10	10	10	10.0	00.0	00.8	.	= n-n, = 0-17 <sup>25</sup> n		
9	6	10	010	00	03.7	06.4	00.0	.	= n-n, = 0-17 <sup>25</sup> n		
10	5	02	020	09	04.3	05.9	.	.	= n-n, △ <sup>0</sup> n-a		
11	2	10	10	10	10.0	00.0	.	.	= 1-2 n-n, = 18 <sup>15</sup> 20 <sup>45</sup>		
12	6	10	040	08	07.3	03.7	.	.	= 1-2 n-9 <sup>30</sup> , = 9 <sup>30</sup> 11 <sup>30</sup> , = 11 <sup>30</sup> 14 <sup>45</sup>		
13	6	08	050	05	06.0	07.1	.	.	= 0-12 n-9 <sup>30</sup> , = 9 <sup>30</sup> 13 <sup>45</sup>		
14	6	090	020	00	03.7	03.6	.	.	= 7 <sup>45</sup> 13 <sup>30</sup>		
15	9	07	060	06	06.3	06.7	.	.	= SW 12 <sup>30</sup> 14 <sup>45</sup>		
16	8	010	06	10	05.7	06.4	.	.	F <sub>WSW</sub> a		
17	8	07	070	00	04.7	00.8	.	.	+ 13 <sup>45</sup> 13 <sup>38</sup>		
18	8	07	09	07	07.7	00.7	.	.	= 0-17 <sup>45</sup> , = 7 <sup>45</sup> 11 <sup>30</sup>		
19	6	07	10	100	05.0	01.5	.	.	= n-n, = 0-12 01 13 <sup>30</sup> 17 <sup>02</sup> n		
20	7	08	08	10	08.7	02.2	09.3	.	= 0-17 <sup>45</sup> , = 8 <sup>45</sup> 12 <sup>45</sup> 16 <sup>30</sup> n		
21	5	10	09	10	05.7	00.1	00.0	.	= 0-17 <sup>45</sup> , + r-7 <sup>15</sup> 10 <sup>50</sup> , = 9 <sup>30</sup> n		
22	4	10	10	10	10.0	00.0	.	.	= n-8 <sup>45</sup> , = 11 <sup>30</sup> n, = 0-8 <sup>45</sup> 11 <sup>30</sup>		
23	5	10	090	08	05.0	01.4	.	.	= 0-12 n-11 <sup>30</sup> , = 11 <sup>30</sup> n		
24	6	10	10	10	10.0	00.0	.	.	= 0-17 <sup>45</sup> , = 8 <sup>45</sup> 12 <sup>45</sup> 16 <sup>30</sup> n		
25	3	10	10	100	10.0	00.0	00.1	.	• = 0-17 <sup>45</sup> , = 14 <sup>22</sup> n, = 1-11 <sup>30</sup> , = 11 <sup>30</sup> n		
26	8	10	020	07	06.3	02.0	09.3	.	= 0-17 <sup>45</sup> , = 10-10, * 2 15 <sup>12</sup> 17 <sup>50</sup> , * 17 <sup>50</sup> 18 <sup>38</sup> , / n; R <sup>1</sup> 14 <sup>04</sup> 14 <sup>45</sup> , = n-n, ■		
27	7	10	010	08	06.3	04.5	00.4	.	• = 0-17 <sup>45</sup> , = 15 <sup>12</sup> 17 <sup>50</sup> , * 2 15 <sup>12</sup> 17 <sup>50</sup> , * 17 <sup>50</sup> 18 <sup>38</sup> , / n; R <sup>1</sup> 14 <sup>04</sup> 14 <sup>45</sup> , = n-n, ■		
28	5	10	10	100	10.0	00.0	00.0	06	= 7 <sup>45</sup> n, ■		
29	4	09	10	09	09.3	00.3	29.0	02	= 0-17 <sup>45</sup> , = 9 <sup>30</sup> n, ■		
30	4	06	030	08	05.7	06.0	.	02	= 0-17 <sup>45</sup> , = 9 <sup>30</sup> n, ■		
MES.					08.1	07.0	07.6	07.5	81.4	62.1	

1	6	08	000	09	05.7	04.0	.	.	= n-j-n		
2	7	10	10	10	10.0	00.1	.	.	= n-j-7 <sup>30</sup> , + r-0-17 <sup>45</sup> 18 <sup>05</sup>		
3	6	10	020	09	07.0	06.0	00.0	.	= n-j-7 <sup>45</sup> 10 <sup>45</sup> , = 0-7 <sup>45</sup> 10 <sup>45</sup>		
4	5	01	000	00	00.3	00.3	06.6	.	= n-j-7 <sup>30</sup> 10 <sup>30</sup> , n, = 0-7 <sup>30</sup> 10 <sup>30</sup>		
5	3	10	10	10	10.0	00.5	.	.	= 1-17 <sup>45</sup> , = 8 <sup>45</sup> 13 <sup>45</sup> , = 13 <sup>45</sup> n		
6	4	09	10	09	09.3	00.0	.	.	= n-j-n, + r-9 <sup>45</sup> 11 <sup>58</sup>		
7	5	10	10	10	10.0	00.0	00.0	.	= n-j-7 <sup>30</sup> , = 0-7 <sup>30</sup> 8 <sup>45</sup> , = 8 <sup>45</sup> n		
8	6	10	10	10	10.0	00.0	.	.	= n-j-n, + r-10 <sup>45</sup>		
9	5	08	090	10	05.0	00.2	00.0	.	= n-j-7 <sup>30</sup> , + r-13 <sup>30</sup> , = 0-7 <sup>30</sup> 9 <sup>45</sup> , = 9 <sup>45</sup> n		
10	3	10	10	10	10	00.0	00.0	.	= 0-12 n-14 <sup>15</sup> 20-20, n, = 14 <sup>15</sup> 20 <sup>30</sup>		
11	4	10	100	10	10.0	00.1	00.0	.	= n-17 <sup>45</sup> 11 <sup>30</sup> , n, = 0-17 <sup>45</sup> 11 <sup>30</sup> , + r-0-17 <sup>45</sup> 16 <sup>40</sup> , = 19 <sup>30</sup> n		
12	7	10	10	10	10.0	00.0	10.3	.	= n-11 <sup>15</sup> , + r-n-10 <sup>45</sup> , 10 <sup>45</sup> n, * 2 15 <sup>12</sup> 17 <sup>50</sup> , * 17 <sup>50</sup> 18 <sup>38</sup>		
13	5	10	090	07	06.7	00.2	02.2	.	= 3n-10 <sup>45</sup> , = 10 <sup>45</sup> n, * 2 15 <sup>12</sup> 17 <sup>50</sup> , * 17 <sup>50</sup> 18 <sup>38</sup>		
14	8	06	010	00	02.3	07.2	00.0	.	= n-8 <sup>45</sup> , F NNE 5 <sup>39</sup>		
15	7	01	010	00	00.7	07.0	.	.	= 1-17 <sup>45</sup> , = rj-10 <sup>15</sup>		
16	4	00	060	00	02.0	04.4	.	.	= n-n, △ <sup>0</sup> n-a		
17	5	02	10	10	07.3	00.0	.	.	= n-n, △ <sup>0</sup> n-9-9, F WSW 19 <sup>36</sup> 19 <sup>57</sup>		
18	6	10	050	04	06.3	04.0	04.0	.	* 0-17 <sup>45</sup> , = 15 <sup>45</sup> 20 <sup>30</sup> , = 0-20 <sup>30</sup> n		
19	1	03	10	10	07.7	01.0	00.4	.	= 1-17 <sup>45</sup> , = 10 <sup>45</sup> 20 <sup>30</sup> , = 2-9 <sup>40</sup> 10 <sup>45</sup> , 20-20, n, = 14 <sup>45</sup> 15 <sup>50</sup>		
20	6	10	070	06	07.7	06.5	.	.	= 1-17 <sup>45</sup> , = 10 <sup>45</sup> 20 <sup>30</sup> , = 0-7 <sup>45</sup> n, = 7 <sup>45</sup> n		
21	6	09	030	00	04.0	06.0	.	.	= n-n, △ <sup>0</sup> n-a		
22	4	03	000	00	01.0	06.5	.	.	= n-j-n, △ <sup>0</sup> n-9, = 1-17 <sup>45</sup> , = 10 <sup>45</sup> 20 <sup>30</sup>		
23	1	10	10	10	10	00	.	.	= 1-17 <sup>45</sup> , = 10 <sup>45</sup> 20 <sup>30</sup> , = 2-9 <sup>40</sup> 17 <sup>30</sup> , 20 <sup>30</sup> n, = 2-17 <sup>30</sup> 20 <sup>30</sup>		
24	2	10	10	10	00	06.7	00.0	.	= n-n, + r-n-rj, △ <sup>0</sup> rj-11 <sup>30</sup> , = 1-17 <sup>45</sup> , = 2-9 <sup>40</sup> 17 <sup>30</sup> , 20 <sup>30</sup> n, = 2-17 <sup>30</sup> 20 <sup>30</sup>		
25	5	10	10	00	06.7	00.0	00.1	.	= n-n, + r-n-rj, △ <sup>0</sup> rj-11 <sup>30</sup> , = 1-17 <sup>45</sup> , = 2-9 <sup>40</sup> 17 <sup>30</sup> , 20 <sup>30</sup> n, = 2-17 <sup>30</sup> 20 <sup>30</sup>		
26	6	10	10	00	06.7	00.1	.	.	= 0-17 <sup>45</sup> , = 8 <sup>30</sup> 9 <sup>30</sup> , = 9 <sup>30</sup> 16 <sup>30</sup> , F WNW 18 <sup>34</sup> 19 <sup>05</sup>		
27	6	00	090	10	06.3	04.9	.	.	= n-n, + r-12 <sup>30</sup> n, = 12 <sup>30</sup> 18 <sup>10</sup>		
28	5	01	090	07	05.7	07.0	00.4	.	= 17 <sup>45</sup> , = 18 <sup>45</sup> n, F 22 <sup>45</sup> 23 <sup>05</sup>		
29	8	04	030	10	05.7	04.1	00.1	.	= n-14 <sup>45</sup> , + r-0-17 <sup>45</sup> , = 12 <sup>30</sup> 12 <sup>45</sup>		
30	6	10	10	C5	08.3	00.0	04.6	.	= n-13 <sup>45</sup> , + r-11 <sup>15</sup> , = 14 <sup>45</sup> 16 <sup>45</sup> , + r-13 <sup>45</sup> 13 <sup>45</sup>		
31	5	09	10	06	08.3	00.2	00.3	.	= n-13 <sup>45</sup> , + r-11 <sup>15</sup> , = 14 <sup>45</sup> 16 <sup>45</sup> , + r-13 <sup>45</sup> 13 <sup>45</sup>		
MES.					07.2	07.2	06.2	06.9	76.1	22.5	

1974 JANUAR

## SPLIT MARJAN

 $\varphi = 43^{\circ}31'$ ,  $N \lambda = 16^{\circ}26'$ , E Gr.,  $\Delta G = +1h\ 06\ min.$ 

BR. ST. 89

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina vjetra D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	752.0	751.5	752.6	11.2	11.5	11.8	11.6	14.0	10.4	-	05.5	09.5	08.9	95	93	85	91	S	3	ENE 4	ESE 5	
2	752.5	751.7	752.5	10.3	11.5	10.2	10.6	12.0	09.6	-	08.7	08.6	08.6	93	84	92	90	E	4	ESE 4	ESE 4	
3	751.6	752.2	753.9	09.2	09.9	09.8	09.6	11.3	08.6	-	07.2	07.8	06.9	83	86	76	82	ENE 3	ESE 4	NE 2		
4	755.6	756.5	758.0	09.9	12.9	10.9	11.2	13.4	08.6	-	07.1	08.2	07.0	78	74	72	75	ENE 2	ESE 2	-	0	
5	757.6	756.8	756.6	08.8	10.1	09.4	09.4	11.2	08.1	-	06.6	07.4	06.2	78	80	70	76	N	1	SSW 1	WSW 1	
6	753.9	751.2	750.5	08.2	09.6	09.8	09.4	10.8	07.3	-	06.3	07.2	07.4	77	81	81	80	ENE 2	ESE 1	SF 2		
7	751.7	753.1	754.2	08.0	11.4	08.0	08.8	11.5	07.2	-	06.8	07.0	05.4	85	69	67	74	N	2	S 1	NE 1	
8	753.7	753.8	754.7	07.3	07.7	06.9	07.3	08.7	06.5	-	04.4	06.7	06.2	55	84	83	74	N	3	W 1	NNW 1	
9	754.4	753.4	752.0	06.0	09.7	08.8	08.3	10.4	05.7	-	04.1	05.2	06.2	5F	57	73	63	NE 1	ESE 4			
10	748.0	748.1	750.8	09.0	09.8	10.3	09.8	11.0	08.0	-	05.3	06.7	06.1	62	74	65	67	ENE 4	SE 1	N	1	
11	754.1	755.4	757.9	07.7	12.2	09.4	09.7	12.4	07.0	-	04.3	05.6	05.0	54	53	57	55	NE 1	-	0	SSE 1	
12	758.6	758.2	758.9	07.0	11.7	10.8	10.1	11.8	06.6	-	05.4	05.6	04.2	71	54	43	56	NNE 1	SSE 1	NNE 1		
13	756.7	755.5	756.0	09.0	11.8	09.2	10.0	12.0	04.5	-	03.3	04.1	03.3	36	40	38	38	NW 1	S 1	N	2	
14	756.9	756.8	757.2	05.7	09.2	06.8	07.1	09.7	05.1	-	02.4	03.7	03.2	35	42	44	40	NE 2	SSE 1	NW 1		
15	757.1	756.9	756.9	03.7	09.0	07.6	07.0	10.0	03.2	-	02.8	02.9	03.8	47	33	43	43	NNE 2	NNE 1	ESE 2		
16	756.8	756.7	756.1	07.6	10.0	08.2	08.5	10.5	06.6	-	03.8	04.8	04.5	48	52	55	52	-	0	-	0	
17	753.3	750.8	751.5	07.7	08.1	08.8	08.4	08.8	06.5	-	05.4	06.9	04.5	68	85	52	68	SSE 1	SE 1	NE 4		
18	754.3	753.4	753.4	06.6	10.4	09.4	09.0	10.5	06.0	-	04.0	02.9	04.2	54	31	43	44	NNW 3	NNW 3	N	3	
19	753.8	753.4	754.1	08.8	11.8	10.8	10.6	12.5	06.0	-	05.0	05.5	05.7	59	53	59	57	W 2	NNW 3	N	3	
20	752.7	752.2	754.2	14.2	17.2	13.8	14.8	17.4	10.6	-	05.6	05.4	04.7	46	37	40	41	N	2	N	1	
21	755.3	754.9	755.9	09.8	13.5	09.7	10.7	14.8	05.3	-	04.6	05.2	04.6	51	45	51	49	N	2	E 2	N 1	
22	756.5	756.3	756.5	06.5	11.6	08.8	08.9	12.4	06.4	-	03.6	04.7	04.9	49	46	58	51	NE 2	SSW 1	NW 1		
23	756.4	756.3	755.3	06.6	11.0	09.6	09.2	11.7	05.9	-	04.1	06.5	06.0	56	66	67	63	NE 2	N 1	N	2	
24	754.2	754.3	753.9	05.4	12.0	09.1	09.6	12.0	06.8	-	03.5	05.1	04.9	43	49	56	49	NE 3	SW 2	E 2		
25	753.0	752.5	752.7	06.3	10.0	07.1	07.6	10.1	05.2	-	04.0	05.4	05.5	56	59	73	63	N	1	SSW 2	NE 1	
26	754.3	754.6	754.5	05.6	11.0	08.2	08.2	11.0	05.0	-	04.8	06.1	04.9	70	62	61	64	NE 2	SSW 1	N 1		
27	753.1	752.0	752.4	06.6	09.6	07.8	08.0	10.6	05.1	-	04.8	06.5	05.8	66	73	73	71	ENE 2	ESE 4	ENE 2		
28	753.0	753.4	754.3	07.3	13.0	10.0	10.1	13.0	06.4	-	05.0	05.5	05.0	65	49	54	56	NE 3	SW 2	NNW 2		
29	754.5	754.8	755.4	06.7	11.4	09.0	09.0	12.6	06.3	-	04.2	05.7	06.5	57	57	76	63	NE 2	SW 1	ESE 1		
30	757.1	757.6	757.9	07.5	11.8	09.3	09.5	12.1	06.8	-	05.0	05.4	05.6	63	52	63	59	ENE 2	S 1	E 1		
31	758.4	758.0	758.1	08.2	11.2	09.5	09.8	11.8	07.7	-	05.7	06.2	06.6	70	63	72	68	E 2	ESE 4	ENE 2		
MES.	754.6	754.3	754.8	08.0	11.0	09.2	09.4	11.7	06.9	-	05.1	05.9	05.6	62	61	63	62	2.0	1.8	1.8		
VRD.	754.6	754.3	754.8	08.0	11.0	09.2	09.4	11.7	06.9	-	05.1	05.9	05.6	62	61	63	62	2.0	1.8	1.8		

1974 FEBRuar

## SPLIT MARJAN

1	756.8	756.0	756.4	09.9	12.4	11.1	11.1	12.4	09.3	-	07.3	07.8	07.2	80	72	73	75	SE	4	ESE 4	ESE 4
2	755.8	755.3	755.3	10.2	13.0	11.4	11.5	13.3	09.9	-	06.9	07.7	08.2	74	69	81	75	E	2	SE 2	SL 5
3	753.2	750.7	748.4	10.5	12.4	10.3	10.9	12.5	09.0	-	06.0	08.8	08.1	84	81	86	84	SE	6	SE 6	E 3
4	745.1	745.3	746.4	09.4	09.2	09.0	09.2	11.0	07.7	-	07.7	07.9	06.5	87	90	76	84	SF	5	SW 2	NNW 1
5	746.3	744.5	743.7	07.5	10.8	07.2	08.2	11.8	06.4	-	06.1	06.4	06.4	78	66	84	76	NE	1	SE 3	F 3
6	740.2	735.6	730.2	08.9	10.8	11.2	10.5	11.7	06.8	-	07.3	07.2	08.4	85	74	84	81	SE	5	SE 6	SSE 6
7	728.5	730.9	734.4	08.0	10.6	07.8	08.6	11.6	07.5	-	04.8	03.2	03.6	59	33	46	46	NW	3	N	1
8	740.6	745.9	751.4	06.0	10.5	08.2	08.2	11.0	05.5	-	03.3	02.9	02.5	47	30	31	36	ENE	2	N	3
9	754.8	755.0	755.1	05.5	11.3	08.8	08.6	11.5	04.7	-	02.8	05.1	05.6	42	50	66	53	NE	2	S 2	ENF 1
10	755.3	755.3	755.3	07.9	12.4	10.0	10.1	13.2	07.4	-	04.7	05.8	06.6	59	54	72	62	ENE	2	ENE 1	WSW 1
11	754.1	752.4	751.4	08.8	13.2	10.0	10.5	13.7	08.5	-	06.8	08.2	07.8	80	72	85	79	NNE	2	SSE 1	ESE 2
12	749.1	746.9	745.5	08.2	12.8	10.8	10.6	12.8	07.9	-	05.9	07.4	07.6	73	66	78	72	ENE	3	SF 5	SE 5
13	742.0	741.2	740.3	11.0	14.7	12.4	12.6	15.0	10.8	-	08.0	08.2	08.6	82	66	81	76	SE	5	S 4	ESE 4
14	738.7	741.6	743.6	10.1	11.9	12.0	11.5	12.5	09.5	-	08.7	07.8	07.8	94	75	74	81	SE	5	SE 5	ESE 3
15	743.5	744.0	744.5	11.2																	

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	6	10•	10•	10	10•	10.0	00.0	32.4	.	R°n, 0°6°18°55'	
2	7	10•	10•	10•	10•	00.0	00.1	50.0	.	•n-n	
3	7	10	10•	09	09	09.7	C6.9	26.2	.	•n-0725, 8, 12°55' 15°45'	
4	8	09	04•	00	04•	04.3	03.7	00.9	.	= 12°55' 13°30'	
5	7	07	09	09	08.3	00.9	.	.	.		
6	7	10•	10	10•	10.0	00.0	00.7	.	•-16°45' 13°45' 17°40' n		
7	8	10•	04•	00	04•	04.7	C6.0	C2.8	.	•-16°30' 8°30' 1	
8	8	10	09	00	06.3	00.2	02.0	.	•-19°45' 12°35'		
9	8	09	09	08	08.7	03.1	C2.0	.	•-19°45' 17°30'	.	
10	8	10	10•	10	10.0	00.0	.	.	•-19°45' 17°30'	.	
11	8	01	07•	00	02.7	C8.3	04.1	.	.		
12	7	03	02•	00	01.7	07.4	.	.	= 10°30' n	.	
13	8	01	05•	00	02.0	00.3	.	.	.		
14	8	04	08	00	04.0	04.6	.	.	• 12°35' 13, = 18°5 n	.	
15	7	00	05•	08	04.3	07.2	.	.	= 9°5 n	.	
16	7	10	10	00	06.7	00.0	.	.	•-18°20' 9°25' = 13°40' 18°20'	.	
17	6	10	10•	06	08.7	00.0	00.2	.	•-10°45' 17°30'	.	
18	8	02	04•	01	02.3	C8.2	11.7	.	.	.	
19	8	09	06	03	06.0	06.0	.	.	.	.	
20	8	07	05	00	04.0	05.5	.	.	.	.	
21	8	01	00•	00	00.3	08.6	.	.	= 8°5 13°30'	.	
22	8	00	00•	00	00.0	C8.5	.	.	= 8- 9°45'	.	
23	8	00	09	02	03.7	03.8	.	.	.	.	
24	8	00	00•	00	00.0	C9.0	.	.	.	.	
25	7	06	09	10	08.3	01.9	.	.	.	.	
MES. WRED.					05.5	06.2	03.6	05.1	138.9	127.1	

1	8	05	07	10	07.3	C4.1	.	.	•-16°50' 17°20'		
2	8	08	07	04	06.3	C5.3	00.1	.	•-13°30' 12°30' 19°40' ESE 6°00' 18°45' 13°18°30' 19°40'	.	
3	7	03	10•	10	07.7	02.0	00.1	.	•-2.6°45' 7°25' 13°50' 14°30' • 17°25' 9°30'	.	
4	7	10•	10•	10	10.0	C8.0	C9.9	.	•-16°20' 9°25' 10°20' 20°30'	.	
5	8	10•	08	10	09.3	04.0	11.2	.	•-16°30' 17°02' 12°50' 13°05'	.	
6	8	09	10•	10•	05.7	00.0	02.4	.	ESE-SE 6°30' 12°45' • 11°55' 17°05' 20°45' n	.	
7	9	10•	04•	04	06.0	08.1	11.7	.	•-16°30' 17	.	
8	8	04	04•	00	02.7	C8.4	.	.	.	.	
9	8	01	01•	00	00.7	09.2	.	.	.	.	
10	8	10	06•	02	06.0	C1.8	.	.	.	.	
11	6	10	07•	00	05.7	02.8	.	.	•-6°20' n	.	
12	8	05	04•	00	03.0	07.4	.	.	•-6°50' 7°30'	.	
13	8	10•	06•	05	07.0	03.7	01.0	.	•-16°30' 15°20'	.	
14	8	10•	09	09	05.3	C1.2	C5.3	.	•-7°45' 8°10'	.	
15	8	10	06	00	05.3	03.0	01.5	.	.	.	
16	8	10	09	04	07.7	03.0	00.1	.	.	.	
17	8	07	07	10	08.0	04.2	.	.	ESE 6°10' n, • 17°20' n	.	
18	8	09	10	10•	09.7	C0.0	.	.	ESE 6°30' 11°30' • 10°30' 11°50' T 11°15' 11°20'	.	
19	8	07	09	09	08.3	03.7	15.7	.	.	.	
20	8	03	07	00	03.3	07.6	00.7	.	.	.	
21	8	07	08	00	05.0	05.1	.	.	•-18°30' 8°55' 12°20' 20°40' i; FNE 23°22' 24	.	
22	6	10	10•	10	10.0	00.0	.	.	•-14°30' 17°30' 16°30' i; FNE 23°22' 24	.	
23	7	10	10•	10	10.0	00.0	08.8	.	FNE 0°-24	.	
24	8	07	05•	00	04.0	08.5	C6.4	.	F0-24	.	
25	8	01	00•	00	00.3	09.3	.	.	F0-24	.	
26	8	10	07•	09	08.7	03.4	.	.	.	.	
27	8	08	05•	00	04.3	08.2	.	.	.	.	
28	8	02•	03•	00	01.7	09.7	.	.	.	.	
MES. WRED.					07.4	06.8	04.8	06.3	131.7	75.1	

1974 MART

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$  N  $\lambda = 16^{\circ}26'$  E Gr.  $\Delta G = +1h\ 06\ min.$ 

BK. ST. 89

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	750.7	749.7	749.1	05.3	12.5	09.0	09.0	13.0	04.9	-	04.0	05.8	05.5	60	53	64	59	NNE 3	SSW 3	ESE 1	
2	746.0	744.3	744.9	07.4	07.1	05.6	06.4	09.1	05.6	-	06.7	06.5	06.1	87	85	89	87	ESE 5	SE 6	S 1	
3	748.2	750.5	751.6	06.5	07.0	08.2	07.7	09.1	04.0	-	06.2	07.4	06.0	85	92	74	84	SE 3	SE 4	ESE 3	
4	750.5	749.3	746.9	10.7	10.2	10.2	10.3	11.7	06.1	-	06.1	08.2	08.2	63	88	88	80	SSE 7	SE 7	SE 8	
5	745.4	745.6	745.3	10.2	12.4	09.8	10.6	13.2	09.8	-	08.9	09.0	08.4	95	84	93	91	SE 7	ESE 1	SE 2	
6	742.2	744.2	747.1	09.5	08.6	06.2	08.6	11.0	07.8	-	06.1	06.4	06.4	68	76	79	74	ENE 4	ESE 7	ENE 1	
7	747.7	748.6	750.0	07.0	10.5	07.6	08.2	12.7	06.4	-	04.0	04.2	02.9	53	44	38	45	ENE 5	NE 5	NE 4	
8	749.9	749.8	751.0	06.8	11.5	07.2	08.2	12.4	06.2	-	03.5	04.3	03.6	47	42	47	45	NNE 5	ESE 2	NE 3	
9	751.4	751.9	753.1	05.8	11.2	08.2	08.4	12.2	05.5	-	03.5	04.4	04.6	50	44	56	50	NE 3	WSW 2	N 1	
10	752.7	752.3	752.5	06.2	12.4	07.8	08.6	13.0	05.8	-	04.5	04.8	04.1	64	45	52	54	NNE 1	WSW 2	NNW 2	
11	753.3	754.4	755.7	06.5	13.1	08.7	09.2	14.0	06.0	-	03.8	04.9	04.2	53	43	50	49	ENE 4	SW 2	ENE 4	
12	756.1	755.7	754.7	06.0	12.8	09.2	09.3	12.9	05.3	-	03.6	05.0	04.2	51	45	48	48	ENE 3	SW 2	ENE 1	
13	752.8	750.3	748.5	06.1	13.3	10.0	09.8	13.4	05.3	-	04.1	05.6	04.4	59	49	48	52	ENE 2	SW 2	NW 2	
14	744.7	740.4	739.8	08.0	15.4	12.6	12.2	15.7	06.2	-	03.4	06.5	05.3	42	50	49	47	NE 2	S 3	SSW 2	
15	759.1	730.0	742.1	10.4	15.4	11.8	12.4	16.1	05.9	-	02.5	03.5	03.6	27	27	35	30	NE 3	NE 5	NE 4	
16	743.1	743.0	744.0	09.5	15.2	11.0	11.7	15.5	09.0	-	04.0	05.4	05.7	45	42	58	48	NE 2	W 3	NNW 2	
17	746.6	748.2	749.5	08.4	15.1	11.4	11.6	15.4	08.0	-	05.2	06.7	08.1	63	52	80	65	ENE 2	SW 2	ESE 2	
18	750.9	750.6	751.4	09.9	15.9	13.7	13.3	16.0	09.0	-	05.0	06.5	06.3	54	48	53	52	NE 2	SE 4	SE 5	
19	752.6	753.4	754.1	12.9	14.8	13.2	13.5	15.0	12.4	-	08.9	08.6	08.2	80	68	72	73	SE 6	SE 6	ESE 5	
20	754.2	753.9	754.9	12.7	15.7	13.5	13.8	16.6	12.0	-	07.0	07.7	06.7	63	58	58	60	SE 5	SE 5	SSE 3	
21	755.1	754.7	754.4	14.1	19.5	15.0	15.9	19.8	13.2	-	02.4	03.6	05.6	20	21	44	28	ENE 3	SW 1	NW 1	
22	753.6	753.2	751.6	11.2	17.5	12.2	13.4	18.0	11.0	-	08.3	08.8	10.1	83	58	94	78	WSW 1	SSW 1	WSW 1	
23	752.7	753.1	753.0	11.2	17.1	12.7	13.9	17.3	10.6	-	09.4	08.8	08.0	94	60	68	74	SE 1	SW 2	NW 1	
24	753.1	752.4	752.0	11.4	16.8	12.6	13.4	17.7	10.6	-	07.5	09.8	09.5	74	68	87	76	ESE 1	SW 2	NNW 2	
25	751.4	751.6	751.5	11.8	18.0	15.8	15.4	19.0	10.5	-	07.9	07.2	06.1	76	46	45	56	ENF 1	SW 1	NNW 1	
26	751.2	750.1	749.3	14.0	19.0	15.6	16.2	19.6	13.7	-	06.3	07.3	08.0	50	44	60	51	ENE 3	SE 4	SE 4	
27	744.4	748.2	748.7	14.3	18.0	13.6	14.9	18.9	13.6	-	09.4	09.1	10.0	77	59	85	74	SE 3	SE 4	NW 2	
28	749.1	750.0	750.1	13.2	17.8	14.2	14.8	18.5	12.7	-	10.4	10.0	10.3	91	65	84	80	ENE 1	SW 3	W 1	
29	751.3	751.5	751.7	11.9	17.3	15.4	15.0	19.2	11.3	-	08.6	09.7	06.6	82	66	65	71	ENE 1	WSW 2	ESE 2	
30	752.3	751.9	752.2	15.0	17.4	14.6	15.4	18.4	14.0	-	08.3	08.4	08.0	65	56	65	62	SE 3	NNW 1	N 1	
31	751.3	749.9	749.9	12.6	15.9	13.1	13.7	16.8	11.4	-	07.9	07.9	09.4	72	58	83	71	E 1	SW 1	N 1	
MES.	WRED. 749.9 749.8 750.0			09.9	14.4	11.4	11.8	15.2	09.0	-	06.0	06.8	06.6	64	56	65	62	3.0	3.1	2.4	

1974 APRIL

SPLIT MARJAN

1	747.7	747.4	748.5	12.9	17.9	14.1	14.6	18.3	10.4	-	08.6	08.8	08.8	77	57	73	69	N 1	WSW 3	ENE 2
2	749.0	750.4	751.8	12.8	18.7	14.2	15.0	19.0	12.4	-	06.9	08.0	06.0	62	50	49	54	ENE 1	WSW 2	ENE 3
3	752.9	752.2	752.1	12.3	17.7	12.6	13.8	18.6	11.4	-	07.0	08.2	07.8	65	54	71	63	NNE 2	WSW 3	ENE 2
4	751.2	749.9	749.3	11.6	16.5	13.2	14.2	18.7	11.0	-	06.5	09.0	07.0	63	56	61	60	NNE 1	SW 2	NW 2
5	748.5	748.4	750.5	12.6	14.9	12.8	13.3	16.5	11.2	-	08.2	08.1	07.7	75	64	69	69	SE 3	SSE 5	ESE 3
6	747.9	747.2	748.5	13.7	19.9	15.3	16.0	20.5	11.9	-	03.9	03.8	03.4	33	22	26	27	NE 3	NNE 2	NE 4
7	750.2	749.1	749.4	13.6	18.8	14.8	15.5	20.4	12.7	-	03.7	04.9	04.1	32	30	33	32	NE 4	WSW 3	NE 4
8	749.1	748.7	749.5	13.2	17.4	13.9	14.6	18.0	12.5	-	05.4	05.0	04.3	48	33	39	39	NNE 2	NNE 2	NNE 4
9	751.2	750.6	750.7	12.0	18.3	14.1	14.6	18.7	10.7	-	04.1	05.0	07.0	39	31	58	43	WSW 1	WSW 3	N 2
10	750.5	748.8	747.3	12.5	16.3	13.1	13.8	16.7	09.9	-	04.9	06.5	06.6	45	47	58	50	NE 2	SE 4	SE 4
11	743.1	741.9	742.0	11.0	11.5	11.6	11.4	14.3	10.2	-	07.4	08.9	08.3	75	86	81	81	ESE 6	ESE 7	SE 5
12	740.8	741.2	741.7	11.4	12.6	13.4	12.7	13.8	11.0	-	09.5	10.0	10.5	94	91	91	92	SE 5	SE 4	ESE 5
13	743.4	744.2	743.4	13.7	15.2	13.2	13.8	16.8	12.1	-	08.4	09.0	09.2	71	70	81	74	ESE 4	SSE 4	ESE 1
14	739.2	736.4	737.0	15.0	13.6	11.8	13.0	16.5	11.5	-	08.2	08.5	05.5	64	73	53	63	SE 3	NE 6	NNE 5
15	738.0	738.9	740.5	10.6	14.8	09.1	10.9	15.0	08.4	-	03.7	03.9	05.7	39	31	65	45	NE 6	NE 4	NE 3
16	740.9	741.2	741.2	09.1	15.0	09.4	10.7	15.5	08.3	-	03.1	04.3	04.2	36	34	47	39	ENE 4	SSW 2	

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Intenzacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	05	050	09	06.3	07.3	.	.	.	• 14° n, T° 7° 05° 7° 4°, F ESE 9° 8° 18° 12°
2	7	10	100	100	10.0	00.0	02.6	.	.	• 18° 10° 14° 20°
3	7	10	10	10	10.0	00.2	34.5	.	.	F - FSE-SSE 0° 24°, 0° 14° 20°
4	6	10	100	100	10.0	00.0	03.5	.	.	FSE 0-12, 0-26° n
5	8	10	10	100	10.0	00.5	12.4	.	.	
6	6	10	10	07	06.0	00.3	16.1	.	.	• tr-16° 11° 20° i, F ESE 8° 19°
7	8	09	09	07	08.3	06.3	00.2	.	.	
8	8	08	09	09	08.7	05.3	.	.	.	
9	8	040	07	09	06.7	05.3	.	.	.	
10	8	010	030	00	01.3	09.5	.	.	.	
11	8	000	000	00	00.0	05.5	.	.	.	
12	8	010	000	00	00.3	10.1	.	.	.	
13	8	000	000	00	00.0	10.1	.	.	.	
14	8	040	050	04	04.3	05.5	.	.	.	
15	8	080	08	03	06.3	09.4	.	.	.	
16	7	030	040	00	02.3	08.6	.	.	.	= 6° 12°
17	8	000	030	05	02.7	09.4	.	.	.	
18	7	020	020	07	03.7	09.9	.	.	.	FSE-SSE 6° 24°
19	7	060	050	00	04.0	05.7	.	.	.	FSE-SSE 0-10° 35°
20	8	06	08	00	04.7	09.7	.	.	.	
21	8	010	000	00	00.3	11.0	.	.	.	Δ' n-9
22	8	000	020	09	03.7	07.7	.	.	.	Δ' n-9, = 15° 12°
23	8	10	070	00	05.7	05.7	.	.	.	Δ' n-12° 19° n; Δ' n-18° 15°
24	7	030	070	00	03.3	09.2	.	.	.	Δ' n-8° 11° 6° 11°
25	7	09	10	00	06.3	04.7	.	.	.	
26	8	000	08	00	02.7	06.7	.	.	.	
27	7	040	050	02	03.7	08.9	.	.	.	= n-n, Δ' n-9
28	6	030	030	00	02.0	08.2	.	.	.	= 1° n-18° 25°
29	6	010	08	07	05.3	05.7	.	.	.	Δ' 0-17° 10° 17° 35°, 23° 24°
30	7	10	10	10	10.0	00.2	.	.	.	• 0-10° 12° 11° 10° 17° 5° ni
31	7	10	080	100	09.3	00.7	01.0	.	.	
MES.		VRED.					70.7			

## SPLIT MARJAN

1974 APRIL

1	6	070	06	07	06.7	04.6	00.9	-	-	= 8-12°
2	7	10	050	05	06.7	03.4	00.0	.	.	• 0-16° 17°
3	8	000	010	00	00.3	10.5	00.0	.	.	
4	7	06	06	00	04.0	07.6	.	.	.	= n-12°
5	7	04	09	10	07.7	02.8	.	.	.	
6	8	070	050	00	04.0	09.1	.	.	.	
7	8	000	070	00	02.3	08.2	.	.	.	
8	8	060	09	00	05.0	06.0	.	.	.	
9	8	000	010	00	00.3	11.0	.	.	.	
10	8	040	080	08	06.7	06.0	.	.	.	
11	7	10	10	10	10.0	00.0	00.4	.	.	• 0-17° 30°
12	6	10	10	10	10.0	00.3	04.8	.	.	• 0-14° 12°
13	7	030	10	10	07.7	03.5	03.5	.	.	• 0-14° 15°
14	6	09	10	09	09.3	01.2	00.4	.	.	• 0-10° 20° 10° 30° 13° 45° T° 10° 45° 11° 10°, FNE 12° 24°
15	8	050	09	10	08.0	03.6	00.3	.	.	FNE 0-12°
16	8	040	10	09	07.7	06.1	00.1	.	.	• 0-15° 20° 15° 30° FNE 17° 15° 24°
17	6	10	10	10	10.0	00.0	00.2	.	.	FNE-ENE 0-24°, • 11° 25° 19° 25°
18	8	10	050	00	05.0	08.0	00.2	.	.	FNE-ENE 0-23°
19	8	020	09	06	05.7	06.1	.	.	.	
20	8	000	010	00	00.3	12.0	.	.	.	
21	8	000	060	09	05.0	09.4	.	.	.	• 12° 12° 12°
22	8	040	090	04	05.7	07.2	.	.	.	• 0-11° 12° 20° 20° n
23	8	010	020	00	01.0	12.4	00.0	.	.	• 0-15° 19°
24	7	08	09	10	09.0	04.9	.	.	.	
25	7	10	10	06	08.7	00.0	01.7	.	.	
26	8	10	040	10	08.0	07.7	01.4	.	.	• 2-27° 30° 10° 35° 18° 9° 0° 10° 50° 8° 2° 9° 9° 9° 2°
27	8	030	10	10	07.7	04.1	08.0	.	.	FSE 16° 24°
28	8	050	10	10	08.3	03.2	.	.	.	F-FSE 0-23°
29	8	060	060	01	04.3	10.3	00.0	.	.	• 0-13° 13°
30	6	080	100	100	09.3	00.0	.	.	.	• 0-19° n
MES.		VRED.					21.5			

1974 MAJ

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$ , N  $\lambda = 16^{\circ}26'$ , E Gr.,  $\Delta G = +1h\ 06\ min.$ 

BR. ST. 89

DOF	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u%			Pravac i jačina vjetra D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	731.6	733.3	735.8	11.1	16.5	12.2	13.5	17.0	09.9	-	09.1	04.0	09.0	92	64	79	78	ESE 5	SSW 2	E 1
2	739.2	741.3	742.9	14.7	17.5	14.2	15.2	18.4	12.1	-	07.4	08.6	09.9	59	57	82	66	NNE 3	NW 2	SSW 1
3	745.1	746.2	745.8	13.4	16.8	13.8	14.4	18.0	12.7	-	10.5	10.8	10.1	91	76	85	84	S 1	SSW 3	SSE 5
4	741.3	742.0	742.7	13.2	14.3	13.2	13.5	16.6	12.5	-	09.6	09.5	06.2	84	78	54	72	SE 7	SSE 5	NNE 1
5	742.5	742.3	743.6	13.4	18.4	13.6	14.8	19.0	12.1	-	09.1	08.5	08.8	79	54	75	69	NNE 3	SW 3	SE 3
6	743.7	745.5	747.3	12.8	18.1	14.2	14.8	18.5	09.3	-	09.6	05.8	09.2	87	63	76	75	ESE 3	SSW 3	SE 3
7	749.1	750.1	751.2	13.2	15.0	14.1	14.1	17.9	11.4	-	08.1	08.6	09.2	71	69	76	72	ENE 2	ENF 2	SE 4
8	751.1	750.2	748.6	13.7	18.3	13.9	15.0	18.5	12.3	-	08.5	09.8	07.3	72	62	61	65	E 2	SSW 1	ENE 3
9	747.1	747.4	747.9	14.0	15.5	14.6	14.7	18.2	12.6	-	06.4	06.7	05.3	54	51	42	49	ENE 3	NW 2	NE 3
10	748.9	748.5	749.3	13.8	18.6	16.2	16.2	20.0	11.9	-	04.8	06.4	06.6	41	40	47	43	ENE 3	WSW 4	ENE 1
11	750.3	750.6	750.1	14.8	21.1	17.2	17.6	21.5	12.3	-	07.5	08.2	06.5	55	44	44	49	ESE 1	SSW 2	SE 5
12	751.1	751.6	752.8	16.8	21.7	16.6	17.9	22.4	15.6	-	08.6	10.0	09.7	60	51	68	60	SSE 5	WSW 2	SSE 2
13	754.2	754.5	754.6	17.0	21.0	19.1	19.0	22.6	13.7	-	08.3	10.7	08.4	57	58	51	55	E 1	WSW 3	WWN 1
14	753.9	753.0	751.4	17.3	22.8	18.6	19.3	23.3	15.4	-	10.3	10.2	08.4	70	49	52	57	E 1	SW 2	NW 1
15	749.5	748.7	747.7	15.4	16.8	15.0	15.6	19.2	11.0	-	07.4	10.3	06.7	57	72	52	60	NE 3	SSW 2	NNE 3
16	747.5	747.7	748.6	14.8	20.4	15.6	16.6	20.6	11.6	-	06.1	07.5	06.6	49	42	65	52	NNE 1	SW 3	ESE 1
17	749.6	750.7	751.7	15.8	20.0	15.8	16.8	20.1	13.5	-	09.3	08.7	08.4	69	50	62	60	ESE 1	SE 2	ESE 2
18	752.7	752.6	752.1	16.2	21.4	18.6	18.7	22.5	13.6	-	06.8	08.7	07.7	49	45	48	47	N 1	SW 1	NNE 5
19	751.7	750.5	751.4	18.5	23.2	19.4	20.1	23.7	16.6	-	08.2	08.7	07.7	52	41	45	46	NNE 2	NNF 5	ESE 3
20	751.6	750.4	749.9	20.2	26.1	21.0	22.1	26.2	18.2	-	08.1	08.9	09.0	40	35	48	43	NE 4	W 2	N 2
21	750.5	751.0	751.0	19.6	26.1	22.4	22.6	27.0	18.3	-	09.4	09.8	07.0	55	39	35	43	SSE 2	WSW 1	NNE 4
22	750.6	747.5	743.1	18.9	24.9	20.4	21.2	26.5	16.0	-	08.2	09.7	07.5	50	41	42	44	ENE 2	SW 2	ESE 3
23	742.7	742.6	742.1	15.6	22.2	17.3	18.1	23.4	11.0	-	08.0	07.4	09.1	60	37	61	53	NNW 2	W 3	WSW 2
24	742.3	742.3	742.8	17.2	17.9	17.4	17.5	20.0	14.6	-	10.3	09.9	11.6	70	64	78	71	SSE 5	SE 5	SE 5
25	747.1	749.1	750.9	17.3	22.3	17.2	18.5	23.0	15.0	-	09.0	06.7	07.7	60	32	52	48	-	0	NNW 2
MES.																				
WRED.	747.8	748.0	748.1	16.0	20.4	17.0	17.6	21.6	13.7	-	08.7	09.6	08.7	64	54	60	59	2.1	2.5	2.5

1974 JUN

SPLIT MARJAN

1	749.2	749.1	750.5	19.3	23.6	15.6	20.5	24.4	18.6	-	12.5	11.0	12.7	75	50	74	66	ESE 5	SE 4	NNW 1	
2	751.7	753.4	754.2	20.1	21.2	20.0	20.3	21.5	18.4	-	08.8	08.6	07.7	50	46	44	47	NE 5	NE 6	NNE 5	
3	754.4	753.4	753.3	18.9	25.4	21.9	22.0	26.0	18.2	-	07.3	06.9	08.0	45	28	41	38	NNE 4	NNF 1	NE 4	
4	753.6	753.3	752.2	21.0	27.0	20.0	22.0	27.2	18.5	-	09.0	11.0	13.8	48	41	78	56	NF 1	SSW 2	SSE 1	
5	752.2	751.8	750.7	21.1	27.4	23.1	23.7	28.5	18.2	-	11.8	12.0	11.6	63	44	55	54	ENE 1	SW 2	NNW 1	
6	748.7	749.0	748.0	21.7	24.4	22.0	22.5	24.7	18.0	-	12.2	11.6	10.2	63	50	52	55	ESE 1	SE 5	SE 3	
7	748.4	749.0	749.4	18.4	24.1	19.8	20.5	25.2	17.6	-	13.8	13.9	10.9	87	62	63	71	N 2	SW 1	NNE 2	
8	751.9	751.5	750.1	18.6	25.8	21.4	21.8	26.5	16.3	-	05.8	07.0	09.1	36	28	47	37	NF 3	SSW 2	NW 1	
9	748.5	746.7	745.8	17.2	23.5	20.9	20.6	24.2	16.8	-	11.3	09.9	10.4	77	46	56	60	ESE 4	SE 5	ESE 3	
10	745.3	744.9	742.2	19.8	22.7	19.9	20.6	23.2	19.0	-	13.4	12.0	13.9	77	58	80	72	SE 6	S 3	SE 6	
11	743.6	745.2	748.6	14.1	18.3	16.7	16.4	20.3	12.3	-	10.1	06.0	07.6	83	38	53	58	NNW 1	NNE 5	NNW 3	
12	747.6	745.5	745.3	17.0	21.7	14.5	17.1	22.3	14.3	-	04.9	09.3	06.2	33	48	49	43	ENE 3	WSW 4	NF 3	
13	744.2	744.2	745.1	16.2	21.8	16.7	17.8	23.0	13.1	-	05.6	07.0	08.1	40	36	56	44	NE 2	SSW 2	NNW 2	
14	746.7	748.1	749.1	17.0	21.5	18.0	18.6	22.3	13.9	-	08.7	10.2	11.8	60	53	76	63	ESE 3	SSE 2	SE 1	
15	750.5	750.3	749.0	17.3	22.5	17.0	18.4	23.0	14.6	-	09.6	09.2	13.0	65	45	89	66	ENE 3	ESE 2	SE 4	
16	748.6	747.8	747.8	17.2	22.8	19.0	19.5	23.7	15.5	-	12.0	11.6	12.4	81	56	75	71	ENE 1	SSE 1	W 1	
17	747.3	746.9	747.6	19.5	25.6	20.2	21.4	26.0	17.1	-	13.1	13.5	15.1	77	55	85	72	SSE 1	SW 3	ESE 1	
18	748.0	747.8	748.2	20.3	26.3	20.8	22.0	27.0	17.1	-	14.0	10.9	13.6	79	42	74	65	SSE 1	SSW 1	NN 1	
19	748.9	748.6	749.7	20.2	26.0	22.4	22.8	27.4													

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insekticija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	100	07	05	07.3	02.4	21.5	.	• 0-16 <sup>30</sup> 9 <sup>6</sup> 15 <sup>50</sup> 16 <sup>40</sup>	
2	8	100	10	09	06.7	00.0	05.5	.	• 0-16 <sup>40</sup> 7 <sup>45</sup>	
3	7	100	10	08	09.3	C3.7	CC.0	.	• 16 <sup>35</sup> 7 <sup>40</sup>	
4	8	10	05	04	07.7	02.2	00.7	.	FSE 6-16 <sup>45</sup> , • 0-17, 6 <sup>35</sup> 9 <sup>50</sup> ; T <sup>15</sup> 17 <sup>12</sup> i	
5	8	09	040	05	06.0	11.1	01.3	.		
6	8	100	060	05	07.0	08.0	00.4	.	• 0-2 7-8 <sup>40</sup> R <sup>1</sup> 7 <sup>20</sup> 7 <sup>40</sup> 7 <sup>2</sup> 7 <sup>40</sup> 8 <sup>20</sup>	
7	8	08	09	08	08.3	04.9	10.2	.	• 0-12 <sup>20</sup> 12 <sup>40</sup> T <sup>1</sup> 13 <sup>40</sup> 14 <sup>35</sup>	
8	8	09	09	06	09.0	00.0	00.2	.	T <sup>1</sup> 10 <sup>55</sup> 10 <sup>55</sup> 10 <sup>25</sup> 14 <sup>30</sup>	
9	8	10	10	09	09.7	C3.4	.	.	• 0-12 <sup>50</sup> 13 <sup>45</sup>	
10	8	000	010	00	00.3	12.6	00.0	.		
11	8	05	C10	02	C3.7	11.2	.	.	= n-8	
12	8	09	030	00	04.0	10.0	00.2	.	✓ n 7 <sup>30</sup> 7 <sup>50</sup> T <sup>1</sup> 7 <sup>30</sup> 7 <sup>35</sup>	
13	8	000	030	01	C1.3	12.6	CC.1	.	= n-7 <sup>50</sup> △ n-8 <sup>30</sup>	
14	8	060	030	07	C5.3	09.3	.	.	= n-9 <sup>30</sup>	
15	8	10	05	01	06.3	06.0	.	.	• 0-18 <sup>20</sup> 11 <sup>20</sup> 14 <sup>40</sup> 14 <sup>20</sup>	
16	8	010	050	10	05.3	13.3	03.6	.	✓ 19 <sup>40</sup> 20 <sup>40</sup> i	
17	8	080	09	08	08.3	05.5	.	.		
18	8	040	06	01	C3.7	08.4	00.0	.		
19	8	070	C30	01	03.7	11.2	.	.		
20	8	000	020	C2	C1.3	13.2	.	.		
21	8	060	090	00	C5.0	10.1	.	.	FNE 23 <sup>35</sup> 24	
22	7	10	050	03	06.0	06.4	.	.	FNE 0-5 <sup>45</sup> T <sup>1</sup> n, • 14 <sup>10</sup> 4 <sup>30</sup>	
23	9	C20	030	10	C5.0	09.1	00.4	.		
24	8	060	10	09	C8.3	C5.7	.	.	• 14 <sup>50</sup> 5 <sup>00</sup>	
25	9	09	09	03	07.0	09.5	00.1	.		
26	8	050	010	00	02.0	13.4	.	.		
27	8	000	020	02	01.2	13.2	.	.		
28	8	030	09	09	R	C7.0	09.7	.	• 0-2 20 <sup>20</sup> 24i, R <sup>1</sup> 20 <sup>25</sup> n, ✓ 12 <sup>30</sup> 23 <sup>45</sup>	
29	7	10	090	05	08.0	04.2	12.0	.	• 0-0 <sup>30</sup> 12 <sup>55</sup> 15 <sup>40</sup> i	
30	8	010	09	09	C6.3	C9.4	C1.7	.		
31	8	09	10	03	07.3	02.2	00.0	.	• 15 <sup>50</sup> 6 <sup>15</sup>	
MES. VRED.		06.4	06.2	04.8	05.8	241.8	67.5			

1	8	090	08	05	C7.3	C6.6	CC.9	.	Tn, • 0-12 <sup>30</sup> 2 <sup>50</sup> 6 <sup>30</sup> 7 <sup>05</sup>	
2	8	040	060	00	02.3	11.6	00.1	.	FNE-NNE 6 <sup>05</sup> -24	
3	8	030	010	00	C1.3	13.3	.	.	FNE NNE 0-12	
4	8	000	000	00	00.0	14.1	.	.		
5	8	000	010	00	00.3	13.3	.	.		
6	8	060	09	09	08.0	06.0	C1.9	.	Tn, • 0-13 <sup>20</sup> 4 <sup>20</sup> 23 <sup>50</sup> 24; FSE 10 <sup>45</sup> 14 <sup>22</sup> i	
7	7	09	040	03	C5.3	09.2	C2.5	.	• 0-6 <sup>20</sup> i	
8	8	010	060	02	03.0	08.0	.	.	• 0-3 <sup>52</sup> 7 <sup>40</sup> i, FSE 21 <sup>30</sup> 24	
9	8	10	060	02	06.0	13.1	00.9	.	FSE 0-Mi, 16-22; • 17 <sup>40</sup> 19 <sup>30</sup>	
10	8	09	08	10	09.0	C5.2	CC.0	.		
11	8	100	040	00	04.7	10.6	C6.3	.	• 17 <sup>30</sup> 7 <sup>10</sup> FNE 13 <sup>10</sup> 16 <sup>33</sup>	
12	8	000	060	06	04.0	10.5	00.0	.	• 17 <sup>45</sup> 17 <sup>00</sup>	
13	8	030	050	01	03.0	14.1	00.0	.		
14	8	10	05	01	C5.3	08.2	.	.	R <sup>1</sup> 19 <sup>45</sup> 11 <sup>55</sup> i, • 1-2 10 <sup>10</sup> 10 <sup>50</sup>	
15	8	050	10	10	08.3	08.0	06.8	.	• 11 <sup>45</sup> 11 <sup>15</sup> i	
16	8	10	09	07	08.7	C1.6	10.5	.	• 0-17	
17	7	000	010	00	00.3	13.7	.	.	△ n <sub>1</sub> = 6 <sup>30</sup> 13 <sup>30</sup>	
18	8	000	060	10	C5.3	11.5	.	.		
19	8	09	040	03	05.3	10.7	.	.		
20	8	030	060	C1	C3.3	11.6	.	.		
21	7	000	050	00	C1.7	10.6	.	.	= n-9 <sup>30</sup>	
22	7	070	030	08	C6.0	C9.5	.	.		
23	7	000	10	10	06.7	06.6	.	.	= n-9 <sup>30</sup> , • 19 <sup>30</sup> 20 <sup>10</sup>	
24	7	09	040	10	C7.7	C8.4	.	.		
25	8	000	050	03	02.7	13.4	00.0	.		
26	8	090	060	00	C5.0	11.0	.	.	F-ESE 3 <sup>50</sup> 17 <sup>30</sup>	
27	8	060	10	04	06.7	05.2	.	.	• 17-2 14 <sup>30</sup> 19 <sup>55</sup> i	
28	8	030	10	10	07.7	06.2	CC.9	.	• 17-2 14 <sup>30</sup> 19 <sup>55</sup> i, V <sup>1</sup> 18 <sup>15</sup> 19 <sup>04</sup> i, T <sup>1</sup> 18 <sup>51</sup> 19 <sup>40</sup>	
29	7	09	10	09	09.3	01.0	.	.		
30	8	08	060	00	04.7	10.3	21.9	.		
MES. VRED.		05.1	05.8	04.1	05.0	284.8	52.7			

$\varphi = 43^{\circ}31'$  N  $\lambda = 16^{\circ}26'$  E Cr.  $\Delta G = +1h\ 06\ min.$ 

BR. ST. 89

D d	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.2	750.7	750.9	22.6	26.8	24.0	24.4	28.2	20.0	-	09.5	02.1	10.8	46	12	48	35	NNE	2	SW	2
2	752.0	751.9	751.6	23.1	30.2	26.4	26.5	31.0	20.5	-	11.3	13.1	09.8	53	41	38	44	NE	1	SW	2
3	751.7	750.2	747.5	24.6	29.3	24.7	25.8	30.2	22.0	-	11.0	13.2	14.7	47	43	63	51	ESE	1	SSW	3
4	747.6	747.7	747.7	24.3	30.2	25.8	26.6	30.7	22.6	-	12.8	13.1	12.3	55	41	49	48	NNW	1	SW	2
5	749.6	750.3	750.5	24.7	29.7	26.2	26.7	30.5	22.0	-	12.9	14.0	14.0	55	45	55	52	ESE	1	SW	3
6	750.7	750.4	748.8	25.0	30.0	25.3	26.4	31.0	22.9	-	15.4	17.9	14.0	65	56	58	60	-	0	SSW	2
7	747.0	747.4	749.7	24.4	19.6	19.9	21.0	27.7	19.0	-	14.9	10.8	06.8	65	63	39	56	ENF	1	NE	6
8	751.9	751.2	752.9	18.6	23.5	20.2	20.6	23.8	17.9	-	06.5	06.5	05.9	40	30	33	34	NE	4	NE	4
9	754.3	753.3	752.4	19.8	24.5	22.3	22.2	26.5	16.6	-	07.3	07.1	09.9	42	40	49	44	NE	3	NNW	4
10	751.0	751.3	751.3	21.2	29.0	23.0	23.8	28.4	19.4	-	13.6	10.8	11.4	77	38	54	55	ESE	1	SW	2
11	750.7	750.7	750.8	23.5	29.3	24.6	25.5	29.6	20.2	-	12.1	11.2	12.8	56	37	55	49	SSE	1	SW	2
12	752.5	752.9	752.4	23.4	30.2	25.5	26.2	31.4	20.4	-	11.8	17.9	12.0	44	40	51	48	NNE	2	SSW	2
13	750.1	750.9	749.9	25.4	31.4	27.6	28.0	31.8	22.6	-	12.7	13.0	12.0	52	38	43	44	ENF	2	SW	3
14	749.8	749.8	750.2	27.6	31.3	27.7	28.6	31.9	25.4	-	10.4	10.6	11.7	37	31	42	37	SF	3	SF	1
15	751.2	751.9	751.3	27.5	34.0	28.8	29.8	34.6	24.6	-	11.6	10.5	12.5	42	26	42	37	NE	2	SW	2
16	750.4	749.9	749.7	28.0	35.3	26.3	31.0	35.8	26.0	-	11.7	10.5	12.2	41	25	38	35	ENE	2	WSW	2
17	747.1	746.2	745.1	27.9	34.3	29.0	30.0	35.3	25.8	-	12.0	13.5	12.4	43	33	41	39	ENF	2	SE	2
18	744.1	745.0	745.2	26.7	31.8	26.4	27.8	32.0	25.6	-	17.1	15.1	12.0	65	43	47	52	SE	3	SW	3
19	743.6	743.7	745.9	24.7	24.3	15.6	20.0	27.2	14.6	-	12.1	12.9	12.0	52	57	90	66	NE	3	ESF	5
20	745.1	746.1	746.0	19.3	21.0	18.8	19.2	21.7	15.0	-	07.5	07.2	06.5	47	39	40	42	NE	6	NE	5
21	746.1	746.8	747.7	18.5	20.7	19.8	19.7	22.6	17.4	-	06.7	07.0	07.5	42	38	43	41	NE	5	NNE	5
22	749.3	749.8	750.0	19.6	23.1	20.2	20.8	24.0	17.9	-	07.0	06.6	06.9	41	31	39	37	NNE	3	NE	3
23	750.1	751.0	751.2	19.5	21.0	21.2	21.0	24.6	18.4	-	06.6	08.6	12.2	51	43	64	53	NNW	1	NNW	2
24	752.1	752.0	751.1	21.3	27.2	22.0	23.1	27.7	18.9	-	11.3	12.9	12.3	59	47	62	56	NNF	1	SSW	2
25	750.1	749.5	749.4	22.2	26.1	23.7	23.9	26.6	20.2	-	11.9	13.2	13.5	59	52	62	58	SE	4	SF	2
26	750.1	750.6	751.4	22.3	29.1	23.8	24.8	29.7	21.0	-	10.2	11.7	10.3	51	39	47	46	NE	4	WSW	3
27	752.2	752.1	752.0	22.1	26.2	22.6	23.9	28.5	19.3	-	09.5	10.4	15.5	48	36	75	53	ENF	1	SW	3
28	752.5	752.1	752.4	22.6	29.3	27.2	26.7	32.1	20.0	-	09.7	13.1	11.0	47	42	41	43	NE	2	ESF	1
29	753.0	752.7	752.5	25.9	32.4	26.5	28.8	33.2	24.0	-	12.6	13.0	12.8	50	36	44	43	NE	1	WSW	3
30	751.8	750.7	749.8	26.8	32.7	27.1	28.4	32.8	25.0	-	13.4	13.6	12.3	51	37	46	45	ENE	2	WSW	3
31	749.3	748.8	748.3	26.0	31.7	29.3	29.1	32.3	23.2	-	11.5	14.5	11.0	46	41	36	41	ENF	1	SSW	2
MES.	VRED.	751.0	750.0	749.9	23.5	28.3	24.4	25.2	29.5	20.9	-	11.2	11.4	11.3	51	39	49	46	2.1	3.0	2.0

1974 AVGUST

SPLIT MARJAN

1	743.5	748.6	748.6	27.1	32.0	29.7	33.6	24.6	-	14.3	17.5	12.6	53	49	40	47	ESE	1	SSW	2	NNW	1	
2	748.9	749.1	749.0	27.8	32.8	26.8	29.6	33.4	26.1	-	13.3	18.7	14.8	48	50	50	49	SE	1	SW	2	ESE	1
3	749.7	750.2	750.2	27.2	34.4	30.8	35.2	25.0	-	15.4	15.2	11.8	57	37	35	43	NE	1	SW	3	NNW	2	
4	751.0	751.1	750.5	28.4	34.2	30.7	31.0	34.8	26.3	-	14.5	15.7	12.4	50	39	37	42	ENE	1	SW	1	WNW	1
5	751.2	750.5	750.2	28.2	35.3	30.7	31.2	35.7	26.4	-	10.1	10.5	10.0	35	25	30	30	FNE	2	SW	3	NNF	1
6	750.0	749.9	750.4	29.2	34.4	24.6	28.2	36.1	24.4	-	08.9	12.1	09.9	29	30	43	34	NE	3	NE	4	NE	4
7	750.2	749.2	748.2	23.7	29.7	25.4	26.0	31.3	22.3	-	07.5	12.4	15.3	34	40	63	46	ENF	5	SW	2	E	1
8	747.4	746.1	745.8	24.8	30.3	25.2	26.4	31.0	22.6	-	13.3	14.5	14.3	57	45	59	54	ESE	1	SSW	3	SSW	5
9	744.5	745.0	746.9	24.8	29.3	24.8	25.9	30.6	23.0	-	14.4	15.3	12.8	61	50	55	55	ESE	2	SSW	4	NNE	3
10	748.9	748.1	746.4	23.0	30.1	25.4	26.0	30.6	21.7	-	09.6	13.3	11.1	46	42	45	44	ENE	2	ESE	3	SE	2
11	742.4	743.9	746.8	22.0	21.9	16.5	20.2	28.3	17.9	-	11.2	13.2	07.6	56	67	48	57	NNE	2	SSE	2	NE	5
12	749.4	749.2	750.9	19.8	27.0	22.1	22.8	27.0	16.6	-	08.1	07.9	07.2	47	29	36	37	NNW	1	NNW	3	NNF	3
13	753.4	752.9	753.6	20.6	27.3	23.6	23.8	28.0	19.0	-	07.6	10.0	13.3	42	37	61	47	NNE	5	SSW	3	NNW	2
14	754.5	754.8	754.8	23.4	29.4	25.5	26.0	30.8	19.2	-	11.8	16.5	13.5	54	54	55	54	W	2	SW	2	SSE	1
15	755.5	755.4	754.8	26.1	33.6	30.1	30.0	33.6	23.6	-	09.1	10.3	12.3	36	26	39	34	NNE	1	SW	2		

SPLIT MARJAN

1974 JUL

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivali h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	010	010	00	00.7	14.1	.	.	.	.
2	9	000	030	00	01.0	14.4	.	.	.	.
3	8	000	020	03	01.7	14.0	.	.	.	.
4	8	000	010	05	02.0	13.8	.	.	.	.
5	8	030	020	00	01.7	13.5	.	.	.	.
6	8	04	020	00	02.0	13.3	.	.	.	.
7	8	09	10	00	06.3	08.1	.	.	.	.
8	8	040	06	00	02.3	10.6	00.0	.	.	.
9	8	000	08	03	02.7	13.0	.	.	.	.
10	8	09	08	05	07.3	09.7	.	.	.	.
11	7	10	030	03	05.3	10.0	.	.	.	.
12	8	000	000	00	00.0	13.5	.	.	.	.
13	8	000	000	00	00.0	13.7	.	.	.	.
14	8	000	000	00	00.0	13.6	.	.	.	.
15	8	000	000	02	00.7	13.0	.	.	.	.
16	8	000	020	02	01.3	11.0	.	.	.	.
17	8	090	010	00	03.3	11.7	.	.	.	.
18	8	010	050	00	02.0	11.8	.	.	.	.
19	8	050	09	100	08.0	05.5	.	.	.	.
20	8	09	07	00	05.3	08.7	17.5	.	.	.
21	8	10	08	04	07.3	05.2	.	.	.	.
22	8	06	08	06	06.7	07.9	.	.	.	.
23	8	10	10	07	09.0	02.5	.	.	.	.
24	8	010	020	03	02.0	12.0	.	.	.	.
25	7	010	000	10	03.7	12.4	.	.	.	.
26	8	020	050	00	02.3	12.8	.	.	.	.
27	8	000	000	00	00.0	13.7	.	.	.	.
28	8	000	010	01	00.7	13.7	.	.	.	.
29	8	000	020	00	00.7	13.3	.	.	.	.
30	7	000	020	00	00.7	13.2	.	.	.	.
31	8	000	010	00	00.3	13.2	.	.	.	.
MES.	VRED.	03.0	03.5	02.1	02.9	356.5	17.5			

SPLIT MARJAN

1974 AUGUST

1	7	000	050	00	01.7	12.8	.	.	T 15 <sup>30</sup> 15 <sup>30</sup>	
2	7	000	010	00	00.3	12.5	.	.	= n-9 <sup>30</sup>	.
3	7	000	030	00	01.0	12.8	.	.		.
4	7	000	010	00	00.3	12.4	.	.		.
5	8	000	000	00	00.0	12.9	.	.		.
6	8	000	050	00	01.7	12.5	.	.	E NE 20 <sup>40</sup> 24	
7	8	000	000	00	00.0	12.9	.	.	E NE 0 <sup>0</sup> 6 <sup>40</sup>	
8	8	000	000	100	03.3	10.1	.	.	T 20 <sup>12</sup> 21 <sup>45</sup> • 20 <sup>46</sup> 22 <sup>15</sup>	
9	8	000	080	00	02.7	11.3	00.0	.		.
10	8	010	060	06	04.3	12.5	.	.		.
11	9	080	08	00	05.3	07.2	.	.	• 7 <sup>03</sup> 12 <sup>35</sup> , T 8 <sup>30</sup> 8 <sup>45</sup> , 11 <sup>35</sup> , 11 <sup>55</sup> , 11 <sup>22</sup> , 11 <sup>25</sup>	
12	9	000	030	00	01.0	11.8	05.2	.		.
13	8	040	080	00	04.0	12.2	.	.		.
14	8	000	000	00	00.0	12.9	.	.		.
15	8	000	000	00	00.0	12.6	.	.		.
16	8	010	010	00	00.7	12.4	.	.		.
17	7	000	000	00	00.0	12.5	.	.		.
18	7	000	000	00	00.0	12.4	.	.		.
19	7	000	000	00	00.0	11.6	.	.		.
20	7	000	040	00	01.3	11.3	.	.	= n-12, T 15-15 <sup>40</sup>	.
21	7	010	020	00	01.0	12.0	.	.	= 8-12	
22	8	000	050	06	03.7	11.3	.	.	• 2 <sup>40</sup> 22 <sup>10</sup> T 2 <sup>20</sup> 20 <sup>40</sup> n	
23	8	09	050	06	06.7	04.8	04.2	.	• T <sup>0</sup> -o-1 C <sup>38</sup> T <sup>22</sup> L <sup>15</sup> 20 <sup>18</sup> 40	
24	8	090	080	07	08.0	04.8	04.1	.	T <sup>1</sup> n-12 <sup>20</sup> , • 0-6 <sup>55</sup> 12 <sup>40</sup> , T <sup>1</sup> 19 <sup>30</sup> 11 <sup>10</sup>	
25	8	10	090	00	06.3	06.6	15.7	.		.
26	8	060	09	06	07.0	05.4	.	.	• 0-13 <sup>50</sup> 7 <sup>05</sup> 10 <sup>04</sup> 10 <sup>45</sup> 13 <sup>30</sup> , T <sup>1</sup> 19 <sup>10</sup> 19 <sup>30</sup>	
27	8	100	060	08	08.0	04.6	06.4	.	T <sup>0</sup> 10 <sup>40</sup> 13 <sup>60</sup> • 0-13 <sup>05</sup> 45 <sup>10</sup> i	
28	8	070	09	10	08.7	04.1	04.2	.	• T <sup>1</sup> 17 <sup>25</sup> 19, T <sup>0</sup> 17 <sup>44</sup> 18 <sup>25</sup>	
29	8	07	070	09	07.7	08.2	00.1	.		.
30	8	000	030	00	01.0	12.0	03.1	.		.
31	8	020	000	04	02.0	10.6	.	.		.
MES.	VRED.	02.4	03.7	02.3	02.8	324.0	25.0			

1974 SEPTEMBAR

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$ , N  $\lambda = 16^{\circ}26'$ , E Gr.  $\Delta G = +1h\ 06\ min.$ 

BR. ST. 89

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.0	750.4	749.8	21.8	26.8	23.9	24.1	27.3	20.7	-	12.7	13.8	12.5	65	52	56	58	ESE 3	ESE 4	ESE 3	
2	750.0	750.5	750.7	23.0	29.0	23.6	24.8	29.0	22.2	-	11.8	16.9	17.5	56	56	80	64	ENE 2	SSE. 3	SE 1	
3	750.9	750.5	750.1	22.8	27.2	24.5	24.6	27.8	22.2	-	15.8	17.2	15.3	76	64	66	69	E 2	SE 4	SE 3	
4	748.8	748.6	749.8	24.3	27.9	24.1	25.1	28.5	23.7	-	15.2	19.0	18.8	67	67	83	72	SE 4	SE 3	WNW 2	
5	751.7	751.2	750.3	21.0	27.8	23.7	24.0	28.3	20.0	-	09.8	11.5	10.6	52	41	48	47	NE 4	SW 2	WNW 2	
6	748.5	746.1	743.9	20.7	27.8	23.0	23.6	28.0	19.6	-	09.4	12.1	12.4	51	43	59	51	NE 2	SSE 2	SW 1	
7	741.5	742.2	744.6	18.4	22.8	15.8	20.2	24.3	16.9	-	12.7	13.8	09.3	80	66	54	67	NNE 2	SW 2	NE 4	
8	747.7	749.7	751.7	20.2	26.9	23.5	23.5	27.1	18.4	-	09.9	11.6	14.1	56	44	65	55	NE 4	SW 3	ENE 2	
9	753.7	754.1	753.7	21.2	28.0	23.6	24.1	28.7	20.2	-	10.6	12.8	14.2	56	45	65	55	NE 2	SW 1	NNW 1	
10	754.0	754.1	754.1	21.3	28.0	23.4	24.0	28.6	20.9	-	12.2	14.2	14.0	64	50	65	60	NE 2	SW 3	NE 2	
11	754.6	754.7	754.8	21.6	28.7	23.5	24.5	29.2	20.6	-	10.0	10.7	10.5	52	36	47	45	NE 5	SSW 2	NE 3	
12	754.9	755.0	755.0	21.0	27.8	23.9	24.2	28.0	20.3	-	09.9	12.4	12.2	53	44	55	51	NE 3	SW 2	NW 1	
13	754.7	754.2	753.9	20.7	28.0	22.0	23.2	28.4	19.6	-	11.7	13.1	10.9	64	46	55	55	NNW 1	SW 2	W 1	
14	753.7	753.3	752.7	19.6	26.1	21.5	22.2	26.5	16.4	-	10.4	12.5	13.6	61	49	71	60	ENE 1	SSW 3	NNW 1	
15	751.8	751.0	751.0	21.1	28.7	23.4	24.2	28.8	20.5	-	09.5	12.7	13.7	50	43	63	52	NE 1	SW 2	- 0	
16	751.6	751.7	752.5	23.1	28.5	24.5	25.2	29.5	22.3	-	10.2	12.5	12.5	48	43	54	48	NE 1	WSW 3	NNE 1	
17	753.4	753.2	753.4	21.6	28.2	23.0	24.0	28.6	20.7	-	10.2	12.2	14.6	52	42	69	54	NE 1	SSW 2	- 0	
18	753.5	753.3	753.1	20.8	27.4	22.8	23.4	27.6	20.2	-	12.1	15.6	17.8	65	57	85	69	NE 2	SSW 2	SSW 1	
19	753.2	752.0	750.8	20.2	26.6	22.1	22.8	27.4	19.5	-	13.4	16.2	15.7	75	62	79	72	NE 1	SW 2	SSE 3	
20	748.4	747.4	745.4	21.4	18.9	18.6	19.4	22.6	17.5	-	15.9	15.0	14.5	83	92	90	88	ESE 5	SW 3	ESE 4	
21	745.7	746.3	745.6	19.4	20.5	21.4	20.8	23.6	17.8	-	13.4	14.8	15.0	77	82	78	79	NNE 2	ESE 4	SE 5	
22	746.9	746.5	747.4	18.8	24.3	21.5	21.5	24.6	17.0	-	13.5	14.0	15.2	83	61	79	74	ENE 1	SW 2	ESE 2	
23	749.0	749.1	749.2	19.3	23.1	21.0	21.1	23.4	19.2	-	13.1	12.6	14.9	78	60	80	73	NNE 2	ESE 3	SE 3	
24	746.4	745.3	742.5	20.0	21.9	19.6	20.3	22.5	17.7	-	12.5	11.8	13.5	71	60	79	70	SSE 4	SSE 4	SSF 5	
25	739.1	740.1	739.6	16.0	16.4	15.2	15.7	19.7	14.4	-	11.2	11.0	09.2	82	79	71	77	NNW 3	SSW 1	INF 2	
MES.	VRED.	749.3	749.5	749.7	19.9	24.7	21.3	21.8	25.7	16.6	-	11.4	12.9	13.0	66	56	68	63	2.6	2.7	2.3

1974 OKTOBAR

SPLIT MARJAN

1	748.6	749.4	750.5	12.7	17.9	12.7	14.5	18.2	12.1	-	07.4	07.6	07.4	57	49	63	60	NNE 3	NNW 4	NNW 3
2	748.2	742.5	745.7	12.1	16.0	12.2	13.1	16.7	10.3	-	09.8	10.1	07.2	92	74	68	78	SE 3	SE 7	NW 1
3	751.9	754.0	753.7	09.1	16.0	13.6	13.1	16.1	07.9	-	05.8	07.2	08.1	66	53	69	63	NE 3	S 2	ESE 2
4	752.4	752.6	751.9	15.4	18.0	17.0	16.8	18.4	12.2	-	09.2	10.0	10.5	70	65	72	69	SE 6	ESE 5	FSE 4
5	749.3	748.2	745.9	15.5	18.9	18.8	18.0	19.5	14.4	-	11.4	12.3	11.4	86	75	70	77	ESE 5	ESE 5	SE 6
6	744.5	747.1	748.5	12.9	18.2	12.6	14.0	18.9	11.6	-	07.0	07.1	06.4	63	45	58	55	RNE 4	SW 2	NE 4
7	746.8	746.0	747.4	12.6	17.5	14.5	14.8	18.1	11.6	-	06.9	08.5	09.4	63	57	76	65	ENE 4	SSW 3	E 2
8	743.0	743.9	746.0	14.6	17.0	14.1	15.4	17.6	13.5	-	11.4	10.5	07.6	92	72	63	76	SSE 2	NE 1	NE 2
9	746.5	747.7	748.3	11.7	17.6	11.5	13.1	18.3	10.3	-	07.4	08.6	06.6	71	57	65	64	NF 3	SSW 1	SE 2
10	751.3	751.9	752.1	10.3	17.3	14.0	13.9	17.4	08.7	-	06.5	08.2	07.8	69	56	65	63	ENE 3	SSW 1	ENE 2
11	751.4	751.7	752.5	12.6	15.7	15.2	14.7	16.7	11.8	-	07.4	09.8	10.4	67	73	80	73	ENE 3	ESE 4	LSF 2
12	751.0	749.9	747.9	16.5	18.0	16.2	17.8	18.2	14.5	-	10.6	10.4	13.1	75	67	84	75	ESE 4	SE 5	SSE 4
13	746.4	746.8	746.8	16.1	17.0	14.8	15.7	18.3	14.6	-	13.2	13.4	12.1	96	92	96	95	ESE 3	ESE 2	E 2
14	746.2	747.3	747.4	13.2	13.3	13.0	13.1	15.0	12.0	-	09.2	09.2	08.8	81	80	79	80	NE 3	NNE 4	ENE 2
15	746.2	745.4	744.2	12.7	12.2	11.7	12.1	13.6	11.1	-	08.1	09.8	08.8	73	92	85	83	NE 3	NE 2	NE 2
16	748.1	749.7	752.0	09.6	14.5	09.2	10.6	15.3	08.0	-	07.7	07.3	06.7	86	59	77	74	WNW 3	SSE 2	NE 2
17	752.5	754.5	754.7	08.8	14.5	11.4	11.5	14.7	07.9	-	06.6	07.6	06.9	78	62	68	69	ENE 2	SW 1	NE 2
18	754.9	754.1	754.3	09.5	15.7	13.9	13.2	15.8	08.4	-	05.5	06.0	06.3	61	45	53	53	NE 4	WSW 2	NW 1
19	753.9	752.9	751.3	10.4	16.3	13.0	13.2	16.4	10.4	-	05.3	07.5	08.2	56	54	73	61	NE 3	SSE 1	NE 2
20	745.3	742.2	736.5	14.9	15.5	15.2	15.2	16.0	12.9	-	08.7	10.2	11.9	69	77	92	79	SSE 5	SSW 6	SSW 6
21	727.5	728.2	729.6	12.3	12.2	08.8	10.5	15.7	08.5	-	10.0	08.9	06.6	93	84	78	85	NW 2	SSW 2	NE 4
22	737.4	730.4	741.0	07.6	12.7	13.3	11.7	13.3	06.6	-	06.4	07.6	07.6	82	69	66	72	NNE 2	SW 4	SSW 5

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_1 = 6.5 \text{ m } h_T = 1.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblakost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrival h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnev				7	7
1	8 09	070	06	07.3	07.7	.	.	.	.	.	.
2	8 09	090	06	08.0	07.0	.	.	.	.	.	.
3	7 09	030	03	05.0	07.6	.	.	.	.	.	.
4	7 010	09	04	04.7	08.4	.	.	.	.	.	.
5	9 070	020	00	03.0	11.2	.	.	.	.	.	.
6	8 000	000	04	01.3	04.4	.	.	.	.	.	.
7	8 09	07	00	05.3	10.4	10.7	.	.	.	.	.
8	8 000	010	00	00.3	11.2	00.5	.	.	.	.	.
9	8 000	010	00	00.3	11.1	.	.	.	.	.	.
10	7 000	040	00	01.3	11.1	.	.	.	=7 <sup>30</sup> 9 <sup>05</sup>	.	.
11	8 060	000	00	02.0	10.1	.	.	.	.	.	.
12	8 000	000	00	00.0	10.9	.	.	.	.	.	.
13	8 000	000	00	00.0	11.2	.	.	.	.	.	.
14	7 000	000	00	00.0	10.8	.	.	.	.	.	.
15	7 000	000	00	00.0	10.7	.	.	.	.	.	.
16	7 000	040	00	01.3	09.6	.	.	.	.	.	.
17	7 060	050	00	03.7	09.3	.	.	.	=8 <sup>05</sup> 14 <sup>30</sup>	.	.
18	6 020	050	00	02.3	08.5	.	.	.	=10-15 <sup>25</sup>	.	.
19	6 030	010	00	01.3	09.2	.	.	.	=10-9 <sup>15</sup> , 10-14 <sup>40</sup> 24i, R <sup>0</sup> 12 <sup>35</sup> 13 <sup>20</sup>	.	.
20	6 09	100	100	09.7	00.0	.	.	.	.	.	.
21	8 080	090	09	08.7	06.3	26.0	.	.	12 12 <sup>40</sup> 14 <sup>10</sup> 21 <sup>15</sup> 22 <sup>15</sup> , T <sup>1-2</sup> 13-13 <sup>20</sup> 24 <sup>30</sup> -24	.	.
22	8 07	060	10	07.7	09.2	12.8	.	.	0-4-4 <sup>10</sup>	.	.
23	8 10	060	08	08.0	06.0	.	.	.	FSE-SW 15-24, 0-2 16 <sup>20</sup> 17 <sup>40</sup> 24 <sup>30</sup> 24i, FSE 0-7 <sup>25</sup>	.	.
24	8 05	10	10	08.3	00.8	.	.	.	0-0-8 <sup>30</sup> 13 <sup>45</sup> 13 <sup>55</sup> 20 <sup>30</sup> 24i, FSE 0-7 <sup>25</sup>	.	.
25	7 10	090	100	09.7	03.5	11.4	.	.	1 <sup>20</sup> 8 <sup>20</sup> i, 8-3-7i, T <sup>1</sup> 6 <sup>35</sup> 7 <sup>30</sup>	.	.
26	9 100	040	00	04.7	06.9	40.5	.	.	.	.	.
27	9 000	010	00	00.3	10.8	00.4	.	.	.	.	.
28	9 000	010	00	00.3	10.7	.	.	.	.	.	.
29	8 09	09	100	09.3	02.8	.	.	.	0-16 <sup>10</sup> 16 <sup>20</sup> 20 <sup>40</sup> 21 <sup>10</sup> , 0-13 <sup>45</sup> 9 <sup>15</sup> 12 <sup>25</sup> 14 <sup>20</sup> , T <sup>1</sup> 6 <sup>40</sup> 7 <sup>10</sup> T <sup>1</sup> 7 <sup>30</sup> , 8-10 <sup>30</sup>	.	.
30	7 100	100	03	07.7	00.4	08.2	.	.	.	.	.
MES. VRED.		04.6	04.4	03.1	04.0	237.8	110.9				

## SPLIT MARJAN

1974 OKTOBAR

1	8 05	030	00	02.7	07.4	24.4	.	• 0-15 <sup>05</sup> 5 <sup>30</sup> 10 <sup>10</sup>			
2	8 100	10	090	09.7	00.0	07.4	.	• 0-3 <sup>30</sup> 22 <sup>00</sup> , E-ESE-SE 8 <sup>10</sup> 15i, R <sup>1</sup> 14 <sup>40</sup> 16 <sup>40</sup> , 8-14 <sup>30</sup> 17 <sup>40</sup>			
3	9 010	050	03	03.0	10.3	16.4	.	FSE 6 <sup>15</sup> -12			
4	8 09	05	08	08.7	04.1	.	.	FSE-SE 10 <sup>05</sup> 5 <sup>30</sup> 18 <sup>30</sup> 24, 18 n-6 <sup>30</sup> , 0-14 <sup>30</sup> 6 <sup>20</sup>			
5	8 09	090	10	09.3	02.5	05.8	.	FSE 0-0 <sup>15</sup> , 0-0 <sup>40</sup> 3 <sup>30</sup> i			
6	8 08	050	00	04.3	08.3	03.8	.	.	.	.	.
7	8 09	050	06	06.7	04.6	.	.	.	.	.	.
8	8 100	060	00	05.3	04.2	C3.7	.	FSE-SSW 4-11 <sup>30</sup> , 5 <sup>20</sup> 12 <sup>30</sup> , 18 n-11 <sup>30</sup> 13 <sup>10</sup>	.	.	
9	9 020	07	00	03.0	08.4	15.6	.	8 <sup>15</sup> 4 <sup>10</sup> 16 <sup>50</sup> 17 <sup>05</sup> , 18 <sup>10</sup> 16 <sup>30</sup> 18 <sup>10</sup> , A 16 <sup>40</sup> 16 <sup>50</sup> , 8-16 <sup>50</sup> 16 <sup>50</sup>	.	.	
10	8 070	030	00	03.3	08.9	07.2	.	4 <sup>35</sup> 5 <sup>40</sup>	.	.	.
11	8 070	09	06	07.3	03.6	.	.	0-10 <sup>20</sup> 13 <sup>00</sup> i			
12	7 090	10	10	09.7	00.0	01.1	.	• 1-14 <sup>30</sup> 24i			
13	7 100	100	100	10.0	00.0	17.9	.	• 10-8 <sup>35</sup> 12-7i			
14	8 10	10	06	08.7	00.0	32.0	.	• 18 <sup>20</sup> 8 <sup>10</sup> 11 <sup>40</sup> 12 <sup>50</sup>			
15	6 10	100	10	10.0	00.0	02.5	.	• 0-17 <sup>40</sup> 19i			
16	8 09	08	03	06.7	05.5	13.4	.	• 0-17-8 <sup>30</sup> , 17-19 <sup>50</sup> , T <sup>1</sup> 16 <sup>05</sup> 18 <sup>30</sup>			
17	8 050	020	00	02.3	C8.1	C7.1	.	• 1n			
18	8 020	040	00	02.0	08.3	.	.	.	.	.	.
19	8 000	020	00	00.7	09.5	.	.	.	.	.	.
20	8 10	100	100	10.0	00.0	.	.	FSE-SSW 10 <sup>10</sup> 19, 0-2 10 <sup>50</sup> 24i	.	.	
21	8 100	09	10	09.7	00.4	27.6	.	• 0-0-13 <sup>05</sup> 16 <sup>25</sup> 18 <sup>55</sup> , T <sup>1</sup> 16 <sup>05</sup> 16 <sup>50</sup>			
22	9 100	07	10	09.0	03.2	06.3	.	T <sup>1</sup> 17 <sup>20</sup> 19 <sup>45</sup> , 0-6 <sup>30</sup> 10 <sup>30</sup> , 23 <sup>30</sup> -24, FSE 13 <sup>40</sup> 23 <sup>40</sup>	.	.	
23	6 100	100	09	09.7	00.0	12.1	.	• 0-0-10 <sup>25</sup> i	.	.	
24	9 08	030	00	03.7	07.2	03.0	.	• 0-1-6-15 11 <sup>30</sup> 11 <sup>50</sup> i	.	.	
25	8 010	010	00	00.7	09.6	00.0	.	.	.	.	.
26	8 04	100	100	08.0	01.4	.	.	• 0-13-12 <sup>10</sup> 20 <sup>50</sup> 23 <sup>20</sup> , ENNE-ENE 22 <sup>20</sup> 24i			
27	9 010	010	02	01.3	09.7	03.5	.	ENNE-ENE 0-12 <sup>25</sup> i			
28	8 040	10	10	08.0	05.8	.	.	FSE 14 <sup>30</sup> 24 <sup>25</sup> , 16 <sup>40</sup> 22 <sup>40</sup> i, • 16 <sup>40</sup> 22 <sup>40</sup> i, T <sup>1</sup> 19 <sup>30</sup> 19 <sup>50</sup>	.	.	
29	8 080	10	09	09.0	02.4	24.0	.	• 0-9 <sup>45</sup> 13 <sup>45</sup> i	.	.	
30	9 100	09	01	06.7	00.9	01.4	.	• 0-17-10 <sup>35</sup> i	.	.	
31	8 10	10	10	10.0	00.1	00.5	.	• 8 <sup>50</sup> 10 <sup>50</sup> i, 14 <sup>02</sup> 16 <sup>40</sup> , 19 <sup>40</sup> 20, T <sup>1</sup> 14 <sup>45</sup> 20 <sup>50</sup> i	.	.	
MES. VRED.		07.0	07.0	05.2	06.4	134.4	241.1				

$\varphi = 43^{\circ}31'$  N  $\lambda = 16^{\circ}26'$  E Gr.  $\Delta G = +1h\ 06\ min.$

BR. ST. 89

EGD	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	741.8	744.6	749.1	07.3	09.8	07.2	07.9	10.3	06.2	-	04.6	03.6	03.3	60	35	44	48	NNE	2	NE	5	NNE	3
2	751.5	751.7	752.5	05.6	11.2	09.8	09.1	12.0	04.8	-	03.1	05.5	05.3	46	55	58	53	ENE	2	SSW	2	ENE	2
3	753.1	754.0	753.9	07.2	09.6	08.5	08.6	10.3	06.8	-	06.6	07.1	06.2	87	80	72	80	ESE	2	I	2	ESE	2
4	751.6	750.8	750.3	08.3	11.9	11.4	11.6	12.8	07.7	-	06.7	07.8	09.3	76	75	92	81	ENE	3	SE	6	SE	4
5	750.0	741.8	753.2	10.7	14.1	14.2	13.3	14.2	10.2	-	08.6	08.3	08.5	89	69	70	76	ENE	4	SSE	4	SE	3
6	754.2	754.3	754.0	14.5	16.1	15.8	15.6	16.5	13.0	-	04.6	09.9	07.9	78	72	59	70	SE	5	SE	5	FSE	5
7	751.3	750.5	750.3	13.4	12.2	10.4	11.6	16.6	10.3	-	05.9	05.9	05.4	51	56	57	55	ENE	6	ENE	6	EKE	6
8	749.8	749.0	750.1	10.3	13.0	10.8	11.4	13.5	09.2	-	04.5	04.6	04.3	46	41	44	44	ESE	5	ENE	6	NE	5
9	749.9	750.5	752.0	11.4	14.2	11.0	11.9	14.5	10.4	-	04.5	05.2	04.5	45	42	46	44	NE	6	NE	6	ESE	4
10	753.6	753.5	754.1	08.9	14.0	10.9	11.2	14.4	08.4	-	04.7	05.5	06.3	55	46	64	55	ENE	3	SSW	1	NNE	2
11	755.6	755.5	755.7	09.3	14.2	11.4	11.6	14.8	08.9	-	05.5	07.0	07.0	62	58	63	63	ENE	2	SSW	1	EKE	2
12	755.0	754.6	754.0	09.9	10.8	11.4	10.9	13.0	09.7	-	06.3	08.7	08.5	69	80	84	81	ENF	3	N	3	E	1
13	753.9	754.8	755.6	10.8	14.8	12.2	12.5	15.0	10.0	-	07.9	09.1	08.2	82	72	77	77	ENE	2	SE	2	ESE	2
14	755.9	756.0	756.6	11.0	14.4	13.3	13.0	15.0	10.2	-	07.7	09.0	09.2	78	73	80	77	E	3	SE	4	SE	3
15	756.5	756.7	756.7	11.7	15.8	13.2	13.5	16.0	11.2	-	07.5	09.0	08.0	73	67	70	70	ESE	3	SE	4	FSE	2
16	755.8	755.3	755.6	12.2	15.6	14.2	14.0	16.0	11.6	-	06.2	06.8	06.5	58	74	70	67	ESE	2	SE	5	SE	5
17	754.5	756.6	757.1	12.5	16.5	13.7	14.1	16.7	12.0	-	05.6	08.3	08.7	61	59	74	65	ENE	2	SSE	3	NNW	1
18	757.1	758.4	756.1	11.1	15.8	13.2	13.3	16.2	11.0	-	07.3	09.8	09.4	74	73	83	77	ENE	2	SSE	1	ESE	2
19	751.7	749.7	752.3	14.2	16.0	13.4	14.2	16.6	11.7	-	09.5	10.0	07.0	79	73	60	71	SSE	6	SSE	6	WNW	3
20	754.3	754.9	754.9	11.2	15.2	17.4	12.8	15.4	10.6	-	07.0	07.5	06.9	70	58	64	64	ENE	2	SWW	2	ENE	2
21	753.6	752.3	752.5	10.8	13.4	11.4	12.0	14.0	10.4	-	05.8	06.6	06.9	60	75	66	67	ENE	4	SSW	5	ENE	2
22	753.5	753.8	754.2	10.6	14.7	11.5	12.1	15.0	09.9	-	05.7	06.2	06.7	60	49	66	58	NE	3	SSW	2	ENE	1
23	754.4	753.2	753.3	09.7	13.1	11.6	11.5	14.1	09.4	-	06.7	08.0	06.9	74	71	67	71	ENE	2	SSW	2	ENE	1
24	752.5	752.7	753.5	10.6	14.4	12.0	12.2	15.0	10.4	-	06.1	07.9	06.8	64	64	64	64	ENF	2	SSE	2	E	2
25	752.1	749.4	747.6	13.4	14.0	14.3	14.0	14.4	11.4	-	08.3	10.7	10.6	72	90	87	83	SE	5	SSW	5	SSE	5
26	746.0	746.0	747.9	10.6	11.5	08.5	09.8	14.6	08.3	-	07.4	05.9	04.5	77	58	54	63	ESE	2	WNW	3	NE	3
27	744.7	743.8	745.3	10.7	10.8	09.2	09.2	11.0	07.3	-	05.8	07.5	05.2	68	82	60	70	ENE	4	NE	2	NE	3
28	742.2	736.8	736.4	09.0	13.4	08.4	09.8	13.8	06.5	-	05.9	09.2	06.2	69	80	75	75	E	3	SE	6	ENE	2
29	741.1	741.8	743.7	07.6	11.4	08.2	08.8	11.6	06.4	-	04.7	05.7	05.1	60	57	63	60	WSW	2	ENE	1	ENE	2
30	746.8	749.6	751.9	06.9	11.6	08.0	08.6	11.7	06.3	-	04.7	05.3	03.5	62	52	43	52	ENF	3	SW	2	ENE	3
MES.	VRED.	751.5	751.4	752.0	10.4	13.4	11.4	11.6	14.2	09.3	-	06.4	07.6	06.8	67	65	66	66	3.2	3.2	3.2	2.4	2.4

## 1974 DECEMBAR

## SPLIT MARJAN

1	752.1	753.7	757.0	07.6	10.5	08.2	08.6	11.5	06.2	-	04.5	05.8	05.1	57	61	63	60	ENE	3	ENE	2	NE	3
2	757.9	758.5	759.2	08.0	11.2	11.3	10.4	11.6	06.8	-	05.0	07.0	05.9	63	70	59	64	NE	1	NNW	1	NNW	2
3	760.1	760.0	760.3	11.4	15.0	13.9	13.6	15.6	10.3	-	05.7	06.6	05.7	57	52	48	52	NNT	2	NNW	2	NNW	2
4	758.9	756.6	754.9	12.2	16.2	12.5	13.4	16.5	11.3	-	05.8	07.2	07.3	55	52	67	58	NE	2	SW	2	SE	1
5	751.7	749.8	746.8	09.2	12.4	09.8	10.3	13.0	08.0	-	05.4	07.1	07.1	62	66	79	69	ENF	1	SSW	1	ENE	1
6	749.5	750.5	751.7	09.6	12.0	10.0	10.4	12.2	08.3	-	04.1	03.2	03.8	45	31	41	39	E	1	LNF	4	NNW	1
7	751.8	751.5	751.3	07.8	11.0	10.0	09.7	11.6	07.4	-	05.8	06.5	06.4	73	66	70	70	ENE	2	NNW	1	NNW	2
8	750.5	750.0	750.6	08.8	10.7	10.2	10.0	11.1	08.1	-	05.8	07.3	06.9	68	76	74	73	ENE	1	SSW	1	NNW	2
9	751.2	751.9	753.4	10.6	13.4	11.7	11.8	14.2	09.1	-	06.1	08.4	08.1	64	73	79	72	NNE	2	SSW	1	SE	1
10	753.9	754.5	755.4	09.2	13.5	10.6	11.0	13.5	09.0	-	05.8	08.4	08.8	67	72	92	77	ENE	2	SW	1	SSE	1
11	754.0	751.1	747.5	09.8	12.3	11.8	11.4	12.3	08.6	-	06.9	08.5	08.2	76	76	79	78	NE	1	SSE	2	SSE	4
12	743.5	742.9	743.2	11.8	08.3	04.2	07.1	12.6	04.2	-	08.2	05.5	05.4	79	67	88	78	SW	2	ENE	4	EKE	4
13	742.7	743.0	743.9	03.9	05.8	04.3	04.6	06.7	03.5	-	04.7	04.2	04.3	78	61	69	69	ENE	2	NNE	3	NNW	2
14	744.8	747.2	748.2	05.4	06.4	06.4	06.2	07															

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijnost O-9	Oblačnost N (0-10)					Insolitacij broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	050	050	00	03.3	06.8	03.1	.	.	.
2	8	020	040	10	05.3	08.2	.	.	.	.
3	7	100	100	08	09.3	00.1	03.3	.	.	.
4	8	10	09	10	09.7	02.4	02.9	.	.	.
5	8	09	10	09	09.3	00.0	27.9	.	.	.
6	8	08	10	10	09.3	01.8	.	.	.	.
7	8	10	10	10	10.0	00.0	00.4	.	.	.
8	8	060	070	01	04.7	07.8	00.2	.	.	.
9	9	020	010	00	01.0	08.9	.	.	.	.
10	9	010	010	00	00.7	09.1	.	.	.	.
11	8	05	08	04	05.7	07.1	.	.	.	.
12	8	09	100	100	09.7	00.8	.	.	.	.
13	8	07	070	00	04.7	02.3	19.6	.	.	.
14	8	02	07	07	05.3	05.2	.	.	.	.
15	8	01	020	00	01.0	07.8	.	.	.	.
16	8	00	060	00	02.0	07.5	.	.	.	.
17	8	08	040	02	04.7	07.7	.	.	.	.
18	8	07	090	06	07.3	05.9	.	.	.	.
19	7	07	09	01	05.7	02.2	.	.	.	.
20	8	08	06	02	05.3	06.4	00.2	.	.	.
21	8	10	10	09	09.7	00.6	.	.	.	.
22	8	01	030	04	02.7	08.1	00.2	.	.	.
23	8	08	08	10	08.7	04.7	.	.	.	.
24	8	10	080	09	09.0	02.2	.	.	.	.
25	7	10	10	100	10.0	00.0	.	.	.	.
26	8	090	040	06	06.3	05.9	05.4	.	.	.
27	8	10	10	00	06.7	00.0	01.5	.	.	.
28	8	09	09	100	09.3	01.8	02.0	.	.	.
29	8	09	070	09	08.3	05.1	08.9	.	.	.
30	8	05	020	00	02.3	08.1	01.0	.	.	.
MES. VRED.		06.6	06.9	05.2	06.2	134.5	76.6			

## SPLIT MARJAN

1974 DECEMBAR

1	8	10	060	00	05.3	03.7	.	.	$\bullet 7^{50} 10^{20} i$	.
2	8	09	10	07	08.7	00.2	00.4	.	.	.
3	8	06	08	01	05.0	06.4	.	.	.	.
4	8	01	020	00	01.0	07.7	.	.	.	.
5	8	01	060	04	03.7	06.7	.	.	.	.
6	8	05	040	00	03.0	05.0	.	.	.	.
7	7	04	10	09	07.7	02.8	.	.	.	.
8	6	10	10	09	09.7	01.1	.	.	$=n-24$	.
9	8	09	08	02	06.3	02.1	.	.	.	.
10	8	00	000	07	02.3	08.0	.	.	.	.
11	7	10	10	10	10.0	00.1	.	.	$\bullet 15^{45} 19^{30} i$	.
12	8	10	10	10	10.0	00.0	01.2	.	$\bullet 0-12^{30} 4^{10} i$	.
13	8	01	10	10	07.0	02.0	10.1	.	$\bullet 16^{22} 17^{50} i$	.
14	8	07	040	00	03.7	05.8	00.1	.	$\bullet 0-24 i$	.
15	8	03	060	00	03.0	07.6	.	.	$\bullet F NNE - NW 0-21^{30} i$	.
16	8	05	010	00	02.0	06.3	.	.	$\bullet F NNE 12^{28} - 15 i$	.
17	8	01	090	02	04.0	07.1	.	.	$\bullet 0-6^{16} 14^{20} i$	.
18	6	10	100	05	08.3	00.0	00.2	.	$\bullet 12^{10} 12^{22} i$	.
19	9	02	000	00	00.7	08.4	06.5	.	$\bullet 12^{42} 13^{32} i$	.
20	8	07	000	00	02.3	07.3	.	.	$\bullet 12^{52} 13^{22} i$	.
21	6	04	060	00	03.3	07.4	.	.	$\bullet n-15^{45}$	.
22	7	00	000	00	00.0	07.7	.	.	$\bullet 12^{22} n-17$	.
23	7	00	000	00	00.0	07.9	.	.	$\bullet 12^{22} n-17$	.
24	7	00	010	10	03.7	07.7	.	.	$\bullet 13^{30} n$	.
25	6	10	10	00	06.7	00.0	.	.	$\bullet 13^{30} n$	.
26	7	04	080	10	07.3	03.9	.	.	$\bullet 9^{30} 14^{10} i$	.
27	6	10	09	09	09.3	06.7	.	.	$\bullet 6^{12} 32^{17} 4^{10} i$	.
28	9	100	030	07	06.7	07.4	06.1	.	.	.
29	8	01	070	05	04.3	06.7	00.2	.	$\bullet F-E NE 10^{30} 24 i$	.
30	8	07	100	09	08.7	00.3	.	.	$\bullet F-E NE 0-20^{30} i$	.
31	8	09	030	00	04.0	07.8	00.2	.	$\bullet F-E NE 0-20^{30} i$	.
MES. VRED.		05.4	05.8	04.1	05.1	151.8	25.0			

$\varphi = 43^{\circ}43'$  N  $\lambda = 18^{\circ}16'$  E Gr.  $\Delta G = +1h\ 13\ min.$ 

BR. ST. 141

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	594.3	593.1	593.9	00.0	-00.4	-01.2	-00.7	00.9	-01.2	-	04.6	04.5	04.2	100	100	100	100	SW	10	SSW	5	S 8
2	593.3	593.0	592.4	-01.8	-01.6	-02.4	-02.0	-00.6	-03.0	-	03.9	04.0	03.8	98	98	98	98	S	8	S	4	S 6
3	591.2	591.4	593.3	-02.8	-03.0	-02.1	-02.5	-01.7	-03.4	-	03.6	03.6	03.8	97	97	98	97	SSW	7	SSW	7	SSW 6
4	595.4	596.2	597.5	-03.8	-01.4	-04.1	-03.4	-01.2	-04.3	-	03.3	03.9	03.2	94	95	94	94	SSW	2	-	0	- 0
5	596.5	595.4	594.9	-04.8	-01.6	-01.8	-02.5	-01.1	-05.1	-	02.9	04.0	03.9	91	98	98	96	N	1	SW	4	SW 5
6	592.5	590.0	589.8	-03.0	-03.2	-04.2	-03.6	-01.2	-05.2	-	03.4	03.5	03.2	93	97	96	95	-	0	SW	5	SW 6
7	591.1	591.9	592.3	-04.2	-04.9	-04.8	-05.7	-03.4	-07.4	-	03.2	03.0	02.4	96	95	89	93	-	0	N	1	- 0
8	591.3	591.6	592.0	-05.6	-06.2	-07.6	-07.0	-06.2	-07.8	-	01.9	02.7	02.4	68	92	93	84	N	7	N	2	N 6
9	592.2	592.0	591.3	-05.8	-08.0	-05.4	-06.2	-05.4	-08.4	-	02.7	02.1	02.6	90	85	86	87	SW	2	NW	2	SW 5
10	589.9	590.0	592.2	-03.4	-02.8	-04.6	-03.8	-02.8	-05.4	-	02.7	03.6	03.1	75	97	96	89	SW	7	S	2	NE 4
11	593.0	595.1	596.6	-06.0	-05.8	-04.8	-05.4	-04.4	-07.4	-	02.6	01.5	01.6	90	51	49	63	NNE	3	-	0	N 4
12	597.3	597.2	595.8	-01.6	-04.2	-07.4	-05.2	-01.4	-07.4	-	02.5	01.8	00.8	62	53	32	49	N	5	N	7	N 10
13	594.1	593.0	593.3	-09.0	-09.0	-11.0	-10.0	-07.2	-11.0	-	01.9	02.0	01.6	84	86	81	84	N	10	N	8	N 6
14	594.2	594.4	594.4	-09.0	-05.4	-06.6	-06.9	-05.2	-12.0	-	01.3	01.1	00.7	55	35	24	38	ESE	3	-	0	-
15	594.2	594.4	594.4	-08.0	-06.6	-06.0	-07.0	-06.0	-08.4	-	00.5	00.5	00.7	20	20	22	N	3	N	4	N 6	
16	593.8	592.5	595.0	-03.2	-02.0	-05.0	-03.8	-02.0	-07.0	-	03.5	03.9	03.0	97	98	95	97	N	8	N	9	N 3
17	592.0	590.4	589.3	-02.4	-02.8	-07.4	-05.0	-01.8	-07.4	-	03.5	03.6	02.4	90	97	93	93	SW	9	-	0	-
18	586.6	586.8	588.7	-09.4	-10.0	-09.1	-09.4	-07.2	-10.4	-	02.1	01.9	02.1	91	91	91	91	N	12	N	10	N 8
19	589.0	589.1	588.7	-10.0	-06.8	-05.4	-06.9	-05.4	-10.0	-	01.9	02.6	02.4	91	94	95	93	N	8	N	10	NNW 10
20	587.4	587.2	589.4	-03.8	-03.6	-04.7	-04.2	-03.2	-05.4	-	03.3	03.4	03.1	96	97	95	96	N	12	N	12	N 11
21	592.0	593.1	594.7	-01.6	-06.2	-06.6	-06.5	-04.7	-07.4	-	02.6	02.7	02.6	94	94	94	94	N	9	NNW	1	N 6
22	596.1	597.2	597.3	-05.0	-02.0	-03.5	-03.5	-01.5	-06.6	-	02.5	00.8	03.1	80	21	89	63	SW	5	N	2	SW 4
23	595.9	593.9	593.7	-03.4	-03.2	-03.7	-03.5	-02.4	-05.4	-	02.7	03.2	03.4	77	87	96	87	-	0	SW	6	NW 3
24	592.4	592.1	592.0	-08.4	-07.6	-08.4	-08.2	-03.6	-08.8	-	02.2	02.4	02.2	92	93	92	92	N	7	N	5	N 4
25	590.6	591.3	592.0	-08.0	-06.8	-07.6	-07.5	-06.4	-08.8	-	02.3	02.5	02.4	90	91	93	91	N	5	N	4	N 4
26	592.4	593.0	593.0	-08.2	-06.2	-05.5	-06.4	-05.4	-08.4	-	02.3	02.7	02.7	92	92	88	91	-	0	-	0	WSW 3
27	591.7	590.9	592.1	-04.6	-02.0	-05.8	-04.6	-02.0	-06.4	-	02.5	03.1	02.8	77	79	94	83	SW	6	N	1	-
28	592.1	592.8	593.5	-06.0	-05.7	-06.6	-06.2	-03.6	-07.2	-	02.8	02.8	02.5	94	95	89	93	N	4	N	5	N 4
29	593.2	593.3	594.3	-06.9	-02.8	-04.6	-04.7	-02.4	-07.2	-	02.5	03.4	03.7	91	91	83	88	-	0	SW	6	NW 3
30	595.3	596.3	596.8	-05.2	-03.4	-02.4	-03.4	-02.0	-06.1	-	01.8	03.1	03.2	59	87	82	76	N	2	S	1	SW 4
31	597.0	596.4	596.3	-04.0	-01.8	-02.4	-02.6	-01.4	-04.4	-	02.4	03.3	02.8	70	83	73	75	WSW	4	SW	6	SW 7
MES.	592.2	592.7	593.2	-05.3	-04.4	-05.2	-05.1	-03.3	-06.9	-	02.6	02.8	02.6	84	84	84	84	5.2	4.7	5.0		

## 1974 FEBRUAR

## BJELAŠNICA

1	595.1	595.4	595.4	-04.2	-02.6	-04.0	-03.7	-02.4	-04.6	-	03.2	03.5	03.3	96	94	96	95	SW	9	SW	6	WSW 5
2	595.2	595.1	595.5	-03.6	-02.4	-04.4	-07.7	-02.1	-04.6	-	03.4	03.8	03.2	97	98	96	97	W	3	SW	5	SW 4
3	591.5	590.1	588.5	-04.0	-03.0	-02.0	-02.8	-02.0	-05.0	-	03.3	03.6	03.9	96	97	98	97	SW	9	SW	10	
4	585.5	584.0	585.9	-03.0	-04.2	-04.6	-04.0	-01.6	-04.8	-	03.6	03.2	03.1	97	96	96	96	SW	8	SW	10	WSW 4
5	585.1	585.0	583.7	-05.0	-03.9	-05.4	-04.0	-03.0	-06.2	-	03.0	03.3	02.9	95	96	95	95	SW	3	SW	6	SW 8
6	580.2	574.2	572.5	-03.6	-03.8	-02.8	-03.2	-02.8	-05.4	-	03.4	03.3	03.6	97	96	97	97	SSW	9	SW	15	SSW 12
7	569.9	572.5	576.0	-04.4	-04.4	-10.4	-07.4	-02.6	-10.4	-	03.2	03.1	01.9	96	94	90	93	S	9	W	5	N 5
8	579.3	583.5	588.2	-04.9	-09.6	-10.0	-09.8	-09.6	-11.4	-	02.0	02.0	01.9	91	91	91	91	N	8	N	9	N 8
9	590.9	592.9	594.0	-12.0	-06.4	-05.0	-07.1	-04.6	-12.2	-	01.6	02.7	03.0	89	94	95	93	3	NW	6	NE 4	
10	593.1	594.2	594.8	-06.4	-03.6	-04.0	-04.5	-03.6	-06.4	-	02.7	03.3	03.3	94	92	96	94	NW	6	N	6	N 1
11	593.6	592.3	591.7	-02.2	-02.8	-02.4	-02.7	-01.6	-04.2	-	03.4	03.2	03.2	93	86	84	88	-	0	NNW	5	W 6
12	588.4	588.7	586.9	-02.4	-02.0	-02.0	-02.1	-00.6	-02.6	-	02.7	03.0	02.6	71	76	67	71	SW	11	SW	6	WSW 8
13	584.0	583.9	583.7	-03.4	-03.2	-03.2	-03.2	-02.0	-03.6	-	03.5	03.5	03.5	97	97	97	97	WSW	7	SW	6	SSW 7
14	582.0	584.1	586.7	-03.4	-03.2	-03.2	-03.2	-02.8	-03.5	-	03.5	03.5	03.5	97	97	97	97	S	8	S	6	SW 8
15	586.5	586.0	587.6	-02.4	-01.8</td																	

BR. ST. 141

 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vjetar 0-9	Oblačnost N (0-10)					Insolacija broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	0	10≡	10≡	10≡	10.0	00.0	.	65	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0-24, [x]	
2	0	10≡	10≡	10≡	10.0	00.0	01.5	65	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0-24, * 3 <sup>12</sup> 4 <sup>45</sup> 22 <sup>35</sup> 23 <sup>45</sup> , + 22 <sup>35</sup> 24, [x]	
3	0	10≡	10≡	10≡	10.0	00.0	01.8	66	V 0-24, ≡ 0-23, F <sub>s-w</sub> 0-24, + 0-16, * 25 <sup>25</sup> 24, * 10 <sup>12</sup> 13 <sup>45</sup> , [x]	
4	8	10	08	00	06.0	02.9	01.0	67	V 0-24, F <sub>s-w</sub> 0-24, ≡ 0-24, [x], 0	
5	1	06	10≡	10≡	08.7	00.9	.	67	V 0-24, * 0-20 <sup>15</sup> , ≡ 0-24, * 9 <sup>25</sup> 24, * 10 <sup>45</sup> 15 <sup>02</sup> 16 <sup>35</sup> 19 <sup>45</sup> 20 <sup>35</sup> , [x], 0	
6	0	09	10≡*	10≡	09.7	00.0	01.0	67	V 0-24, ≡ 0-24, F <sub>s-w</sub> 0 <sup>25</sup> 14 <sup>30</sup> 24, + 0-0 <sup>25</sup> 24, * 12 <sup>20</sup> 19 <sup>45</sup> 23 <sup>25</sup> 24, [x]	
7	0	10*	10≡	00	06.7	00.0	07.7	75	V 0-24, F <sub>s-w</sub> 0-14 <sup>5</sup> , ≡ 0-17 <sup>15</sup> , * 0-9 <sup>45</sup> , + 0-2 <sup>45</sup> , * 17 <sup>25</sup> 24, + 25 <sup>30</sup> 24, [x]	
8	0	10	10≡*	10≡	10.0	00.0	00.4	75	V 0-24, + 0-24, * 0-24, F <sub>n</sub> 0 <sup>20</sup> 8 <sup>30</sup> 16 <sup>25</sup> 22 <sup>45</sup> , ≡ 9 <sup>25</sup> 24, * 11 <sup>45</sup> 19 <sup>45</sup> , [x]	
9	8	09	05	00	04.7	05.4	01.4	77	V 0-24, * 0-16 <sup>5</sup> , + 0-2 <sup>45</sup> , ≡ 10 <sup>15</sup> 18 <sup>45</sup> , * 10 <sup>25</sup> 24, F <sub>s-w</sub> 20 <sup>30</sup> 24, [x], 0	
10	0	09	10≡	10≡	09.7	00.0	.	72	V 0-24, * 0-9, F <sub>s-w</sub> 0-10 <sup>5</sup> , ≡ 3 <sup>25</sup> 24, * 12 <sup>20</sup> 13 <sup>45</sup> , [x]	
11	8	01	05○	02	02.7	07.9	00.0	72	V 0-24, ≡ 0-2, * 2-24, [x], 0	
12	8	08	04○	00	04.0	07.2	.	70	V 0-24, * 0-24, F <sub>n</sub> 0 <sup>25</sup> 24, [x], 0	
13	0	00	10≡	00	03.2	00.0	.	68	V 0-24, * 0-24, F, F <sub>s-w</sub> 0-24, ≡ 7 <sup>25</sup> 20, [x]	
14	8	02	05○	00	02.3	08.9	.	66	V 0-24, * 0-24, F <sub>n</sub> 0-24, [x], 0	
15	8	01	04○	00	01.7	08.5	.	63	V 0-24, * 0-24, F <sub>n</sub> 18 <sup>30</sup> 24, [x], 0	
16	0	10≡	10≡	04	08.0	00.0	00.6	62	V 0-24, ≡ 0-24, F <sub>n</sub> 0-18 <sup>45</sup> , ≡ 10 <sup>25</sup> 18 <sup>45</sup> , * 4-5 <sup>30</sup> , + 4-10 <sup>45</sup> 14 <sup>30</sup> , [x]	
17	0	03	10≡*	10≡*	07.7	00.0	.	60	V 0-24, * 0-7 <sup>45</sup> , F, F <sub>n</sub> 0-24, * 10 <sup>25</sup> 23, + 4-18-24, [x]	
18	0	10≡	10≡	10≡	10.0	00.0	04.4	72	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0-24, [x], 0	
19	0	10≡	10≡*	10≡	10.0	00.0	.	72	V 0-24, ≡ 0-24, F, F <sub>n</sub> 0-24, * 12 <sup>25</sup> 15, + 4-12 <sup>25</sup> 24, [x]	
20	0	10≡	10≡	10≡	10.0	00.0	01.7	76	V 0-24, ≡ 0-24, F <sub>n</sub> 0-24, + 0-24, [x]	
21	0	10≡	10≡	10≡	10.0	00.0	.	74	V 0-24, ≡ 0-22 <sup>10</sup> , F, F <sub>n</sub> 0-24, + 9, * 22 <sup>10</sup> 24, [x]	
22	9	00	00○	00	00.0	09.6	.	74	V 0-24, F <sub>n</sub> 0-17 <sup>5</sup> , # 17 <sup>45</sup> 24, [x], 0	
23	8	00	08	10≡*	06.0	04.9	.	71	V 0-24, * 0-12 <sup>45</sup> , F, F <sub>n</sub> 0-24, * 14 <sup>25</sup> 24, * 20 <sup>45</sup> 23 <sup>50</sup> , [x], 0	
24	1	10≡	00○	00	02.3	02.7	00.5	71	V 0-24, ≡ 0-12 <sup>45</sup> , F, F <sub>n</sub> 0-24, * 12 <sup>25</sup> 15, + 4-12 <sup>25</sup> 24, [x]	
25	8	09	09	00	06.0	01.7	.	70	V 0-24, * 0-24, F <sub>n</sub> 7 <sup>45</sup> 18 <sup>45</sup> , * 17 <sup>25</sup> 18 <sup>45</sup> , [x], 0	
26	8	00	00○	00	00.0	09.6	00.0	68	V 0-24, * 0-24, [x], 0	
27	2	00	00≡	04	01.3	03.7	.	66	V 0-24, * 0-24, F <sub>s-w</sub> 4 <sup>45</sup> 14 <sup>45</sup> , ≡ 10 <sup>25</sup> 16 <sup>45</sup> , ≡ 16 <sup>45</sup> 18 <sup>22</sup> , [x], 0	
28	0	10≡	10≡	10≡	10.0	00.3	.	64	V 0-24, * 0-16 <sup>45</sup> , ≡ 5 <sup>25</sup> 14 <sup>45</sup> , ≡ 5 <sup>25</sup> 14 <sup>45</sup> , F <sub>n</sub> 9 <sup>10</sup> 14 <sup>45</sup> , [x], 0	
29	9	00	00○	00	00.0	09.8	.	62	V 0-24, * 0-24, F <sub>n</sub> 11 <sup>45</sup> 16 <sup>45</sup> , [x], 0	
30	9	00	04○	03	02.3	09.2	.	60	V 0-24, * 0-24, + 10 <sup>20</sup> 23 <sup>25</sup> , F <sub>s-w</sub> 22 <sup>25</sup> 24, [x], 0	
31	8	05	07○	00	04.0	06.7	.	57	* 0-24, F <sub>s-w</sub> 0-24, [x], 0	
MES. VRFD.		06.2	07.1	04.9	06.1	99.9	22.2			

## BJELAŠNICA

1974 FEBRUAR

1	0	10≡	10≡	00≡	06.7	00.0	.	56	V 0-0 <sup>25</sup> F, F <sub>s-w</sub> 0-21, ≡ 0 <sup>25</sup> 24, V 4 <sup>45</sup> 24, [x]	
2	0	00≡	10≡	10≡	06.7	00.0	.	55	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0 <sup>25</sup> 6 <sup>45</sup> , [x]	
3	0	10≡	10≡	10≡	10.0	00.0	.	54	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0-24, [x]	
4	0	10≡*	10≡	10≡	10.0	00.0	11.4	72	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0 <sup>25</sup> 10 <sup>45</sup> , * 20 <sup>25</sup> 18 <sup>45</sup> 14 <sup>25</sup> 16 <sup>45</sup> , + 0 <sup>25</sup> 22 <sup>20</sup> , R 1 <sup>25</sup> 6 <sup>02</sup> , [x]	
5	0	04	10≡	10≡	08.0	00.0	00.3	74	V 0-24, ≡ 0-3 <sup>10</sup> 7 <sup>50</sup> 24, + 3 <sup>25</sup> 7 <sup>50</sup> F, F <sub>s-w</sub> 8 <sup>20</sup> 24, [x]	
6	0	10≡	10≡	10≡	10.0	00.0	.	74	V 0-24, ≡ 0-24, F, F <sub>s-w</sub> 0-24, + 4-16 <sup>45</sup> 24, [x]	
7	8	10≡*	08○	02	06.7	01.6	05.0	79	V 0-24, * 0-9 <sup>15</sup> F, F <sub>s-w</sub> w-nw 0-16 <sup>30</sup> , + 0-12 <sup>25</sup> , * 3 <sup>25</sup> 8 <sup>45</sup> , [x], 0	
8	8	10≡	05○	10≡	08.3	02.5	00.2	81	V 0-24, F, F <sub>n</sub> 24, + 4-16 <sup>45</sup> , ≡ 5 <sup>25</sup> 17 <sup>30</sup> , ≡ 20 <sup>25</sup> 24, [x], 0	
9	9	00○	08○	01	03.0	06.6	.	78	V 0-24, F, F <sub>n</sub> sw-nw 0-22 <sup>25</sup> 13 <sup>30</sup> 14 <sup>20</sup> , 21 <sup>20</sup> 24, + 0-2 <sup>25</sup> , ≡ 0-0 <sup>45</sup> , [x], 0	
10	9	03	02○	00	01.7	08.8	.	77	V 0-24, F <sub>n</sub> nw 0-14 <sup>50</sup> , [x], 0	
11	9	00○	00○	00	00.0	09.6	.	76	V 0-24, * 7 <sup>10</sup> 10 <sup>45</sup> F, F <sub>w</sub> 18 <sup>45</sup> 24, [x], 0	
12	9	00○	00○	00	00.0	09.4	.	73	V 0-11 <sup>30</sup> F, F <sub>n</sub> b-24, [x], 0	
13	0	10≡	10≡	10≡*	10.0	00.0	.	70	F, F <sub>s-w</sub> -ws 0-24, ≡ 1 <sup>25</sup> 24, V 8-24, + 8 <sup>15</sup> 10 <sup>45</sup> , + 8 <sup>25</sup> 24, [x]	
14	0	10≡	10≡	10≡	10.0	00.0	01.5	72	V 0-24, F, F <sub>s-w</sub> -ws 0-24, + 4-12 <sup>25</sup> , ≡ 0-0 <sup>35</sup> , [x]	
15	7	10≡*	08	10≡	09.3	00.0	09.5	81	V 0-24, ≡ 0-13 <sup>40</sup> F, F <sub>n</sub> ne-s sw 0-20 <sup>20</sup> 15 <sup>20</sup> , * 5 <sup>25</sup> 7 <sup>45</sup> , 10 <sup>20</sup> 11 <sup>20</sup> , ≡ 20 <sup>20</sup> 11 <sup>20</sup> , [x]	
16	8	06	08	03	05.7	00.0	03.9	84	V 0-24, F, F <sub>s-w</sub> 3 <sup>20</sup> 24, ≡ 3 <sup>25</sup> 11 <sup>45</sup> , 19 <sup>45</sup> 24, [x]	
17	8	10≡	08	10≡	05.3	00.0	00.0	82	V 0-24, F, F <sub>s-w</sub> -sw 0-24, + 0-11 <sup>40</sup> , [x]	
18	8	10≡	08	04	07.3	00.0	.	80	F, F <sub>s-w</sub> 0-24, ≡ 0 <sup>25</sup> 24, V 1 <sup>15</sup> 24, * 2-4 <sup>30</sup> 10 <sup>32</sup> 12 <sup>45</sup> 17 <sup>45</sup> , + 2-4 <sup>25</sup> 24, [x]	
19	0	10≡	10≡	10≡	10.0	00.0	01.7	81	F, F <sub>s-w</sub> 0-13 <sup>40</sup> 8-17; ≡ 0-2, H-24, V 0-24, + 1 <sup>25</sup> 24, [x]	
20	0	08	10≡	10≡	05.3	00.0	01.6	84	V 0-24, * 0-24, + 0-14 <sup>40</sup> , F, F <sub>n</sub> 0-24, V 0-24, + 1 <sup>25</sup> 24, [x]	
21	0	05	10≡	10≡	08.3	00.0	01.4	86	= 0-24, V 0-24, * 4-5 <sup>40</sup> 10 <sup>45</sup> 17 <sup>40</sup> , * 5 <sup>25</sup> 7 <sup>45</sup> , [x]	
22	0	10≡	10≡	10≡*	10.0	00.0	01.7	88	V 0-24, ≡ 0-24, * 10 <sup>40</sup> 12 <sup>45</sup> 16 <sup>45</sup> 24, + 20 <sup>25</sup> 24, F <sub>s-w</sub> 20 <sup>20</sup> 24, [x]	
23	0	10≡	10≡*	10≡	10.0	00.0	07.7	100	V 0-24, ≡ 0-24, * 0-14 <sup>20</sup> 12 <sup>40</sup> 23 <sup>40</sup> , + 0-15 <sup>45</sup> , F, F <sub>s-w</sub> 0-15, [x]	
24	0	10≡	10≡	10≡	10.0	00.0	01.4	102	V 0-24, ≡ 0-24, + 5-24, F, F <sub>n</sub> 5 <sup>25</sup> 24, [x]	
25	0	10≡	10≡	10≡	10.0	00.0	.	100	V 0-24, ≡ 0-24, + 0-14 <sup>40</sup> , F, F <sub>n</sub> 0-24, [x]	
26	0	10≡	10≡	10≡	10.0	00.0	.	100	V 0-24, ≡ 0-24, F, F <sub>n</sub> 0-24, [x]	
27	9	10≡	00○	00○	03.3	09.3	.	100	V 0-24, * 0-7 <sup>30</sup> , F, F <sub>n</sub> 0-11, * 7 <sup>25</sup> 24, [x], 0	
28	9	00○	00○	00	00.0	10.7	.	98	V 0-24, * 0-24, ≡ 21 <sup>20</sup> 24, [x], 0	
MES. VRFD.		07.4	07.7	06.8	07.3	58.5	47.3			

1974 MART

## BJELAŠNICA

 $\varphi = 43^{\circ}43'$ , N  $\lambda = 18^{\circ}16'$ , E Gr.  $\Delta G = +1h\ 13\ min.$ 

BR. ST. 141

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	589.5	589.5	588.9	-03.8	-02.6	-02.4	-02.6	-02.4	-05.0	-	03.3	03.6	03.8	96	97	98	97	S	3	S	3	S	3
2	586.5	585.9	585.8	-02.2	-02.4	-01.6	-02.0	-01.6	-02.4	-	02.9	02.9	03.3	75	75	80	77	W	7	SW	6	SW	6
3	586.7	589.2	590.7	-03.0	-01.6	-02.2	-02.2	-01.6	-03.0	-	03.4	03.3	03.5	93	80	90	88	SW	7	SW	7	SW	8
4	589.9	589.7	588.0	-02.4	-03.2	-03.0	-02.9	-02.8	-06.0	-	02.6	03.4	03.6	67	93	97	86	SW	10	SW	13	SW	15
5	587.1	587.2	587.4	-03.0	-02.4	-01.6	-02.3	-01.8	-03.4	-	03.6	03.8	03.9	97	98	98	98	S	12	S	7	S	7
6	585.5	586.7	586.8	-01.4	-00.8	-04.2	-02.6	-00.6	-04.2	-	04.1	04.3	03.2	99	99	96	98	S	7	S	4	N	5
7	586.8	588.2	588.3	-09.2	-08.3	-10.4	-09.6	-04.2	-10.4	-	02.1	02.3	01.9	91	92	90	91	N	5	N	6	NNW	7
8	588.4	588.9	589.4	-10.2	-08.2	-08.4	-08.8	-07.4	-10.6	-	01.9	02.2	02.2	90	90	90	90	N	5	N	3	N	3
9	589.3	590.0	591.6	-06.8	-05.6	-05.6	-05.9	-04.4	-08.8	-	02.6	02.8	02.9	94	92	95	94	N	1	ENE	2	E	4
10	591.2	591.3	591.9	-05.6	-03.5	-04.6	-04.6	-03.0	-05.8	-	02.9	03.4	03.1	95	97	96	96	N	1	-	0	NNW	3
11	592.1	593.7	594.1	-03.4	-05.0	-08.6	-06.4	-02.3	-08.6	-	03.5	02.9	02.2	97	93	92	94	S	1	-	C	N	2
12	594.2	594.2	593.8	-08.0	-01.6	-04.6	-04.7	00.0	-09.0	-	02.1	02.3	02.4	82	57	75	71	N	1	ESE	3	-	0
13	592.3	591.1	590.5	-06.0	-05.0	-04.0	-04.8	-04.0	-06.2	-	01.8	01.7	01.6	63	53	48	55	N	2	N	1	-	0
14	588.0	585.7	584.6	-04.4	-04.0	-06.2	-05.2	-02.6	-06.2	-	01.2	02.7	02.7	35	80	92	69	E	4	N	4	N	4
15	582.0	581.6	583.0	-07.0	-06.0	-07.0	-06.8	-05.6	-08.2	-	02.5	02.8	02.5	93	94	93	93	N	6	N	9	N	7
16	583.0	584.6	585.7	-07.2	-05.2	-05.0	-05.6	-04.4	-07.3	-	02.5	03.0	02.9	93	95	91	93	N	4	N	2	W	3
17	586.6	589.8	591.8	-05.0	-02.0	01.2	01.2	01.2	-05.6	-	01.4	02.7	02.1	45	68	41	51	N	5	W	2	NNW	2
18	591.9	592.6	591.6	-00.5	00.0	00.4	00.1	01.3	-01.3	-	02.8	03.7	03.2	63	80	69	71	WSW	5	SW	7	SW	11
19	592.9	594.5	594.5	00.6	01.6	01.2	01.2	02.2	-00.2	-	02.9	04.3	04.0	61	83	80	75	SW	10	SW	8	SW	9
20	595.2	597.1	595.9	00.6	01.6	01.6	01.4	02.4	00.4	-	02.0	02.6	02.5	42	51	48	47	SW	9	WSW	6	SW	10
21	598.2	599.0	599.5	01.0	05.0	02.4	02.7	07.4	00.8	-	01.8	02.9	03.1	38	45	56	46	SW	6	-	0	-	0
22	590.4	597.8	596.3	06.4	04.4	03.6	04.5	06.8	02.4	-	02.4	04.1	03.6	33	65	61	53	-	0	E	2	S	5
23	594.5	595.6	595.6	02.8	02.8	02.8	02.8	03.6	01.0	-	03.2	03.2	03.2	57	57	57	57	S	8	S	7	SW	5
24	596.8	597.2	595.7	02.4	04.8	03.6	03.6	05.6	02.4	-	03.4	04.2	04.0	62	66	67	65	E	3	S	2	S	5
25	594.4	595.6	595.6	02.2	03.8	02.8	02.9	04.0	02.2	-	03.2	04.5	04.5	59	75	81	72	SW	10	S	6	S	5
26	594.9	594.6	593.0	02.4	04.6	03.2	03.4	04.8	02.0	-	04.1	03.8	04.3	74	60	75	70	SW	6	SSW	3	SSW	5
27	591.9	591.9	592.4	01.8	05.0	00.8	02.1	05.0	00.2	-	03.9	04.0	04.2	74	61	86	74	SW	3	SSW	2	FNE	3
28	592.0	593.1	594.0	02.4	04.0	01.0	02.1	04.4	00.4	-	04.6	03.6	04.3	84	59	86	76	SSE	4	-	0	-	0
29	594.4	595.2	595.8	02.4	04.2	03.6	03.4	05.4	00.2	-	03.1	03.3	04.3	56	54	73	61	W	2	-	0	S	3
30	595.4	594.6	595.0	00.8	01.2	01.8	01.4	03.6	00.6	-	04.5	04.9	04.4	93	98	85	92	N	3	N	3	SW	4
31	593.5	592.7	592.2	01.4	01.0	-00.6	00.3	02.2	-00.6	-	04.8	04.9	04.4	95	100	100	98	SSE	3	-	0	NE	3
MES.	591.1	591.4	591.6	-02.0	-00.8	-01.6	-01.5	00.4	-03.2	-	02.9	03.4	03.3	74	78	80	77	4.9	3.8	4.7			
WRED.	588.4	588.8	588.5	-03.5	-02.0	-03.1	-02.9	-01.3	-04.4	-	03.3	03.6	03.4	51	89	91	90	5.5	4.7	5.3			

1974 APRIL

## BJELAŠNICA

1	590.2	590.6	590.9	-01.0	-01.0	-01.8	-01.4	01.2	-01.8	-	04.3	04.3	03.9	100	100	98	99	NE	2	-	0	-	0
2	590.9	592.5	593.4	-02.2	00.2	-02.4	-01.7	00.3	-02.4	-	03.8	04.7	03.8	98	100	98	99	-	0	-	C	N	1
3	593.5	593.9	593.9	-01.6	-01.4	-02.4	-02.0	00.0	-03.0	-	04.0	04.1	03.8	98	100	98	99	SSW	1	N	2	N	2
4	592.5	592.3	591.5	-03.6	-01.6	-01.8	-02.2	-01.0	-03.8	-	03.4	03.9	02.0	97	97	45	81	N	2	N	3	NF	3
5	590.7	591.5	591.5	-01.2	00.0	-01.4	-01.0	00.0	-02.2	-	04.0	02.6	02.0	96	56	48	67	E	2	E	2	NE	3
6	590.6	590.6	591.0	-04.0	-02.0	-03.6	-03.4	-01.6	-04.6	-	02.0	02.2	02.1	58	45	55	55	NE	4	NNE	5	N	6
7	591.0	591.0	591.1	-04.6	-02.0	-03.6	-03.4	-01.6	-04.6	-	02.5	02.6	03.0	77	66	84	76	W	6	N	3	N	4
8	588.6	589.9	589.4	-04.2	-04.2	-04.4	-04.3	-03.6	-04.6	-	03.2	03.2	03.2	96	96	96	96	N	9	N	7	N	8
9	589.4	591.8	592.3	-06.2	-03.4	-04.0	-04.2	-03.2	-06.2	-	02.7	03.5	03.3	94	97	96	96	N	8	N	7	N	2
10	592.7	591.9	589.1	-03.4	00.0	-00.8	-01.2	00.0	-04.2	-	03.5	04.2	03.9	97	91	90	93	S	2	S	5	SW	7
11	586.0	585.0	584.6	-02.4	-00.8	-01.6	-01.6	00.0	-02.4	-	03.8	04.3	04.0	98	99	98	98	SW	10	SW	9	SW	9
12	584.6	585.0	585.5	-00.2	00.6	00.2	00.2	01.0	-01.6	-	04.4	04.6	04.7	97	97	100	98	SW	7	SW	7	SW	9
13	587.2	588.4	588.0	-01.2	01.2	00.8	00.4	01.4	-01.8	-	04.2	04.3	04.7	99</td									

BR. ST. 141

 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Isotakta broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w		
		14	7	14	21	Sred Dies				7	7	
1	7	06	020	00	02.7	07.8	.	96	V0-24, $\equiv 0-4^{50} 18^{00} 24$ , $\boxed{\square}$ , $\circ$			
2	7	10	09	10 $\equiv$ *	05.7	00.0	.	93	V0-24, $\equiv 0-1^{15} F_{Esw} 20-24$ , $\equiv 06^{15} 11^{15} 16^{30} 24$ , $\equiv 17^{50} 24$ , $\equiv 17^{56} 24$ , $\boxed{\square}$			
3	0	10	10	10 $\equiv$	10.0	00.0	00.2	98	V0-24, $F_{Esw} 0-24$ , $\equiv 0-8^{15} * 0-4^{30} + 0-14^{10} \equiv 8^{45} 24$ , $\boxed{\square}$			
4	0	05	10 $\equiv$	10 $\equiv$	08.3	00.0	.	98	V0-24, $F_{Esw} 0-24$ , $\equiv 0-2^{20} \equiv 7^{40} 24$ , $\equiv 11^{45} 24$ , $\boxed{\square}$			
5	0	10	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	.	98	V0-24, $F_{Esw} 0-24$ , $\equiv 0-24, + 0-24, 8^{35} 17^{50} 23^{20} 24$ , $\boxed{\square}$			
6	0	10	10 $\equiv$	10 $\equiv$ *	10.0	00.0	15.5	117	V0-24, $F_{Esw} 0-24$ , $\equiv 0-2^{20} 15-24$ , $\equiv 0-24, * 0-2^{30} 15-24$ , $\equiv 0-24$ , $\boxed{\square}$			
7	0	10	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	17.3	132	V0-24, $\equiv 0-3^{15} 24$ , $\equiv 0-2^{30} 11^{15} 16^{30} 24$ , $\equiv 17^{50} 23^{45} 24$ , $F_{Esw} 0-24$ , $\boxed{\square}$			
8	0	10	10 $\equiv$	10 $\equiv$ *	10.0	00.0	07.6	145	V0-24, $\equiv 0-24, + 0-4^{20} * 0-2-4^{20} 21^{00} F_{Esw} 0-6$ , $\boxed{\square}$			
9	0	10	10 $\equiv$	10 $\equiv$	10.0	00.0	09.6	157	V0-24, $\equiv 0-24, * 21^{45} 24$ , $\boxed{\square}$			
10	8	10	00	10 $\equiv$	06.7	05.8	01.6	163	V0-24, $\equiv 0-24, 13^{15} 24$ , $\equiv 0-24$ , $\boxed{\square}$			
11	8	10 $\equiv$ *	00	10 $\equiv$	06.7	09.6	02.3	165	V0-24, $\equiv 0-7^{15} 18^{15} 24$ , $\equiv 2^{15} 7^{15} \# 7^{15} 18^{15}$ , $\boxed{\square}$ , $\circ$			
12	8	00	01	00	00.3	11.0	00.0	162	V0-24, $\equiv 0-2^{15} 24$ , $\boxed{\square}$ , $\circ$			
13	8	00	00	00	00.0	10.9	.	161	V0-24, $\equiv 0-13^{15} 24$ , $\boxed{\square}$ , $\circ$			
14	8	08	09	00	05.7	06.6	.	159	V0-24, $\equiv 0-24, * 15^{45} 20^{30}$ , $\boxed{\square}$ , $\circ$			
15	0	10	10 $\equiv$	10 $\equiv$ *	10.0	00.0	.	158	V0-24, $\equiv 0-5^{30} F_{Esw} 0-24$ , $\equiv 5^{30} 24$ , $\equiv 9^{15} 21^{45} + 9^{15} 24$ , $\boxed{\square}$			
16	0	10	10 $\equiv$	10 $\equiv$	02	07.3	00.0	164	V0-24, $F_{Esw} 0-6$ , $\equiv 0-19^{45} + 0-6^{15}$ , $\boxed{\square}$			
17	8	00	03	00	01.0	10.9	.	164	V0-24, $\equiv 0-12^{15} F_{Esw} 0-24$ , $\boxed{\square}$ , $\circ$			
18	8	05	03	01	03.0	09.8	.	162	F, $E_{sw}$ 0-24, $\boxed{\square}$ , $\circ$			
19	8	04	00	00	01.3	09.8	.	157	F, $E_{sw}$ 0-24, $\boxed{\square}$ , $\circ$			
20	8	08	08	08	08.0	05.4	.	140	F, $E_{sw}$ 0-24, $\boxed{\square}$ , $\circ$			
21	9	00	00	00	00	06.0	11.7	.	120	F, $E_{sw} 0-7^{30}$ , $\boxed{\square}$ , $\circ$		
22	9	00	00	07	02.3	10.8	.	100	F, $E_{sw} 0-24$ , $\boxed{\square}$ , $\circ$			
23	9	07	10	05	07.3	02.8	.	90	F, $E_{sw} 0-22^{15}$ , $\boxed{\square}$ , $\circ$			
24	8	03	05	06	04.7	09.8	.	65	F, $E_{sw} 0-24$ , $\boxed{\square}$ , $\circ$			
25	8	09	10	00	06.3	00.2	.	60	F, $E_{sw} 0-24$ , $\boxed{\square}$ , $\circ$			
26	8	03	08	02	04.3	06.0	.	52	F, $E_{sw}$ 0-10 <sup>30</sup> 24 <sup>15</sup> , $\boxed{\square}$ , $\circ$			
27	8	04	08	04	05.3	07.4	.	46	F, $E_{sw}$ 0-5 <sup>30</sup> 15 <sup>15</sup> 24 <sup>15</sup> , $\equiv 15^{20} 18^{20} \# 18^{20} 18^{20} \equiv 18^{40} 19^{40}$ , $\boxed{\square}$ , $\circ$			
28	7	10	07	01	06.0	05.1	03.5	47	$\equiv 6^{55} 11, * 14^{45} 12^{25} \# 15^{55} 16^{55}$ , $\boxed{\square}$ , $\circ$			
29	9	00	07	10	05.7	05.6	00.6	46	F, $E_{sw} 0-20^{30} \# 14^{20} 24$ , $\boxed{\square}$ , $\circ$			
30	1	10	10 $\equiv$	10	10.0	00.0	.	42	$\equiv 11^{20} 11^{40} \equiv 21^{40} 21^{20} \# 23^{80}$ , $\boxed{\square}$			
31	0	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	00.8	40	$\equiv 0-24, * 2^{20} 6, 14^{20} 22^{20}, * 10^{20} 11^{20} \# 13^{20} 14^{20}$ , $\boxed{\square}$			
MES.					06.5	06.4	05.7	06.2	151.0	62.8		

## BJELAŠNICA

1974 APRIL

1	0	10	10 $\equiv$	10 $\equiv$	10 $\equiv$	10.0	00.0	01.2	41	$\equiv 0-24, * 10^{05} M$ , $\boxed{\square}$	
2	C	10	10	10	10	10.0	00.0	00.0	40	$\equiv 0-24, \boxed{\square}$	
3	1	00	00	10	10 $\equiv$	06.7	06.1	.	40	$\equiv 0-6^{20} 10^{45} 24, * 6^{20} 10^{45}$ , $\boxed{\square}$ , $\circ$	
4	8	09	04	00	04.3	07.6	.	39	$\equiv 0-0^{30} \boxed{\square}$ , $\circ$		
5	8	10	09	06	08.3	03.1	.	38	$\equiv 6^{30} 10^{30} \# 18^{05} 18^*$ , $\boxed{\square}$ , $\circ$		
6	8	08	06	04	06.0	09.5	00.0	38	F, $E_{sw}$ 0-10 <sup>30</sup> 24 <sup>15</sup> , $\boxed{\square}$ , $\circ$		
7	8	09	09	08	08.7	05.0	.	37	F, $E_{sw}$ 0-24, $\equiv 22^{30} 24$ , $\boxed{\square}$ , $\circ$		
8	0	0	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	03.1	35	F, $E_{sw}$ 0-24, $\equiv 0-24, * 0^{25} 24^{10} + 2^{30} 24$ , $\boxed{\square}$	
9	0	10	10 $\equiv$	10 $\equiv$	10	10.0	00.0	03.0	44	F, $E_{sw}$ 0-17 <sup>40</sup> $\equiv 0-17^{40} V0-24$ , $\equiv 0-14^{40}$ , $\equiv 11^{20} 14^{30}$ , $\boxed{\square}$	
10	9	00	07	07	04.7	08.1	.	40	V0-24, $E_{sw} 17^{30} 24$ , $\boxed{\square}$ , $\circ$		
11	0	10	10 $\equiv$	10 $\equiv$	10 $\equiv$ *	10.0	00.0	.	39	V0-24, $F_{Esw} 0-24$ , $\equiv 5^{15} 24, * 8^{10} 10^{45} + 4^{80} 24$ , $\equiv 16^{45} 24$ , $\boxed{\square}$	
12	0	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	00.6	40	V0-24, $F_{Esw} 0-24$ , $\equiv 0-24, * 0-8^{45} + 0-11, * 12^{45} 22^{20} \# 14^{20} 16^{30}$ , $\boxed{\square}$	
13	9	02	08	10	06.7	02.0	02.2	44	V0-24, $F_{Esw} 0-10^{30}$ , $\equiv 14^{45} 24$ , $\boxed{\square}$ , $\circ$		
14	0	10	10 $\equiv$	10 $\equiv$	10 $\equiv$ *	10.0	00.0	03.2	47	V0-24, $\equiv 0-24, * 14^{45} 17^{40} \# 17^{40} 18^{05} 24$ , $\boxed{\square}$	
15	0	10 $\equiv$ *	10	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	03.0	47	V0-24, $\equiv 0-24, * 0-24, * 15^{40} 15^{20} 24$ , $\equiv F_{Esw} 3^{30} 14^{20} + 5^{20} 14^{20} 24$ , $\boxed{\square}$	
16	0	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	09.0	56	V0-24, $\equiv 0-24, + 0-24, * 0-24, F_{Esw} 20^{20} 24$ , $\boxed{\square}$	
17	C	10	10	10 $\equiv$ *	10 $\equiv$ *	10.0	00.0	13.6	72	V0-24, $\equiv 0-24, * 0-13^{40} 24, + 0-22^{30} F_{Esw} 0-18^{40}$ , $\boxed{\square}$	
18	C	10	10 $\equiv$ *	10 $\equiv$ *	10	10.0	00.0	14.2	83	V0-24, $\equiv 0-24, * 0-6^{20} 3^{20} 26^{20} 23^{20} 24$ , $\equiv 9^{10} 24, F_{Esw} 0-24$ , $\equiv 0-24$ , $\boxed{\square}$	
19	0	10	10 $\equiv$	10 $\equiv$	10 $\equiv$ *	10.0	00.0	09.9	92	V0-24, $\equiv 0-24, * 0-3, 13^{20} 16^{20} F_{Esw} 0-24$ , $\equiv 0-24$ , $\boxed{\square}$	
20	8	10	02	00	04.0	04.0	09.6	01.4	94	V0-15, $\equiv 0-9^{10} F_{Esw} 0-7^{30} 03^{20} 24$ , $\equiv 0-4^{20} 0-4$ , $\boxed{\square}$	
21	8	00	06	06	05.3	10.3	.	86	F, $E_{sw} 0-8^{30} 24$ , $\equiv 18^{10} 24$ , $\equiv 19^{10} 19^{45}$ , $\boxed{\square}$ , $\circ$		
22	C	10	10 $\equiv$ *	10	10.0	01.3	00.2	78	$\equiv 0-24, F_{Esw} 18^{30} 10^{40} 15^{20} 24, * 7^{10} 15^{30} + 13^{20} 24, V23^{20} 24$ , $\boxed{\square}$ , $\circ$		
23	7	10	06	06	05.3	08.6	00.6	79	$\equiv 0-8^{10} 12^{20} 12^{20} + 4^{10} 0-8^{30} 24, F_{Esw} 0-7^{20} V0-10^{20} \# 14^{10} 13^{10}$ , $\boxed{\square}$ , $\circ$		
24	8	00	06	04	03.3	08.6	00.1	77	F, $E_{sw} 9-24, \equiv 15^{15} 18^{16}$ , $\boxed{\square}$ , $\circ$		
25	8	10	10	10 $\equiv$	10.0	00.0	.	73	F, $E_{sw} 0-13^{20} + 4^{8-9^{10}} * 8-9^{10} 14^{20} 23$ , $\equiv 15-24$ , $\boxed{\square}$		
26	0	02	10	10 $\equiv$ *	10	07.3	02.1	04.0	78	$\equiv 0-24, * 0^{20} 2, 10^{30} 14^{20} + 3^{20} 24, F_{Esw} 3^{30} 2$	

$\varphi = 43^{\circ}43'$ ,  $N \lambda = 18^{\circ}16'$ , E Gr.  $\Delta G = +1h\ 13\ min.$ 

BR. ST. 141

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	575.9	578.3	579.9	-02.4	-00.4	-00.6	-01.0	-00.4	-02.4	-	03.6	04.4	04.4	94	100	99	98	S	9	S	4	-	0
2	581.8	584.7	586.0	-00.4	00.0	-00.4	-00.3	00.0	-00.6	-	04.3	04.4	04.3	96	97	96	96	SW	6	NW	7	NW	3
3	588.3	588.7	587.8	00.4	01.0	00.4	00.6	01.8	-00.6	-	04.4	04.8	04.7	94	97	100	97	W	2	SW	7	SW	9
4	586.1	584.0	585.0	-01.8	-01.6	-01.4	-01.6	00.4	-02.0	-	03.9	04.0	04.1	98	98	99	98	SW	7	SW	9	SW	10
5	583.3	584.8	585.3	-01.6	-00.2	-00.8	-00.8	-00.2	-01.6	-	04.0	04.5	04.3	98	100	99	99	SW	9	SW	7	SW	7
6	585.6	587.0	588.0	-01.8	00.0	-00.8	-00.8	00.0	-02.4	-	03.9	04.4	04.3	98	97	99	98	SW	8	SW	8	SW	7
7	591.0	592.4	592.5	-00.8	01.2	00.0	00.1	01.4	-01.4	-	04.3	03.4	04.4	99	68	97	88	SW	7	SW	6	SW	7
8	593.0	592.7	590.6	-00.4	02.2	-00.6	00.2	02.2	-01.0	-	04.5	05.4	04.4	100	100	99	100	SW	2	S	2	N	6
9	589.2	589.4	589.9	-02.6	-02.0	-02.8	-02.6	-00.6	-03.0	-	03.7	03.9	03.6	97	98	97	97	N	8	N	6	NNE	6
10	589.7	591.7	592.3	<u>-03.2</u>	-01.4	-00.2	-01.2	00.0	<u>-04.0</u>	-	03.5	04.1	04.5	97	99	100	99	N	8	NF	4	WSW	3
11	593.0	594.6	594.7	00.2	01.0	02.4	01.5	02.8	-00.2	-	04.5	04.9	04.5	97	100	83	93	W	3	SW	2	SW	7
12	594.3	595.0	596.1	03.0	04.4	01.4	02.6	05.2	01.4	-	04.3	04.1	04.9	76	65	97	75	SW	10	SSW	5	N	3
13	596.3	597.7	598.2	-00.2	02.0	03.4	02.2	03.4	-00.2	-	04.5	05.1	04.1	100	97	70	89	N	5	N	2	W	2
14	597.1	596.7	595.5	03.4	07.6	05.0	05.2	07.6	02.4	-	04.1	04.3	04.4	70	55	68	64	NW	4	W	2	SW	4
15	593.0	590.7	589.1	01.4	-02.4	-02.3	-01.4	05.0	-03.0	-	05.1	03.8	03.8	100	98	98	99	N	2	N	5	N	5
16	588.5	589.6	590.8	-02.6	-00.6	-C1.0	-C1.3	-00.4	-C3.2	-	03.7	04.4	04.2	97	100	99	99	N	2	NW	3	NW	3
17	591.4	593.1	593.5	00.0	01.6	-00.4	00.2	01.8	-01.6	-	04.2	05.1	04.5	92	100	100	97	SW	3	SW	4	N	3
18	592.8	594.0	593.1	-01.0	00.0	01.0	00.2	01.0	-01.1	-	04.2	04.6	04.9	99	100	100	100	N	7	N	4	N	4
19	592.8	593.4	594.7	01.0	01.8	02.4	01.9	02.4	00.7	-	04.9	05.2	05.4	100	100	100	100	N	9	N	8	N	6
20	595.0	595.8	595.9	02.0	05.4	04.6	04.2	05.8	01.8	-	05.3	04.3	04.9	100	64	77	80	N	6	N	5	N	5
21	596.0	595.9	595.2	02.4	03.6	03.2	03.1	04.6	02.0	-	05.3	05.8	05.6	57	57	57	57	N	5	N	5	N	6
22	595.1	592.7	588.5	03.4	07.6	04.2	04.8	07.6	02.0	-	04.4	04.9	04.0	76	62	97	78	N	3	SW	5	SW	6
23	587.0	587.8	587.3	-02.8	00.0	00.6	-00.4	04.2	-02.8	-	03.6	04.3	04.6	97	94	97	96	NW	8	NF	3	NF	3
24	586.8	587.3	587.2	00.6	03.0	02.6	02.2	03.4	00.6	-	04.6	05.4	05.4	97	94	97	96	NF	3	SW	5	SW	6
25	589.7	592.2	593.6	01.4	03.4	01.8	02.1	03.4	01.4	-	04.9	05.2	04.3	97	89	83	90	SW	9	NW	6	-	0
26	595.4	596.4	596.3	00.0	04.0	04.2	03.1	04.8	-00.6	-	04.2	03.6	03.4	91	59	55	68	NW	2	C	-	0	0
27	595.2	595.6	594.8	03.6	06.5	05.8	05.4	07.4	02.8	-	02.6	02.9	03.5	44	40	51	45	NW	3	N	2	-	0
28	593.0	592.2	590.4	06.8	09.0	06.0	07.0	09.4	04.2	-	04.2	04.2	03.9	57	48	55	53	SW	5	SSW	6	SSW	6
29	588.5	590.8	592.2	02.8	03.0	03.2	03.0	06.2	02.4	-	05.1	04.8	05.3	92	84	92	89	S	8	W	4	W	4
30	595.0	597.2	597.5	04.2	07.4	08.0	08.9	09.0	03.0	-	05.2	05.8	05.7	84	75	71	77	N	3	N	2	NW	4
31	597.3	587.7	597.5	07.8	<u>10.0</u>	06.8	07.8	<u>10.6</u>	06.4	-	05.4	05.6	05.3	68	61	72	67	SSW	7	SSW	7	SSW	7
MES.	WRED.			590.9	591.3	591.6	00.7	02.5	01.8	01.7	03.5	00.0	-	04.3	04.6	04.6	90	85	88	88	5.5	4.6	4.7

1974 JUN

BJELAŠNICA

1	595.4	594.9	595.8	05.2	07.6	04.2	C5.3	08.0	04.2	-	06.0	07.8	06.2	90	100	100	\$7	SSW	A	SW	C	WWH	7
2	595.9	596.0	595.4	03.0	02.2	02.0	02.3	04.4	01.4	-	05.7	05.4	05.3	100	100	100	100	N	8	N	2	N	3
3	595.7	597.7	596.2	01.2	02.4	02.6	02.3	03.0	01.0	-	05.0	05.4	05.6	100	100	100	100	NNE	0	N	9	N	7
4	598.3	600.0	594.6	03.4	08.4	09.0	07.4	09.0	02.0	-	05.8	05.7	03.6	100	69	42	70	N	7	NE	-	0	0
5	598.0	599.1	598.2	10.6	11.4	10.0	10.6	12.4	08.7	-	02.6	05.2	05.6	28	52	61	47	-	0	SW	1	-	0
6	597.0	596.0	594.5	10.6	11.0	07.5	09.2	12.0	07.5	-	02.6	06.0	05.2	28	60	66	51	SW	4	SW	6	WSW	6
7	593.3	594.6	595.3	06.0	06.8	02.0	04.2	07.6	02.0	-	07.0	07.4	05.3	100	100	100	100	SW	5	SW	2	N	3
8	596.1	596.8	596.0	-01.0	05.0	05.4	03.7	06.6	-03.0	-	02.3	04.8	04.5	57	73	67	64	N	3	NW	1	SW	2
9	594.7	593.2	592.4	05.0	08.4	06.2	06.4	08.4	04.7	-	03.9	05.2	04.2	60	63	59	61	SW	6	SSW	8	SSW	7
10	590.7	590.2	589.3	04.2	06.6	05.6	05.5	06.6	04.0	-	06.2	05.1	06.0	100	70	88	86	SSW	7	SSW	7	SSW	7
11	586.2	586.2	587.9	00.4	-01.2	-01.6	-01.0	05.6	-01.6	-	04.4	04.0	04.0	94	96	98	96	SW	3	NW	7	NW	0
12	589.2	589.4	588.6	-02.8	-00.4	-02.2	-01.9	-00.4	-02.8	-	03.6	04.3	03.8	97	97	98	97	NW	8	NW	3	NW	7
13	587.2	587.6	588.5	-00.6	01.6	00.2	00.4	01.6	<u>-03.4</u>	-	04.4	04.5	04.5	99	88	97	95	NNW	2	SW			

BR. ST. 141

 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intenziteta broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	0	10≡	10≡	08	09.3	00.0	04.2	67	F-Fs-sw 0-12 <sup>0</sup> ≡ 0-16 <sup>30</sup> 22 <sup>45</sup> 24; * 0-4 <sup>30</sup> 9 <sup>0</sup> 16 <sup>0</sup> , 22 <sup>30</sup> 24; + + 0-8 <sup>0</sup> , V0-24, # 30 <sup>0</sup> 16 <sup>0</sup> , [22 <sup>0</sup> , ]		
2	0	10≡*	10≡	03	07.7	00.0	02.2	68	≡ 0-15 <sup>0</sup> V0-24, * 8 <sup>0</sup> , F-NW 3 <sup>0</sup> 15 <sup>0</sup> , [ ]		
3	0	03	10≡	10≡	07.7	00.0	.	66	V0-10 <sup>30</sup> 22 <sup>45</sup> 24, # 30 <sup>0</sup> 16 <sup>0</sup> , F-SW 1 <sup>20</sup> 24, = 8 <sup>30</sup> 24, [ ]		
4	0	10≡*	10≡*	10≡*	10.0	00.0	00.0	62	≡ 0-24, F-Fs-sw 0-24, V0-24, * 5 <sup>30</sup> 7 <sup>40</sup> , M <sup>20</sup> 23 <sup>40</sup> , + + 7 <sup>30</sup> 24, [ ]		
5	0	10≡	10≡	10≡	10.0	00.0	05.0	67	≡ 0-24, F-Fs-sw 0-24, V0-24, + + 0-24, * 11 <sup>30</sup> 15 <sup>30</sup> 17 <sup>30</sup> , 19 <sup>30</sup> , [ ]		
6	0	10≡	10≡	10≡	10.0	00.0	00.1	68	≡ 0-24, F-Fs-sw 0-24, V0-24, + + 0-24, A 14 <sup>30</sup> 17 <sup>30</sup> , [ ]		
7	0	10≡	10≡	10≡*	10.0	00.0	00.0	65	≡ 0-10 <sup>30</sup> 13 <sup>30</sup> 24, F-FN 0-24, + + 0-6 <sup>30</sup> 16 <sup>30</sup> 24, V0-11 <sup>20</sup> * 16 <sup>30</sup> 23 <sup>30</sup> , [ ]		
8	8	10≡	10	10≡	10.0	00.0	01.4	68	≡ 0-24, F-FN-SW 0-40, V0-24, 17 <sup>30</sup> 24, V0-9 <sup>30</sup> 22 <sup>30</sup> 24, + + 0-2 <sup>30</sup> , A 15 <sup>30</sup> 16 <sup>30</sup> 18 <sup>30</sup> , [ ]		
9	0	10≡	10≡	10≡	10.0	00.0	00.4	67	≡ 0-24, F-FN-NNE-NE 0-24, V0-24, A 15 <sup>30</sup> 20 <sup>30</sup> , [ ]		
10	8	10≡	04○	00	04.7	10.0	00.5	68	≡ 0-8, V0-13 <sup>30</sup> , F-FN-NNE-NE 0-11 <sup>30</sup> , [ ], ○		
11	8	01○	05○	00	02.0	11.0	.	64	F-Fs-sw 10 <sup>30</sup> 24, [ ], ○		
12	8	00	05○	10≡	05.0	05.5	.	52	F-FN-sw 0-16 <sup>30</sup> 23 <sup>30</sup> 24, = 12 <sup>30</sup> 14, + 20 <sup>30</sup> 22 <sup>40</sup> , [ ], ○		
13	8	10≡	08○	03	C7.0	02.1	C1.2	40	≡ 0-24, F-FN-C-7 <sup>30</sup> , [ ], ○		
14	8	04○	07○	03	04.7	09.5	.	36	≡ 0-24, F-FN-NNE-NE 0-24, V0-24, A 15 <sup>30</sup> 20 <sup>30</sup> , [ ]		
15	0	10≡*	1C≡*	10≡*	10.0	00.0	02.4	34	≡ 0-24, 0-3-7 <sup>30</sup> * 7 <sup>30</sup> 14, + 19 <sup>30</sup> 22 <sup>30</sup> , + + 12 <sup>30</sup> 24, F-N 12 <sup>30</sup> 24, V16 <sup>15</sup> 24, [ ]		
16	0	10≡	10≡	04	08.0	04.2	05.4	43	≡ 0-14 <sup>45</sup> + + 0-6, F-N 0-6 <sup>15</sup> , V0-24, # 7 <sup>30</sup> 13 <sup>30</sup> , [ ], ○		
17	0	08	10≡	10≡	C5.3	00.0	02.3	42	≡ V0-8 <sup>30</sup> , F-FN-sw 0-9 <sup>30</sup> 24, # 9 <sup>30</sup> 10 <sup>30</sup> , 9 <sup>30</sup> 24, + 12 <sup>30</sup> 13 <sup>30</sup> , A 14 <sup>30</sup> 18 <sup>30</sup> , [ ]		
18	0	10≡	10≡	10≡	10.0	00.0	02.7	40	≡ 0-24, F-FN 0-24, A 15 <sup>30</sup> 22 <sup>30</sup> , [ ]		
19	0	10≡	10≡	10≡	10.0	00.0	00.9	37	≡ 0-24, F-FN 0-24, [ ]		
20	8	10≡	06	06	07.3	04.5	.	35	≡ 0-9 <sup>15</sup> , F-FN 0-8 <sup>30</sup> , [ ], ○		
21	0	10≡	10≡	10≡	10.0	00.0	.	34	F-N 0 <sup>30</sup> 24, = 4 <sup>30</sup> 24, + 7 <sup>30</sup> 7 <sup>30</sup> 10 <sup>25</sup> 10 <sup>35</sup> 16 <sup>50</sup> 18 <sup>40</sup> , [ ]		
22	8	C6○	08	10≡*	08.0	08.1	02.3	33	≡ 0-5 <sup>40</sup> , 20 <sup>30</sup> 24, F-FN-sw 0-24, + 19 <sup>30</sup> 24, F-22 <sup>30</sup> 24, [ ], ○		
23	8	00≡	C7	C7	04.7	04.7	03.8	35	≡ F-FN-sw 0-9 <sup>20</sup> ≡ 0-11 <sup>15</sup> + 0-15 <sup>30</sup> 22 <sup>30</sup> 24, V2 <sup>30</sup> 12 <sup>30</sup> , [ ], ○		
24	8	10≡	10●	10≡*	10.0	00.7	00.0	35	≡ 0-2 <sup>30</sup> , F-FN 0-24, A 12 <sup>30</sup> 22 <sup>30</sup> , [ ]		
25	8	10●	00○	00	C3.3	01.4	04.3	35	≡ 0-8 <sup>20</sup> , F-FN 0-20 <sup>30</sup> , * 4 <sup>30</sup> 6 <sup>30</sup> 7 <sup>30</sup> 8 <sup>30</sup> 11 <sup>30</sup> , # 300-600 8 <sup>30</sup> 12 <sup>30</sup> , [ ], ○		
26	8	10≡	01○	00	03.7	09.5	C1.3	32	≡ 2 <sup>30</sup> 8 <sup>30</sup> , [ ], ○		
27	8	00○	02○	00	00.7	14.3	.	32	≡ F-FN 0-2 <sup>30</sup> 24, [ ], ○		
28	9	02○	08	07	05.7	09.0	.	27	≡ F-Fs-sw 0-2 <sup>30</sup> 24, [ ], ○		
29	0	10≡	10≡*	03	07.7	00.9	11.2	20	≡ F-E 0-9 <sup>10</sup> ≡ 1 <sup>30</sup> 15 <sup>20</sup> , + 2 <sup>30</sup> 4 <sup>30</sup> 12 <sup>35</sup> 14 <sup>50</sup> , ▲ 12-12 <sup>35</sup> , [ ], ○		
30	8	02○	08	04	04.7	09.2	14.0	15	≡ F-FN 0-20 <sup>30</sup> , * 4 <sup>30</sup> 6 <sup>30</sup> 7 <sup>30</sup> 8 <sup>30</sup> 11 <sup>30</sup> , # 300-600 12 <sup>30</sup> , [ ], ○		
31	9	03○	08○	06	05.7	07.1	.	13	≡ F-FN 0-24, [ ], ○		
MES.											
WRED.		07.4	08.0	06.6	07.3	111.7	65.7				

## BJELAŠNICA

1974 JUN

1	0	10≡*	1C≡	10≡	10≡	1C-C	00.0	11.1	1C	F-Fssw-sw-wew-nw 0-24, ≡ 2 <sup>30</sup> 24, ▲ 4 <sup>30</sup> 4 <sup>50</sup> * 4 <sup>30</sup> 7 <sup>30</sup> 21 <sup>45</sup> 24, [ ]	
2	0	10≡*	10≡*	10≡*	10.0	00.0	14.9	08	F-N-NNE-NW-NNW 0-24, ≡ 0-24, + 0-2 <sup>30</sup> , 9 <sup>30</sup> 24, [ ]		
3	0	10≡*	10≡	10≡	10.0	00.0	05.3	04	F-F 0-24, ≡ 0-24, + 0-8 <sup>30</sup> , [ ]		
4	8	10≡	04○	00	04.7	C8.1	.	C3	F-FN 0-8 <sup>30</sup> , [ ]		
5	8	01○	04○	C6	C3.7	11.1	.	02	# 800-800 23 <sup>30</sup> 8, T 17 <sup>30</sup> 17 <sup>30</sup> , R 19 <sup>30</sup> 22 <sup>30</sup> , [ ], ○		
6	8	08	09	05	07.3	04.4	.	01	# 800-4 <sup>30</sup> 8, F-Fs-sw 9, 24, + 9 <sup>30</sup> 10 <sup>30</sup> , [ ], ○		
7	0	10≡	10≡	10≡	10.0	00.0	06.6	.	F-FN-sw 0-8 <sup>30</sup> 21 <sup>30</sup> 24, ≡ 1 <sup>30</sup> 24, + 2 <sup>30</sup> 19 <sup>30</sup> 22 <sup>30</sup>		
8	8	00○	05○	00	01.7	10.8	05.9	.	= 0-3 <sup>25</sup> , F-FN 0-3 <sup>30</sup> , [ ], ○		
9	8	09	09	04	07.3	03.8	.	.	F-Fsw-sw 4 <sup>30</sup> 24, # 800-5 <sup>30</sup> 7 <sup>30</sup> , + 10 <sup>30</sup> 10 <sup>30</sup> , [ ], ○		
10	8	10≡	08	10	09.3	01.2	00.0	.	F-Fsw 0-24, ≡ 3 <sup>30</sup> 11, [ ], ○		
11	0	10	10≡*	1C≡*	10.0	00.0	03.2	01	F-Fssw-sw-wew-nw 0-24, ≡ 1-6 <sup>0</sup> 9 <sup>30</sup> 24, + 1 <sup>30</sup> 10 <sup>30</sup> * 1 <sup>30</sup> 5 <sup>50</sup> 18 <sup>10</sup> 24, # 300-600 6 <sup>30</sup> 9 <sup>30</sup> 2 <sup>30</sup>		
12	8	10≡	05○	10≡*	08.3	03.7	00.2	01	F-FN-NW-10 <sup>45</sup> 4 <sup>0</sup> 7 <sup>45</sup> , # 0-9 <sup>30</sup> 16 <sup>30</sup> 21 <sup>45</sup> , + 0-16 <sup>45</sup> , L-10 <sup>35</sup> V16 <sup>29</sup> 24, + + 20 <sup>45</sup> 24, [ ]		
13	9	04○	04	10≡	06.0	08.1	00.1	01	E 21 <sup>40</sup> ; V0-15 <sup>10</sup> , [ ], ○		
14	0	01○	10≡	10≡	07.0	04.4	C1.1	C1	Fsw 3 <sup>30</sup> 23, # 3 <sup>30</sup> 6 <sup>30</sup> 4 <sup>30</sup> 9 <sup>30</sup> , = 9 <sup>30</sup> 10 <sup>30</sup> * 9 <sup>45</sup> 11 <sup>30</sup> , = 13 <sup>30</sup> 23 <sup>30</sup> , [ ], ○		
15	9	03	03○	10≡	05.3	07.5	.	.	= 2 <sup>30</sup> 6 <sup>30</sup> 24, Fsw 3, + 4 <sup>30</sup> 14 <sup>30</sup> 20 <sup>30</sup> , 6 <sup>30</sup> 9 <sup>30</sup> , [ ], ○		
16	0	00○	00≡	00≡	00.0	03.7	00.0	.	= 0-2 <sup>45</sup> 7 <sup>45</sup> 9 <sup>25</sup> , 13 <sup>30</sup> 24, + 4 <sup>30</sup> 6 <sup>30</sup> 2 <sup>30</sup> 7 <sup>30</sup> , + 21 <sup>45</sup> 22 <sup>30</sup> , [ ]		
17	8	10≡	08○	08	08.7	04.4	C1.3	.	= 0-10 <sup>30</sup>		
18	8	00○	07	04	03.7	05.1	.	.	13 <sup>30</sup> -16 <sup>05</sup> + 15 <sup>35</sup> 15 <sup>50</sup> , + 15 <sup>30</sup> 17 <sup>30</sup> = 17 <sup>30</sup> 18 <sup>30</sup> , [ ]		
19	0	10≡	10≡	10≡	10.0	00.0	09.0	.	# 300-600 4 <sup>30</sup> 4 <sup>0</sup> 24, + 13 <sup>30</sup> 17 <sup>30</sup> , F-N 5 <sup>30</sup> 24, + 13 <sup>30</sup> 17 <sup>30</sup> , [ ]		
20	0	10≡	1C≡	10≡	10.0	03.7	00.5	.	= 0-24, F-FN 0-10 <sup>30</sup> , [ ]		
21	0	10≡	10≡*	10≡	10.0	00.0	.	.	= 0-23 <sup>30</sup> + 12 <sup>30</sup> 17 <sup>30</sup> , # 6 <sup>30</sup> 2 <sup>30</sup> 24		
22	8	C2○	10	04	05.3	06.3	C1.8	.	# 6 <sup>30</sup> 0-9 <sup>30</sup> , = 10 <sup>30</sup> Fsw 12 <sup>30</sup> 23, + 13 <sup>45</sup> 15 <sup>05</sup> , + 14 <sup>30</sup> 14 <sup>40</sup> , + 14 <sup>30</sup> 14 <sup>20</sup> , [ ]		
23	8	08○	06○	08	07.3	06.0	04.0	.	Fsw-wsw 4 <sup>30</sup> 24, [ ], ○		
24	8	09	10	10≡	05.7	C2.6	.	.	F-Fsw 0-24, ≡ 0-24, + 0-5 <sup>30</sup> 8 <sup>30</sup> 11 <sup>30</sup> 14 <sup>30</sup> 24, + 13 <sup>30</sup> 20 <sup>30</sup> , 23 <sup>30</sup> 24, [ ]		
25	7	09	08	08	08.3	00.0	01.7	.	F-Fsw 0-11 <sup>30</sup> , + 0-4 <sup>30</sup> 9 <sup>30</sup> 10 <sup>40</sup> , + 0-2 <sup>30</sup> 9 <sup>30</sup> 10 <sup>40</sup>		
26	9	04○	04○	05	04.3	13.5	C1.1	.	* 4 <sup>30</sup> 9 <sup>20</sup> , [ ]		
27	9	10	07	09	08.7	06.8	.	.	F-Fs-sw 0-24, + 15 <sup>35</sup> 15 <sup>45</sup> , = 22 <sup>30</sup> 24, [ ]		
28	0	10≡	10≡	09	09.7	00.0	04.4	.	F-Fs-sw 0-12 <sup>30</sup> , + 17 <sup>30</sup> 24, = 0-17 <sup>30</sup> 22 <sup>30</sup> 24, + 0-30 4 <sup>30</sup> 22 <sup>40</sup> 23 <sup>30</sup>		
29	0	10≡	10≡	10≡*	10.0	00.0	01.4	.	F-Fsw 0-24, ≡ 0-24, + 0-3 <sup>30</sup> 5 <sup>30</sup> 12 <sup>30</sup> 24, + 13 <sup>30</sup> 24 <sup>30</sup>		
30	0	10≡*	10≡	10≡	10.0	00.0	13.8	.	F-Fsw-sw-wew-nw 0-24, + 0-12 <sup>30</sup> , + 14 <sup>30</sup> 17 <sup>30</sup> , = 0 <sup>30</sup> 24,		
MES.											
WRED.		07.3	07.7	07.7	07.5	115.2	87.4				

$\varphi = 43^{\circ}43'$  N  $\lambda = 19^{\circ}10'$  E Gr.  $\Delta G = +1h\ 13\ min.$

BR. ST. 141

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u%			Pravac i jačina vetro D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	593.6	597.7	598.4	04.4	09.2	10.2	08.5	11.6	04.2	-	06.3	04.9	05.0	100	56	53	70	NW	7	K	5	-	0
2	599.0	599.5	599.1	10.6	11.0	08.2	09.5	11.6	08.2	-	04.3	05.8	08.2	45	100	100	82	W	2	-	C	N	3
3	599.5	597.8	595.5	08.6	13.2	10.2	10.6	13.8	05.4	-	02.4	05.4	06.8	29	47	73	50	N	2	S	3	SW	8
4	596.7	596.4	595.3	10.6	13.0	10.2	11.0	13.6	06.6	-	07.0	08.9	08.2	73	79	88	80	Sk	2	SW	2	SSW	2
5	597.2	598.6	598.9	10.4	12.6	11.4	11.4	13.4	08.6	-	06.5	08.6	08.9	69	78	88	78	NW	3	-	O	SW	3
6	598.6	598.9	596.6	13.4	15.0	10.6	12.4	15.2	10.0	-	07.2	07.2	06.6	63	56	65	63	-	0	S	6	SW	6
7	595.1	594.9	593.6	11.8	00.6	00.4	03.2	12.0	-00.2	-	07.3	04.8	04.7	71	100	100	90	SW	3	NNE	0	NNE	1
8	593.4	594.5	595.3	-00.3	01.2	00.8	00.6	01.6	-00.4	-	04.5	05.0	04.9	100	100	100	100	N	0	N	7	N	8
9	595.5	597.7	597.4	00.4	04.8	05.8	04.2	06.2	06.2	-	04.7	04.0	04.7	100	62	68	77	N	0	N	5	N	3
10	597.1	597.7	598.3	06.0	08.8	07.0	07.2	09.6	05.0	-	05.0	04.2	06.8	71	49	90	70	N	4	N	3	S	5
11	598.2	599.3	599.5	05.6	10.6	09.6	08.8	10.8	04.0	-	04.0	05.7	06.7	59	60	74	64	N	6	-	O	NW	4
12	599.2	600.2	600.8	10.8	14.8	12.6	12.7	14.8	09.0	-	05.5	05.0	06.0	56	47	55	53	SW	5	SW	4	SW	4
13	600.3	600.1	598.9	13.8	17.0	12.6	14.0	17.2	11.0	-	05.0	05.4	04.4	42	37	40	40	SW	3	SW	3	SW	5
14	599.1	599.7	599.3	14.2	17.0	12.8	14.2	17.2	10.8	-	05.6	06.7	05.4	46	46	49	47	SW	6	SW	7	SW	6
15	600.2	601.5	601.2	14.7	17.6	14.6	15.2	17.6	12.2	-	05.0	06.2	05.2	41	41	42	41	-	0	S	3	S	3
16	600.2	600.0	600.8	16.2	18.6	16.0	16.7	19.0	13.4	-	04.8	06.4	06.2	35	40	46	40	SW	4	SW	4	SW	4
17	598.0	598.4	596.1	15.2	18.0	14.6	15.6	18.4	14.6	-	05.4	05.4	04.9	41	35	39	38	SW	6	S	9	S	7
18	594.4	593.4	594.1	12.6	15.8	11.6	13.2	15.8	11.6	-	06.1	06.0	07.8	52	44	76	57	SW	4	S	9	S	8
19	597.3	592.3	592.3	10.8	12.8	07.4	09.6	13.0	07.4	-	09.5	07.7	07.5	98	70	98	89	SW	6	S	5	S	4
20	590.9	591.5	591.4	02.2	00.8	-00.5	00.5	07.4	-01.0	-	03.9	04.9	04.4	72	100	100	91	NW	7	NW	7	NW	5
21	589.8	589.9	590.2	00.6	00.8	01.4	01.0	01.4	-00.5	-	04.8	04.9	05.1	100	100	100	100	NW	7	NW	7	NW	7
22	591.9	592.5	592.3	01.6	01.6	01.8	01.7	01.8	00.8	-	05.1	05.1	05.2	100	100	100	100	NW	2	NW	8	NW	9
23	592.0	593.0	595.1	02.6	03.4	03.6	03.3	03.8	01.8	-	05.5	05.8	05.9	100	100	100	100	NW	8	NW	7	NK	7
24	596.7	598.4	596.6	06.0	09.0	08.4	08.0	10.8	03.6	-	06.8	05.9	06.8	97	68	82	82	NW	6	NW	3	NW	3
25	596.6	597.1	596.8	07.6	12.0	05.6	09.7	12.0	07.0	-	05.5	06.6	06.7	70	63	74	69	SW	6	SW	6	SW	4
26	597.1	598.0	598.0	06.4	06.0	05.7	05.7	09.6	05.2	-	07.0	07.0	06.6	98	100	100	99	NW	2	NW	2	NW	2
27	598.0	599.4	599.7	10.0	12.4	11.2	11.2	12.4	05.0	-	02.1	06.9	06.4	23	64	64	50	-	0	-	0	SW	2
28	599.7	600.4	600.6	11.6	13.0	11.6	12.2	13.8	09.6	-	04.4	08.1	06.6	43	68	64	58	SW	2	NF	2	NW	1
29	601.4	601.7	601.7	10.3	13.6	11.6	11.9	14.0	10.0	-	04.6	06.8	08.0	47	58	78	61	-	0	-	C	-	0
30	600.9	600.3	599.7	14.4	15.4	14.7	14.6	17.0	10.0	-	04.2	08.5	06.7	34	65	55	51	-	0	-	O	-	0
31	598.6	598.8	598.8	14.4	15.2	13.2	14.0	17.0	12.2	-	08.1	08.0	10.3	66	61	90	72	-	0	-	C	-	0
MES.	VRED.	596.7	597.4	597.2	09.0	10.8	09.0	09.4	12.0	06.7	-	05.4	06.3	06.4	66	68	76	70	3.6	3.8	4.0		

1	598.7	599.1	599.0	15.0	15.6	13.2	14.2	16.6	12.2	-	07.4	06.2	07.7	58	46	66	57	-	0	NN	?	-	0
2	599.7	599.7	599.9	14.2	16.2	12.8	14.5	16.4	12.0	-	06.7	07.6	07.7	55	55	65	58	N	3	ENE	3	-	0
3	599.7	600.9	601.2	15.2	17.0	14.8	15.4	17.8	12.6	-	05.9	14.5	12.6	46	100	100	82	N	2	ENE	4	ESE	3
4	601.0	601.4	601.9	15.6	19.6	15.6	16.6	16.8	13.6	-	06.4	07.7	06.4	48	45	48	47	S	3	-	C	NNW	3
5	601.1	601.1	601.4	15.8	17.4	15.4	16.0	17.6	14.0	-	04.4	07.3	06.1	32	45	46	42	-	0	-	0	W	3
6	600.2	600.2	599.7	11.0	09.0	06.0	08.0	15.4	06.0	-	09.8	08.6	07.0	100	100	100	100	N	4	I	?	N	5
7	598.0	598.0	597.7	05.0	09.4	11.0	09.1	11.0	03.0	-	04.7	05.7	03.5	72	64	35	57	N	3	N	2	W	7
8	596.0	596.0	594.8	13.0	16.0	12.4	13.4	16.2	10.0	-	04.3	05.9	06.5	38	43	60	47	SW	4	SSW	3	SW	5
9	594.1	593.0	594.3	10.0	11.0	06.0	09.2	13.8	08.0	-	05.6	06.5	08.0	61	66	100	76	S	2	SSW	7	N	5
10	596.5	596.5	594.8	05.4	12.6	09.8	09.4	13.0	04.0	-	04.7	05.6	04.0	70	52	44	55	NNE	2	S	2	SW	5
11	591.6	590.3	591.7	07.6	07.4	01.0	04.2	10.0	01.0	-	06.7	07.7	04.9	86	100	100	95	SSW	5	SW	4	N	7
12	590.8	593.8	594.5	01.8	03.8	02.6	02.7	04.2	00.8	-	05.2	05.1	05.5	100	84	100	95	N	8	N	5	N	4
13	595.0	598.0	599.1	02.2	06.6	07.0	05.7	07.0	02.0	-	05.4	03.9	01.9	100	54	26	60	N	3	N	7	N	7
14	599.6	602.2	602.1	08.0	12.6	11.4	11.0	13.0	07.0	-	05.5	05.1	04.7	65	47	46	53	N	2</				

BR. ST. 141

 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijeme 0-9	Obločnost N (0-10)					Insolacija broj sati	Precipitacija P mm	Snežni pokrivač h cm	Razvoj vremena w		
		14	7	14	21	Sred Dnes				7	7	
1	8	10≡	040	00	04.7	05.5	02.7	.	.	F <sub>N-NW</sub> 0-14 <sup>00</sup> ≡ 0-8 <sup>45</sup> 0 <sup>15</sup> 3 <sup>00</sup> ○		
2	0	030	10≡	10≡	07.7	05.0	.	.	.	F <sub>N-NW</sub> 0-12 <sup>45</sup> 13 <sup>20</sup> ≡ 9 <sup>45</sup> 22 <sup>00</sup> ○		
3	9	000	010	00	00.3	15.0	02.8	.	.	F <sub>NW</sub> 17 <sup>45</sup> 24 <sup>0</sup> ○		
4	1	050	10≡	10≡	08.3	05.1	00.7	.	.	F <sub>E-O</sub> 0-3 <sup>0</sup> 0-2 <sup>45</sup> 2 <sup>40</sup> ≡ 50 <sup>00</sup> 4 <sup>20</sup> 7 <sup>20</sup> 22 <sup>40</sup> 24 <sup>1</sup> ≡ 7 <sup>30</sup> 22 <sup>0</sup> 22 <sup>20</sup> 24 <sup>1</sup> ≡ 15 <sup>20</sup> 10 <sup>30</sup> ○		
5	8	000	080	00	02.7	06.0	.	.	.	F <sub>N-NW</sub> 0-9 <sup>45</sup> 10 <sup>20</sup> ≡ 0-8 <sup>20</sup> 20 <sup>0</sup> ≡ 0-8 <sup>20</sup> 20 <sup>0</sup> ≡ 9 <sup>45</sup> 9 <sup>55</sup> ≡ 15 <sup>20</sup> 10 <sup>30</sup> ○		
6	8	000	080	00	02.7	11.2	.	.	.	0-17 <sup>20</sup> ≡ 0 <sup>00</sup> 2 <sup>40</sup> 8 <sup>20</sup> F <sub>S</sub> 13 <sup>20</sup> 24 <sup>0</sup> ○		
7	0	08	10≡*	10≡	05.3	00.0	.	.	.	F <sub>E-N-NNE</sub> SW 0-24 <sup>0</sup> ≡ 8 <sup>45</sup> 24 <sup>1</sup> ≡ 9 <sup>45</sup> 10 <sup>05</sup> 18 <sup>05</sup> 9 <sup>55</sup> ≡ 10 <sup>45</sup> 12 <sup>20</sup> ≡ 12 <sup>45</sup> 13 <sup>30</sup> ≡ 13 <sup>30</sup> 14 <sup>30</sup> ○		
8	C	10≡	10≡	10≡	10	10.0	14.0	0.0	.	F <sub>E-N-NNE</sub> 0-24 <sup>0</sup> V <sub>300</sub> 9 <sup>00</sup> ○		
9	8	09	050	01	05.0	04.7	.	.	.	F <sub>E-N</sub> 0-16 <sup>00</sup> ≡ 0-4 <sup>55</sup> ○		
10	8	10	080	10	05.3	06.2	.	.	.	• 21 <sup>20</sup> 24 <sup>20</sup> ≡ 21 <sup>20</sup> 24 <sup>0</sup> ○		
11	8	010	06	00	02.3	06.7	00.2	.	.	≡ 0-3 <sup>45</sup> F <sub>S</sub> 0 <sup>10</sup> 8 <sup>00</sup> ○		
12	8	050	010	00	02.0	14.7	.	.	.	F <sub>NW</sub> 3 <sup>45</sup> 11 <sup>20</sup> ○		
13	P	000	000	00	00.0	14.8	.	.	.	○		
14	9	000	000	00	00.0	14.6	.	.	.	F <sub>E-SW</sub> 0 <sup>20</sup> ○		
15	9	000	000	00	00.0	13.8	.	.	.	F <sub>E-S</sub> 0-3 <sup>0</sup> ○		
16	9	000	010	00	00.3	14.5	.	.	.	○		
17	9	020	020	00	01.3	13.1	.	.	.	F <sub>E-SW</sub> 1 <sup>40</sup> 24 <sup>0</sup> ○		
18	9	000	040	00	01.3	13.5	.	.	.	F <sub>E-SW</sub> 0-05 <sup>45</sup> 23 <sup>45</sup> ○		
19	8	10≡	10	10≡*	10.0	01.3	00.0	.	.	≡ 0 <sup>05</sup> 9 <sup>45</sup> 14 <sup>00</sup> 24 <sup>0</sup> F <sub>SW</sub> 2 <sup>45</sup> 9 <sup>05</sup> ≡ 2 <sup>45</sup> 3 <sup>10</sup> 12 <sup>25</sup> 44 <sup>35</sup> 24 <sup>00</sup> 23 <sup>10</sup> ≡ 21 <sup>45</sup> 24 <sup>0</sup> ○		
20	0	10≡	10≡*	10≡*	10.0	00.0	03.2	.	.	≡ 0.24 <sup>0</sup> ≡ 0 <sup>00</sup> 3 <sup>45</sup> 12 <sup>45</sup> 23 <sup>20</sup> ≡ 12 <sup>45</sup> 23 <sup>20</sup> ≡ 0-2 <sup>45</sup> F <sub>NW</sub> 4 <sup>50</sup> 19 <sup>50</sup> ≡ 17 <sup>45</sup> 19 <sup>50</sup> ○		
21	0	10≡*	10≡	10≡	10.0	00.0	00.3	.	.	≡ 0-24 <sup>0</sup> F <sub>NW</sub> 1 <sup>40</sup> 24 <sup>0</sup> ≡ 2 <sup>45</sup> 17 <sup>45</sup> 14 <sup>45</sup> 20 <sup>45</sup> ○		
22	0	10≡*	10≡	10≡	10	00.0	01.0	.	.	≡ 0-24 <sup>0</sup> F <sub>E-SW</sub> 0-24 <sup>0</sup> ≡ 2 <sup>45</sup> 9 <sup>20</sup> 21 <sup>40</sup> 23 <sup>00</sup> ≡ 15 <sup>40</sup> 16 <sup>45</sup> ○		
23	0	10≡	10≡	10≡	10	00.0	00.1	.	.	≡ 0-24 <sup>0</sup> F <sub>NW</sub> 0-24 <sup>0</sup> ≡ 8 <sup>45</sup> 11 <sup>05</sup> ○		
24	8	10≡	07	01	06.0	05.4	00.0	.	.	≡ 0-7 <sup>45</sup> F <sub>NW</sub> 0-9 <sup>45</sup> ○		
25	8	010	020	02	01.7	13.3	.	.	.	F <sub>E-SW</sub> 0 <sup>20</sup> 16 <sup>00</sup> ○		
26	C	10≡	10≡	10≡	10.0	00.0	00.0	.	.	≡ 6-24 <sup>0</sup> 5 <sup>45</sup> 5 <sup>55</sup> ○		
27	9	000	000	00	00.0	14.5	.	.	.	≡ 0-0 <sup>30</sup> 4 <sup>00</sup> -10 <sup>00</sup> 5 <sup>45</sup> 9 <sup>20</sup> ○		
28	9	000	010	03	01.3	13.4	.	.	.	○		
29	9	010	020	00	01.0	12.4	.	.	.	≡ 18 <sup>40</sup> 19 <sup>40</sup> ○		
30	P	000	040	00	01.3	11.1	.	.	.	○		
31	8	000	050	00	01.7	11.2	.	.	.	≡ 2 <sup>30</sup> 7 <sup>30</sup> 21 <sup>40</sup> 24 <sup>0</sup> ≡ 15 <sup>40</sup> 16 <sup>20</sup> F <sub>N</sub> 15 <sup>40</sup> 16 <sup>20</sup> ○		
MES.	VRED.	04.4	05.4	03.8	04.5	256.4	15.8					

1	8	000	09	00	03.0	08.0	03.2	.	.	T 0-17 <sup>30</sup> 21 <sup>00</sup> 24 <sup>0</sup> ≡ 0 <sup>00</sup> 3 <sup>0</sup> 8 <sup>0</sup> F <sub>N</sub> 10 <sup>45</sup> 11 <sup>45</sup> 11 <sup>45</sup> 15 <sup>45</sup> ≡ 14 <sup>45</sup> 14 <sup>45</sup> ○	
2	8	000	020	00	00.7	14.1	02.5	.	.	≈ 0-7 <sup>40</sup> 24 <sup>0</sup> ○	
3	8	000	040	00	01.3	13.6	.	.	.	≈ 0-7 <sup>40</sup> ○	
4	P	000	050	00	01.7	10.8	.	.	.	○	
5	8	000	000	00	00.0	14.2	.	.	.	○	
6	0	10≡	10≡	10≡	10.0	01.1	.	.	.	≡ 5 <sup>45</sup> 24 <sup>0</sup> ○	
7	8	000	020	00	00.7	12.5	.	.	.	≡ 0-6 <sup>20</sup> F <sub>N</sub> 3-5 <sup>30</sup> ≡ 5 <sup>00</sup> 3 <sup>00</sup> 8 <sup>30</sup> ○	
8	P	000	030	03	02.0	13.0	.	.	.	F <sub>N</sub> 18 <sup>20</sup> 24 <sup>0</sup> ≡ 15 <sup>23</sup> 24 <sup>0</sup> ≡ 23 <sup>40</sup> 24 <sup>0</sup> ○	
9	6	09	10≡*	10≡	05.7	04.4	03.2	.	.	F <sub>E-SW</sub> SW 0-5 <sup>45</sup> ≡ 15 <sup>24</sup> 24 <sup>0</sup> ≡ 15 <sup>02</sup> 13 <sup>45</sup> 15 <sup>45</sup> ≡ 0-1 <sup>0</sup> 13 <sup>20</sup> 15 <sup>30</sup> ≡ 20 <sup>0</sup> 15 <sup>20</sup> 20 <sup>40</sup> ○	
10	8	030	040	00	02.3	12.8	03.6	.	.	F <sub>E-SW</sub> SW 0-5 <sup>30</sup> ≡ 19 <sup>30</sup> 24 <sup>0</sup> ≡ 0-2 <sup>30</sup> 5 <sup>00</sup> 3 <sup>00</sup> 9 <sup>0</sup> , ○	
11	0	10*	10≡*	10≡	10.0	00.0	15.8	.	.	F <sub>E-SSW-SW</sub> SW 0-24 <sup>0</sup> ≡ 4 <sup>05</sup> 7 <sup>02</sup> 14 <sup>40</sup> 14 <sup>40</sup> 13 <sup>45</sup> 6 <sup>55</sup> ≡ 8 <sup>45</sup> 5 <sup>45</sup> ≡ 8 <sup>15</sup> 24 <sup>0</sup> ○	
12	8	050	08	10≡	07.7	07.6	09.1	.	.	≡ 0-4 <sup>50</sup> 17 <sup>20</sup> 24 <sup>0</sup> F <sub>N</sub> 0-24 <sup>0</sup> ≡ 5 <sup>00</sup> 4 <sup>50</sup> 9 <sup>20</sup> ○	
13	8	10	06	00	05.3	07.0	00.2	.	.	F <sub>E-N</sub> 0-24 <sup>0</sup> ≡ 0-9 <sup>45</sup> ≡ 5 <sup>00</sup> 8 <sup>20</sup> ○	
14	8	00	01	00	00.3	13.7	00.0	.	.	F <sub>E-N</sub> 0-24 <sup>0</sup> ○	
15	8	00	04	00	01.3	12.8	.	.	.	F <sub>E-N-NNE</sub> 0-24 <sup>0</sup> ○	
16	7	10	08	10	05.3	04.9	.	.	.	F <sub>E-N-NNE</sub> 0-24 <sup>0</sup> ≡ 0 <sup>00</sup> 13 <sup>20</sup> 16 <sup>20</sup> 24 <sup>0</sup> ○	
17	8	00	01	00	00.3	13.3	.	.	.	≈ 0 <sup>30</sup> 8 <sup>10</sup> ≡ 0 <sup>00</sup> 13 <sup>20</sup> 16 <sup>20</sup> 24 <sup>0</sup> ○	
18	8	00	00	00	00.0	13.6	.	.	.	≈ 0 <sup>30</sup> 8 <sup>10</sup> ≡ 0 <sup>00</sup> 13 <sup>20</sup> 16 <sup>20</sup> 24 <sup>0</sup> ○	
19	8	00	01	00	00.3	13.2	.	.	.	○	
20	8	00	02	00	00.7	13.0	.	.	.	○	
21	8	04	08	04	05.3	06.7	.	.	.	T 13-15 <sup>05</sup> ≡ 15 <sup>05</sup> 16 <sup>20</sup> ○	
22	8	00	02	03	01.7	12.2	00.8	.	.	≈ 0 <sup>00</sup> 1-10 <sup>00</sup> 2 <sup>0</sup> 9 <sup>0</sup> T 20-12 <sup>15</sup> ○	
23	8	06	08	00	04.7	05.2	.	.	.	F <sub>NW</sub> 2-23 <sup>0</sup> ≡ 0 <sup>00</sup> 1-10 <sup>00</sup> 2 <sup>0</sup> 9 <sup>0</sup> ≡ 15 <sup>40</sup> 15 <sup>55</sup> ○	
24	8	08	06	10	08.0	03.3	00.0	.	.	F <sub>NW</sub> 4 <sup>00</sup> 12 <sup>00</sup> ≡ 4 <sup>00</sup> 24 <sup>00</sup> ≡ 0 <sup>00</sup> 6 <sup>00</sup> 17 <sup>00</sup> ≡ 10 <sup>20</sup> 12 <sup>0</sup> ○	
25	1	10	10	05	08.3	03.2	02.0	.	.	≈ 0-0 <sup>10</sup> 13-19 <sup>40</sup> ≡ 0 <sup>00</sup> 12 <sup>00</sup> 17 <sup>00</sup> ≡ 13 <sup>00</sup> 17 <sup>00</sup> 16 <sup>00</sup> ○	
26	8	04	10	02	05.3	04.1	05.2	.	.	≈ 0 <sup>00</sup> 0 <sup>20</sup> 10 <sup>20</sup> ≡ 0-3-SW 3-9 <sup>20</sup> 14 <sup>20</sup> 24 <sup>0</sup> ≡ 15 <sup>05</sup> 15 <sup>40</sup> 23 <sup>40</sup> 24 <sup>0</sup> ○	
27	8	08	10	08	08.7	02.0	10.4	.	.	≈ 0-2 <sup>40</sup> 16 <sup>20</sup> 19 <sup>40</sup> 23 <sup>40</sup> 24 <sup>0</sup> ≡ 0-9 <sup>40</sup> 22 <sup>00</sup> 24 <sup>0</sup> ≡ 0 <sup>00</sup> 4 <sup>20</sup> 6 <sup>20</sup> ○	
28	7	04	08	10	07.3	05.0	01.3	.	.	≈ 0-4 <sup>40</sup> 12 <sup>00</sup> 13 <sup>20</sup> 15 <sup>20</sup> 16 <sup>20</sup> 22 <sup>20</sup> ○	
29	8	07	05	02	04.7	06.9	21.3	.	.	F <sub>E-SW</sub> 0-24 <sup>0</sup> ≡ 0 <sup>00</sup> 2 <sup>20</sup> 14 <sup>40</sup> 16 <sup>40</sup> 16 <sup>45</sup> ≡ 24 <sup>20</sup> 24 <sup>0</sup> ≡ 16 <sup>40</sup> 16 <sup>45</sup> 16 <sup>45</sup> ○	
30	0	00	10	10	06.7	07.6	14.2	.	.	F <sub>E-SW</sub> 0-11 <sup>20</sup> ≡ 0-6 <sup>40</sup> ≡ 4 <sup>20</sup> 8 ≡ 13 <sup>00</sup> 14 <sup>20</sup> 18 <sup>20</sup> 20 <sup>20</sup> ○	
31	8	00	03	02	01.7						

$\varphi = 43^{\circ}43'$  N  $\lambda = 18^{\circ}16'$  E Gr.  $\Delta G = +1h\ 13\ min.$ 

BR. ST. 141

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost v%				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	597.0	597.5	597.3	09.4	12.0	09.8	10.2	12.8	08.0	-	05.3	06.6	05.9	60	63	64	62	N	4	S	7	SW	7
2	596.9	597.9	598.4	09.0	12.4	10.0	10.4	12.8	08.4	-	07.6	07.1	08.4	89	65	91	82	SW	6	SW	7	SW	7
3	598.2	598.4	598.1	10.0	13.2	06.4	09.0	13.2	06.4	-	06.3	07.9	05.5	69	70	76	72	SW	6	SW	6	SW	6
4	597.0	596.8	597.0	11.8	14.6	05.0	11.1	14.6	06.4	-	05.4	07.4	06.9	52	59	80	64	SW	7	SW	4	SW	5
5	597.3	598.7	597.9	05.4	07.6	10.0	08.2	10.0	05.0	-	06.4	06.4	02.1	95	81	23	66	N	5	N	2	N	2
6	596.4	594.9	592.5	13.2	14.6	12.2	13.0	14.6	09.4	-	02.5	04.4	02.9	22	35	27	28	NW	1	-	0	SW	3
7	589.1	590.2	591.9	06.6	07.0	05.2	06.0	12.4	04.6	-	06.4	07.5	06.6	88	100	100	96	SW	7	SW	2	N	2
8	594.2	597.1	599.2	05.0	06.0	06.4	06.0	07.2	05.0	-	06.5	07.0	07.2	100	100	100	100	NW	4	N	2	SW	3
9	600.3	601.8	601.6	09.4	13.0	10.4	10.8	13.2	06.4	-	06.6	06.0	07.3	74	54	77	68	-	0	S	2	S	3
10	601.1	601.7	601.9	10.0	12.6	10.0	10.6	13.4	09.0	-	06.9	07.8	09.2	75	71	100	82	S	4	N	1	N	3
11	602.2	602.5	602.4	04.0	07.0	06.2	05.8	10.0	03.6	-	06.1	07.5	07.1	100	100	100	100	N	5	NNE	3	E	3
12	600.8	601.2	601.4	08.0	12.0	09.0	09.5	12.0	06.0	-	06.8	07.2	07.4	84	69	86	80	S	4	-	0	-	0
13	600.3	600.7	600.6	10.0	11.0	10.0	10.2	12.2	08.7	-	05.4	06.2	07.0	59	63	76	66	SW	2	N	1	-	0
14	600.2	600.4	599.5	08.8	10.0	07.2	08.3	12.0	07.2	-	06.1	08.0	07.6	71	87	100	86	S	1	-	0	N	3
15	599.3	598.6	598.9	08.6	09.4	07.8	08.4	09.6	07.2	-	03.0	07.2	07.9	35	81	100	72	NNE	5	R	4	N	3
16	599.4	599.3	599.6	06.9	08.2	07.0	07.2	08.4	06.4	-	07.4	05.8	06.0	100	71	80	84	N	4	NNF	2	E	3
17	599.1	599.9	599.6	08.4	11.4	08.4	09.2	11.8	06.8	-	05.0	05.6	05.5	61	55	67	61	SW	5	SSW	3	SW	5
18	599.5	599.7	599.5	08.8	11.2	09.0	09.5	11.2	07.4	-	04.9	05.8	07.3	57	58	84	66	SSW	3	SW	2	SW	2
19	598.8	598.7	598.2	07.6	09.4	07.2	07.8	09.6	07.2	-	07.6	06.6	07.6	98	74	100	91	NNW	5	N	4	-	0
20	595.5	594.3	592.7	07.8	10.4	06.4	07.8	10.8	06.4	-	06.5	06.2	07.0	82	65	98	82	SSW	5	S	7	5	11
21	592.5	593.2	593.2	05.6	07.8	07.2	07.0	08.2	05.4	-	06.8	07.9	07.6	100	100	100	100	S	7	S	7	S	7
22	592.4	594.3	594.9	07.0	07.2	06.8	07.0	07.4	06.2	-	07.5	07.6	07.4	100	100	100	100	SSW	8	SW	8	SSW	8
23	594.6	594.8	593.0	06.8	07.4	05.6	06.4	08.0	05.6	-	07.4	07.2	06.8	100	93	100	98	SSW	5	SW	8	SW	8
24	590.8	590.8	586.8	05.2	06.0	04.8	05.2	06.0	04.8	-	06.6	07.0	06.5	100	100	100	100	SW	10	SW	8	SW	8
25	584.7	583.6	592.5	04.2	03.0	01.2	02.4	05.0	01.2	-	06.2	05.7	05.0	100	100	100	100	SW	9	SW	8	SW	8
26	578.9	577.7	563.0	00.9	-01.6	-02.8	-01.6	01.8	-02.8	-	04.9	04.1	03.6	100	100	97	99	NW	8	NW	8	NW	0
27	587.5	592.8	595.0	-03.0	-02.2	-01.0	-01.8	01.0	-03.0	-	03.6	03.8	04.3	97	98	100	98	NW	10	NW	7	NW	2
28	594.3	594.1	594.0	00.9	03.6	03.0	02.6	04.6	-01.0	-	04.3	04.4	04.6	88	74	81	81	-	0	SW	4	SW	4
29	592.2	593.2	594.0	03.4	05.0	04.8	04.5	05.8	03.0	-	03.8	05.4	06.3	66	82	97	82	SW	8	SW	8	SW	9
30	593.1	593.1	593.2	05.0	06.4	04.2	05.0	06.4	04.0	-	06.5	07.2	06.2	100	100	100	100	SW	8	SW	9	SW	6
MES.	VRFD.			595.4	595.9	595.9	06.8	08.5	06.7	07.2	09.5	05.3	-	05.9	06.5	06.4	81	79	87	E2	5.2	4.5	4.7

1	592.1	592.1	592.1	01.8	C2.2	-00.6	C0.7	04.2	-00.6	-	05.2	C5.1	04.4	100	94	100	98	SW	5	S	4	4	
2	590.2	598.5	587.9	-02.0	01.0	-00.6	-00.6	02.2	-02.0	-	04.0	04.9	04.4	100	100	100	100	SW	7	SW	8	N	2
3	591.5	593.8	594.6	-02.4	-01.2	-C1.4	-01.6	-00.6	-02.4	-	03.8	04.2	03.7	98	100	89	96	SW	4	SW	6	SW	8
4	593.7	595.2	596.2	-00.6	02.4	03.0	02.0	03.0	-01.4	-	03.4	05.4	03.6	78	100	63	80	SW	9	SW	6	W	3
5	593.6	593.1	592.0	03.4	04.0	04.3	04.0	04.3	02.4	-	05.8	06.1	06.2	100	100	100	100	SW	7	SSW	6	SSW	6
6	589.0	590.1	591.7	04.0	02.0	-00.8	01.1	04.4	-00.8	-	06.1	05.3	04.3	100	100	100	100	SSW	5	SSW	5	SW	5
7	590.0	589.4	589.0	01.0	03.0	04.0	C3.0	04.2	-00.8	-	04.9	05.7	06.1	100	100	100	100	SW	4	SSW	5	S	2
8	586.0	585.7	589.0	01.2	00.8	00.0	00.5	04.2	-00.2	-	05.0	04.9	04.6	100	100	100	100	SSW	8	SSW	12	SW	6
9	588.8	589.5	590.1	-01.0	00.1	-C0.2	-00.3	00.4	-01.2	-	04.2	04.4	04.5	99	95	100	98	SSW	11	SSW	11	SW	6
10	592.0	593.7	594.4	-01.6	-00.2	-01.8	-01.4	00.6	-02.8	-	03.7	03.8	03.3	92	84	82	86	SW	6	SW	5	S	5
11	593.7	594.3	594.4	00.0	01.2	00.6	00.6	01.6	-C1.8	-	03.7	04.2	04.5	81	84	94	86	SSW	4	SW	7	SSW	8
12	594.8	593.4	592.1	01.2	02.8	03.5	02.8	03.5	-00.2	-	04.9	04.2	05.9	97	75	100	91	SSW	7	S	8	SSW	11
13	591.5	592.0	592.0	05.2	04.8	03.2	04.1	05.4	03.0	-	06.6	06.5	05.8	100	100	100	100	SSW	8	SSW	6	SSW	6
14	590.6	590.6	591.2	03.8	03.8	03.6	03.7	04.4	03.2	-	06.0	06.0	05.9	100	100	100	100	S	5	SSW	7	SW	3
15	590.5	589.9	587.9	03.6	04.8</td																		

BR. ST. 141

$$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intensiteta broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w			
		14	7	14	21	Sred Dies				7	7		
1	8	07	08 0	04	06.3	06.9	.	.	.	0-8 <sup>10</sup> E E s-ssw-sw 0 <sup>20</sup> 5 <sup>30</sup> 11 <sup>30</sup> 24 <sup>0</sup> 10 <sup>20</sup> 10 <sup>20</sup> 0			
2	8	10 <sup>30</sup>	08 0	C2	06.7	03.8	08.2	.	.	F <sub>sw</sub> 0-24, $\equiv 4^{20} 10^{20} \cdot 4^0 19^{40} 24, 0$			
3	8	04 0	08 0	01	04.3	07.5	.	.	.	F <sub>ssw-sw</sub> 0-24, $\Delta 0-8^{30}$			
4	8	06	06	10 <sup>30</sup>	07.3	09.1	.	.	.	F E s-ssw-sw 0-17 <sup>45</sup> 13 <sup>45</sup> 8 <sup>45</sup> 19 <sup>20</sup> 20 <sup>45</sup> $\Delta 19^{20} 19^{45}$ $\equiv 17^{45} 24$ $\bullet 22^{45} 24$			
5	9	03 0	02 0	CC	01.7	11.2	06.2	.	.	$\equiv 0-4^{15}$ , $\bullet 1^{10} 0^{15}$ , $\# 300-600$ , $\Delta 20-1125$			
6	9	00 0	00 0	C1	00.3	09.4	.	.	.	# 300-600 5 <sup>45</sup> 11 <sup>45</sup> E F <sub>sw</sub> 21 <sup>40</sup> 24, 0			
7	9	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	.	.	.	F F <sub>sw</sub> 0-18 <sup>40</sup> $\equiv 12^{40} 24$ $\bullet 8^{25} 18^{45}$			
8	9	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.6	03.3	.	.	$\equiv 300-600 0^{10} 10^{20}$ $\Delta 1^{45} 6^{45} \# 1^{45} 2^{45}$ $\# 300-600 12^{40} 24$			
9	8	00 0	02 0	00	CC.7	12.1	.	.	.	# 300-600 3-8 <sup>30</sup> $\equiv 10^{40} 24$ , $\bullet 19^{40} 23$ , 0			
10	8	00 0	06 0	10 <sup>30</sup>	05.3	09.3	.	.	.	A 0 <sup>40</sup> 7 <sup>30</sup> # 300-3-8 <sup>30</sup> $\equiv 10^{40} 24$ , $\bullet 19^{40} 23$ , 0			
11	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	C7.4	.	.	= 0-24, F E s-ssw-sw 0-8 <sup>00</sup>			
12	8	02 0	05 0	00	02.3	08.8	.	.	.	= 0-5 <sup>10</sup> # 300-5 <sup>40</sup> 11 <sup>20</sup> 20 <sup>45</sup> 24, $\Delta 20-24$ , 0			
13	8	00 0	03 0	00	01.0	10.1	.	.	.	A 0-8 <sup>20</sup> 20 <sup>30</sup> 24, $\# 300-500$ , $\Delta 11-20-24$			
14	6	00 0	03 0	10 <sup>30</sup>	04.3	11.1	.	.	.	A 0-8 <sup>20</sup> # 300-0-11-20-23-24, $\equiv 16^{45} 23$ , 0			
15	8	00 0	05 0	10 <sup>30</sup>	05.0	10.2	.	.	.	# 300-0-11, $\Delta K^{45} 24$ , 0			
16	8	10 <sup>30</sup>	04 0	00	04.7	06.7	.	.	.	# 300-0-10 <sup>30</sup> F <sub>ssw-sw</sub> 0-24 <sup>0</sup> 8 <sup>40</sup> 15 <sup>30</sup> 17 <sup>20</sup> 20 <sup>40</sup> 24 <sup>0</sup> 24 <sup>0</sup>			
17	8	02 0	09 0	00	03.7	08.6	.	.	.	F <sub>sw</sub> 0-12 <sup>40</sup> $\equiv 4^{40} 2^{40} 14^{40}$ $\# 300-600 12^{40} 24$			
18	8	01 0	09	10 <sup>30</sup>	06.7	05.9	.	.	.	A 0-8 <sup>20</sup> 20 <sup>30</sup> 24, $\# 300-500$ , $\Delta 15^{40} 20$ , $\# F_{sw}$ 23 <sup>20</sup> 24			
19	8	00 0	04 0	00	01.3	06.0	.	.	.	A 0-8 <sup>20</sup> 20 <sup>30</sup> 24, $\# 300-500$ , $\Delta 15^{40} 20$ , $\# F_{sw}$ 23 <sup>20</sup> 24, $\# 20^{40} 24$ , $\equiv 21^{45} 24$			
20	8	01	10	10 <sup>30</sup>	07.0	04.2	.	.	.				
21	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	21.4	.	.	F E s-24, $\equiv 0-24$ , $\bullet 0-8^{40} 16^{30} 17^{45} 23^{20} 24$			
22	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	22.5	.	.	F E s-24, $\equiv 0-24$ , $\bullet 0-3, 13^{20} 17^{20}$ , $\# 3-5^{40} 10^{40} 13^{20}$ , $\bullet 0-9^{20} 14^{40}$			
23	8	10	10	10 <sup>30</sup>	10.0	00.0	C5.4	.	.	F E s-24, $\equiv 0-5^{45} 14^{30} 21$ , $\# 3^{20} 3^{30} 8^{40} 12^{40}$			
24	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	00.0	.	.	F E s-24, $\equiv 0-9^{45} 12^{20} 24$ , $\# 14^{20} 5^{40}$			
25	0	10 <sup>30</sup>	10 <sup>30</sup>	05	08.3	00.0	05.0	.	.	F E s-24, $\equiv 0-20^{45} 23^{20} 24$ , $\# 0-0^{40} 15^{40} 18^{45} + 12^{40} 12^{45} 24$			
26	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	01.4	C2	.	# 300-0-10 <sup>30</sup> F E s-24, $\equiv 0-20^{45} 18^{45} 11^{40} 20^{40}$ , $\# 0-3^{40} 17^{40} 24$			
27	9	10 <sup>30</sup>	05	00	05.0	05.0	C1.5	C8	.	$\equiv 300-600 4^{45} 11^{45}$ F E s-24, $\# 0-17^{45} 17^{45}$			
28	9	00 0	00 0	00	00.0	10.6	.	02	.	F E s-20 <sup>20</sup> 24, $\equiv 20^{40} 24$			
29	9	04 0	10	10 <sup>30</sup>	08.0	04.4	.	.	.	F E s-0-24, $\equiv 0-24$ , $\bullet 10^{20} 10^{20}$			
30	0	10 <sup>30</sup>	10 <sup>30</sup>	10 <sup>30</sup>	10.0	00.0	.	.	.				

BIBLIOTECA

1974 CKTCBAR

$\varphi = 43^{\circ}43'$ ,  $N \lambda = 18^{\circ}16'$ , E Gr.,  $\Delta G = +1h\ 13\ min.$ 

BK. ST. 141

D G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vетра D, f (0-12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	582.7	583.6	585.1	-06.0	-04.2	-09.8	-08.7	-04.6	-05.8	-	02.8	02.1	02.0	94	91	91	92	N	2	N	7	N	10
2	583.6	584.1	590.6	-10.2	-05.0	-04.8	-06.2	-04.8	-10.4	-	01.9	03.0	02.9	90	95	92	92	NNW	5	WSW	0	SW	6
3	591.4	592.4	592.8	-06.8	-05.4	-04.8	-05.4	-03.6	-07.4	-	02.5	02.7	02.9	89	87	92	89	NNW	6	WSW	2	SW	2
4	591.4	591.4	591.1	-04.2	-02.0	-02.0	-02.6	-02.0	-04.8	-	03.2	03.9	03.9	96	98	98	97	SW	5	SW	7	SW	9
5	591.6	592.4	594.3	-03.4	-01.2	-01.2	-01.8	-01.2	-03.4	-	03.5	04.2	04.2	97	95	98	98	SW	0	SW	8	SW	8
6	596.0	596.4	598.3	-01.0	-00.8	-00.4	-00.6	-00.4	-01.2	-	04.2	04.3	04.4	95	99	100	99	SW	7	SW	8	NW	3
7	595.3	593.4	592.2	-01.6	-03.2	-03.4	-02.9	-00.4	-03.4	-	04.0	03.5	03.5	98	97	97	97	NW	4	NW	4	NW	5
8	591.1	589.6	591.1	-05.0	-06.0	-06.4	-06.0	-03.4	-06.4	-	03.0	02.8	02.7	95	94	94	94	NW	5	NW	7	NW	7
9	592.0	592.4	593.2	-05.8	-04.8	-04.8	-05.0	-04.4	-06.8	-	02.8	03.1	03.1	94	95	95	95	NW	9	N	8	N	8
10	594.2	594.2	594.5	-02.0	-02.0	-03.0	-02.5	-02.0	-04.8	-	03.2	03.2	02.9	82	82	80	81	-	0	SW	2	-	0
11	595.7	596.0	596.4	-04.0	-00.8	-00.8	-01.6	-00.6	-04.2	-	02.7	04.2	04.2	78	96	96	90	-	0	SSW	4	SSW	3
12	595.1	594.3	593.9	-01.0	00.0	00.0	00.0	00.0	-01.2	-	03.6	04.5	04.4	85	98	99	94	SW	7	SW	7	SW	8
13	594.6	595.5	596.6	-08.6	-00.2	00.0	00.2	00.0	-01.6	-	04.1	04.4	04.4	93	97	97	96	SW	5	SW	4	SW	4
14	590.3	590.2	596.6	-01.0	-00.2	-01.0	00.0	-02.0	-	04.0	04.4	04.2	98	97	99	98	SW	6	SW	8	SW	8	
15	597.7	597.8	598.3	-00.2	01.0	00.8	00.6	01.4	-01.2	-	04.4	04.6	04.3	97	94	88	93	N	4	SW	7	SW	5
16	597.5	596.4	597.9	00.8	01.6	01.0	01.1	02.0	00.6	-	03.8	04.4	04.1	79	85	83	82	SSW	7	SSW	8	SSW	7
17	599.1	599.3	599.3	03.0	02.6	02.2	02.5	04.2	00.6	-	02.1	03.6	03.1	37	65	58	53	N	3	SW	2	SW	3
18	598.5	598.6	598.1	02.2	05.0	05.2	04.4	07.4	01.2	-	03.5	02.4	03.9	65	27	58	53	SW	7	W	2	-	0
19	594.2	590.2	592.5	01.0	01.0	-00.2	00.4	05.2	-00.2	-	03.8	04.5	04.5	76	91	100	89	SSW	11	SSW	13	WSW	11
20	594.9	595.3	596.1	-02.0	-00.4	-01.2	-01.2	-00.2	-03.0	-	01.9	03.0	02.3	47	68	55	57	NW	2	SW	6	SW	5
21	595.4	593.6	593.5	-01.4	-01.0	-01.4	-01.4	-00.4	-02.4	-	03.4	04.2	04.1	P2	99	99	93	SW	5	SW	6	SW	4
22	593.6	594.4	594.6	-02.0	-01.6	-02.0	-02.2	-01.0	-03.0	-	03.6	04.0	03.2	97	98	80	92	N	3	WSW	2	W	5
23	594.7	594.3	593.4	00.0	01.6	00.2	00.5	02.2	-02.4	-	01.9	03.1	04.7	42	60	100	67	NWW	3	-	0	SSW	4
24	593.5	593.4	593.4	-03.5	-02.4	-01.2	-02.1	00.2	-03.5	-	03.4	01.8	04.2	97	98	99	98	NHE	2	-	0	SW	5
25	591.5	590.1	588.5	-02.0	-00.4	-00.4	-00.8	00.0	-03.2	-	03.9	04.5	04.5	98	100	99	99	SSW	8	SSW	9	SSW	10
26	587.8	587.1	587.9	-01.0	-02.4	-04.0	-02.0	-00.4	-04.0	-	04.2	03.8	03.3	99	98	96	98	WSW	4	SW	4	SW	4
27	585.0	584.6	586.8	-07.0	-03.6	-06.8	-06.0	-03.6	-07.0	-	02.5	03.4	02.6	93	97	94	95	SW	5	SW	4	-	0
28	580.9	573.2	577.1	-04.0	-02.2	-05.6	-04.4	-00.2	-06.8	-	03.3	03.8	02.9	96	98	95	96	SW	8	SW	14	NW	8
29	580.8	582.0	584.0	-09.2	-07.8	-05.2	-06.8	-05.2	-09.2	-	02.1	02.4	03.0	91	93	95	93	NW	6	W	3	SW	5
30	595.7	598.6	590.1	-07.8	-08.2	-08.2	-08.1	-05.6	-08.2	-	02.4	02.3	02.3	93	92	92	92	NW	7	NH	2	NH	3
MES. VRKD.	592.2	591.8	592.6	-02.9	-01.9	-02.3	-02.4	-00.7	-04.0	-	C3.2	C3.6	C3.6	86	90	91	89	4.9	5.5	5.4			

1	589.8	592.5	595.1	-06.0	-06.0	-05.0	-05.5	-05.0	-07.8	-	02.8	02.8	03.0	94	94	95	94	SW	10	SW	7	NW	3
2	595.6	594.8	596.8	-05.6	-04.0	-04.0	-04.4	-04.0	-05.6	-	02.9	03.3	03.3	95	96	96	96	-	0	NW	8	NW	7
3	596.5	597.2	597.8	-04.0	-02.0	-01.6	-02.3	-01.4	-04.0	-	03.3	03.9	04.0	96	98	98	97	NW	9	N	9	N	9
4	597.5	596.5	595.5	-01.8	01.4	-02.8	-02.8	-02.1	-01.0	-	03.9	04.1	03.6	98	99	97	98	N	8	N	6	N	6
5	592.7	591.1	589.7	-03.7	-02.8	-00.8	-01.9	-00.8	-03.6	-	03.5	03.5	04.0	97	94	93	95	N	5	-	0	SW	5
6	589.2	589.6	589.8	-07.0	-09.0	-08.4	-08.2	-00.6	-10.4	-	02.5	02.1	02.2	93	92	92	92	N	7	N	5	N	5
7	583.7	590.3	590.2	-06.9	-05.6	-04.8	-05.5	-04.4	-08.4	-	02.6	02.9	03.1	94	95	95	95	N	7	NW	7	NW	7
8	589.4	588.0	586.8	-03.4	-02.4	-03.2	-03.0	-02.0	-05.0	-	03.2	03.8	03.5	90	98	97	95	WNN	7	NW	11	N	12
9	589.8	591.0	593.1	-04.0	-02.8	-02.4	-02.9	-02.4	-04.4	-	03.3	03.6	03.8	96	97	98	97	N	8	N	11	N	9
10	594.6	595.3	595.9	-01.4	00.8	-02.0	-02.0	-01.6	-07.6	-	04.1	04.2	03.9	95	96	98	98	N	6	NWW	4	N	5
11	594.8	589.5	586.1	-01.0	-02.0	-02.4	-02.0	-01.2	-02.6	-	03.9	03.9	03.8	93	98	98	96	SW	5	SW	9	SW	9
12	586.1	585.5	584.1	-02.4	-02.4	-04.6	-03.5	-02.2	-04.6	-	03.8	03.8	03.1	98	98	96	97	SSW	9	-	0	SSW	6
13	581.2	582.1	582.0	-01.6	-04.0	-10.0	-06.4	-01.6	-10.0	-	04.0	03.3	01.9	98	96	91	95	SSW	8	SSW	7	N	6
14	583.5	583.2	584.1	-12.0	-12.4	-13.0	-12.6	-10.0	-13.0	-	01.6	01.6	01.5	89	89	88	89	N	11	N	10	N	11
15	583.5	584.8	585.3	-12.6	-11.4	-10.4	-11.2	-10.4	-13.0	-	01.5	01.7	01.9	88	89	90	89	N	11	N	10	N	10
16	586.3	588.6	589.1	-09.4	-09.4	-10.0	-05.7	-09.0	-10.4														

BR. ST. 141

 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijeme V. o.	Oblačnost N (0-10)					Intensitet sunc broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	0	10*=	10=	10=	10=	10.0	00.0	07.8	68	V0-24, $\equiv 0-24, F_{N-SW} 0-24, + + 0-24, * 0-24, 8$ [X]	
2	0	040	10=	10=	08.0	05.9	00.6	67	V0-24, $\equiv 0-625, 13.5-24, F_{N-SW-NW} 0-24, + + 0-24, * 0-24, 6-11.5-11.5-23, [X], O$		
3	8	08	030	10=	07.0	08.2	00.8	65	V0-24, $\equiv 0-2-20-24, F_{N-SW-NW} 0-24, + + 0-9.5$ [X]		
4	0	10=	10=	10=	10.0	00.0	.	65	V0-24, $\equiv 0-24, F_{N-SW} 7.5-24, * 17.5-18.5-18.5-24, [X]$		
5	0	10=	10=	10=	10=	10.0	00.0	00.1	65	V0-24, $F_{N-SW} 0-24, \equiv 0-24, + + 0-24, [X]$	
6	0	10=	10=	10	10.0	00.0	.	65	V0-24, $F_{N-SW} 0-18^{\circ}, \equiv 0-18^{\circ}, + + 0-18^{\circ}$ [X]		
7	0	10=	10*=	10=	10.0	00.0	.	67	V0-24, $\equiv 0-24, F_{N-SW} 19.5-24, [X]$		
8	0	10=	10=	10*=	10.0	00.0	01.9	70	V0-24, $\equiv 0-24, * 0-4.5-4.5, F_{N-SW} 7.5-24, + + 0-7.5-24, [X]$		
9	0	10*=	10=	10=	10.0	00.0	03.3	78	V0-24, $F_{N-SW-NW} 0-24, * 0-9.5-9.5-24, [X]$		
10	9	000	000	00	00.0	C9.4	00.1	78	V0-24, $F_{N-SW-NW} 0-12.5, \equiv 0-12.5-4-0-12.5-4-0-12.5-4-12.5-12.5, [X], O$		
11	9	000	040	00	01.3	09.7	.	75	V0-10-20-30-40-50-60-70-80-90-100-110-120-130-140-150-160-170-180-190-200-210-220-230-240-250-260-270-280-290-300-310-320-330-340-350-360-370-380-390-400-410-420-430-440-450-460-470-480-490-500-510-520-530-540-550-560-570-580-590-600-610-620-630-640-650-660-670-680-690-700-710-720-730-740-750-760-770-780-790-800-810-820-830-840-850-860-870-880-890-900-910-920-930-940-950-960-970-980-990-1000-1010-1020-1030-1040-1050-1060-1070-1080-1090-1100-1110-1120-1130-1140-1150-1160-1170-1180-1190-1200-1210-1220-1230-1240-1250-1260-1270-1280-1290-1300-1310-1320-1330-1340-1350-1360-1370-1380-1390-1400-1410-1420-1430-1440-1450-1460-1470-1480-1490-1500-1510-1520-1530-1540-1550-1560-1570-1580-1590-1600-1610-1620-1630-1640-1650-1660-1670-1680-1690-1700-1710-1720-1730-1740-1750-1760-1770-1780-1790-1800-1810-1820-1830-1840-1850-1860-1870-1880-1890-1900-1910-1920-1930-1940-1950-1960-1970-1980-1990-2000-2010-2020-2030-2040-2050-2060-2070-2080-2090-2100-2110-2120-2130-2140-2150-2160-2170-2180-2190-2200-2210-2220-2230-2240-2250-2260-2270-2280-2290-2300-2310-2320-2330-2340-2350-2360-2370-2380-2390-2400-2410-2420-2430-2440-2450-2460-2470-2480-2490-2500-2510-2520-2530-2540-2550-2560-2570-2580-2590-2600-2610-2620-2630-2640-2650-2660-2670-2680-2690-2700-2710-2720-2730-2740-2750-2760-2770-2780-2790-2800-2810-2820-2830-2840-2850-2860-2870-2880-2890-2900-2910-2920-2930-2940-2950-2960-2970-2980-2990-3000-3010-3020-3030-3040-3050-3060-3070-3080-3090-3010-3020-3030-3040-3050-3060-3070-3080-3090-3100-3110-3120-3130-3140-3150-3160-3170-3180-3190-3110-3120-3130-3140-3150-3160-3170-3180-3190-3200-3210-3220-3230-3240-3250-3260-3270-3280-3290-3210-3220-3230-3240-3250-3260-3270-3280-3290-3300-3310-3320-3330-3340-3350-3360-3370-3380-3390-3310-3320-3330-3340-3350-3360-3370-3380-3390-3400-3410-3420-3430-3440-3450-3460-3470-3480-3490-3410-3420-3430-3440-3450-3460-3470-3480-3490-3500-3510-3520-3530-3540-3550-3560-3570-3580-3590-3510-3520-3530-3540-3550-3560-3570-3580-3590-3600-3610-3620-3630-3640-3650-3660-3670-3680-3690-3610-3620-3630-3640-3650-3660-3670-3680-3690-3700-3710-3720-3730-3740-3750-3760-3770-3780-3790-3710-3720-3730-3740-3750-3760-3770-3780-3790-3800-3810-3820-3830-3840-3850-3860-3870-3880-3890-3810-3820-3830-3840-3850-3860-3870-3880-3890-3900-3910-3920-3930-3940-3950-3960-3970-3980-3990-3910-3920-3930-3940-3950-3960-3970-3980-3990-4000-4010-4020-4030-4040-4050-4060-4070-4080-4090-4010-4020-4030-4040-4050-4060-4070-4080-4090-4100-4110-4120-4130-4140-4150-4160-4170-4180-4190-4110-4120-4130-4140-4150-4160-4170-4180-4190-4200-4210-4220-4230-4240-4250-4260-4270-4280-4290-4210-4220-4230-4240-4250-4260-4270-4280-4290-4300-4310-4320-4330-4340-4350-4360-4370-4380-4390-4310-4320-4330-4340-4350-4360-4370-4380-4390-4400-4410-4420-4430-4440-4450-4460-4470-4480-4490-4410-4420-4430-4440-4450-4460-4470-4480-4490-4500-4510-4520-4530-4540-4550-4560-4570-4580-4590-4510-4520-4530-4540-4550-4560-4570-4580-4590-4600-4610-4620-4630-4640-4650-4660-4670-4680-4690-4610-4620-4630-4640-4650-4660-4670-4680-4690-4700-4710-4720-4730-4740-4750-4760-4770-4780-4790-4710-4720-4730-4740-4750-4760-4770-4780-4790-4800-4810-4820-4830-4840-4850-4860-4870-4880-4890-4810-4820-4830-4840-4850-4860-4870-4880-4890-4900-4910-4920-4930-4940-4950-4960-4970-4980-4990-4910-4920-4930-4940-4950-4960-4970-4980-4990-5000-5010-5020-5030-5040-5050-5060-5070-5080-5090-5010-5020-5030-5040-5050-5060-5070-5080-5090-5100-5110-5120-5130-5140-5150-5160-5170-5180-5190-5110-5120-5130-5140-5150-5160-5170-5180-5190-5200-5210-5220-5230-5240-5250-5260-5270-5280-5290-5210-5220-5230-5240-5250-5260-5270-5280-5290-5300-5310-5320-5330-5340-5350-5360-5370-5380-5390-5310-5320-5330-5340-5350-5360-5370-5380-5390-5400-5410-5420-5430-5440-5450-5460-5470-5480-5490-5410-5420-5430-5440-5450-5460-5470-5480-5490-5500-5510-5520-5530-5540-5550-5560-5570-5580-5590-5510-5520-5530-5540-5550-5560-5570-5580-5590-5600-5610-5620-5630-5640-5650-5660-5670-5680-5690-5610-5620-5630-5640-5650-5660-5670-5680-5690-5700-5710-5720-5730-5740-5750-5760-5770-5780-5790-5710-5720-5730-5740-5750-5760-5770-5780-5790-5800-5810-5820-5830-5840-5850-5860-5870-5880-5890-5810-5820-5830-5840-5850-5860-5870-5880-5890-5900-5910-5920-5930-5940-5950-5960-5970-5980-5990-5910-5920-5930-5940-5950-5960-5970-5980-5990-6000-6010-6020-6030-6040-6050-6060-6070-6080-6090-6010-6020-6030-6040-6050-6060-6070-6080-6090-6100-6110-6120-6130-6140-6150-6160-6170-6180-6190-6110-6120-6130-6140-6150-6160-6170-6180-6190-6200-6210-6220-6230-6240-6250-6260-6270-6280-6290-6210-6220-6230-6240-6250-6260-6270-6280-6290-6300-6310-6320-6330-6340-6350-6360-6370-6380-6390-6310-6320-6330-6340-6350-6360-6370-6380-6390-6400-6410-6420-6430-6440-6450-6460-6470-6480-6490-6410-6420-6430-6440-6450-6460-6470-6480-6490-6500-6510-6520-6530-6540-6550-6560-6570-6580-6590-6510-6520-6530-6540-6550-6560-6570-6580-6590-6600-6610-6620-6630-6640-6650-6660-6670-6680-6690-6610-6620-6630-6640-6650-6660-6670-6680-6690-6700-6710-6720-6730-6740-6750-6760-6770-6780-6790-6710-6720-6730-6740-6750-6760-6770-6780-6790-6800-6810-6820-6830-6840-6850-6860-6870-6880-6890-6810-6820-6830-6840-6850-6860-6870-6880-6890-6900-6910-6920-6930-6940-6950-6960-6970-6980-6990-6910-6920-6930-6940-6950-6960-6970-6980-6990-7000-7010-7020-7030-7040-7050-7060-7070-7080-7090-7010-7020-7030-7040-7050-7060-7070-7080-7090-7100-7110-7120-7130-7140-7150-7160-7170-7180-7190-7110-7120-7130-7140-7150-7160-7170-7180-7190-7200-7210-7220-7230-7240-7250-7260-7270-7280-7290-7210-7220-7230-7240-7250-7260-7270-7280-7290-7300-7310-7320-7330-7340-7350-7360-7370-7380-7390-7310-7320-7330-7340-7350-7360-7370-7380-7390-7400-7410-7420-7430-7440-7450-7460-7470-7480-7490-7410-7420-7430-7440-7450-7460-7470-7480-7490-7500-7510-7520-7530-7540-7550-7560-7570-7580-7590-7510-7520-7530-7540-7550-7560-7570-7580-7590-7600-7610-7620-7630-7640-7650-7660-7670-7680-7690-7610-7620-7630-7640-7650-7660-7670-7680-7690-7700-7710-7720-7730-7740-7750-7760-7770-7780-7790-7710-7720-7730-7740-7750-7760-7770-7780-7790-7800-7810-7820-7830-7840-7850-7860-7870-7880-7890-7810-7820-7830-7840-7850-7860-7870-7880-7890-7900-7910-7920-7930-7940-7950-7960-7970-7980-7990-7910-7920-7930-7940-7950-7960-7970-7980-7990-8000-8010-8020-8030-8040-8050-8060-8070-8080-8090-8010-8020-8030-8040-8050-8060-8070-8080-8090-8100-8110-8120-8130-8140-8150-8160-8170-8180-8190-8110-8120-8130-8140-8150-8160-8170-8180-8190-8200-8210-8220-8230-8240-8250-8260-8270-8280-8290-8210-8220-8230-8240-8250-8260-8270-8280-8290-8300-8310-8320-8330-8340-8350-8360-8370-8380-8390-8310-8320-8330-8340-8350-8360-8370-8380-8390-8400-8410-8420-8430-8440-8450-8460-8470-8480-8490-8410-8420-8430-8440-8450-8460-8470-8480-8490-8500-8510-8520-8530-8540-8550-8560-8570-8580-8590-8510-8520-8530-8540-8550-8560-8570-8580-8590-8600-8610-8620-8630-8640-8650-8660-8670-8680-8690-8610-8620-8630-8640-8650-8660-8670-8680-8690-8700-8710-8720-8730-8740-8750-8760-8770-8780-8790-8710-8720-8730-8740-8750-8760-8770-8780-8790-8800-8810-8820-8830-8840-8850-8860-8870-8880-8890-8810-8820-8830-8840-8850-8860-8870-8880-8890-8900-8910-8920-8930-8940-8950-8960-8970-8980-8990-8910-8920-8930-8940-8950-8960-8970-8980-8990-9000-9010-9020-9030-9040-9050-9060-9070-9080-9090-9010-9020-9030-9040-9050-9060-9070-9080-9090-9100-9110-9120-9130-9140-9150-9160-9170-9180-9190-9110-9120-9130-9140-9150-9160-9170-9180-9190-9200-9210-9220-9230-9240-9250-9260-9270-9280-9290-9210-9220-9230-9240-9250-9260-9270-9280-9290-9300-9310-9320-9330-9340-9350-9360-9370-9380-9390-9310-9320-9330-9340-9350-9360-9370-9380-9390-9400-9410-9420-9430-9440-9450-9460-9470-9480-9490-9410-9420-9430-9440-9450-9460-9470-9480-9490-9500-9510-9520-9530-9540-9550-9560-9570-9580-9590-9510-9520-9530-9540-9550-9560-9570-9580-9590-9600-9610-9620-9630-9640-9650-9660-9670-9680-9690-9610-9620-9630-9640-9650-9660-9670-9680-9690-9700-9710-9720-9730-9740-9750-9760-9770-9780-9790-9710-9720-9730-9740-9750-9760-9770-9780-9790-9800-9810-9820-9830-9840-9850-9860-9870-9880-9890-9810-9820-9830-9840-9850-9860-9870-9880-9890-9900-9910-9920-9930-9940-9950-9960-9970-9980-9990-9910-9920-9930-9940-9950-9960-9970-9980-9990-10000-10010-10020-10030-10040-10050-10060-10070-10080-10090-10010-10020-10030-10040-10050-10060-10070-10080-10090-10100-10110-10120-10130-10140-10150-10160-10170-10180-10190-10110-10120-10130-10140-10150-10160-10170-10180-10190-10200-1		

$\varphi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1h\ 14\ min.$

BR. ST. 143

D D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	709.4	709.2	710.9	01.6	02.4	01.4	01.8	03.0	01.2	-	05.0	05.2	04.9	97	92	97	95	W NW	2	W NW	2	
2	710.3	708.8	709.2	00.8	03.0	02.6	02.2	03.1	06.8	-	04.8	05.3	05.3	98	94	97	96	-	0	W NW	1	
3	708.3	707.7	709.2	02.1	04.4	03.2	03.2	04.5	01.9	-	05.2	05.8	05.5	98	93	95	95	W NW	1	W SW	2	
4	712.1	712.2	714.1	00.9	03.2	02.2	02.1	03.5	00.0	-	04.7	05.4	05.3	97	94	98	96	-	0	SW 1	0	
5	713.2	712.0	711.5	00.0	03.6	02.6	02.2	04.0	-00.1	-	04.4	05.5	05.2	96	92	97	95	-	0	-	0	
6	709.2	706.8	705.8	01.8	05.2	04.2	03.8	05.5	01.5	-	03.0	05.9	05.6	95	89	91	92	ESE	2	-	C SSE	1
7	707.6	709.1	704.5	02.9	02.6	02.5	02.6	04.6	02.2	-	05.6	05.2	05.0	100	94	90	95	W	1	W	1	
8	709.4	709.3	710.6	00.0	02.4	01.0	01.1	02.7	-06.3	-	04.4	04.9	04.8	96	90	97	94	E	1	-	C	0
9	710.1	708.9	708.2	00.4	04.8	-00.1	01.2	05.6	-00.1	-	04.4	04.3	03.8	93	67	84	81	FNE	1	SE	3	
10	705.9	706.7	709.4	-01.4	01.4	01.2	00.6	01.9	-01.5	-	03.8	04.4	04.6	92	87	91	90	S	2	W NW	1	
11	711.9	712.6	714.9	-01.3	01.3	00.8	00.4	01.6	-01.4	-	03.8	04.3	04.0	92	85	83	87	-	0	SW 1	ESE 2	
12	715.6	715.1	715.5	-01.4	03.2	01.0	01.0	04.5	-01.5	-	03.6	04.3	04.6	92	75	93	87	-	0	-	C	0
13	714.5	712.9	713.2	-01.6	-00.4	-01.8	-01.4	01.0	-02.5	-	03.8	03.0	03.7	92	85	92	90	SE	2	SW 1	-	
14	714.3	713.2	713.5	-05.0	01.3	-02.4	-02.1	02.5	-05.1	-	02.9	03.2	03.0	91	64	77	77	ESE	1	W NW	1	
15	714.0	713.0	713.5	-06.0	01.0	-02.4	-02.4	01.3	-06.4	-	02.8	03.2	03.2	94	65	84	81	SE	4	W	1	
16	712.8	712.4	711.9	-02.0	-00.1	00.5	-00.3	01.0	-03.0	-	03.4	04.1	04.3	87	91	91	90	-	0	-	C NW	2
17	706.5	705.9	709.3	-01.2	03.0	00.4	00.6	04.5	-01.5	-	04.0	05.1	04.6	94	91	96	94	E	1	-	C WSW	2
18	709.4	708.7	708.8	00.0	02.2	00.4	00.8	03.1	-00.5	-	04.4	03.8	04.1	96	71	86	84	-	0	W NW	2	
19	709.9	710.2	710.5	-01.9	00.8	01.0	00.2	02.0	-02.5	-	03.7	04.4	04.6	92	40	93	92	-	0	-	C	0
20	709.3	708.9	711.1	00.6	04.2	02.8	02.6	04.5	00.5	-	04.5	05.6	05.2	93	91	94	93	-	0	-	C	0
21	712.8	710.4	713.5	02.2	03.0	02.2	02.4	03.6	01.6	-	05.3	05.1	04.9	95	89	90	92	SE	1	W	1	
22	713.3	712.1	711.6	-00.2	02.6	01.0	02.2	08.7	-00.2	-	04.4	04.5	04.2	93	62	85	80	ESE	1	W	1	
23	712.2	712.7	711.4	-04.2	-01.3	-00.1	-01.4	01.3	-04.5	-	03.2	03.9	04.4	96	93	96	95	ESE	1	W	1	
24	711.4	710.4	710.7	-00.4	03.4	-00.2	00.2	01.6	-00.5	-	04.5	04.3	04.2	100	85	93	93	-	0	-	C	0
25	709.0	708.6	709.3	-03.4	01.2	-00.5	-00.8	01.6	-03.4	-	03.0	03.7	04.0	85	73	91	83	ESE	2	W NW	1	
26	711.2	710.5	710.2	-04.6	-00.2	-02.4	-02.4	00.0	-05.6	-	02.8	03.6	03.7	87	80	96	88	E	1	W	1	
27	709.4	707.7	708.3	-04.9	02.2	00.4	-00.5	03.6	-05.7	-	02.7	03.7	04.1	85	70	86	80	-	0	-	C	0
28	709.5	710.1	710.5	-01.9	02.2	00.4	02.3	03.5	-02.4	-	03.8	04.6	04.6	96	85	96	92	-	0	SE	1	
29	710.7	709.7	710.5	-04.2	-00.7	-02.0	-02.2	00.8	-04.2	-	02.9	04.0	04.0	88	93	100	94	-	0	W NW	1	
30	713.4	713.2	714.1	-04.5	-01.0	-02.0	-02.4	-00.7	-04.5	-	03.1	03.9	03.9	94	91	98	94	SSE	1	-	C SSE	1
31	714.2	713.5	713.6	-03.8	02.0	-00.2	-00.6	03.6	-04.0	-	03.2	04.2	04.0	92	79	89	87	-	0	W NW	1	
MES.	VRED.	711.0	710.5	711.1	-01.3	02.1	00.6	00.5	03.0	-01.7	-	04.0	04.5	04.4	94	84	92	90	SE	2	0.7	0.7

## 1974 FEBRUAR

## SARAJEVO

1	712.3	711.1	711.2	-03.0	09.6	02.6	03.0	10.5	-04.4	-	03.3	05.3	04.6	86	85	82	77	ESE	2	W	1	-	0
2	711.3	710.3	711.4	00.4	12.2	03.2	04.8	12.4	-00.4	-	04.0	05.0	04.7	84	47	61	71	SE	2	W NW	1	-	0
3	709.7	707.9	704.8	01.8	10.0	04.0	07.4	10.6	-00.8	-	04.1	04.6	05.7	79	52	66	56	SE	4	SW	1	SE	1
4	702.6	700.0	701.0	02.5	09.6	03.6	04.8	11.0	00.9	-	05.2	05.0	05.0	95	56	85	79	SSE	4	SW	3	-	0
5	701.7	700.0	699.2	00.3	09.0	02.5	03.8	10.5	00.0	-	04.3	04.5	04.3	91	53	77	74	ESE	1	W	2	-	0
6	698.1	692.1	686.8	01.6	07.4	06.3	06.4	08.5	-00.2	-	04.3	04.0	05.2	83	52	67	66	SW	1	S	6	SSE	4
7	697.9	684.4	691.0	04.0	07.5	-00.1	02.8	09.5	-00.2	-	05.7	02.7	02.9	94	25	62	64	W	1	W NW	4	ESE	1
8	698.5	702.2	706.9	-03.5	02.4	-00.6	-00.6	05.0	-03.9	-	02.9	04.1	03.2	83	74	77	72	SE	1	E	2	-	0
9	709.7	709.0	709.7	-05.1	08.9	02.4	02.8	09.5	-05.6	-	02.6	02.4	03.2	84	28	59	57	ESE	4	W NW	1	ESE	1
10	710.1	709.8	710.3	-00.4	12.2	03.0	04.6	12.8	-00.9	-	03.4	04.2	04.3	72	40	75	62	SE	1	W SW	2	ESE	3
11	708.8	706.1	705.7	00.4	12.6	03.2	04.8	13.3	-00.2	-	03.8	04.9	04.5	81	45	78	68	ESE	4	W	2	SSE	1
12	704.1	701.7	701.3	01.0	14.2	04.2	05.9	15.8	00.5	-	03.7	04.4	04.2	74	36	68	56	ESE	3	W	1	E	2
13	699.4	698.3	698.0	04.8	10.3	07.3	07.6	12.0	01.5	-	04.6	05.4	04.8	71	56	75	67	NNW	1	S	4	ESE	2
14	697.0	698.6	701.3	06.4	11.3	05.8	07.2	12.6	05.5	-	05.3	04.8	04.6	73	47	67	62	ESE	2	SW	2	E	2
15	701.3	700.6	701.0	04.0	12.2	07.2	07.7	13.5	03.6	-	05.6	05.5	04.7	91	52	62	68	-	0	W	1	ESE	1
16	701.9	701.3	703.1	03.4	11.8	07.5	07.6	12.2	02.5	-	05.1	05.7	05.4	88	55	69	71	-	0	SW	1	SE	2
17	705.2	706																					

BR. ST. 143

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vrijednost 0-9	Obločnost N (0-10)					Insolacijia broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	5	09	10•	10	05.7	00.0	00.7	.	n-n, 11 <sup>20</sup> 14 <sup>15</sup> 17 <sup>16</sup> 19 <sup>12</sup> n	
2	3	10•	10•	10•	10.0	00.0	00.6	.	n-16, 16-n, 19 <sup>15</sup> 21 <sup>15</sup>	
3	2	10•	10•	08	06.3	00.0	00.4	.	n-19, 21 <sup>15</sup> n, orj-8, = 19 21 <sup>15</sup>	
4	2	10•	10•	10•	10.0	00.0	00.1	.	n-n	
5	3	01•	06•	10	05.7	00.0	.	.	n-8, = n-7 <sup>20</sup> , 13 <sup>10</sup> , = 7 <sup>20</sup> 13 <sup>10</sup> , 11 <sup>20</sup> 14 <sup>15</sup> , 15 <sup>15</sup> , = 15, 11	
6	5	10	10•	10•	10.0	00.0	00.2	.	n-n, 10 <sup>10</sup> n	
7	5	10•	10•*	10	10.0	00.0	05.5	.	• n-8 <sup>20</sup> 15-16; = n-n, 8 <sup>20</sup> 13 <sup>20</sup>	
8	4	10	10	10	10.0	00.0	01.6	.	n-8 <sup>20</sup> , = n-n, * 9 <sup>15</sup> 11 <sup>20</sup> , 14 <sup>15</sup> K 15 10 <sup>20</sup> 12, * 13 <sup>20</sup> , 15 <sup>20</sup>	
9	7	06	09	00	05.0	02.2	01.5	00	= n-10, 20-n	
10	3	09	10•	10*	05.7	00.0	.	.	n-7 <sup>20</sup> , = n-11 <sup>20</sup> , 15-17, * 8 12 <sup>20</sup> , 12 <sup>20</sup> * 13 <sup>20</sup> , 12 18 <sup>20</sup> , 12 <sup>20</sup> , 11 <sup>20</sup> , 11	
11	5	10	10	07	05.0	00.0	00.4	00	n-9=n-n	
12	6	10	10	02	07.3	00.7	.	.	n-8 <sup>20</sup> =n-n	
13	5	10•	10	10	10.0	00.0	.	.	n-9=n-10, = 10-n	
14	5	05	03•	00	02.7	05.8	.	.	n-10 <sup>20</sup> =n-n, 12, 13 <sup>20</sup> n	
15	4	10	00•	00	03.3	04.8	.	.	n-11, 17-n, = n-n	
16	3	10*	10•	10•	10.0	00.0	00.1	00	= n-7 <sup>20</sup> * rj-10, = 7 <sup>20</sup> n, A 14 <sup>20</sup> 12 <sup>20</sup> , * 12 <sup>20</sup> 15 <sup>15</sup> , [X]	
17	2	02	10•	10*	07.3	00.0	02.0	C1	= 7 <sup>20</sup> 12, 22-n, = 12-17, * 12 <sup>20</sup> 17 <sup>20</sup> * 16 <sup>20</sup> n, * 16 <sup>20</sup> 17, = 16 <sup>20</sup> 17, [X]	
18	7	10*	09*	10*	09.7	01.6	16.4	14	* n-rj, 20-n, = 9 <sup>20</sup> 12, [X]	
19	5	10	10*	10*	10.0	00.0	01.5	09	= n-n, * 8 <sup>20</sup> n, [X]	
20	5	10•	10•	10•	10.0	00.0	17.5	19	• n-n, = n-n, [X]	
21	7	10•	10•	10	10.0	00.0	06.0	C7	= n-n, orj-7 <sup>20</sup> , * 12 <sup>20</sup> 15, [X]	
22	6	00	00•	00	00.0	00.0	08.1	05	= 8 <sup>20</sup> 12, * 12, 18 <sup>20</sup> [X]	
23	3	03•	10•	10*	07.7	00.7	.	04	n-9, = 9-n, * 18 <sup>20</sup> 21 <sup>20</sup> , [X]	
24	4	10•	10	10	10.0	00.0	00.8	03	= n-12 <sup>20</sup> , = 12 <sup>20</sup> n, [X]	
25	5	10	10	09	09.7	00.0	.	C2	= n-n, [X]	
26	5	10	10	10	10.0	03.5	.	02	= n-n, [X]	
27	2	00	00•	04	01.2	04.7	.	02	= n-10 <sup>20</sup> 17 <sup>20</sup> n, = 10 <sup>20</sup> 16 <sup>20</sup> , = 11 <sup>20</sup> 15 <sup>15</sup> , [X]	
28	2	10*	10•	00	06.7	00.0	00.3	02	= n-12, * rj-12, = 12-13, = 12-10 <sup>20</sup> , = 11 <sup>20</sup> n, [X]	
29	3	10	10•	10•	10.0	00.3	00.5	02	= n-9, = 9 <sup>20</sup> 12 <sup>20</sup> , = 9 <sup>20</sup> 12, [X]	
30	2	10	10•	10•	10.0	00.0	.	02	* n-8 <sup>20</sup> n, = 8 <sup>20</sup> 12, = 8 <sup>20</sup> 13, = 9 <sup>20</sup> n, [X]	
31	3	10•	10•	00•	06.7	01.5	.	02	= n-14 <sup>20</sup> , = 14 <sup>20</sup> n, [X]	
MES.										
VRFD.	08.2	08.6	07.4	08.1	33.4	57.2				

1	4	03	01	00	03	02.3	07.7	.	02	$\equiv n-10, = 13-n$
2	6	02	06	00	02	02.7	07.7	.	.	$\sqcup n-9 = n-10, 19-21^{\circ}, \Delta 20^{\circ} 45^{\circ}, 21^{\circ} 30^{\circ}$
3	7	08	07	00	05	06.7	02.6	.	.	$\sqcup n-8^{\circ} = n-n, 08^{\circ} 55^{\circ} 03^{\circ} 17^{\circ} 30^{\circ} 19^{\circ} 5^{\circ}, 22^{\circ} 45^{\circ}, 21^{\circ}$
4	8	10*	06	00	08	08.0	02.8	40.7	00	$\bullet 0-8^{\circ}, *n-j, \Delta 20^{\circ} 5^{\circ}, F_{se}, 6^{\circ} 30^{\circ}, 0^{\circ} 45^{\circ}$
5	8	07	06	08	07.0	06.5	00.1	.	.	$\sqcup n-8^{\circ} = n-10, F_{sw}, 13^{\circ} 25^{\circ}$
6	8	05	10	10*	08.3	03.3	.	.	.	$\sqcup n-8^{\circ} = n-17^{\circ}, \equiv 17^{\circ} 10^{\circ}, F_s, SW, 9^{\circ} 25^{\circ}, 19^{\circ} 15^{\circ}, 21^{\circ} 50^{\circ}, 22^{\circ}, \bullet 0-10^{\circ}, 24^{\circ}$
7	8	10*	06	00	01	05.7	03.3	09.8	.	$\bullet 0-8^{\circ}, F_g, 0^{\circ}, 17^{\circ} 45^{\circ}, 14^{\circ}, *8^{\circ}, 8^{\circ}, *5^{\circ}, 5^{\circ}, 8^{\circ}, 12^{\circ}$
8	7	10	03	03	03	05.3	04.9	01.6	00	.
9	7	01	07	00	01	03.0	05.7	00.2	00	$\sqcup n-9 = n-n_j$
10	7	01	03	00	01.3	09.2	.	.	.	$\sqcup n-8^{\circ}$
11	7	00	00	00	00	00.0	09.6	.	.	$\sqcup n-8^{\circ}, = n-10$
12	8	00	01	00	00	00.3	09.4	.	.	$\sqcup n-10, = 9^{\circ} 20^{\circ}, 9^{\circ} 30^{\circ}$
13	8	08	08	10	08.7	05.5	.	.	.	$\equiv 9^{\circ} 10, \bullet 9^{\circ} 9^{\circ}, 15^{\circ} 40^{\circ}, 16^{\circ}, 18^{\circ}, n$
14	8	09	10	10	05.7	03.3	00.0	.	.	$= n-10, \bullet n_j, 9^{\circ} 20^{\circ}, 10^{\circ} 30^{\circ}$
15	7	10	07	10	05.0	05.3	00.2	.	.	.
16	7	10	08	09	09.0	02.3	00.0	.	.	$= n-n_j$
17	8	07	08	08	07.7	05.8	.	.	.	$\Delta n-8^{\circ}$
18	8	10	09	10	09.7	00.5	.	.	.	$\equiv n-10, F_s, 22^{\circ} 55^{\circ}, 24^{\circ}$
19	8	09	06	07	07.3	03.9	07.2	.	.	$F_{se}, 0^{\circ}, \bullet n_j, \bullet n-n_j$
20	7	05	08	08	07.0	03.4	.	.	.	$= n-n_j, \equiv 8^{\circ}, 10^{\circ}, \bullet 13^{\circ}, 0$
21	5	10	10	10	10.0	00.0	00.0	.	.	$= n-n$
22	7	10	10	10*	10.0	00.0	.	.	.	$= n-10, \bullet 7^{\circ} 55^{\circ}, 13^{\circ} 20^{\circ}, 17^{\circ}, 24^{\circ}$
23	4	10*	10	10*	10.0	00.0	10.4	04	.	$\bullet 0-7^{\circ}, 20^{\circ}, n_j, *10^{\circ}, \equiv n-10, = 10-n, \boxed{n}$
24	6	10	10	10	10.0	00.0	00.7	00	.	$= n-n$
25	6	10	10*	10*	10.0	00.0	.	.	.	$= n-n, \Delta 8^{\circ}, n$
26	7	10	10	10	10.0	00.0	00.0	00	.	$= n-10$
27	7	09	01	02	04.0	C8.5	.	.	.	$= 12^{\circ}, n$
28	6	09	07	00	05.3	04.6	.	.	.	.

$\varphi = 43^{\circ}52'$ , N  $\lambda = 18^{\circ}26'$ , E Gr.  $\Delta G = +1h\ 14\ min.$

BR. ST. 143

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenog pore e mm			Relativna vlažnost % %			Pravac i jačina veta D, f (0-12)										
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21								
1	707.5	709.3	709.3	-03.0	07.0	01.5	01.6	08.6	-04.1	-	02.8	03.6	03.7	76	48	72	65	-	0	WSW 2	E 2							
2	703.1	709.9	701.2	-01.4	08.8	05.2	04.4	09.2	-02.6	-	03.5	03.7	04.5	85	44	62	66	ESE 3	-	0	NNW 2							
3	703.6	705.6	707.1	02.1	08.8	02.6	04.0	10.5	02.0	-	04.5	03.9	03.5	84	46	62	64	-	0	SW 2	ESE 3							
4	707.0	707.1	705.0	04.0	08.2	08.6	07.4	10.6	00.0	-	03.6	05.4	04.9	55	67	59	62	E 3	SSE 1	LSE 4								
5	703.2	704.4	702.4	08.2	09.0	06.1	07.4	09.6	05.1	-	05.1	06.3	06.6	62	73	92	76	ESE 5	ESE 5	-	0							
6	700.9	700.6	702.7	04.8	10.6	03.7	05.7	11.5	03.7	-	04.9	04.5	05.5	76	47	92	72	SE 4	SE 4	-	0							
7	705.2	707.4	707.7	00.0	04.6	-00.2	00.0	04.0	-00.3	-	04.3	04.2	04.0	93	88	89	90	NNW 2	-	C	NNW 1							
8	707.9	706.5	707.5	-00.2	02.0	01.0	01.0	02.9	-00.4	-	04.1	04.5	03.8	91	85	78	85	SF 2	WNW 1	ESE 2								
9	707.5	707.5	709.2	-00.4	03.6	01.4	01.5	04.0	-00.6	-	03.5	04.1	04.4	78	70	87	78	F 1	SSE 1	NW 1								
10	700.4	705.4	709.3	00.1	03.8	02.4	02.2	05.0	00.0	-	04.4	04.6	04.4	95	76	81	84	NW 2	SW 2	W 2								
11	710.3	711.6	713.1	00.2	02.3	02.1	01.7	02.9	-00.1	-	04.3	04.6	03.9	92	85	73	84	NNW 2	WNW 1	E 1								
12	713.0	711.1	711.3	01.0	05.6	03.2	03.3	06.4	00.6	-	03.8	04.1	03.9	78	60	67	68	ESE 3	S 3	SE 2								
13	708.9	705.2	705.4	-01.4	09.2	03.6	03.8	11.1	-02.2	-	03.4	04.0	04.6	93	45	76	68	ESF 2	W 1	ESE 2								
14	703.7	707.6	699.9	-02.0	06.6	04.0	03.2	08.9	-02.0	-	03.7	04.8	04.1	94	66	60	76	ESE 1	W 2	SE 2								
15	703.2	698.1	700.3	-01.2	08.0	02.6	03.0	09.0	-01.2	-	03.4	03.8	04.6	81	48	82	70	SE 1	ENE 4	F 2								
16	699.8	700.1	700.4	01.8	08.2	03.4	04.2	08.7	00.5	-	04.5	04.0	04.6	87	49	79	72	ESE 1	WSW 1	ESE 2								
17	702.4	703.3	704.2	00.0	16.4	05.2	08.7	17.0	-00.7	-	03.8	04.1	04.3	82	29	49	53	ESE 3	W 1	ESE 3								
18	705.8	705.0	706.3	04.0	19.3	13.6	12.6	19.5	02.7	-	04.1	05.0	04.2	68	30	36	45	SE 2	W 1	S 5								
19	708.5	707.5	709.6	09.8	20.2	10.9	12.9	20.7	08.4	-	04.2	05.5	04.9	47	31	51	43	SE 2	SSW 5	SSE 2								
20	710.3	709.9	711.0	00.8	20.0	11.6	13.0	20.2	05.7	-	03.1	03.5	04.4	36	20	43	33	ESE 2	SE 1	ESE 2								
21	712.2	710.1	711.0	06.2	27.0	12.6	14.0	24.7	04.3	-	02.4	02.3	03.6	34	10	32	25	SE 2	SW 2	ESE 2								
22	711.0	708.2	708.1	06.4	24.4	14.0	14.7	24.5	05.5	-	04.4	04.8	05.2	62	21	43	42	FSE 2	ENE 4	ESE 2								
23	707.9	703.4	709.4	09.1	18.1	12.2	12.9	19.5	07.0	-	05.5	04.2	06.3	63	27	59	50	F 3	SSW 2	E 2								
24	710.8	707.4	708.0	05.8	21.4	14.2	13.9	22.5	04.5	-	05.8	04.5	06.4	83	34	53	57	SE 3	W 2	SE 2								
25	708.4	707.7	708.3	09.1	19.2	13.4	13.8	19.8	06.6	-	06.0	05.5	06.6	69	33	57	53	ESE 2	-	E 4								
26	708.4	706.1	705.6	06.8	20.4	12.8	13.2	20.9	04.8	-	05.8	05.6	06.9	79	31	62	57	ESE 3	S 2	ESE 2								
27	704.7	703.5	705.4	08.2	15.5	10.4	11.1	20.0	07.3	-	06.4	06.6	07.9	79	50	84	71	SE 1	E 5	N 2								
28	705.9	705.2	707.1	07.6	17.3	05.4	10.9	19.5	07.2	-	07.2	05.8	07.8	92	39	88	73	SSE 1	-	0	ESE 2							
29	705.6	707.0	704.2	05.1	19.4	12.8	12.5	20.5	03.5	-	05.9	06.1	06.1	90	36	55	60	E 2	SF 3	ESE 3								
30	722.1	707.4	703.7	08.3	15.6	10.8	11.4	15.7	06.9	-	06.1	06.2	06.2	74	47	64	62	ESE 4	ESE 3	ESE 2								
31	708.3	706.9	704.6	07.2	09.7	07.0	07.6	11.0	06.2	-	07.0	07.2	06.9	92	83	92	89	-	0	NW 2	-	0						
MES.	WRED.								706.8 705.9 706.7			03.7	12.3	07.2	07.7	13.5	02.5	-	04.6	04.8	05.1	76	49	68	64	2.1	2.2	2.0

1974 APRIL

SARAJEVL

1	704.9	704.8	706.0	06.2	08.2	06.6	07.0	09.3	06.0	-	06.7	07.2	06.4	95	86	87	90	-	0	F	I	ESE 3
2	706.6	707.5	709.4	05.7	09.5	07.4	07.5	09.8	05.2	-	05.8	06.1	05.8	85	65	75	76	ESE 2	-	C	SW 2	
3	709.6	708.7	709.4	06.4	12.6	07.1	08.3	14.7	06.2	-	06.3	05.7	05.0	87	52	66	68	-	0	ENE 2	ESE 3	
4	708.4	705.6	706.0	03.2	16.6	08.2	09.0	17.0	01.7	-	04.2	04.8	03.8	73	34	46	51	ESE 2	NE 1	ESE 2		
5	705.6	704.4	705.6	03.8	15.0	09.0	09.8	17.4	02.0	-	04.1	04.0	03.6	68	31	39	46	SF 2	W 1	E	5	
6	706.4	704.8	706.5	03.8	15.5	08.6	09.1	17.0	02.2	-	03.8	03.7	03.8	63	26	45	45	ESE 2	NE 3	E 3		
7	707.2	705.6	706.1	05.3	14.1	08.0	08.8	15.6	04.5	-	04.4	03.3	04.3	66	27	54	49	SE 3	NW 2	SSW 3		
8	705.7	705.4	706.4	05.9	08.2	05.9	06.4	09.2	04.0	-	06.7	06.5	05.9	96	79	85	87	E 2	WSW 3	-	1	
9	708.0	707.2	707.6	03.2	12.8	06.7	07.4	13.6	02.2	-	05.4	04.2	04.4	94	38	60	64	-	0	ENE 2	ENE 2	
10	707.2	703.8	703.1	03.5	17.6	11.6	11.2	18.0	01.0	-	04.3	04.2	04.7	72	28	45	48	ESE 2	W 2	-	0	
11	700.0	698.7	698.6	07.4	11.9	09.0	09.3	13.0	05.8	-	04.9	06.2	07.3	63	59	85	69	ESE 1	WNW 1	E 1		
12	697.9	697.5	698.8	07.2	14.8	09.6	10.3	16.9	03.9	-	06.3	06.9	07.5	82	55	84	74	ESE 2	-	0		
13	700.3	699.9	700.9	07.8	18.0	10.5	11.7	18.5	04.3	-	05.9	06.3	06.8	74	41	71	62	-	0	S 1	W 2	
14	697.9	696.5	698.1	08.2	05.1	00.7	03.7	11.0	00.6	-	07.8	06.2	04.6	95	94	95	95	NNW 2	NNW 1	SSW 1		
15	697.7	697.4	698.8	00.6	03.4	01.8	01.9	04.6	00.3	-	04.6	04.7	04.9	97	81	94	91	-	0	ESE 1	NW 2	
16	699.3	699.3	699.8	01.0	04.3	02.2	02.4	05.1	00.4	-	04.8	04.9	05.0	97	79	94	90	W 2	SE 3	-	0	
17	699.2	699.3	699.9	00.5	02.2	01.0																

BR. ST. 143

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Den	Vrijeme 0-9	Oblačnost N (0-10)					Intenzitet broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6 10	020	00	04.0	C7.0	.	.	.	W n-9 = n-730 N-D, = 730 N		
2	7 08	06	10	08.0	C1.0	.	.	.	= n-7, 17-19.60		
3	6 10	06	00	05.3	C5.1	.	.	.	= n-D		
4	8 08	10	09	09.0	C0.0	.	.	.			
5	8 09	10	10	09.7	C0.0	00.1	.	.	• n-8 <sup>o</sup> 2015, FSE 2 <sup>o</sup> 2 <sup>o</sup> 4 <sup>o</sup> , 7 <sup>o</sup> 7 <sup>o</sup>		
6	8 09	08	10*	09.0	C3.2	04.3	.	.	• 16 <sup>o</sup> 23 <sup>o</sup>		
7	4 10*	10*	10	10.0	C0.0	C4.9	00	.	= n-7, *4 <sup>o</sup> n, □		
8	7 10*	10	10	10.0	C0.0	C4.3	02	.	*n-9 <sup>o</sup> , □		
9	7 10	10	10*	10.0	C0.3	00.1	00	.	= n-7, *2015 n		
10	5 10	10	10	10.0	C0.0	C1.1	01	.	*n-n, = n-n, □		
11	5 10*	10	10	10.0	C0.0	C1.3	01	.	*n 8 <sup>o</sup> = n-n, □		
12	8 09	09	09	09.0	C0.1	C0.1	00	.	= n-9 <sup>o</sup>		
13	6 02	000	00	00.7	C9.6	.	.	.	W n-8 <sup>o</sup> = n-n		
14	5 07	090	00	05.3	C1.7	.	.	.	W n-8 <sup>o</sup> = n-n, □ 13-15		
15	8 06	10	10*	06.7	C0.0	.	.	.	W n 8 <sup>o</sup> = n-10, F 11 <sup>o</sup> 13 <sup>o</sup> , • 17 n		
16	6 10	10	00	06.7	C0.9	C0.0	.	.	= n-n		
17	5 000	010	00	00.3	C9.5	.	.	.	W n-8 <sup>o</sup> = n-8 <sup>o</sup>		
18	8 010	010	08	03.3	C1.1	.	.	.	= n-8 <sup>o</sup> = 9 <sup>o</sup> N, F 6 21 <sup>o</sup> 23 <sup>o</sup>		
19	8 010	000	00	00.3	C0.9	.	.	.	= n-8 <sup>o</sup>		
20	8 040	070	00	03.7	C6.9	.	.	.			
21	8 000	000	00	00.0	C1.9	.	.	.	= 7 <sup>o</sup> 9 <sup>o</sup>		
22	8 000	00	00	00.0	10.8	.	.	.	△ 0-7 <sup>o</sup> 9 <sup>o</sup> = 7 <sup>o</sup> 9 <sup>o</sup>		
23	9 07	100	08	08.3	C2.7	.	.	.	• 13 <sup>o</sup> 13 <sup>o</sup>		
24	8 000	02	07	03.0	C8.7	C0.0	.	.			
25	8 08	10	02	06.7	C0.0	.	.	.			
26	8 07	09	04	06.7	C7.0	.	.	.	= 7 <sup>o</sup> 9 <sup>o</sup> N		
27	8 070	10	00	05.7	C5.1	.	.	.	= 7 <sup>o</sup> 9 <sup>o</sup> , F 13 <sup>o</sup> 14 <sup>o</sup> , • 14 <sup>o</sup> 14 <sup>o</sup>		
28	8 050	060	00	03.7	C4.1	C0.0	.	.	△ 0-7 <sup>o</sup> = 8 <sup>o</sup> 10 <sup>o</sup> 11 <sup>o</sup> 12 <sup>o</sup> 13 <sup>o</sup> 14 <sup>o</sup>		
29	8 000	050	06	03.7	C8.2	C1.4	.	.	= 5 <sup>o</sup> 9 <sup>o</sup>		
30	7 10	10	09	09.7	C0.0	.	.	.	= 5 <sup>o</sup> 9 <sup>o</sup> 12 <sup>o</sup> 23 <sup>o</sup> , W 2 <sup>o</sup> 12 <sup>o</sup> 14 <sup>o</sup> 18 <sup>o</sup> , = 12 <sup>o</sup> 15 <sup>o</sup> 18 <sup>o</sup> 22 <sup>o</sup>		
31	4 100	10	10*	10.0	C0.0	00.4	.	.	• n 12 <sup>o</sup> 17 <sup>o</sup> 23 <sup>o</sup> , W 2 <sup>o</sup> 12 <sup>o</sup> 14 <sup>o</sup> 18 <sup>o</sup> 22 <sup>o</sup>		
MES. VRED.		06.4	06.8	05.2	06.1	126.2	18.0				

## SARAJEVC

1974 APRIL

1	6 10*	10*	10*	10*	10.0	00.0	01.4	.	= 0-18 <sup>o</sup> , • 2 <sup>o</sup> 16 <sup>o</sup> 20 <sup>o</sup> 23		
2	7 10	10	10	10	10.0	00.0	C1.0	.	= 0-11		
3	8 09	09	07	08.3	C2.3	.	.	.	= 0-9 <sup>o</sup>		
4	8 000	040	00	01.3	C1.7	.	.	.	= 0-9 <sup>o</sup> 14.45		
5	6 010	09	05	05.0	06.4	.	.	.			
6	7 050	010	00	02.0	C1.2	.	.	.	△ 2 <sup>o</sup> 8 <sup>o</sup>		
7	6 08	070	06	06.7	05.6	.	.	.	= 5 <sup>o</sup> 24		
8	7 09	09*	07	08.3	C0.4	C2.7	.	.	= 0-21 <sup>o</sup> , • 2 <sup>o</sup> 6 <sup>o</sup> 8 <sup>o</sup> 11 <sup>o</sup> 17 <sup>o</sup> 20 <sup>o</sup> , ▲ 11 <sup>o</sup> 14 <sup>o</sup> , ▲ 11 <sup>o</sup> 14 <sup>o</sup> 17 <sup>o</sup>		
9	8 10	06	00	05.3	06.0	03.2	.	.	= 0-11		
10	8 000	080	02	03.3	C7.4	.	.	.	△ 3 <sup>o</sup> 8		
11	8 10	10*	10	10.0	00.0	.	.	.	• 13 <sup>o</sup> 20 <sup>o</sup>		
12	8 06	10	02	06.0	C2.5	C0.9	.	.	• 12 <sup>o</sup> 19 <sup>o</sup>		
13	8 030	050	08	05.3	05.4	00.5	.	.	= 6 <sup>o</sup> 9 <sup>o</sup> = 18 <sup>o</sup> 20 <sup>o</sup>		
14	4 10	10*	10*	10*	10.0	00.0	C0.9	.	• 0-0 <sup>o</sup> 5 <sup>o</sup> 10 <sup>o</sup> 14 <sup>o</sup> 19 <sup>o</sup> , = 5 <sup>o</sup> 15 <sup>o</sup> 18 <sup>o</sup> 20 <sup>o</sup> , = 11 <sup>o</sup> 12 <sup>o</sup> 14 <sup>o</sup> 15 <sup>o</sup> , = 11 <sup>o</sup> 12 <sup>o</sup> 14 <sup>o</sup> 16 <sup>o</sup>		
15	5 10*	10	10*	10*	10.0	00.0	C4.9	00	* 0-11, 2 <sup>o</sup> 24 <sup>o</sup> = 2 <sup>o</sup> 21 <sup>o</sup> 24 <sup>o</sup> , ▲ 14 <sup>o</sup> 14 <sup>o</sup>		
16	7 10*	10*	10*	10*	10.0	00.0	C7.0	00	* 0-8 <sup>o</sup> 23 <sup>o</sup> 24 <sup>o</sup> = 0-23 <sup>o</sup> 24 <sup>o</sup> = 8-23 <sup>o</sup> , ▲ 10 <sup>o</sup> 11 <sup>o</sup> 12 <sup>o</sup> 13 <sup>o</sup> 14 <sup>o</sup> 15 <sup>o</sup>		
17	6 10*	10*	10*	10*	10.0	00.0	C12.7	05	* 0-10 <sup>o</sup> 13 <sup>o</sup> 15 <sup>o</sup> 17 <sup>o</sup> 19 <sup>o</sup> 21 <sup>o</sup> , ▲ 11 <sup>o</sup> 12 <sup>o</sup> 13 <sup>o</sup> 14 <sup>o</sup> 15 <sup>o</sup> 16 <sup>o</sup>		
18	6 10*	10*	10*	10*	10.0	00.0	C6.5	02	* 0-4 <sup>o</sup> 5 <sup>o</sup> 4 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup> = 0-12 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup>		
19	7 10*	10	08	05.3	C2.0	C8.4	00	.	* 0-5 <sup>o</sup> 6 <sup>o</sup> 5 <sup>o</sup> 7 <sup>o</sup> 7 <sup>o</sup> = 0-17 <sup>o</sup> 10 <sup>o</sup> 16 <sup>o</sup> 20 <sup>o</sup> 24 <sup>o</sup> , ▲ 13 <sup>o</sup> 17 <sup>o</sup>		
20	7 030	050	10	06.0	09.5	C1.0	.	.	= 0-12 <sup>o</sup> , ▲ 14 <sup>o</sup> 8 <sup>o</sup> 4 <sup>o</sup> 6 <sup>o</sup> 3 <sup>o</sup> = 0-12 <sup>o</sup> 12 <sup>o</sup> 12 <sup>o</sup>		
21	8 000	09	10	06.3	06.1	.	.	.	= 7 <sup>o</sup> 9 <sup>o</sup> = 8 <sup>o</sup> 14 <sup>o</sup> 17 <sup>o</sup>		
22	7 09	09*	03	07.0	02.9	C1.5	.	.	= 3 <sup>o</sup> 6 <sup>o</sup> 23 <sup>o</sup> 24 <sup>o</sup> = 13 <sup>o</sup> 14 <sup>o</sup>		
23	8 09	08*	01	06.0	06.1	C1.7	.	.	= 0-7 <sup>o</sup> 5 <sup>o</sup> 17 <sup>o</sup> 18 <sup>o</sup> 15 <sup>o</sup>		
24	8 000	060	10	05.3	08.9	00.0	.	.	• 3 <sup>o</sup> 4 <sup>o</sup> 9 <sup>o</sup> 14 <sup>o</sup> 14 <sup>o</sup> 14 <sup>o</sup> = 15 <sup>o</sup> 24		
25	7 10	10	10*	10*	10.0	00.0	C3.0	.	• 0-0 <sup>o</sup> 11 <sup>o</sup> 11 <sup>o</sup> 15 <sup>o</sup> 15 <sup>o</sup> = 0-2 <sup>o</sup> 14 <sup>o</sup> 18 <sup>o</sup> ▲ 13 <sup>o</sup> 13 <sup>o</sup> F 12 <sup>o</sup> 12 <sup>o</sup>		
26	7 000	10*	07	05.7	06.6	03.1	.	.	• 4 <sup>o</sup> 16 <sup>o</sup>		
27	8 020	10	10	07.3	06.1	05.0	.	.	F 2 <sup>o</sup> 19 <sup>o</sup> 13 <sup>o</sup> 13 <sup>o</sup> = 16 <sup>o</sup> 16 <sup>o</sup>		
28	8 09	10	09	09.3	02.0	00.0	.	.	* 13 <sup>o</sup> 5 <sup>o</sup>		
29	8 09	09	00	06.0	06.7	C3.0	.	.	F 13 <sup>o</sup> 9 <sup>o</sup> 9 <sup>o</sup> 17 <sup>o</sup> 17 <sup>o</sup> = 15 <sup>o</sup> 19 <sup>o</sup> 19 <sup>o</sup> R 15 <sup>o</sup> 16 <sup>o</sup>		
30	8 09	10	08	09.0	00.0	00.3	.	.			
MES. VRED.		06.7	08.5	06.7	07.3	114.1	66.2				

1974 MA

## SARAJEVO

 $\varphi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1h\ 14\ min.$ 

BR. ST. 143

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	7	14	21
1	689.5	690.1	692.2	09.2	13.2	10.6	10.9	15.0	07.3	-	05.7	06.1	07.0	66	53	72	64	SW	1	SSW	3	-	0
2	694.1	698.3	699.1	08.2	09.2	08.9	08.8	10.1	07.5	-	07.8	07.7	07.3	95	88	86	90	W	3	WSW	1	-	0
3	701.2	701.1	702.0	08.6	16.8	11.3	12.0	17.2	06.7	-	07.2	06.5	06.5	86	45	65	65	SE	1	S	2	S	2
4	700.3	699.4	699.6	11.2	11.0	07.8	09.4	13.6	07.2	-	05.9	06.5	07.1	59	66	90	72	S	2	E	3	-	0
5	698.4	698.3	699.6	10.4	12.1	06.5	08.9	15.8	05.6	-	06.0	06.2	06.5	63	58	90	70	S	2	S	2	NE	1
6	699.5	701.9	703.5	07.7	11.6	08.6	09.6	14.1	04.0	-	06.0	07.3	06.9	77	71	77	75	-	0	SSW	1	-	0
7	705.5	705.4	707.7	08.2	16.4	10.0	11.2	16.7	05.4	-	06.5	06.1	07.3	79	44	79	67	ESE	1	SW	2	NNW	1
8	707.4	706.2	705.2	10.4	12.2	05.6	10.4	14.5	07.0	-	06.8	07.1	06.6	72	67	74	71	ESE	1	SE	1	ENE	4
9	704.3	704.4	705.1	08.4	10.4	07.6	08.5	11.8	07.4	-	06.5	05.6	06.3	78	59	80	72	WSW	2	-	0	-	0
10	705.7	704.4	704.6	05.6	16.8	10.8	11.0	18.0	03.6	-	05.9	04.8	05.3	86	34	55	58	-	0	SW	2	ESE	3
11	706.6	706.2	706.9	07.6	19.5	14.0	13.8	20.9	04.4	-	05.4	06.2	07.0	69	36	58	54	E	2	W	2	-	0
12	707.9	706.8	710.3	11.5	19.0	10.8	13.0	20.9	08.7	-	06.8	07.2	09.1	67	44	93	68	WSW	1	NW	2	-	0
13	711.6	711.7	711.4	10.2	15.3	10.6	11.7	17.6	07.0	-	08.5	07.2	06.5	91	55	68	71	-	0	NNW	1	SSE	2
14	710.6	707.6	707.3	09.2	22.7	16.6	16.3	22.9	06.2	-	06.9	07.3	07.4	79	35	52	55	SE	2	NW	2	NNW	2
15	707.8	706.8	705.4	07.7	05.4	06.6	06.6	16.6	05.1	-	07.6	06.4	06.7	96	94	92	94	WNW	2	E	3	-	0
16	704.3	704.6	705.1	06.4	09.8	05.1	08.6	12.5	05.5	-	06.8	06.8	06.3	95	75	73	81	-	0	W	1	SE	1
17	706.0	707.3	708.7	07.7	12.6	10.8	10.5	15.5	04.2	-	06.1	08.6	06.7	78	79	69	75	SE	1	M	1	-	0
18	709.6	709.6	709.7	08.2	10.9	10.0	09.8	11.3	07.6	-	07.3	08.6	08.6	90	88	93	90	-	0	-	0	-	0
19	709.0	708.5	709.0	10.0	15.7	12.6	12.8	17.0	05.3	-	09.0	07.0	07.1	98	52	64	71	-	0	SE	1	-	0
20	709.3	707.3	708.0	10.4	22.0	12.8	14.5	22.5	07.2	-	08.5	08.7	07.1	90	44	64	66	-	0	S	2	ESE	1
21	709.4	708.6	709.6	09.5	17.8	13.6	13.6	18.3	08.0	-	08.6	10.0	09.2	96	65	79	80	-	0	W	1	-	0
22	707.9	703.3	700.0	09.4	20.8	17.1	16.1	21.5	06.7	-	07.7	08.1	07.3	87	44	50	60	-	0	WSW	1	N	4
23	701.3	700.0	699.6	06.9	15.3	10.4	10.8	17.5	06.4	-	06.8	06.0	06.0	91	46	64	67	-	0	WNW	2	ESE	2
24	699.9	699.3	700.2	09.4	17.4	15.5	14.4	18.0	07.3	-	07.2	08.0	07.6	81	54	57	64	-	0	S	4	SW	2
25	703.6	704.1	707.0	09.0	16.9	13.0	13.0	19.1	04.3	-	08.2	06.8	07.0	95	47	63	68	SE	1	W	2	-	0
26	709.9	709.2	708.6	09.4	19.2	12.6	13.6	19.8	06.5	-	07.4	06.3	06.7	84	38	61	61	-	0	SW	1	ENE	1
27	709.8	706.5	705.7	08.6	22.4	14.7	15.1	22.4	05.5	-	06.6	07.3	08.0	78	36	64	59	-	0	W	2	ESE	2
28	704.5	701.7	701.0	11.1	22.8	16.2	16.6	23.1	08.3	-	07.8	07.9	07.7	79	38	56	58	-	0	W	2	E	2
29	701.3	702.0	704.5	11.1	14.1	12.3	12.4	18.6	10.1	-	08.9	10.5	09.7	90	87	90	89	W	2	NE	1	-	0
30	708.1	707.9	708.6	10.9	22.4	16.0	16.3	22.5	09.8	-	09.2	10.2	10.2	94	50	75	73	-	0	WNW	1	ESE	2
31	708.7	708.4	708.3	14.6	21.5	15.8	16.9	26.0	11.4	-	09.8	09.2	10.2	78	48	75	67	ESE	1	ESE	1	ENE	1
MES.	VRED.	704.9	704.4	705.0	09.2	15.9	11.7	12.2	17.8	06.8	-	07.3	07.4	07.4	83	56	72	70	0.8	1.6	1.1	1.1	1.1

1974 JUN

## SARAJEVO

1	706.9	705.5	708.6	14.0	21.8	13.4	15.6	22.1	12.1	-	10.2	11.6	10.8	85	59	94	79	W	1	WSW	1	W	1
2	710.2	711.6	711.9	11.4	12.6	11.5	11.8	14.2	11.4	-	09.9	09.0	09.4	98	82	92	91	WNW	2	W	1	-	0
3	711.8	712.3	711.9	11.5	15.6	12.7	13.1	16.8	10.4	-	08.6	07.2	07.8	85	54	71	70	E	1	NNW	1	ESE	1
4	711.7	710.0	710.4	11.0	23.2	15.9	16.5	23.8	08.2	-	08.0	11.9	09.6	81	56	71	69	ESE	1	WSW	2	ESE	1
5	710.0	708.4	708.4	12.8	27.0	18.8	19.4	27.0	09.8	-	08.8	07.4	11.3	79	28	69	59	-	0	W	2	W	3
6	707.2	705.7	705.1	15.1	23.6	19.2	19.4	24.6	11.5	-	10.7	11.4	08.8	83	51	53	62	ESE	2	W	1	-	0
7	704.8	706.9	709.1	13.5	13.5	11.8	12.6	19.2	11.2	-	10.9	10.0	08.1	94	87	78	86	ESE	2	WNW	2	ESE	2
8	710.7	708.6	707.6	09.9	19.5	13.2	14.0	20.2	08.0	-	06.9	07.2	08.1	75	42	71	63	W	2	WNW	2	SE	2
9	705.7	703.8	703.2	11.1	22.1	19.2	17.9	22.7	08.2	-	08.3	09.6	06.9	83	48	41	57	-	0	WNW	2	S	4
10	702.4	701.5	700.2	17.6	20.4	18.4	18.7	21.5	13.2	-	07.4	09.0	08.3	49	50	52	50	S	4	ESE	4	S	2
11	699.1	702.5	704.8	08.8	09.9	07.1	08.2	19.0	07.1	-	08.1	06.6	07.2	95	72	95	87	E	2	W	3	-	0
12	704.2	702.0	703.2	06.9	16.4	07.7	09.7	17.1	05.2	-	07.1	05.4	07.2	95	39	91	75	-	0	W	2	-	0
13	701.0	700.2	701.7	06.9	12.0	09.3	09.4	16.8	05.0	-	06.5	07.4	07.1	87	71	81	80	-	0	-	0	SE	1
14	702.8	703.6	705.2	08.9	17.4	14.0	13.6	17.6	04.9	-	06.3	07.0	08.2	74	47	68	63	-	0	WNW	3	-	0
15	707.1	705.8	706.4	13.4	23.6	16.2	17.4	23.6	11.0	-													

BR. ST. 143

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vidljivost 0-9	Oblakost N (0-10)					Instalacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	09	09	09	09.0	01.2	06.6	.	.	• H <sup>25</sup> H <sup>40</sup> 13 <sup>40</sup> 16 <sup>21</sup> 24 <sup>24</sup>	
2	5	10	10	08	09.3	00.0	03.0	.	.	• 0-12 <sup>30</sup> = 4 <sup>24</sup> 24	
3	6	08	06	02	05.3	02.7	01.7	.	.	= 0-19 <sup>30</sup> 15 <sup>20</sup> 18 <sup>20</sup>	
4	7	09	10	10	09.7	00.6	00.3	.	.	F <sub>sw</sub> M <sup>11</sup> 25 <sup>25</sup> • H <sup>20</sup> 14, 17 <sup>20</sup> 22 <sup>20</sup>	
5	8	06	09	05	06.7	03.1	02.9	.	.	• 12 <sup>25</sup> 18 <sup>25</sup> F <sub>sw</sub> 13 <sup>45</sup> , 18 <sup>25</sup> 18 <sup>25</sup>	
6	8	04	08	09	07.0	04.2	02.2	.	.	• H-13 <sup>40</sup> 16 <sup>45</sup> 24 <sup>20</sup> , F <sub>sw</sub> 13 <sup>40</sup>	
7	8	04	04	10	06.0	05.4	01.6	.	.	• 16 <sup>20</sup> 10 <sup>40</sup> 19 <sup>25</sup> 21 <sup>25</sup>	
8	7	04	10	09	07.7	01.2	00.3	.	.	• 10 <sup>25</sup> 15 <sup>45</sup>	
9	6	10	10	10	10.0	00.0	CC.7	.	.	= 1 <sup>24</sup> 15 <sup>45</sup> 17 <sup>45</sup>	
10	7	00	03	00	01.0	11.8	00.2	.	.	= 0-2 <sup>25</sup> , △ 1 <sup>25</sup> 17 <sup>45</sup>	
11	7	01	08	00	03.0	09.7	.	.	.	△ 2-5 <sup>45</sup>	
12	7	05	08	10	05.0	04.7	.	.	.	• 7 <sup>25</sup> 05 <sup>55</sup> 18 <sup>50</sup> 20 <sup>30</sup> , R 48 <sup>45</sup>	
13	6	10	10	00	06.7	02.8	02.8	.	.	= 1 <sup>20</sup> 20 <sup>50</sup>	
14	8	00	04	03	02.3	08.3	.	.	.	≤ 20 <sup>50</sup> 22 <sup>50</sup>	
15	5	10	10	10	10.0	00.0	01.6	.	.	= 3-15 <sup>50</sup> 20-24, • 3 <sup>20</sup> 17 <sup>45</sup> 20-21 <sup>50</sup>	
16	7	10	10	04	08.0	03.0	11.8	.	.	= 0-11 <sup>25</sup> 1-5 <sup>45</sup> 23-24, • 6 <sup>20</sup> B <sup>80</sup> 13 <sup>45</sup> 13 <sup>50</sup>	
17	6	09	10	03	07.3	04.0	01.2	.	.	= 0-17 <sup>50</sup> 6 <sup>25</sup> 6 <sup>25</sup> 6 <sup>25</sup> = 6 <sup>45</sup> 24, • 7 <sup>25</sup> 44 <sup>50</sup>	
18	5	10	10	10	10.0	00.0	02.8	.	.	= 0-24, • 3 <sup>25</sup> 13	
19	6	10	05	09	05.3	02.2	01.9	.	.	= 0-24, • 1 <sup>25</sup> 5 <sup>50</sup>	
20	7	01	06	02	03.0	07.5	.	.	.	= 0-10 <sup>55</sup> , △ 3 <sup>25</sup> 7 <sup>25</sup> 21 <sup>25</sup> 24	
21	6	10	10	09	09.7	02.2	04.0	.	.	△ 0-4 <sup>20</sup> 4 <sup>20</sup> 9 <sup>25</sup> 14-17 <sup>25</sup> , = 6-21 <sup>25</sup> , R <sub>sw</sub> 14-14 <sup>20</sup>	
22	6	05	09	10	08.0	03.6	04.7	.	.	△ 2 <sup>25</sup> 6 <sup>25</sup> = 4 <sup>25</sup> 20, • 17 <sup>25</sup> 18 <sup>50</sup> 20 <sup>45</sup> 24, R <sub>sw</sub> 20 <sup>50</sup> , R <sub>sw</sub> 21 <sup>25</sup> 23 <sup>45</sup>	
23	7	08	06	09	07.7	07.0	17.0	.	.	• 0-5, 2 <sup>25</sup> 23 <sup>25</sup> 23 <sup>25</sup>	
24	7	09	10	10	09.7	04.9	00.4	.	.	= 10 <sup>25</sup> 18 <sup>25</sup> 24, • 2 <sup>25</sup> 3 <sup>25</sup> 13 <sup>25</sup> 14, R <sub>sw</sub> 13 <sup>45</sup>	
25	8	09	03	04	07.0	04.9	07.6	.	.	= 0-5, △ 2 <sup>25</sup> 6 <sup>25</sup> , 12 <sup>25</sup> 13 <sup>25</sup> , R <sub>sw</sub> 5 <sup>25</sup>	
26	8	03	01	00	01.3	13.0	00.0	.	.	△ 23-24	
27	8	00	03	00	01.0	14.0	.	.	.	△ 0-8 <sup>05</sup>	
28	8	01	10	05	05.3	07.8	.	.	.	△ 23-24	
29	7	09	09	03	07.0	01.6	11.2	.	.	△ 0-2 <sup>25</sup> 20 <sup>25</sup> 24, = 0 <sup>45</sup> 6 <sup>15</sup> 23 <sup>30</sup> 24, • 2 <sup>25</sup> 6 <sup>25</sup> 13 <sup>25</sup> 16 <sup>25</sup> , F <sub>sw</sub> 5 <sup>55</sup> 6 <sup>25</sup> , △ 13 <sup>25</sup> 13 <sup>45</sup> , R <sub>sw</sub> 13 <sup>45</sup>	
30	7	10	04	09	07.7	05.8	03.4	.	.	= 0-10 <sup>55</sup> , △ 0-10 <sup>30</sup> 20 <sup>45</sup> 24	
31	8	04	10	06	06.7	07.0	.	.	.	△ 0-7 <sup>25</sup> , △ 18 <sup>25</sup> 19 <sup>25</sup>	
MES. VRKD.		06.5	07.9	06.1	06.8	144.2	51.1				

1	7	10	09	10	C9.7	C2.2	CC.9	.	.	= 5-24, • 5 <sup>25</sup> 10 <sup>10</sup> 19 <sup>25</sup> 24	
2	6	10	10	10	10.0	00.0	21.6	.	.	• 0-10 <sup>25</sup> 15 <sup>45</sup> 17 <sup>25</sup> 19 <sup>25</sup> 24, = 1-24	
3	7	09	10	08	C9.0	C3.0	C1.7	.	.	• 0-5 <sup>25</sup> , = 0-9 <sup>25</sup> 17 <sup>25</sup> 24	
4	6	00	04	00	01.3	13.5	.	.	.	= 0-24, △ 9 <sup>25</sup> 8 <sup>25</sup>	
5	7	00	01	10	C9.7	C3.7	12.4	.	.	= 0-15 <sup>25</sup> , △ 2-9, • 17 <sup>25</sup> 10 <sup>25</sup> 21 <sup>25</sup> , R <sub>sw</sub> 19 <sup>45</sup> 22 <sup>25</sup>	
6	8	06	09	C5	06.7	C4.7	C9.6	.	.	• 10-10 <sup>25</sup> R <sub>sw</sub> 10 <sup>45</sup>	
7	6	10	10	10	C0.0	00.0	C5.7	.	.	• 1 <sup>25</sup> 11 <sup>25</sup> = 7 <sup>25</sup> n	
8	8	00	03	00	01.0	13.0	04.3	.	.	= 0-1 <sup>25</sup> △ 20-24	
9	7	04	05	C5	C7.7	C3.3	.	.	.	△ 0-8 <sup>25</sup> = 6-9 <sup>25</sup> , 9 <sup>25</sup> 10 <sup>40</sup> F <sub>sw</sub> 20 <sup>50</sup>	
10	7	03	05	00	04.0	07.9	00.2	.	.	F <sub>sw</sub> 8, 14 <sup>25</sup> , 48 <sup>25</sup> 49 <sup>25</sup> , 22 <sup>25</sup> 23 <sup>25</sup>	
11	7	10	10	10	10.0	00.5	C9.9	.	.	• 3 <sup>25</sup> 6 <sup>25</sup> H <sup>40</sup> 12 <sup>45</sup> 17 <sup>25</sup> 19 <sup>25</sup> = 3 <sup>25</sup> 6 <sup>25</sup> 18 <sup>25</sup> 24, F <sub>sw</sub> w 2 <sup>25</sup> , 13 <sup>25</sup> 18 <sup>25</sup> 18 <sup>25</sup> 18 <sup>25</sup> , R <sub>sw</sub> 4 <sup>25</sup>	
12	7	01	09	10	06.7	07.4	02.0	.	.	= 0-9 <sup>25</sup> 17 <sup>25</sup> 17 <sup>25</sup> 17 <sup>25</sup>	
13	8	C7	07	03	C5.7	C9.6	C2.0	.	.	• 0 <sup>25</sup> 6 <sup>25</sup> 22 <sup>25</sup> 24, = 5-9 <sup>25</sup> , • 12-15 <sup>25</sup> 18 <sup>25</sup> 18 <sup>25</sup> , F <sub>sw</sub> 12 <sup>25</sup> , R <sub>sw</sub> 13 <sup>25</sup> 13 <sup>25</sup>	
14	8	01	07	09	05.7	04.5	01.6	.	.	△ 0-8	
15	P	01	04	10	C5.0	C9.4	.	.	.	△ 3-9-24, = 6-9 <sup>25</sup>	
16	7	01	10	10	07.0	07.4	.	.	.	△ 0-9 <sup>25</sup> 20 <sup>25</sup> 24, = 3-9 <sup>25</sup> 23-24	
17	7	04	C5	07	05.3	C9.4	.	.	.	△ 0-7 <sup>25</sup> 17 <sup>25</sup> 17 <sup>25</sup> 17 <sup>25</sup>	
18	6	00	03	09	04.0	09.6	.	.	.	• 0-24, △ 0 <sup>25</sup> M <sup>10</sup> 11 <sup>25</sup> 12, 20-22 <sup>25</sup>	
19	6	10	10	10	10.0	00.0	02.1	.	.	= 0-24, △ 23-24	
20	6	04	10	10	C8.0	04.1	CC.5	.	.	= 0-24, △ 0-9 <sup>25</sup> 17 <sup>25</sup>	
21	6	C9	06	06	C8.0	C1.4	.	.	.	= 0 <sup>25</sup> 7 <sup>25</sup> = 0-9 <sup>25</sup> , 17 <sup>25</sup> 13 <sup>25</sup> , △ 13 <sup>25</sup> 14 <sup>25</sup> , F <sub>sw</sub> 13 <sup>45</sup>	
22	5	C1	08	03	04.0	08.4	00.5	.	.	△ 0 <sup>25</sup> 10 <sup>30</sup>	
23	7	07	06	04	05.7	08.5	C2.5	.	.	• 14 <sup>25</sup> 44 <sup>25</sup> 18 <sup>25</sup> 18 <sup>25</sup> 22 <sup>25</sup> 24, F <sub>sw</sub> 18 <sup>25</sup> 18 <sup>25</sup>	
24	7	09	07	09	C8.3	C3.3	.	.	.	• 0-5, 7 <sup>25</sup> 14 <sup>25</sup> , = 3-9 <sup>25</sup> , △ 23 <sup>25</sup> 24	
25	7	10	07	07	08.0	07.3	14.0	.	.	= 0-24, △ 0-9 <sup>25</sup> 17 <sup>25</sup>	
26	8	02	03	01	02.0	12.5	C1.2	.	.	△ 0-7 <sup>25</sup>	
27	8	10	05	08	09.0	05.7	.	.	.	• F <sub>sw</sub> 5 <sup>25</sup> 5 <sup>25</sup> 0 <sup>25</sup> 12 <sup>25</sup> 14 <sup>25</sup> 15 <sup>25</sup>	
28	7	10	10	10	10.0	02.2	10.6	.	.	• 2 <sup>25</sup> 6 <sup>25</sup> 14 <sup>25</sup> 5 <sup>25</sup> 17 <sup>25</sup> 22 <sup>25</sup>	
29	7	09	09	10	09.3	02.4	00.1	.	.	△ 0-7 <sup>25</sup> 7 <sup>25</sup> 17 <sup>25</sup> 24, = 17 <sup>25</sup> 24, △ 19 <sup>25</sup> 20, △ 20 <sup>25</sup> 22	
30	6	10	10	07	C9.0	01.4	31.1	.	.	• 0-0 <sup>25</sup> 3 <sup>25</sup> 45, = 0-10 <sup>25</sup>	
MES. VRKD.		05.8	07.6	07.0	06.8	175.4	122.7				

$\varphi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1h\ 14\ min.$

BR. ST. 143

D E G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	707.7	708.0	708.4	12.6	23.4	16.5	17.4	23.9	10.6	-	09.5	09.9	05.5	87	46	66	66	-	0	W	2	-	0
2	710.3	710.2	711.3	13.9	23.3	17.3	18.0	24.0	11.7	-	09.4	11.0	09.0	79	51	61	64	-	0	-	C	ESE	3
3	711.0	707.1	705.5	12.9	26.0	19.6	19.5	26.4	10.2	-	08.5	06.1	05.4	76	24	55	52	W	1	W	2	-	0
4	706.9	707.1	707.5	17.2	20.3	18.0	18.4	20.8	15.3	-	11.5	10.8	10.6	78	61	69	65	-	0	SE	4	ESE	3
5	703.4	707.0	708.9	16.2	26.7	20.7	21.1	26.8	13.2	-	10.2	13.2	13.2	74	50	72	65	-	0	W	3	ESE	2
6	708.7	704.7	706.1	16.5	27.8	19.8	21.0	28.1	14.2	-	11.8	14.2	12.4	84	51	72	69	-	0	W	3	-	0
7	704.8	710.1	709.0	17.6	10.9	05.4	11.8	20.0	09.4	-	11.6	09.1	08.4	77	93	95	88	-	0	SW	2	-	0
8	709.7	704.0	710.0	09.2	14.4	09.5	10.8	16.9	07.0	-	08.3	07.1	06.9	95	58	75	76	-	0	NNW	3	ESE	2
9	711.4	709.9	709.2	08.8	20.6	14.4	14.6	21.3	06.9	-	07.3	07.7	07.8	86	42	63	64	-	0	W	3	ESE	1
10	708.8	708.9	708.4	17.0	21.2	17.6	17.1	22.0	10.4	-	08.9	09.6	10.6	85	51	70	69	W	1	NNW	1	SSE	2
11	710.5	709.6	709.9	15.6	24.2	16.8	18.4	24.8	13.7	-	10.5	08.5	10.1	79	37	70	62	-	0	NNW	2	-	0
12	709.5	709.4	709.7	16.4	29.8	20.5	22.0	29.8	12.6	-	10.4	10.5	12.0	74	33	65	57	ESE	2	W	3	-	0
13	710.3	707.9	708.1	17.0	31.0	21.2	22.6	31.0	13.6	-	10.6	12.1	10.5	73	36	56	55	ESE	1	W	2	-	0
14	708.3	707.5	708.2	18.3	30.8	21.2	22.5	31.0	13.7	-	09.2	09.8	11.7	58	29	62	50	ESE	3	W	2	-	0
15	709.7	709.2	709.8	16.8	32.0	22.8	23.6	32.0	14.0	-	09.4	11.3	11.0	66	32	53	50	E	3	NW	2	-	0
16	709.3	708.1	707.7	18.0	31.8	22.8	23.8	32.4	15.7	-	11.1	11.4	12.7	72	32	61	55	ESE	2	SW	2	-	0
17	706.2	704.1	703.7	20.4	33.0	25.8	26.2	33.1	16.7	-	11.2	09.0	05.8	62	24	40	42	ESE	1	WSW	4	-	0
18	702.5	701.9	703.2	20.4	29.6	20.1	22.6	29.8	17.8	-	10.5	09.3	10.5	58	30	60	49	-	0	SSW	4	-	0
19	702.8	703.7	704.2	17.5	14.4	12.9	14.4	20.2	12.8	-	12.9	10.8	10.7	86	88	96	90	W	1	-	C	WSW	1
20	704.5	705.6	705.6	11.5	10.8	10.8	11.0	13.2	10.3	-	09.7	08.9	05.3	96	92	95	94	NNW	1	W	1	-	0
21	710.4	703.9	704.6	10.4	11.9	10.8	11.0	12.9	09.8	-	08.8	08.6	09.3	93	83	95	90	-	0	W	1	-	0
22	706.2	707.3	707.1	10.7	12.5	11.2	11.4	13.3	10.3	-	05.3	09.0	09.1	97	83	91	90	W	1	-	0	-	0
23	706.0	707.2	708.6	10.8	12.9	11.8	11.9	13.0	10.2	-	09.3	10.6	09.9	95	95	96	95	-	0	W	2	SE	1
24	709.0	707.9	707.5	11.9	24.6	19.4	18.8	24.9	10.3	-	09.9	10.4	11.2	96	45	67	69	-	0	NW	2	-	0
25	707.6	705.9	708.3	14.6	27.2	16.8	18.7	27.2	11.7	-	09.3	11.2	11.4	75	41	81	66	SE	2	W	3	SW	2
26	710.3	710.4	710.8	12.9	18.4	13.2	14.4	18.5	12.8	-	08.5	10.2	08.8	76	64	77	72	ESE	3	SSE	3	E	2
27	710.8	709.2	709.7	10.3	25.0	17.6	17.8	25.4	08.7	-	08.4	11.3	10.9	86	48	72	69	-	0	W	1	S	2
28	710.6	709.6	711.2	14.0	27.8	20.5	20.7	27.8	10.8	-	09.5	11.8	10.7	79	42	59	60	ESE	1	W	1	-	0
29	712.5	711.2	711.9	15.2	27.8	20.9	21.2	28.4	13.2	-	10.9	15.5	11.9	84	55	64	68	SE	1	NNW	2	E	1
30	711.2	709.2	708.2	16.9	29.0	21.3	22.1	29.4	14.3	-	11.9	10.0	13.9	82	33	72	63	-	0	W	1	ESE	2
31	708.2	706.6	707.4	17.4	30.4	21.3	22.6	30.5	15.8	-	12.2	11.3	15.6	82	35	82	66	SSE	1	NNW	1	ESE	2
MES. MRED.	708.3	707.8	708.1	14.6	23.5	17.5	18.3	24.5	12.2	-	10.0	10.3	10.6	80	51	71	68	0.6	2.0	0.8			

1	707.8	707.1	707.8	18.8	28.9	20.5	22.2	28.9	16.6	-	13.1	14.9	13.7	81	50	76	69	SE	1	SW	2	E	2
2	708.4	707.3	708.0	16.7	30.4	22.1	22.8	30.4	14.8	-	11.6	13.3	13.6	81	41	68	63	ESE	2	WSW	1	E	2
3	709.9	708.4	709.3	17.4	32.1	23.0	23.9	32.2	15.6	-	11.7	12.0	13.3	78	33	62	58	-	0	WSW	1	E	2
4	710.2	708.7	708.9	18.2	32.6	23.7	24.6	32.4	16.0	-	11.8	10.1	13.7	75	27	62	55	ESE	1	-	0	SE	1
5	710.5	708.6	708.7	18.6	32.2	21.8	23.6	32.4	16.7	-	13.5	08.8	10.4	64	24	53	54	ESE	1	NW	1	-	0
6	710.8	711.7	711.9	16.8	20.5	16.6	17.6	21.8	14.7	-	11.7	11.0	09.8	81	61	69	70	-	0	E	1	NW	2
7	710.6	707.4	707.1	12.5	24.2	17.3	17.8	25.0	10.2	-	08.9	10.3	10.2	82	46	69	66	-	0	W	2	ESE	2
8	705.9	703.6	702.7	13.2	29.2	22.0	21.6	29.8	11.2	-	09.0	10.8	12.0	79	36	61	59	-	0	NW	2	-	0
9	704.0	701.6	705.9	16.0	27.5	14.8	17.0	26.1	14.3	-	11.6	13.3	11.9	85	65	94	81	N	1	WNW	2	-	0
10	708.2	705.8	704.6	13.5	25.1	17.8	18.6	25.4	10.3	-	09.5	10.0	10.5	82	42	68	64	E	1	E	2	ESE	2
11	701.9	700.5	706.0	13.5	16.9	11.6	13.4	21.2	11.6	-	11.2	12.7	08.1	97	86	79	88	ESE	3	W	2	W	3
12	706.7	706.6	708.3	08.0	17.7	13.5	13.2	19.3	06.9	-	07.6	07.7	08.2	95	51	71	72	-	0	W	4	-	0
13	710.5	710.3	711.8	12.6	22.0	13.5	15.4	22.2	11.4	-	08.9	07.5	08.9	81	38	77	65	-	0	W	2	-	0
14	713.0	712.2	713.1	11.4	27.0	16.7	16.0	27.4	08.2	-	07.8	10.4	08.8	77	39	54	57	ESE	1	WNW	2	SE	2
15	714.4	713.2	713.7	13.3	29.0	19.8	20.5	29.3	11.4	-	09.3	13.0											

BR. ST. 143

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_i = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavina R mm	Snežni pokrivenje h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	03	04	00	02.3	11.2	02.2	.	= 0-10 <sup>30</sup> △ 0 <sup>45</sup> -8 <sup>30</sup> , 20 <sup>30</sup> 24		
2	8	07	05	07	06.3	04.1	.	.	△ 0-8 <sup>30</sup>		
3	8	00	00	00	00.0	14.0	.	.	△ 0 <sup>20</sup> 9, 21 <sup>30</sup> 24		
4	7	10	10	10	10.0	00.0	.	.	△ 0-9 <sup>30</sup>		
5	8	00	01	02	01.0	10.2	.	.	= 1 <sup>0</sup> 9, △ 1 <sup>0</sup> 9, 20 <sup>30</sup> 24		
6	8	00	08	00	02.7	07.5	.	.	△ 0-8 <sup>30</sup> 21 <sup>30</sup> 24, R 13 <sup>30</sup> 13 <sup>55</sup> 13 <sup>55</sup> 44 <sup>45</sup> △ 14-11 <sup>05</sup>		
7	6	06	10	00	05.3	03.6	00.6	.	△ 0-8 <sup>30</sup> 9 <sup>30</sup> 14 <sup>30</sup> R 9 <sup>30</sup> 10 <sup>05</sup> = 10 <sup>30</sup> 15		
8	8	10	10	01	07.0	02.1	13.0	.	= 1 <sup>0</sup> 8, △ 20 <sup>30</sup> 24		
9	8	10	01	02	05.0	09.3	.	.	△ 0-9, 21 <sup>30</sup> 24		
10	8	10	08	10	05.3	04.5	00.0	.	△ 0-6, △ 5 <sup>30</sup> 17 <sup>20</sup>		
11	7	05	10	02	05.7	08.5	00.0	.	△ 0-9, 21 <sup>30</sup> 24		
12	8	04	00	00	01.3	13.5	.	.	△ 0-8 <sup>30</sup> 22 <sup>30</sup> 24		
13	8	00	00	00	00.0	14.0	.	.	△ 0-8		
14	8	00	00	00	00.0	13.9	.	.	△ 0-8		
15	8	00	00	00	00.0	13.2	.	.	△ 0-8		
16	8	00	01	03	01.3	12.1	.	.	F <sub>sw</sub> 14 <sup>40</sup>		
17	8	04	01	00	01.7	11.6	.	.	△ 3 <sup>0</sup> 7 <sup>30</sup> F <sub>s</sub> 12 <sup>05</sup> 12 <sup>25</sup>		
18	8	00	01	02	01.0	11.2	.	.	= 0-9, 14 <sup>30</sup> 24, △ 0 <sup>30</sup> 9, △ 10 <sup>30</sup> 13 <sup>0</sup> , △ 14 <sup>45</sup> 16 <sup>05</sup> 18 <sup>30</sup> 24, R 21 <sup>30</sup> 22 <sup>30</sup>		
19	7	09	10	10	04.7	05.5	.	.	● 0-1 <sup>05</sup> 18 <sup>30</sup> 24, △ 0-24, R 0-1		
20	6	10	10	10	10.0	00.0	14.5	.	● 0-9, 21 <sup>30</sup> 24, △ 0-24, R 0-1		
21	6	10	10	10	10.0	00.0	01.0	.	= 0-24, △ 0-9 <sup>30</sup> 24, △ 9 <sup>30</sup> 10 <sup>30</sup> 10 <sup>30</sup>		
22	7	10	10	10	10.0	00.0	11.4	.	● 0-9 <sup>30</sup> 14 <sup>30</sup> 15 <sup>30</sup> , △ 20 <sup>30</sup> 23 <sup>30</sup> , △ 0-12, 21 <sup>30</sup> 24, R 9 <sup>30</sup> 11 <sup>30</sup>		
23	7	10	10	09	09.7	00.0	04.2	.	= 0-20, △ 0 <sup>30</sup> 11 <sup>30</sup> , 16 <sup>30</sup> 17 <sup>30</sup>		
24	8	10	01	00	03.7	09.6	05.8	.	= 9-11		
25	8	00	03	07	03.3	12.4	.	.	△ 0 <sup>15</sup> 8		
26	8	10	10	03	07.7	00.0	.	.	△ 22 <sup>15</sup> 24		
27	8	00	00	00	00.0	13.4	.	.	△ 0-8 <sup>30</sup> 21 <sup>30</sup> 24		
28	8	00	01	01	00.7	12.8	.	.	△ 0-7 <sup>30</sup> 22 <sup>30</sup> 24		
29	8	00	01	01	00.7	13.1	.	.	△ 0-9, 21 <sup>30</sup> 24, △ 8 <sup>30</sup> 11		
30	7	00	01	00	00.3	12.9	.	.	△ 0-9, △ 8 <sup>30</sup> 11 <sup>30</sup> , △ 18 <sup>30</sup> R 17 <sup>30</sup> 13 <sup>30</sup>		
31	8	00	01	00	00.3	12.6	.	.	△ 0-8, △ 8 <sup>30</sup> 11 <sup>30</sup> , △ 18 <sup>30</sup> R 17 <sup>30</sup> 13 <sup>30</sup>		
MES. VR ED.		04.4	04.5	03.2	04.1	252.2	53.1				

1	8	01	06	00	02.3	08.5	C1.7	.	△ 0-8, 23-24, △ 8 <sup>30</sup> 12, △ 14 <sup>30</sup> 14 <sup>40</sup>		
2	8	00	01	00	00.3	12.9	C0.0	.	△ 0-8, 23-24, △ 6-9		
3	7	00	03	00	01.0	12.8	.	.	△ 0-8, 23-24		
4	8	00	02	C1	01.0	13.0	.	.	△ 0-7 <sup>30</sup> , △ 3 <sup>30</sup> 7 <sup>30</sup>		
5	8	00	00	00	00.0	12.6	.	.	△ 0-8, △ 5 <sup>30</sup> 9		
6	8	05	10	02	05.7	00.6	.	.	△ 0 <sup>30</sup> 8, 22 <sup>30</sup> 24		
7	8	01	01	00	00.7	12.8	.	.	△ 0-8, 20 <sup>30</sup> 24, △ 4 <sup>30</sup> 9 <sup>30</sup>		
8	7	00	01	03	C1.3	12.4	.	.	△ 0-7 <sup>30</sup> , △ 2 <sup>30</sup> M, 23-24, R 23 <sup>30</sup> 24		
9	8	09	10	C2	07.0	C6.5	C1.2	.	R 0-25, 10 <sup>30</sup> 15 <sup>30</sup> , △ 0-6, △ 0 <sup>30</sup> 6 <sup>30</sup> , 14 <sup>30</sup> 15 <sup>30</sup> , △ 13 <sup>30</sup>		
10	8	01	04	00	01.7	12.6	05.0	.	△ 0-9, 23-24		
11	7	10	10	10	10.0	00.9	C4.3	.	△ 0-3 <sup>20</sup> 18, 3 <sup>30</sup> 4 <sup>30</sup> 14 <sup>30</sup> , △ 3 <sup>30</sup> 9 <sup>30</sup> 12 <sup>45</sup> 14 <sup>45</sup> , △ 12 <sup>45</sup> 14 <sup>45</sup> 14 <sup>45</sup>		
12	8	06	09	06	07.0	05.1	06.1	.	△ 0-9, 23-24, △ 6-8 <sup>30</sup>		
13	8	06	04	02	04.0	C9.3	.	.	△ 0-8, 21 <sup>30</sup> 24		
14	8	00	01	00	00.3	13.2	.	.	△ 0-8, 21 <sup>30</sup> 24		
15	8	04	01	00	01.7	12.1	.	.	△ 0-8, 23 <sup>30</sup> 24		
16	8	01	07	00	02.7	08.5	.	.	△ 0-8, 21 <sup>30</sup> 24, △ 22 <sup>30</sup> 9 <sup>45</sup>		
17	6	00	01	00	00.3	12.2	.	.	△ 0-7 <sup>30</sup> 20 <sup>30</sup> 24, △ 0-20		
18	7	00	00	00	00.0	12.7	.	.	△ 0-8, 21 <sup>30</sup> 24		
19	8	00	00	00	00.0	12.5	.	.	△ 0-8, 23-24, △ 6-9		
20	8	00	01	00	00.3	12.1	.	.	△ 0-8, 22 <sup>30</sup> 24		
21	8	03	05	08	05.3	03.1	.	.	△ 0-8, 8 <sup>30</sup> M, 18, 14 <sup>20</sup> 15 <sup>30</sup> , △ 14 <sup>45</sup> 16 <sup>45</sup> , △ 14 <sup>55</sup> 15 <sup>10</sup>		
22	8	00	01	02	C1.0	12.4	C5.5	.	△ 3-8 <sup>30</sup> , △ 5-9, △ 20 <sup>30</sup> 22 <sup>30</sup> , R 22 <sup>30</sup> 23 <sup>30</sup> , △ 22 <sup>30</sup> 22 <sup>35</sup>		
23	8	02	05	04	03.7	07.2	00.1	.	R 10 <sup>35</sup> 15 <sup>35</sup> 15 <sup>35</sup> , △ 6-8 <sup>30</sup> 18 <sup>30</sup>		
24	6	09	09	00	06.0	02.0	C2.5	.	△ 3-6 <sup>30</sup> , △ 7-24, △ 10 <sup>30</sup> 13 <sup>30</sup> , R 12 <sup>30</sup> 13 <sup>30</sup>		
25	7	10	08	R	10	09.3	03.2	01.0	= 0-9, △ 14 <sup>45</sup> 18, R 13 <sup>45</sup> , △ 14 <sup>45</sup> 14 <sup>45</sup> , R 16 <sup>45</sup> 16 <sup>45</sup> , △ 14 <sup>45</sup> 14 <sup>45</sup> , △ 23-23, △ 15 <sup>15</sup> 17 <sup>40</sup>		
26	7	09	09	R	02	06.7	C3.7	1C.5	△ 5-9, △ 8 <sup>30</sup> 12, R 13 <sup>35</sup> 14 <sup>20</sup> , △ 13 <sup>30</sup> 17 <sup>20</sup>		
27	8	09	07	10	08	06.7	04.5	C0.8	= 8-11, R 14 <sup>30</sup> 15 <sup>30</sup> , △ 14 <sup>45</sup> 15 <sup>45</sup> , △ 20 <sup>30</sup> 21 <sup>30</sup>		
28	8	10	10	R	10	10.0	02.2	C3.2	△ 5 <sup>30</sup> 8, △ 8-12, 24 <sup>30</sup> 24, R 12 <sup>30</sup> 18, △ 12 <sup>30</sup> 22 <sup>30</sup>		
29	8	05	06	03	04.7	09.1	15.2	.	△ 0-11, △ 5-9, 12 <sup>30</sup> 22 <sup>30</sup>		
30	8	00	10	C1	03.7	06.0	.	.	△ 0-8, 21 <sup>30</sup> 24, △ 12-12 <sup>30</sup> , R 12 <sup>30</sup> 13 <sup>30</sup> , △ 12 <sup>30</sup> 13 <sup>30</sup>		
31	7	00	C3	00	01.0	C9.0	13.1	.	△ 0-11, 19 <sup>30</sup> 24, △ 7-13 <sup>30</sup>		
MES. VR ED.		03.2	04.7	02.4	03.5	266.5	74.7				

$\psi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1h\ 14\ min.$ 

BR. ST. 143

D E F G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21		
1	707.8	707.1	707.2	13.1	25.4	17.4	18.3	25.4	12.1	-	10.2	11.7	11.5	91	48	77	72	ESE 2	-	0	SE 1	
2	707.9	708.1	708.2	14.8	25.4	17.8	19.0	26.2	13.6	-	12.0	12.6	12.0	95	52	78	75	SE 2	2	W 1	-	0
3	708.8	707.4	707.8	15.3	28.2	19.6	20.7	28.5	13.5	-	10.4	12.5	13.9	80	43	81	68	ESE 3	WSW 2	-	0	
4	706.6	705.2	708.5	16.6	28.6	15.4	19.0	29.6	14.6	-	11.3	11.4	12.2	80	39	93	71	-	0	SW 2	-	0
5	710.8	709.6	709.0	13.3	22.2	14.3	16.0	22.5	12.3	-	09.9	10.2	10.1	88	51	82	73	-	0	NW 1	E	2
6	707.6	705.0	701.0	09.6	26.0	17.2	17.5	26.5	06.7	-	08.1	12.3	05.8	91	45	66	65	-	0	-	C SSE 2	
7	698.8	700.6	703.2	15.0	14.7	13.2	14.0	18.1	12.8	-	08.7	11.4	10.9	68	91	96	85	SE 2	2	W 1	WSW 1	
8	707.0	709.3	711.1	13.0	17.1	14.2	14.6	18.5	12.4	-	10.8	11.3	11.2	96	77	92	88	-	0	-	0 E	1
9	712.7	711.4	711.2	11.9	24.4	16.8	17.5	25.0	11.5	-	10.1	13.5	12.5	97	59	87	81	-	0	W 2	SE 3	
10	712.0	711.0	713.1	13.2	26.7	15.8	19.5	27.0	12.2	=	10.9	12.8	13.2	96	41	78	71	-	0	W 3	=	0
11	715.5	714.5	715.1	13.2	18.3	16.0	15.9	19.8	13.2	-	09.2	10.5	10.1	80	66	74	73	-	0	-	0 SE 2	
12	713.7	712.1	703.0	13.3	23.4	16.1	17.2	23.8	12.8	-	10.4	12.1	11.9	91	56	87	78	-	0	WSW 2	-	0
13	712.4	710.8	711.7	15.2	25.5	16.7	18.5	26.0	15.0	-	11.4	12.1	11.9	88	49	83	73	ESE 1	WSW 1	-	0	
14	712.3	711.2	711.4	15.6	23.6	16.1	17.8	23.6	14.2	-	11.5	12.3	11.1	86	56	81	74	-	0	W 3	ENE 1	
15	711.0	709.4	710.5	11.6	23.2	16.6	17.0	23.6	10.7	-	09.6	12.5	11.3	93	58	80	77	ESE 2	NW 2	E	3	
16	711.0	710.0	711.4	12.8	23.4	14.5	16.3	23.8	11.5	-	10.3	10.6	09.9	93	49	80	74	SE 1	NW 1	ESE 2		
17	711.8	710.2	710.8	10.4	23.0	15.6	16.2	23.3	09.2	-	08.6	12.0	11.7	91	57	88	79	SE 2	WSW 1	-	0	
18	711.1	709.7	710.3	11.4	25.0	17.1	17.6	25.1	10.2	-	09.0	10.1	11.9	89	42	82	71	SE 2	WW 2	-	0	
19	710.8	709.4	709.2	12.5	23.2	15.8	16.8	23.7	11.5	-	10.4	11.3	11.4	96	53	85	78	E 1	WSW 1	ESE 2		
20	706.7	704.0	704.5	12.4	23.0	16.4	17.0	24.7	11.2	-	09.9	12.0	11.5	91	57	82	77	ESE 1	WSW 1	-	0	
21	703.9	703.6	704.2	13.8	20.0	15.3	16.1	21.0	12.5	-	11.3	12.0	10.8	96	65	83	SSE 2	N 1	-	0		
22	703.8	705.8	706.9	14.0	17.0	15.2	15.4	20.3	13.5	-	11.0	13.0	10.6	92	90	82	88	S 2	-	0		
23	706.0	705.9	706.0	12.6	20.6	14.6	15.6	20.8	12.4	-	10.2	10.9	09.2	94	60	74	76	SE 1	W 2	E 2		
24	703.7	702.4	700.2	14.9	18.3	14.4	15.5	20.5	11.7	-	09.2	09.4	09.8	72	55	79	70	N 2	SSW 5	-	0	
25	695.6	696.2	705.7	16.0	15.1	09.4	12.5	17.3	09.4	-	08.1	08.1	07.5	59	63	65	69	S 5	NW 2	-	0	
26	691.1	692.6	699.7	06.7	07.7	06.2	07.2	11.0	06.1	-	07.7	07.6	06.7	92	96	95	94	ESE 3	W 3	-	0	
27	705.9	707.3	708.7	06.0	14.7	06.4	08.4	15.0	05.0	-	06.8	05.3	06.2	97	42	85	75	-	0	W 2	E 2	
28	700.1	705.6	706.1	02.9	19.9	04.2	10.3	20.3	02.3	-	05.4	06.6	07.2	95	39	82	72	-	0	WSW 1	-	0
29	704.5	701.5	706.0	07.5	18.9	16.8	17.0	21.2	05.5	-	06.2	08.5	07.9	80	52	55	62	E 1	S 2	S 4		
30	705.4	703.7	716.3	17.2	18.0	09.6	13.6	20.3	09.1	-	07.8	10.7	08.8	53	69	98	73	S 3	ENE 1	NW 1		
MES.	VRED.	707.4	706.8	707.6	12.6	21.4	14.8	15.6	22.4	11.0	-	09.5	10.6	10.5	87	58	82	76	1.3	1.4	0.9	

BR. ST. 143

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijnost O. -	Oblačnost N (0-10)					Insolacij broj sati	Podzemne R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	08	020	04	04.7	06.4	00.1	.	.	0-0-8 <sup>30</sup> 18 <sup>45</sup> 24, 0-5 <sup>35</sup> 6	
2	7	09	070	01	05.7	08.7	05.5	.	.	0-5 <sup>35</sup> 20-24, 13 <sup>45</sup> 6 <sup>30</sup> , 0-5 <sup>35</sup> 5 <sup>15</sup> , 0-5 <sup>35</sup> 6 <sup>30</sup>	
3	8	040	020	00	02.0	10.6	.	.	.	0-8 <sup>30</sup> 20 <sup>24</sup> , 24	
4	8	05	020	10	05.7	09.9	.	.	.	0-8 <sup>30</sup> 18 <sup>30</sup> 20 <sup>24</sup> , 18 <sup>45</sup> 19 <sup>20</sup> , 0-19 <sup>20</sup> 20 <sup>25</sup> , 0-20 <sup>30</sup> 21 <sup>15</sup>	
5	9	030	010	00	01.3	11.8	14.6	.	.	0-20-24	
6	8	000	000	07	02.3	11.0	.	.	.	0-9 <sup>15</sup> 19-24	
7	6	08	100	10	09.3	00.2	.	.	.	0-8 <sup>30</sup> 0-9 <sup>15</sup> 19 <sup>30</sup> 23 <sup>50</sup> 24, 18 <sup>45</sup> 19 <sup>55</sup> 10 <sup>30</sup> , 0-19 <sup>30</sup> 23 <sup>50</sup>	
8	6	10	10	07	09.0	00.3	07.5	.	.	0-24, 0-4 <sup>30</sup> , 0-3 <sup>25</sup> 6 <sup>30</sup> , 0-20-24	
9	7	000	010	00	00.3	00.2	.	.	.	0-3 <sup>30</sup> 6-11 <sup>30</sup> , 0-10 <sup>30</sup> 18 <sup>30</sup> 24, 0-3 <sup>30</sup> 6	
10	8	000	010	10	03.7	05.8	.	.	.	0-11 <sup>30</sup> , 0-7 <sup>30</sup> 19 <sup>30</sup> 19 <sup>25</sup> , 0-21 <sup>30</sup> 23 <sup>30</sup> , 0-22 <sup>30</sup> 23 <sup>15</sup>	
11	7	10	10	10	10.0	01.6	01.2	.	.	0-6 <sup>30</sup> , 22 <sup>30</sup> 24	
12	7	09	010	00	03.3	07.0	.	.	.	0-9 <sup>30</sup> 20-24, 0-6-11 <sup>30</sup> 21 <sup>30</sup> , 23, 0-23-24	
13	8	10	010	00	03.7	07.5	.	.	.	0-9 <sup>30</sup> 20 <sup>30</sup> , 0-24, 0-6-11, 0-21 <sup>30</sup> 24	
14	6	09	040	05	06.0	05.4	.	.	.	0-8 <sup>45</sup> 19 <sup>30</sup> 24, 0-24, 0-11 <sup>30</sup>	
15	7	000	060	09	05.0	08.1	.	.	.	0-9, 0-19-24, 0-11 <sup>30</sup>	
16	7	10	050	00	05.0	05.1	.	.	.	0-0-10 <sup>30</sup> 19 <sup>30</sup> 24, 0-5-13 <sup>30</sup>	
17	7	000	030	00	01.0	01.0	.	.	.	0-0-9 <sup>30</sup> 20 <sup>30</sup> , 0-24, 0-10 <sup>30</sup> 24, 0-14 <sup>30</sup> 24, 0-24	
18	6	03	040	10	05.7	05.1	.	.	.	0-9, 0-18, 0-18 <sup>45</sup> 20 <sup>30</sup> , 0-19 <sup>30</sup> 19 <sup>35</sup>	
19	7	10	0F	00	06.0	06.5	00.1	.	.	0-8 <sup>30</sup> 20-24, 0-5-11 <sup>30</sup> 13 <sup>35</sup> 15 <sup>05</sup> 16	
20	8	000	09	10	06.3	06.3	00.0	.	.	0-0-9 <sup>30</sup> , 0-12, 0-7 <sup>30</sup> 8 <sup>30</sup> , 0-15 <sup>35</sup> 16 <sup>20</sup> , 0-20 <sup>35</sup> 24, 0-16 <sup>20</sup> 16 <sup>10</sup> , 0-20 <sup>40</sup> 26 <sup>45</sup>	
21	8	10	09	06	08.3	02.8	13.0	.	.	0-10 <sup>30</sup> 0-6 <sup>30</sup> 10 <sup>30</sup> , 0-22 <sup>30</sup> 23	
22	8	05	040	04	06.0	02.8	16.4	.	.	0-15, 0-15, 0-15, 0-15	
23	6	10	07	00	05.7	03.3	02.1	.	.	0-3, 0-19 <sup>30</sup> 24, 0-3-3-3 <sup>30</sup> 6 <sup>45</sup> 17 <sup>05</sup> 9 <sup>50</sup> 40 <sup>30</sup> , 0-5 <sup>30</sup> 9	
24	8	08	08	08	08.3	04.5	00.3	.	.	0-8, 0-16 <sup>30</sup> 24, 0-18 <sup>30</sup> 20-20 <sup>30</sup>	
25	7	08	09	02	04.3	02.1	04.6	.	.	0-20 <sup>20</sup> 25, 0-7 <sup>30</sup> 8 <sup>30</sup> , 0-14-13, 0-15 <sup>20</sup> 15 <sup>40</sup>	
26	5	10	10	10	10.0	00.0	03.8	.	.	0-4 <sup>30</sup> 0-3 <sup>30</sup> 10 <sup>35</sup> 24, 0-10 <sup>30</sup> 4 <sup>30</sup>	
27	8	10	040	00	04.7	06.5	14.7	.	.	0-6 <sup>35</sup> , 0-18 <sup>30</sup> 24	
28	7	000	000	00	00.0	10.6	.	.	.	0-10 <sup>30</sup> 20-24, 0-7 <sup>30</sup> 12 <sup>30</sup>	
29	8	010	09	09	06.3	06.8	.	.	.	0-8 <sup>40</sup> , 0-18 <sup>30</sup> 24, 0-24	
30	7	080	09	10	09.0	02.3	.	.	.	0-18 <sup>30</sup> 10 <sup>35</sup> , 0-15-24	
MES. VRED.			05.4	05.4	04.7	05.4	185.6	84.5			

1	8	10	030	10	07.7	03.7	19.4	.	.	0-11 <sup>30</sup> , 0-3 <sup>25</sup> 4, 0-10 <sup>30</sup> M, 0-6-7 <sup>30</sup> 9 <sup>40</sup> 10 <sup>10</sup> , 0-20 <sup>30</sup> 24	
2	7	10	10	06	09.7	00.0	03.6	.	.	0-6 <sup>35</sup> , 0-6 <sup>35</sup> 7 <sup>30</sup> , 0-13 <sup>45</sup> 22 <sup>20</sup> , 0-15 <sup>45</sup> 16 <sup>30</sup> , 0-18 <sup>45</sup> 21 <sup>40</sup>	
3	8	09	010	04	04.7	09.5	06.3	.	.	0-18 <sup>30</sup> 24	
4	9	080	030	09	04.7	04.1	.	.	.	0-7 <sup>30</sup> 20 <sup>30</sup> 24	
5	7	10	08	03	07.0	01.3	00.7	.	.	0-6 <sup>40</sup> , 0-20-24, 0-6 <sup>40</sup> , 0-22 <sup>30</sup> , 0-6 <sup>40</sup> , 0-22 <sup>30</sup> 24, 0-5 <sup>20</sup> 24	
6	7	10	10	10	10.0	00.0	08.0	08.0	.	0-0-8 <sup>30</sup> , 11 <sup>35</sup> , 0-12 <sup>30</sup>	
7	5	10	10	10	10.0	00.0	11.8	.	.	0-14 <sup>30</sup> , 0-7-12 <sup>30</sup> , 0-11 <sup>35</sup> , 0-15 <sup>35</sup> , 0-18 <sup>30</sup> , 0-16-16 <sup>05</sup> , 0-16 <sup>20</sup> , 0-16 <sup>35</sup>	
8	7	08	09	00	05.7	01.4	02.2	.	.	0-3 <sup>45</sup> 16 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-18 <sup>30</sup> , 0-18 <sup>30</sup>	
9	8	10	040	10	08.0	05.5	07.6	.	.	0-4 <sup>30</sup> 16 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-17 <sup>30</sup> , 0-18 <sup>30</sup> , 0-18 <sup>30</sup>	
10	8	08	040	00	04.0	09.1	02.3	.	.	0-3 <sup>20</sup> 4 <sup>30</sup> , 0-6 <sup>30</sup>	
11	8	08	010	09	06.0	06.1	.	.	.	0-5 <sup>30</sup> 20 <sup>05</sup> 24, 0-4 <sup>30</sup> 6 <sup>45</sup> , 0-8 <sup>30</sup> 10 <sup>30</sup> , 0-5 <sup>30</sup> 7 <sup>30</sup> , 0-6 <sup>30</sup> 8 <sup>30</sup>	
12	8	05	10	07	07.3	00.8	.	.	.	0-3 <sup>45</sup> , 0-3 <sup>45</sup> 7 <sup>30</sup>	
13	6	10	10	10	10.0	00.0	00.0	07.3	.	0-2 <sup>45</sup> , 0-22 <sup>30</sup> , 0-24	
14	4	10	10	10	10.0	00.0	00.0	27.2	.	0-24, 0-11 <sup>30</sup> , 0-15-20 <sup>20</sup> , 0-15 <sup>30</sup> 15	
15	4	10	10	10	10.0	00.0	00.0	06.7	.	0-15, 0-20 <sup>20</sup> 24, 0-25 <sup>30</sup> 17 <sup>20</sup> , 0-25 <sup>30</sup> 13 <sup>20</sup> , 0-20 <sup>30</sup> 21 <sup>30</sup> , 0-13 <sup>20</sup> 20 <sup>30</sup> , 0-22 <sup>15</sup> 24, 0-15-20 <sup>35</sup>	
16	6	07	10	06	07.7	01.9	23.7	.	.	0-0-25 <sup>30</sup> 10 <sup>35</sup> 12 <sup>20</sup> , 0-14 <sup>25</sup> 10 <sup>35</sup> 22, 0-20-24, 0-8 <sup>45</sup> 10 <sup>35</sup> , 0-8 <sup>45</sup> 16 <sup>30</sup>	
17	8	10	040	00	04.7	07.6	05.4	.	.	0-5 <sup>40</sup> 7 <sup>30</sup> , 0-23 <sup>45</sup> 24, 0-6 <sup>40</sup> , 0-8 <sup>40</sup> , 0-8 <sup>40</sup> , 0-18-24	
18	6	000	060	00	02.0	08.4	.	.	.	0-0-8, 0-6-7 <sup>30</sup> , 0-24, 0-7 <sup>30</sup> , 0-10 <sup>30</sup> , 0-18 <sup>30</sup> 24	
19	6	10	040	00	04.7	06.0	.	.	.	0-5-11-10 <sup>30</sup> , 0-0-3-20 <sup>30</sup> 24, 0-3-10 <sup>30</sup> , 0-5-10 <sup>30</sup> , 0-10 <sup>30</sup>	
20	7	10	10	06	08.7	00.5	00.5	.	.	0-11 <sup>30</sup> 15 <sup>30</sup> , 0-15 <sup>30</sup> 24, 0-24	
21	8	10	10	10	10.0	00.5	00.2	01	.	0-0 <sup>15</sup> , 0-6-7 <sup>30</sup> , 0-11 <sup>30</sup> 17 <sup>30</sup> , 0-23 <sup>45</sup> 23 <sup>45</sup> , 0-23 <sup>45</sup> 24	
22	7	040	10	10	08.0	02.0	06.4	15.5	.	*0-3, 0-8 <sup>30</sup> , 0-12 <sup>30</sup> , 0-24, 0-8 <sup>30</sup> , 0-13 <sup>30</sup> , 0-16 <sup>30</sup> , 0-16 <sup>30</sup>	
23	4	10	10	10	10.0	00.0	00.0	27.1	.	0-24, 0-24, 0-24, 0-24, 0-24, 0-24	
24	8	010	030	09	04.3	08.4	36.4	.	.	0-0 <sup>40</sup> , 0-2, 0-6 <sup>30</sup> , 0-11 <sup>30</sup> , 0-24 <sup>30</sup> , 0-24	
25	8	09	040	00	04.3	07.6	*	.	.	0-0-9, 0-18 <sup>30</sup> 24, 0-5 <sup>20</sup> 11	
26	7	070	10	10	09.0	04.8	.	.	.	0-0-7 <sup>30</sup> , 0-7 <sup>30</sup> , 0-12 <sup>30</sup> , 0-18 <sup>30</sup> , 0-18 <sup>30</sup> 24	
27	8	010	050	00	02.0	06.4	11.5	.	.	0-2 <sup>30</sup> , 0-6-7 <sup>30</sup> , 0-23 <sup>45</sup>	
28	6	08	030	10	07.0	04.7	.	.	.	0-0-6, 0-15 <sup>30</sup> , 0-24, 0-15 <sup>30</sup> 24	
29	6	10	10	10	10*	10.0	00.0	18.0	01	0-0-2, 0-0-0, 0-2 <sup>30</sup> , 0-8 <sup>30</sup> , 0-8 <sup>30</sup> , 0-9 <sup>30</sup> , 0-12 <sup>30</sup> , 0-17, *3 <sup>30</sup> -5, 0-8 <sup>30</sup> , 0-9 <sup>30</sup> , 0-17-24, 0-3 <sup>30</sup>	

$\varphi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1h\ 14\ min.$

BR. ST. 143

D e n g	Vazdušni pritisak P mm			Temperatura výzduchu T °C								Napón vodene pare e mm			Relativna vláznost u %			Pravac i jačina vjetra D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	709.7	702.0	705.0	60.0	60.0	60.0	60.0	60.0	-00.3	-	04.5	04.3	04.4	98	90	97	95	-	0	NNW	2	-	0
2	706.1	705.9	707.0	-01.6	05.1	00.9	01.3	06.0	-01.8	-	03.9	04.1	04.2	95	62	85	81	-	0	NNW	2	-	0
3	708.5	708.4	709.2	00.2	07.8	02.6	03.3	09.5	-00.2	-	04.3	04.0	04.5	91	50	82	74	-	0	NNW	2	ESE	2
4	708.1	707.2	707.3	02.3	08.6	06.0	05.7	09.3	01.5	-	04.6	05.2	05.3	86	62	76	75	ESE	3	S	2	E	3
5	707.2	708.5	710.6	05.2	11.6	06.4	07.4	12.4	05.0	-	04.8	06.1	05.8	73	59	80	71	ESE	3	E	1	ESE	2
6	712.2	713.8	712.6	02.6	15.0	06.7	07.8	15.5	02.5	-	05.3	06.0	05.7	95	47	78	73	-	0	SW	1	F	2
7	712.0	709.8	709.4	05.2	05.0	03.8	04.4	06.7	03.6	-	06.0	06.4	05.7	90	97	94	94	-	0	-	0	-	0
8	708.7	708.7	709.4	02.3	02.2	01.3	01.8	03.8	01.2	-	05.2	05.1	04.8	97	95	95	96	-	0	NNW	1	NW	2
9	709.7	710.0	710.7	01.7	03.4	03.4	03.0	03.8	01.7	-	04.8	05.2	05.4	94	88	92	91	-	0	-	0	-	0
10	710.0	709.0	709.8	02.7	09.7	02.1	04.2	09.7	02.0	-	05.3	05.4	04.7	95	60	89	81	-	0	ESE	2	ESE	4
11	712.0	711.0	711.0	-01.1	05.0	01.4	01.7	05.3	-01.1	-	04.2	05.5	04.5	98	83	97	93	-	0	NNW	1	-	0
12	711.1	709.9	709.8	-00.1	07.0	03.2	03.4	08.2	-01.0	-	04.2	05.6	05.0	96	71	86	84	E	1	-	0	L	1
13	710.1	710.4	711.1	02.6	08.4	06.4	06.0	08.5	01.5	-	04.8	06.1	05.7	88	74	80	75	ESE	2	-	0	ESE	2
14	711.1	711.5	712.2	00.4	13.6	04.6	05.8	13.6	00.1	-	04.5	05.4	05.2	95	46	82	74	SE	2	w	2	ESE	1
15	711.0	711.6	712.3	01.8	15.4	05.0	07.2	15.3	01.7	-	04.8	06.3	05.7	92	48	83	74	ESE	2	WSW	1	ESE	1
16	711.4	710.3	712.0	03.1	16.6	05.8	07.8	16.7	02.9	-	04.9	06.1	05.6	85	43	84	71	ESE	4	WSW	1	ESE	2
17	711.4	712.2	713.0	02.2	14.9	06.4	07.7	14.9	02.6	-	04.8	06.0	05.2	84	48	71	68	ESE	2	-	0	ESE	3
18	712.5	711.1	710.8	07.7	17.0	06.4	08.1	17.4	02.1	-	04.5	06.5	05.7	80	44	79	68	ESE	3	-	0	ESE	2
19	708.4	704.9	707.6	05.9	15.7	08.3	09.6	16.6	03.6	-	05.4	05.4	07.1	77	40	86	68	ESE	2	S	4	NNW	1
20	711.4	710.2	711.2	03.4	12.7	03.4	05.7	12.7	02.5	-	05.3	05.1	04.6	91	47	78	72	-	0	-	0	-	0
21	710.2	709.0	709.5	01.0	06.7	04.6	04.4	07.0	00.6	-	03.9	05.2	05.8	79	71	85	80	ESE	2	-	0	-	0
22	710.4	709.1	709.7	07.3	11.0	02.6	05.0	11.3	02.7	-	05.5	05.6	05.0	95	57	86	80	-	0	-	0	ESE	1
23	710.0	705.5	708.8	01.8	08.9	05.6	05.5	08.9	00.8	-	04.6	05.7	05.8	89	67	85	80	-	0	C	-	0	0
24	708.7	708.6	708.0	01.6	08.3	06.8	05.9	04.0	01.3	-	04.8	05.7	05.6	94	70	76	80	ESE	2	-	0	ESE	1
25	705.1	705.6	702.6	03.3	11.6	11.8	09.6	12.0	02.4	-	04.9	06.6	06.3	85	65	80	70	SE	2	S	4	S	2
26	703.0	703.9	704.1	06.9	02.8	02.2	03.3	11.8	02.0	-	06.4	05.3	04.8	93	54	85	92	-	0	-	0	N	1
27	701.3	701.2	702.7	00.5	02.7	-00.2	00.6	03.1	-00.8	-	04.4	05.1	04.4	93	95	95	95	-	0	-	0	C	-
28	697.1	697.6	700.6	-01.5	13.6	03.3	02.2	19.4	-02.4	-	03.6	05.5	04.6	88	58	98	81	SE	2	S	5	W	1
29	707.1	707.0	707.1	-01.2	-01.1	-03.0	-02.6	01.0	-03.5	-	03.4	04.0	03.5	95	54	95	95	-	0	-	0	-	0
30	703.6	106.1	702.1	-03.6	-02.2	-04.0	-03.4	-02.0	-04.0	-	03.3	03.7	03.3	93	56	96	95	NNW	1	-	0	ESE	1
MES.	708.2	707.5	702.4	01.7	08.5	02.7	04.4	09.3	01.0	-	04.7	05.4	05.2	90	67	88	81	I.	1	I.	1	I.	1

1	707.5	708.9	712.0	-05.6	02.2	00.5	-00.6	03.2	-06.5	-	02.9	04.3	04.6	95	80	97	91	-	0	-	0	-	0	
2	712.7	715.0	715.4	-02.0	0.0	00.8	00.1	01.0	-02.4	-	03.8	04.6	04.7	96	55	97	96	SSE	1	-	C	-	0	
3	716.4	716.4	717.0	00.9	02.2	02.2	01.9	02.3	00.7	-	04.7	05.3	05.3	97	98	98	96	-	0	-	0	-	0	
4	715.4	713.3	711.5	02.5	05.0	01.4	02.8	05.3	01.6	-	05.4	06.2	05.1	98	54	97	96	-	0	-	C	-	ESE	2
5	707.0	706.2	705.4	-00.6	01.4	00.6	00.5	02.0	-00.6	-	04.3	04.9	04.7	96	57	98	98	ESE	1	S	1	-	0	
6	707.0	707.1	707.3	00.6	04.2	01.0	01.7	04.4	00.0	-	04.7	04.4	04.0	98	72	82	64	CNE	2	w	2	ENE	2	
7	707.3	708.4	705.9	00.3	04.2	02.3	02.3	04.6	-00.9	-	04.3	05.1	04.7	91	82	87	87	-	0	-	0	-	0	
8	708.0	707.1	706.1	01.9	05.9	04.0	04.4	06.0	01.4	-	04.3	05.8	06.1	81	64	94	86	ESE	2	-	0	NNW	1	
9	707.1	708.9	710.3	04.5	04.0	04.6	04.3	05.2	04.3	-	06.1	06.1	06.1	96	94	94	95	NNW	1	-	C	-	0	
10	710.4	710.2	710.3	03.7	05.4	03.6	04.1	06.8	02.9	-	05.9	06.2	05.6	99	92	94	95	0	-	0	-	0	0	
11	703.7	707.4	703.5	00.2	04.6	08.0	05.2	08.1	-00.2	-	04.5	05.6	05.8	97	65	72	66	ESF	1	-	0	NW	2	
12	700.1	702.4	701.2	00.0	00.2	-00.9	01.8	02.1	-00.9	-	05.4	04.4	04.1	63	55	96	85	NNW	2	-	C	-	NNW	1
13	697.1	697.6	700.6	-02.1	0.0	00.4	-00.9	01.2	-02.1	-	03.7	04.4	04.1	94	53	96	94	NN	1	-	0	-	0	
14	702.4	706.3	707.3	-02.3	-01.6	-02.8	-02.2	-00.6	-02.3	-	03.7	03.6	03.4	96	92	92	93	NN	2	w	2	NN	2	
15	703.0	706.5	706.0	-03.7	-02.6	-02.4	-02.4	-02.8	-03.7	-	03.2	03.3	03.2	91	86	85	87	w	2	w	2	-	0	
16	707.4	706.3	709.1	-01.4	01.1</																			

BK. ST. 143

$$H_s = 630 \text{ m} \quad H_b = 637.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.0 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacij broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	3	10*	10*	10	10.0	00.0	04.2	06	= 0° 3° - 5° 30° 20° 24°	= 0° 3° 3,5° 20° 24° * 0° 25° 19° 25°
2	5	10**	01.0	09	06.7	05.9	05.4	10	= 0° 6° 8° 24°	= 6° 8° 24°
3	8	09	05.0	08	07.3	06.3	.	03	= 6° 12°	[X]
4	7	10*	10	06	08.7	02.1	00.0	.	= 4° 7°	= 4° 11° 10° 23° 23°
5	8	07	06	08	07.0	02.5	00.0	.		
6	8	09	07	08	08.0	04.5	.	.	= 7° 13° 22° 24	
7	3	10***	10***	10*	10.0	00.0	.	.	= 0° 6° 20° 24°	= 0° 20° 24°
8	5	10*	10	10*	10.0	00.0	09.4	.	= 0° 12°	= 0° 24°, 11° 13° 25° 22° 24°, 14° 16° 25° 20° 20° * 20° 20°
9	6	10*	10	10	10.0	00.0	01.6	.	= 0° 10°	= 0° 24°, 22° 24
10	7	10	01.0	00	02.7	02.9	00.0	.	= 0° 11°	= 0° 4° 18° 23° 25°, 23° 24
11	3	10**	00.0	10**	06.7	01.3	.	.	= 10° 8° 20°	= 10° 20° 24
12	4	00**	00.0	07	02.3	03.2	.	.	= 0° 14° 17° 24°	= 0° 14° 17° 24° = 0° 14° 17° 24°
13	3	09	10**	03	07.3	00.0	.	.	= 0° 8° 20° 24°	= 0° 9° 23° 24°, 8° 10° 20°, 12° 20° 14° 30°
14	6	00	03.0	00	01.0	07.2	.	.	= 0° 14° 30°	= 0° 3° 23° 24°, 13° 20° 8° 20°
15	5	00	00.0	00	00.0	06.8	.	.	= 0° 10° 20°	= 0° 10° 20°, 20° 24
16	5	00	00.0	00	00.0	07.1	.	.	= 0° 10° 20° 24	= 0° 20° 20°
17	5	03	05.0	00	02.7	05.0	.	.	= 0° 8° 15° 24°	= 0° 8° 15° 24°
18	6	07	03.0	00	03.3	04.0	.	.	= 0° 8° 20° 24°	= 5° 10° 40°
19	8	08	08	09	08.3	03.1	.	.	= 0° 8° 10° 18° 24°	= 10° 10° 18° 24°, 10° 10° 18° 24°, 10° 10° 18° 24°
20	8	10	00.0	01	03.7	05.7	00.0	.	= 5° 10° 20°	= 5° 8°, 20° 20° 24
21	4	05	10	10	05.7	00.8	.	.	= 0° 4° 15° 20° 24°	= 8° 11° 15° 20° 24°
22	6	08	03.0	00	03.7	04.4	00.0	.	= 0° 8° 11° 15° 20° 24°	= 0° 8° 11° 15° 20° 24°
23	5	08	09	10	09.0	00.7	.	.	= 4° 8° 11° 15° 20° 24°	
24	4	09	07	08	08.0	01.7	.	.	= 0° 24°	= 0° 11° 15° 20° 24°
25	8	09	10	10	05.7	00.0	.	.	= 0° 8° 12° 15° 20° 24°	
26	5	10*	10*	10	10.0	00.0	15.2	.	= 0° 15° 25°	= 15° 25°, 8° 15° 25°
27	3	10*	10**	06	08.7	00.0	03.4	.	= 0° 8° 20° 24°	= 24° 24°, 11° 15° 20° 24°
28	8	08	10	10**	04.3	00.5	08.9	03	= 17° 20° 24° 24°	= 17° 20° 24° 24°
29	2	01	10**	10**	07.0	01.7	22.1	20	* 0° 3°	= 0° 10° 20° 24° 24°
30	3	10**	10**	02.0	07.3	00.0	.	14	= 0° 20° 20° 24° 24°	

MES.  
WREC.

SARAJEVO

1375-1376

1	5	07	08	10	06.3	00.5	.	07	$\equiv -0.14^{20} V C M_1 \equiv 14^{20} 24, \equiv 20-24^{\circ}, [x]$
2	1	10	10	10	06.0	00.0	.	07	$\equiv 0-6^{20} V 0.9 \equiv 6-24, \bullet 14^{20} 24, \bullet 12^{20} 12, [x]$
3	0	10	10	10	10.0	00.0	03.0	05	$\equiv 0-24, \bullet 0-24^{20} 9^{20} 24, \bullet 23^{20} 24, [x]$
4	2	10	10	10	06.7	00.0	04.4	.	$\bullet 0-8^{20} \bullet 16, \bullet 8^{20} 13, \bullet 13^{20} 24, \bullet 13^{20} 13, [x]$
5	3	04	10	10	06.0	00.0	00.4	.	$\equiv 0-3^{20} 7^{20} 24, \bullet 6-24, \bullet 6-7^{20}$
6	6	10	07	08	08.3	01.8	01.8	.	$\equiv 0-0^{16} \bullet 10^{20} 14^{20} \bullet 14^{20} 5^{20} 8^{20} 8^{20} 11^{20} 11^{20}$
7	4	10*	10	09	09.7	00.2	00.0	.	$\equiv 2^{20} 24, \bullet 2^{20} 8^{20}$
8	5	10	10	10	10.0	00.0	00.0	.	$\equiv 0-2^{20} M 24, \bullet 11^{20} 24, [x]$
9	5	10	10	10	10.0	00.0	03.6	.	$\equiv 0-24, \bullet 0-11^{20} \bullet 11^{20} 17^{20}$
10	3	10	10	10	10.0	01.7	01.0	.	$\equiv 0-2^{16} 19^{20} 24, \equiv 2^{20} 9^{20} 13^{20} 17^{20}$
11	5	09	09	09	09.0	00.2	.	.	$\equiv 0-8^{20} M 24, \bullet 2-4^{20} \equiv 8^{20} 11^{20} \bullet 47^{20} 24$
12	4	08	10*	10*	05.3	00.0	00.1	.	$\bullet 0-5^{20} 6^{20} 10^{20}, \bullet 5^{20} 24, \equiv 10^{20} 20^{20}, \equiv 20-24, [x]$
13	6	03	10	10*	07.7	00.2	16.1	12	$\times 0-3^{20} 17^{20} 24, \equiv 0-3^{20} 17^{20}, \equiv 3^{20} 24, [x]$
14	6	10*	10*	10*	10.0	00.0	05.9	13	$\times 0-24, \equiv 0-24, [x]$
15	5	10*	10*	10*	10.0	00.0	01.8	15	$\times 0-24, \equiv 0-24, [x]$
16	5	10	10	10	10.0	00.0	01.8	10	$\bullet 0-3, 9^{20} 12, \equiv 0-24, [x]$
17	3	00	06	00	02.0	05.4	00.0	07	$\equiv 0-2^{16} 8^{20} M 18-24^{15}, \equiv M-18, [x]$
18	5	09	10*	10	05.7	00.0	.	04	$\bullet 8^{20} 5^{20} 15^{20} \bullet 12^{20} 12^{20} \bullet 12^{20} 16, \equiv 12^{20} 14^{20}, [x]$
19	6	10	09	10*	05.7	01.8	05.6	07	$\equiv 7^{20} 24, \times 9^{20} 10^{20} \times 19^{20} 24, [x]$
20	5	07	10	00	05.7	00.2	00.0	07	$\times 0-2^{20}, \equiv 0-15^{20} 20^{20} 22^{20}, \equiv 15^{20} 18^{20}, \equiv 18^{20} 24, [x]$
21	3	02	08	10	06.7	00.0	.	04	$\equiv 0-13^{20} V 0-12^{20} \equiv 5-7^{20} \equiv 13^{20} 24, [x]$
22	3	10	10	10	10.0	00.0	.	04	$V 0-24, \equiv 0-13^{20} 13^{20} 24, \equiv 13^{20} 13^{20}, [x]$
23	3	10	06	00	03.3	00.0	.	04	$V 0-24, \equiv 0-9.2^{20} 24, \equiv 9-23, [x]$
24	3	10	06	00	03.3	00.0	.	04	$\equiv 0-9^{20} V 0-9, 11^{20} 24, \equiv 9^{20} 24, [x]$
25	3	04	10	10	08.0	00.0	.	04	$\equiv 0-24, V 0-24, [x]$
26	3	10	00	08	06.0	00.1	.	04	$\equiv 0-6^{20} 9, 18, V 0-10^{20} \equiv 6^{20} 9, \equiv 18-24, [x]$
27	3	10	04	08	07.3	03.3	.	04	$\equiv 0-1^{20} \bullet 12^{20} 4^{20} \equiv 4^{20} 17^{20}, [x]$
28	2	10	10	09	06.7	00.0	.	03	$\equiv 0-9, 19^{20} 24, \equiv 9-19^{20} 10-13^{20} 14^{20}, \times 19^{20} 20, [x]$
29	4	10	05	01	05.3	00.8	00.1	02	$\equiv 0-5, 19^{20} 4^{20} 18^{20} 24, \equiv 5^{20} 18^{20}, [x]$
30	1	01	10*	10	07.0	00.0	.	.	$\equiv 0-14^{20}, \bullet 9-10^{20} 10^{20} \times 10^{20} 23, \equiv 15^{20} 17^{20}, F 18^{20} 22^{20}, [x]$
31	7	10*	10*	09	05.7	00.0	08.0	04	$\times 6^{20} 19^{20}, F 9^{20}, [x]$

PES.  
IVRED.

$\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1h\ 22\ min.$

BR. ST. 173

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	756.2	756.2	757.0	02.9	03.5	03.2	03.2	04.7	02.6	02.4	05.6	05.7	05.3	98	97	92	96	SW 1	WSW 1	ESE 2	
2	757.3	756.3	755.4	02.0	02.8	01.6	02.0	03.2	01.4	00.9	04.2	04.4	04.1	79	78	80	79	ESE 4	ESE 5	ESE 5	
3	753.8	753.7	754.8	02.0	06.1	02.6	03.4	06.6	01.4	00.4	04.2	04.6	04.5	79	65	81	75	ESE 4	FSE 4	ESE 4	
4	757.1	757.9	750.7	03.5	08.0	01.6	04.2	08.4	02.3	01.0	04.5	04.9	04.4	77	61	79	72	SE 4	SE 4	ESE 4	
5	759.0	758.1	757.1	01.4	05.7	01.8	02.7	05.7	01.4	-00.5	04.1	04.7	04.3	81	66	82	77	ESE 4	ESE 3	ESE 3	
6	754.6	752.3	751.5	01.4	05.3	00.8	02.1	06.0	00.8	00.4	04.2	04.8	03.8	82	72	78	78	ESE 2	ESE 2	ESE 4	
7	753.2	755.1	756.6	-01.0	00.1	00.3	-00.1	00.8	-01.1	-01.2	04.0	04.3	04.4	94	93	93	93	ESE 3	ESE 2	SE 1	
8	755.4	755.4	756.6	-00.2	01.0	-00.2	00.1	01.2	-00.4	-01.9	04.0	03.9	03.7	89	80	82	84	ESE 3	ESE 3	ESE 3	
9	757.2	756.6	756.0	-02.0	01.1	-01.4	-00.9	01.7	-02.0	-02.0	03.0	03.0	03.3	76	60	80	72	ESE 4	SE 4	SE 5	
10	752.6	756.0	756.5	-01.5	00.8	-02.2	-01.3	01.2	-02.2	-02.6	03.4	03.1	02.9	82	64	75	74	ESE 6	ESE 4	SE 4	
11	759.2	750.5	740.9	-02.8	00.2	-02.4	-01.8	00.2	-03.1	-03.0	03.0	03.2	03.0	80	68	79	76	ESF 3	ESE 3	SE 2	
12	759.2	740.1	740.8	-01.6	04.4	02.5	02.0	04.7	03.5	-04.2	03.5	04.4	04.4	85	71	79	78	SE 2	WNW 1	USE 2	
13	760.2	760.3	761.2	01.0	02.0	-02.2	-00.4	02.5	-02.2	-03.0	04.2	03.7	03.1	85	65	79	78	ENE 1	-0	ESE 3	
14	761.7	760.8	760.2	-04.6	01.6	-02.4	-02.0	02.3	-05.0	-06.1	02.6	02.6	02.4	81	50	62	64	ESE 3	SE 2	ESE 3	
15	760.5	759.6	759.8	-05.9	01.9	-02.7	-02.4	02.2	-06.3	-09.8	02.5	03.1	02.6	83	60	68	70	-0	ENE 2	ESE 2	
16	757.9	758.2	756.8	-05.3	-00.4	-00.2	-01.6	00.2	-06.1	-07.3	02.3	02.0	02.2	72	67	72	71	ESE 4	-0	-0	
17	749.5	751.2	752.4	00.8	00.0	03.1	02.0	03.1	-00.9	-02.6	03.9	04.6	05.4	81	95	95	90	ESE 3	RNW 2	RNW 2	
18	752.1	751.9	753.0	07.8	04.2	02.7	02.8	04.4	01.6	00.8	04.2	04.1	04.0	75	66	74	72	W 3	NW 4	NW 3	
19	754.6	754.4	752.9	-01.4	03.7	03.2	02.2	04.6	-01.5	-04.4	03.8	04.4	05.3	92	74	92	86	RNW 1	W 3	NW 2	
20	750.6	751.3	751.4	06.8	08.3	06.6	07.1	09.5	03.2	02.8	06.6	06.4	07.7	89	77	79	82	RNW 3	NW 4	NW 4	
21	755.7	756.0	757.6	05.4	05.9	06.1	05.5	06.6	04.6	04.3	05.2	05.4	05.9	78	78	83	80	WNW 2	W 2	W 2	
22	758.4	757.6	756.4	04.4	04.2	04.6	05.4	08.9	04.0	03.2	05.5	05.2	05.4	88	64	85	79	WNW 1	W 2	SE 3	
23	755.7	757.2	755.2	-00.4	03.5	02.6	02.1	04.5	-00.9	-03.3	04.2	04.8	04.9	94	82	89	88	SW 1	W 2	NW 2	
24	756.4	755.5	755.0	02.0	05.3	02.4	03.0	05.4	01.7	00.1	05.0	05.0	05.2	95	76	88	86	SSK 1	SSK 1	SE 1	
25	754.6	753.2	754.3	-01.4	02.6	00.6	03.1	-01.5	-02.2	-04.0	04.0	04.9	04.6	97	89	97	94	SE 2	WNW 1	WNW 1	
26	755.6	755.4	754.9	00.6	07.6	02.8	03.4	08.6	-00.4	-00.7	04.5	04.6	05.2	95	59	92	82	-0	WNW 2	ESE 2	
27	753.1	751.9	752.2	00.4	08.8	03.4	04.0	09.7	00.4	-03.0	04.0	04.1	04.9	84	48	P 3	72	SE 2	WNW 1	ESE 1	
28	753.7	754.6	755.3	01.4	03.2	03.2	02.8	03.5	01.2	-02.7	04.7	05.1	05.0	93	84	86	89	NW 2	WNW 2	NW 2	
29	755.7	754.7	755.0	02.8	04.0	03.8	04.6	08.3	02.7	02.0	05.0	05.6	04.5	89	70	75	78	ESE 2	SE 3	ESE 4	
30	757.6	758.9	759.6	01.4	07.8	00.9	02.8	07.6	00.9	00.0	03.8	04.8	03.9	75	60	75	71	SE 4	SE 4	ESE 5	
31	758.8	756.0	757.7	00.4	09.2	03.7	04.2	09.3	00.0	-01.2	03.7	04.5	04.5	79	52	76	69	ESE 4	SSK 3	ESE 3	
MES.	VRFD.	756.0	756.0	756.4	00.5	04.2	01.6	02.0	04.8	-00.2	-01.4	04.1	04.4	04.3	85	71	82	79	2.5	2.4	2.6

1974 FEBRUAR

BEOGRAD

1	756.0	755.0	754.5	C2.2	12.1	06.5	07.0	12.8	00.7	-04.0	04.1	05.2	05.0	76	45	67	64	SE 1	WNW 1	EST 2
2	754.2	753.9	754.2	07.4	12.0	04.7	05.9	13.2	06.2	00.5	05.2	06.6	06.0	68	60	66	65	SE 1	SSW 1	SE 2
3	754.1	752.4	756.5	06.5	16.3	10.0	10.7	16.9	06.5	00.0	04.8	05.2	05.3	66	37	58	54	SE 2	SSE 2	SE 2
4	747.0	744.4	744.0	10.0	11.1	07.6	09.3	12.6	07.8	07.0	05.5	06.6	05.5	60	64	70	65	SSW 2	SE 3	ESE 3
5	744.7	744.9	742.5	05.6	09.0	05.6	06.4	09.5	05.1	01.2	06.4	05.4	07.0	57	94	83	81	MSH 3	SH 1	ESE 2
6	734.5	733.2	729.2	05.5	14.2	11.7	10.8	15.4	05.2	00.3	04.5	04.5	05.1	67	37	49	51	SSF 2	S 3	SSI 4
7	726.2	729.8	734.0	05.2	05.0	02.5	03.8	11.7	02.5	04.4	06.3	05.2	05.1	96	86	94	90	WSW 2	SSW 1	SW 1
P	741.4	745.6	751.1	01.2	05.4	02.4	02.8	07.0	00.5	-01.6	04.6	04.2	04.4	91	63	81	73	WSW 1	WNW 2	WNW 1
9	753.1	752.4	752.5	00.4	09.5	07.5	06.2	10.0	-00.4	-04.9	04.0	03.9	03.5	84	44	45	56	SE 2	SSW 2	SE 2
10	752.6	753.3	753.7	05.1	12.6	07.3	08.1	13.8	04.4	-00.6	03.6	05.6	05.6	54	52	73	60	SE 2	SE 2	SE 2
11	751.7	749.6	747.7	04.4	15.7	09.5	09.5	15.4	03.9	-00.6	04.9	05.8	05.3	78	43	62	61	-0	ESE 2	SE 2
12	747.0	745.1	744.2	05.2	16.9	10.8	10.9	17.6	04.2	-01.9	04.9	05.3	05.3	74	37	55	55	ESE 1	SE 1	ESE 2
13	743.1	742.0	742.3	06.8	15.6	07.7	09.4	15.8	06.6	03.1	05.2	05.3	05.3	70	40	67	59	SE 3	SE 3	ESE 4
14	742.5	743.1	744.8	05.4	10.6	06.7	07.4	11.6	05.3	04.4	05.3	05.7	05.8	79	60	79	73	ESE 4	EST 4	EST 4
15	745.8	745.0	745.4	05.6	12.8	07.8	08.5	12.8	05.											

BR. ST. 173

 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w						
		14	7	14	21	Sred Dies				7	7					
1	5	10	10•	10	10.0	00.0	02.6	•	• <sup>0-2</sup> = <sup>0-0-22<sup>30</sup></sup>	<sup>0-10<sup>30</sup></sup>	<sup>15<sup>30</sup></sup>	F ESE 22 <sup>30</sup> 24				
2	7	09	10	05	09.0	00.0	05.4	•	• <sup>0-5<sup>45</sup></sup>	<sup>6<sup>45</sup></sup>	<sup>11<sup>45</sup></sup>	F ESE 0-24 <sup>1</sup>				
3	7	09	08	06	07.7	01.3	00.6	•	F ESE 0-24 <sup>1</sup>	F ESE 17 <sup>30</sup>	8 <sup>20</sup>	• <sup>0-9<sup>30</sup></sup>	<sup>11<sup>45</sup></sup>	<sup>18<sup>30</sup></sup>	10 <sup>30</sup>	
4	8	08	05•	00	04.3	04.0	00.1	•	F ESE 0-24 <sup>1</sup>							
5	8	07	08•	09	06.0	01.3	•	•	F ESE 0-24 <sup>1</sup>							
6	7	10	00•	07	05.7	05.5	•	•	F ESE 13 <sup>30</sup> 24							
7	6	10*	10*	10	10.0	00.0	02.7	01	• <sup>0-3<sup>45</sup></sup>	<sup>1-15<sup>30</sup></sup>	<sup>3<sup>45</sup></sup>	X <sup>3-45<sup>30</sup></sup>	<sup>8<sup>45</sup></sup>	<sup>15<sup>30</sup></sup>	<sup>18<sup>30</sup></sup>	<sup>24<sup>30</sup></sup>
8	7	10	05	10	09.7	00.0	01.3	02	• <sup>0-12<sup>30</sup></sup>	F ESE 23 <sup>30</sup> 24 <sup>1</sup>	X <sup>0-23<sup>45</sup></sup>	2 <sup>45</sup>	• <sup>0-9<sup>30</sup></sup>	<sup>11<sup>45</sup></sup>	<sup>18<sup>30</sup></sup>	<sup>24<sup>30</sup></sup>
9	7	10	05	00	04.3	02.5	00.0	•	• <sup>0-2<sup>15</sup></sup>	F ESE 0-24 <sup>1</sup>	E <sup>0-19<sup>30</sup></sup>	2 <sup>00</sup>	• <sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	
10	7	02	04•	10	05.3	05.5	•	•	F ESE-SE 0-4 <sup>27</sup>	F ESE-SE 13 <sup>30</sup> 24 <sup>1</sup>						
11	7	10	05	00	04.3	00.0	•	•	F ESE-SE 0-4 <sup>29</sup>							
12	7	10	03•	10	07.7	04.1	•	•	X <sup>0-17<sup>45</sup></sup>	8 <sup>30</sup>						
13	7	10	05•	00	05.0	02.2	00.0	•	• <sup>0-12<sup>30</sup></sup>	2 <sup>45</sup>						
14	7	00	03•	00	01.0	07.5	•	•	• <sup>0-2<sup>15</sup></sup>	0-10 <sup>30</sup>	2 <sup>25</sup>	24	• <sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	
15	7	00	00•	00	00.0	07.3	•	•	• <sup>0-2<sup>15</sup></sup>	0-10 <sup>30</sup>	2 <sup>25</sup>	24	• <sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	<sup>0-2<sup>15</sup></sup>	
16	8	09	09	10	05.3	00.0	•	•	• <sup>0-15<sup>45</sup></sup>	6 <sup>45</sup>	F ESE 6 <sup>45</sup>					
17	6	08	10•	10	05.3	00.0	•	•	• <sup>0-19<sup>30</sup></sup>	16 <sup>45</sup>	22 <sup>30</sup>	2 <sup>30</sup>	• <sup>0-15<sup>30</sup></sup>	<sup>18<sup>30</sup></sup>	<sup>24<sup>30</sup></sup>	
18	7	10	10	C5	08.3	00.0	03.1	•	F NW 5 <sup>35</sup> 5 <sup>35</sup>	8 <sup>35</sup>						
19	6	04	10	10•	08.0	02.0	•	•	• <sup>0-13<sup>30</sup></sup>	9 <sup>35</sup>	18 <sup>30</sup>	4 <sup>30</sup>	• <sup>0-13<sup>30</sup></sup>	<sup>0-13<sup>30</sup></sup>	<sup>0-13<sup>30</sup></sup>	
20	6	10	10	10	10.0	00.0	10.0	•	• <sup>0-6<sup>45</sup></sup>	22 <sup>30</sup>	23 <sup>30</sup>	1 <sup>30</sup>	• <sup>0-6<sup>45</sup></sup>	<sup>0-6<sup>45</sup></sup>	<sup>0-6<sup>45</sup></sup>	
21	7	10	10	10	10.0	00.0	00.0	•	• <sup>0-22<sup>30</sup></sup>	24						
22	7	10	08	00	06.0	03.7	•	•	• <sup>0-0-10<sup>45</sup></sup>	= <sup>0-2<sup>30</sup></sup>	6 <sup>00</sup>	9 <sup>15</sup>	10 <sup>30</sup>	11 <sup>45</sup>	12 <sup>30</sup>	
23	7	10	08•	10•	09.3	01.3	•	•	• <sup>0-2<sup>30</sup></sup>	5 <sup>45</sup>	= <sup>0-17<sup>15</sup></sup>	11 <sup>45</sup>	22 <sup>30</sup>	14 <sup>30</sup>	15 <sup>30</sup>	
24	7	10	09	C5	08.0	00.7	01.1	•	• <sup>0-2<sup>30</sup></sup>	10 <sup>45</sup>	= <sup>0-2<sup>30</sup></sup>	26 <sup>45</sup>	5 <sup>30</sup>	6 <sup>30</sup>	7 <sup>30</sup>	
25	5	04≡	10	10≡	08.0	00.2	•	•	• <sup>0-0-10<sup>45</sup></sup>	= <sup>0-2<sup>30</sup></sup>	26 <sup>45</sup>	5 <sup>30</sup>	6 <sup>30</sup>	7 <sup>30</sup>	8 <sup>30</sup>	
26	7	10	00•	00	03.3	05.1	•	•	• <sup>0-0-24<sup>30</sup></sup>	= <sup>0-2<sup>45</sup></sup>	23 <sup>30</sup>	2 <sup>45</sup>	3 <sup>45</sup>	4 <sup>30</sup>	5 <sup>30</sup>	
27	7	C2	00•	00	00.7	04.3	•	•	• <sup>0-2<sup>30</sup></sup>	20 <sup>30</sup>	2 <sup>45</sup>	2 <sup>45</sup>				
28	6	10	10•	10•	10.0	00.0	03.3	•	• <sup>0-0-15<sup>30</sup></sup>	F ESE 14 <sup>00</sup>	24 <sup>30</sup>	2 <sup>45</sup>				
29	6	10	00•	00	03.3	06.6	00.0	•	• <sup>0-0-15<sup>30</sup></sup>	F ESE 0-24 <sup>1</sup>	L <sup>0-2<sup>30</sup></sup>	5 <sup>45</sup>				
30	7	C1	03•	00	01.3	07.2	•	•	• <sup>0-0-10<sup>45</sup></sup>	F ESE 0-10 <sup>45</sup>						
31	7	01	05•	03	02.0	06.1	•	•	• <sup>0-0-10<sup>45</sup></sup>	F ESE 0-10 <sup>45</sup>						
MES.	VRED.	07.5	06.6	05.5	06.5	83.4	76.6									

BECGRAD

1974. JUN

1	8	04	C2•	02	02.7	CE.0	•	•	• <sup>0-0-9<sup>16</sup></sup>	= <sup>0-0-42<sup>30</sup></sup>	24 <sup>30</sup>	0-24 <sup>30</sup>	0-24 <sup>30</sup>
2	8	10•	10	08	05.3	CE.0	00.0	•	• <sup>0-0-6<sup>15</sup></sup>	= <sup>0-0-24<sup>30</sup></sup>	0-6 <sup>15</sup>	8 <sup>30</sup>	9 <sup>30</sup>
3	8	05	00•	C6	02.7	CE.0	00.0	•	• <sup>0-0-5<sup>45</sup></sup>	= <sup>0-0-15<sup>45</sup></sup>	14 <sup>00</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
4	7	10	10	10	09.7	CE.0	•	•	• <sup>0-0-0<sup>45</sup></sup>	F ESE 0-0 <sup>45</sup>	14 <sup>00</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
5	7	10•	04•	00	04.7	04.1	00.9	•	• <sup>0-0-6<sup>05</sup></sup>	= <sup>0-10<sup>30</sup></sup>	10 <sup>30</sup>	22 <sup>30</sup>	24
6	8	06	07•	10•	07.7	CE.0	CE.0	•	• <sup>0-0-5<sup>45</sup></sup>	F ESE 0-4 <sup>45</sup>	13 <sup>45</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
7	7	10•	10	C3	07.7	CE.0	CE.0	•	• <sup>0-0-4<sup>30</sup></sup>	F ESE 0-4 <sup>30</sup>	17 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
8	7	04	01•	02	02.3	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	12 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
9	8	02	05	05	05.3	03.7	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	12 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
10	8	01	03•	00	01.3	07.4	•	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	16 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
11	8	00	00•	00	00.0	00.2	•	•	• <sup>0-0-3<sup>30</sup></sup>	F ESE 0-3 <sup>30</sup>	20 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
12	8	00	00•	00	00.0	00.1	•	•	• <sup>0-0-3<sup>30</sup></sup>	F ESE 0-3 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>	0-24 <sup>30</sup>
13	8	04	01•	10	05.0	07.1	•	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	10 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
14	7	09	10	04	07.7	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	11 <sup>45</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
15	7	09	10	00	06.3	01.9	00.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	11 <sup>45</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
16	7	04	03•	00	02.3	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	16 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
17	8	00	00•	07	02.3	CE.0	•	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	23 <sup>30</sup>	0-23 <sup>30</sup>	0-23 <sup>30</sup>
18	8	04	08	10	05.0	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	23 <sup>30</sup>	0-23 <sup>30</sup>	0-23 <sup>30</sup>
19	8	09	06•	04	06.3	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	14 <sup>00</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
20	8	08	10	10	05.3	CE.0	CE.0	•	• <sup>0-0-2<sup>30</sup></sup>	F ESE 0-2 <sup>30</sup>	14 <sup>00</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
21	6	10•	10	10	10.0	00.0	04.4	•	• <sup>0-0-12<sup>30</sup></sup>	= <sup>0-12<sup>30</sup></sup>	12 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
22	6	10	10	C6	05.7	CE.0	CE.0	•	• <sup>0-0-24</sup>	= <sup>0-3<sup>30</sup></sup>	3 <sup>30</sup>	0-14 <sup>30</sup>	0-14 <sup>30</sup>
23	7	10•	10	09	05.7	CE.0	00.0	•	• <sup>0-0-9<sup>45</sup></sup>	F ESE 10 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>	0-24 <sup>30</sup>
24	7	09	10	10	05.7	CE.0	CE.0	•	• <sup>0-0-19<sup>20</sup></sup>	F ESE 0-19 <sup>20</sup>	14 <sup>00</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>
25	7	10	09	10	05.7	CE.0	CE.0	•	• <sup>0-0-10<sup>45</sup></sup>	F ESE 10 <sup>30</sup> 24 <sup>30</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>	0-24 <sup>30</sup>
26	7	10	06•	10	06.7	CE.0	CE.0	•	• <sup>0-0-10<sup>45</sup></sup>	F ESE 0-10 <sup>45</sup>	24 <sup>30</sup>	0-24 <sup>30</sup>	0-24 <sup>30</sup>
27	8	00•	06	00	02.0	CE.0	CE.0	•	• <sup>0-0-9<sup>45</sup></sup>	F ESE 0-9 <sup>45</sup>	23 <sup>30</sup>	0-23 <sup>30</sup>	0-23 <sup>30</sup>
28	8	00•	04•										

$\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1\text{h }22\text{ min.}$

BR. ST. 173

D E O	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	753.9	752.5	751.8	-01.4	06.6	01.0	01.0	07.0	-02.0	-03.3	02.8	02.8	02.8	68	35	58	55	ESE	5	ESE	4	ESE	4
2	748.9	747.7	746.5	-00.5	07.4	01.1	02.3	07.7	-00.6	-01.8	02.9	02.9	03.2	65	38	65	56	SE	4	ESE	5	ESF	5
3	749.8	751.9	754.4	00.5	07.4	02.4	03.2	08.0	00.1	-01.0	03.4	03.6	03.7	72	46	68	62	ESE	4	ESE	4	ESE	4
4	754.9	754.3	753.2	02.0	09.8	05.7	05.8	10.2	01.2	00.0	04.2	04.3	04.8	79	48	70	66	ESF	4	ESE	5	ESF	6
5	751.6	750.4	749.4	04.2	03.9	02.7	03.6	07.2	02.6	04.2	04.6	05.2	04.6	69	86	86	80	ESE	6	ESE	5	SE	5
6	749.3	748.9	750.6	02.4	02.9	01.5	02.3	04.6	01.7	01.0	04.1	04.8	05.0	76	84	95	85	ESE	5	ESE	5	ESE	2
7	751.6	752.9	753.7	02.4	02.9	02.2	02.4	03.4	01.4	01.0	04.8	05.2	04.2	89	92	77	86	E	2	ENF	1	ESI	2
8	753.9	753.4	754.3	-00.6	04.0	01.4	01.6	05.2	-01.0	-01.0	04.1	04.1	04.0	95	68	78	80	SF	2	ESE	2	ESO	3
9	754.7	755.0	756.1	-00.4	01.6	06.7	00.6	02.1	-00.6	-00.6	03.5	04.1	04.2	78	80	86	81	ESF	3	ESF	3	ESI	3
10	756.0	755.9	756.3	00.8	04.6	01.0	01.8	05.2	-00.3	00.0	03.9	04.3	03.8	81	67	76	75	ESF	3	ESE	5	ESI	4
11	757.7	759.0	760.2	-00.6	02.3	02.5	01.7	03.4	-00.7	-01.0	04.1	04.9	04.4	94	90	81	88	ESE	3	ESF	2	ENI	2
12	740.4	756.7	757.4	00.9	10.0	01.7	04.6	10.3	00.7	-01.4	03.8	03.8	02.8	78	41	47	55	E	2	SE	2	SE	3
13	754.6	752.0	750.7	01.3	11.1	04.9	05.6	11.9	00.4	-02.7	03.6	04.2	04.2	72	42	65	60	ESE	2	SSE	3	SE	3
14	748.5	746.2	744.9	01.2	11.5	07.8	07.1	12.7	00.6	-01.3	04.1	04.5	03.5	81	44	44	56	SE	2	ESE	3	SE	4
15	743.2	743.5	744.4	04.4	07.8	06.2	06.2	08.3	04.2	02.3	04.5	04.6	06.3	72	58	74	68	SSW	1	SSE	1	-	0
16	744.0	743.4	743.9	04.2	09.6	06.4	06.6	10.2	03.8	02.8	05.3	04.5	04.8	85	50	67	67	SE	1	SSW	1	SSF	2
17	744.8	745.7	746.9	03.5	16.0	11.4	10.6	16.8	03.0	-01.7	04.9	05.3	05.2	83	39	52	58	SSE	1	NNW	2	SW	2
18	748.0	747.0	746.8	09.8	20.6	15.7	15.4	21.8	08.2	04.2	05.5	04.9	05.6	61	27	42	43	SE	1	W	2	SE	2
19	750.2	749.8	750.4	11.8	26.2	15.5	19.0	26.6	10.0	04.4	06.1	04.6	05.4	59	19	32	37	SE	2	NW	2	S	3
20	753.6	753.0	753.2	11.0	23.5	17.0	17.1	24.4	10.0	03.4	03.9	04.8	04.9	40	22	34	32	SE	1	SW	2	ESI	2
21	754.9	754.2	754.6	12.8	25.0	18.0	18.4	25.9	11.5	03.6	04.7	07.0	05.9	42	29	38	36	SE	1	ESE	2	ESI	4
22	754.4	753.0	751.5	14.0	24.8	16.2	17.8	25.3	12.0	10.2	05.6	05.0	05.6	46	21	40	34	SE	4	SE	3	SSE	2
23	751.3	750.0	751.4	14.0	25.7	19.3	19.6	26.0	13.7	11.2	05.7	06.6	08.1	47	27	48	41	SE	3	SE	2	-	0
24	751.1	753.1	752.7	14.1	22.0	16.0	17.0	22.3	13.0	09.0	07.4	06.7	07.1	61	34	52	49	SE	3	SE	4	SE	4
25	753.4	753.0	753.3	08.2	13.7	08.0	09.4	16.0	08.0	07.7	05.5	05.3	04.7	68	47	58	56	SE	6	ESE	2	ESE	2
26	752.5	750.0	749.4	07.1	19.2	13.4	13.0	19.5	06.0	04.8	04.7	06.7	06.0	66	40	52	53	ESE	5	SE	2	ESE	2
27	747.6	746.0	747.6	09.8	20.0	15.2	15.2	21.5	08.6	06.1	05.3	06.7	06.4	58	37	45	48	SE	2	NE	2	ENI	1
28	749.6	749.6	751.0	10.2	20.3	13.5	13.5	20.5	09.0	05.0	06.0	06.0	05.2	64	34	45	48	ISE	3	ESE	3	SE	2
29	753.2	753.0	753.3	07.5	17.6	11.2	12.2	18.0	08.5	07.4	05.0	04.3	04.1	54	35	41	45	ESE	4	SE	2	ESI	2
30	754.9	756.0	754.4	07.2	11.1	09.1	09.4	11.3	08.0	06.7	03.7	03.6	03.6	46	36	42	41	ESE	4	ESE	5	ESI	2
31	751.1	752.5	752.1	07.7	10.7	09.2	09.4	11.0	08.3	06.7	04.5	04.0	04.8	53	41	55	50	SE	3	ESE	3	ESI	1
MES.	WRED.			751.8	751.4	751.6	05.6	12.9	08.6	08.9	13.7	04.8	02.8	04.6	04.8	04.8	68	47	59	58	3.0	3.0	3.1

## 1974 APRIL

## BEOGRAD

1	750.9	751.4	751.7	07.0	05.8	10.0	05.2	11.3	06.6	05.6	05.4	04.5	04.5	71	50	45	57	ESE	5	ESE	5	ESE	2
2	752.8	753.5	755.0	06.5	11.2	07.2	08.2	12.0	06.5	05.6	03.9	04.2	03.9	54	41	51	49	ESE	5	ESE	4	ESF	3
3	755.7	754.2	754.3	04.4	14.0	09.5	09.8	15.3	03.2	-00.8	03.7	03.6	03.6	60	29	40	43	SI	2	ESE	2	ESI	2
4	753.2	751.6	750.5	05.0	15.7	10.7	10.5	16.2	04.4	00.8	03.5	03.9	03.8	54	29	39	41	ESE	1	NNE	2	ENF	1
5	749.9	750.0	750.7	08.0	17.3	12.0	12.3	17.3	06.2	00.0	04.1	03.4	03.6	51	23	34	36	ESE	2	SE	2	NE	2
6	751.1	750.4	750.1	08.4	17.7	12.5	12.8	18.0	05.6	-00.9	03.9	03.7	04.5	47	24	41	37	SE	2	ENE	2	NE	1
7	750.2	748.4	748.5	07.4	17.1	13.5	12.9	18.2	06.9	03.7	04.6	04.2	04.3	59	29	40	45	NNW	2	NW	3	NW	1
8	748.6	748.0	749.5	07.9	14.4	10.2	10.7	15.6	07.5	06.0	06.3	04.0	02.3	78	33	35	49	NNW	3	NW	4	NNF	2
9	751.1	750.9	750.6	04.6	15.7	10.0	10.1	16.7	04.1	01.0	03.8	04.3	04.8	60	32	52	48	NNW	1	NW	2	ESE	1
10	750.4	748.0	745.7	10.0	20.6	14.7	15.2	20.7	07.8	01.6	05.0	05.5	04.9	52	30	39	40	SSE	3	ESE	2	ESI	2
11	743.9	741.8	741.5	10.9	20.2	14.0	14.8	20.2	08.8	06.6	04.8	05.5	05.2	50	31	44	42	ESE	3	SSE	3	SE	3
12	741.2	740.2	741.3	11.1	21.0	13.6	14.9	21.5	10.1	09.0	05.9	06.6	09.2	59	35	79	58	ESE	3	LSE	3	SSW	1
13	742.0	742.2	744.6	13.6	20.0	12.2	14.5	20.6	12.2	09.6	02.2	04.8	08.6	71	48	80	66	SW	1	NW	2	NNF	3
14	744.0	742.6	742																				

HR. ST. 173

 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijednost 0-9	Oblečnost N (0-10)					Instalacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	00	020	00	00.7	CC.1	.	.	.	F ESE 2 <sup>08</sup> 24i, F ESE 4 <sup>38</sup>	
2	8	00	040	C3	02.3	CC.8	.	.	.	F ESE 0-8 <sup>16</sup> i, F ESE 8 <sup>46</sup> 24i	
3	8	04	040	00	02.7	CC.3	.	.	.	F ESE 0-8 <sup>16</sup> i, F ESE 8 <sup>46</sup> 24i	
4	8	00	090	06	05.0	06.8	.	.	.	F ESE 0-4 <sup>48</sup> i, F ESE 4 <sup>48</sup> 24i	
5	7	09	100	100	05.7	CC.0	.	.	.	F ESE 0-2 <sup>46</sup> i, 0 <sup>945</sup> 23 <sup>45</sup> i	
6	7	09	05	10	05.3	00.0	10-2	.	.	F ESE 0-15 <sup>03</sup> X <sup>0902</sup> 10 <sup>50</sup> 15 <sup>50</sup> 16 <sup>40</sup> * 12 <sup>50</sup> 13 <sup>50</sup> i, F ESE 15 <sup>23</sup> 19 <sup>10</sup> 22 <sup>16</sup> , 0 <sup>1143</sup> 17 <sup>35</sup>	
7	6	10	100	10	10.0	00.0	CC.0	.	.	* 0 <sup>070</sup> 10 <sup>53</sup> 16 <sup>53</sup> 17 <sup>15</sup> , 0 <sup>832</sup> 10 <sup>53</sup> * 917 <sup>0</sup> 17 <sup>40</sup> i, F ESE 17 <sup>09</sup> 17 <sup>42</sup>	
8	7	09	05	10	05.3	03.4	02.9	01	.	X <sup>0118</sup> 5 <sup>30</sup> F E 16 <sup>05</sup> 24i, [X]	
9	7	10*	10*	10*	10.0	00.0	CC.0	.	.	F ESE 0-15 <sup>05</sup> X <sup>0300</sup> 9 <sup>45</sup> M <sup>50</sup> 24i	
10	7	09*	08	10	05.0	02.5	00.2	.	.	* 0 <sup>0330</sup> 6 <sup>45</sup> 11 <sup>30</sup> F ESE 16 <sup>55</sup> 19 <sup>26</sup> 22 <sup>02</sup> 24, F ESE 19 <sup>26</sup> 22 <sup>02</sup> [X]	
11	6	10*	10*	10	10.0	00.0	CC.0	01.3	C2	F ESE 0-8 <sup>22</sup> 9 <sup>25</sup> 10 <sup>07</sup> * 0 <sup>230</sup> 13 <sup>45</sup> X <sup>01315</sup> 15 <sup>15</sup> , 0 <sup>02246</sup> 23 <sup>15</sup> , [X]	
12	8	000	010	00	00.3	09.3	00.8	.	.	= 0 <sup>430</sup> 8 <sup>15</sup> i, F ESE 17 <sup>09</sup> 17 <sup>42</sup>	
13	8	000	000	00	00.0	CC.0	CC.6	.	.	F ESE 7 <sup>50</sup> 8 <sup>15</sup> i, △ 2 <sup>15</sup> 24	
14	8	05	050	02	04.0	08.1	.	.	.	□ 0 <sup>085</sup> F ESE 20 <sup>55</sup> 21 <sup>49</sup>	
15	7	10	10	100	10.0	00.0	CC.0	.	.	F ESE 0 <sup>6</sup> 2 <sup>55</sup> i, 0 <sup>2010</sup> 24i	
16	7	10	08	00	06.0	00.9	00.0	.	.	△ 0 <sup>1945</sup> 24	
17	7	00	030	C3	02.0	08.5	.	.	.	△ 0 <sup>0230</sup> 0 <sup>1945</sup> 24	
18	8	040	020	04	03.2	09.4	.	.	.	△ 0 <sup>320</sup> 7 <sup>30</sup>	
19	8	090	020	00	03.7	09.5	.	.	.	△ 0 <sup>436</sup> 6 <sup>30</sup>	
20	8	010	050	03	02.0	06.7	06.7	.	.	.	
21	8	000	000	00	00.0	10.1	.	.	.	0 <sup>1130</sup> 8 <sup>46</sup> F ESE 14 <sup>43</sup> 22 <sup>53</sup>	
22	8	000	000	00	00.0	10.4	.	.	.	F ESE 2 <sup>35</sup> 18 <sup>50</sup> i	
23	8	080	050	09	07.3	08.0	.	.	.	F ESE -SE 0 <sup>08</sup> 10 <sup>50</sup> 16 <sup>02</sup> 17 <sup>50</sup> i, 0 <sup>1830</sup> 19 <sup>15</sup> , 0 <sup>01845</sup> 18 <sup>49</sup>	
24	8	010	050	02	02.7	09.0	CC.1	.	.	F ESE 3 <sup>42</sup> 22 <sup>20</sup> i, F ESE 22 <sup>20</sup> 21	
25	8	06	08	00	06.7	04.2	.	.	.	F N6 0-24i	
26	7	07	000	00	00.7	CC.0	.	.	.	F ESE 0-4 <sup>29</sup> i, F ESE 4 <sup>29</sup> 10 <sup>51</sup>	
27	7	050	000	00	01.7	CC.1	.	.	.	△ 0 <sup>230</sup> 24	
28	7	000	000	00	00.0	CC.0	CC.1	.	.	△ 1 <sup>2</sup> 0-6, F ESE 5 <sup>40</sup> 10 <sup>40</sup> 16 <sup>02</sup> 24i	
29	7	000	000	00	00.0	CC.0	CC.0	.	.	F ESE -SE 0-24i, F ESE 5 <sup>41</sup> 6 <sup>04</sup> 8 <sup>49</sup> 12 <sup>10</sup> 17 <sup>53</sup> 23 <sup>42</sup>	
30	7	10	10	10	10.0	00.0	CC.0	.	.	F ESE -SE 0-4 <sup>46</sup> i, 8 <sup>53</sup> 24i, 0 <sup>830</sup> 11 <sup>30</sup>	
31	7	10	10	10	10.0	00.0	CC.0	.	.	.	
MES. WRED.			04.9	05.1	04.4	04.8	179.8	21.5			

## BEOGRAD

1974 APRIL

1	7	10	10	10	10.0	CC.0	CC.1	CC.0	.	F ESE 0 <sup>05</sup> 1 <sup>50</sup> 11 <sup>40</sup> 24i, F ESE 1 <sup>50</sup> 10 <sup>30</sup> 4 <sup>50</sup> i	
2	7	10	0E0	03	07.0	01.8	00.0	.	.	F ESE 0-23 <sup>68</sup> i, F ESE 2 <sup>06</sup> , 0 <sup>0545</sup>	
3	7	020	020	00	01.2	1C.6	.	.	.	F ESE 9 <sup>08</sup> 9 <sup>25</sup> i	
4	8	050	000	00	01.7	09.4	.	.	.	.	
5	8	000	020	00	00.7	CC.0	CC.6	.	.	.	
6	8	000	030	05	02.7	10.0	.	.	.	△ 0 <sup>2245</sup> 24	
7	8	030	060	10	06.3	07.9	.	.	.	△ 0 <sup>0645</sup> F N-NW 13 <sup>40</sup> 16 <sup>00</sup> i, △ 0 <sup>1545</sup> 15 <sup>55</sup> i, 0 <sup>01940</sup> 23 <sup>45</sup>	
8	8	08	060	01	05.0	07.5	00.1	.	.	* 0 <sup>250</sup> 3 <sup>40</sup> i, F N-NW 9 <sup>42</sup> 17 <sup>02</sup> i	
9	8	000	040	00	01.3	09.0	.	.	.	F NWW 14 <sup>40</sup> △ 0 <sup>1945</sup> 24	
10	8	020	030	00	01.7	09.5	.	.	.	△ 0 <sup>0416</sup>	
11	8	10	090	04	07.7	01.3	.	.	.	F SE -SE 14 <sup>45</sup> 17 <sup>04</sup>	
12	8	09	060	09	08.0	05.5	.	.	.	F w 18 <sup>55</sup> 19 <sup>19</sup> i, 0 <sup>1900</sup> 22 <sup>40</sup> i	
13	8	09	060	09	08.0	06.4	00.3	.	.	* 0 <sup>0515</sup> 6 <sup>20</sup> 6 <sup>60</sup> 12 <sup>15</sup> 12 <sup>21</sup> 14 <sup>55</sup> 20 <sup>45</sup> ; F w 12 <sup>40</sup> , ♀ 12 <sup>21</sup> 12 <sup>30</sup> 16 <sup>32</sup> 16 <sup>37</sup>	
14	5	10	10	10	10.0	CC.0	00.0	02.1	.	* 0 <sup>07810</sup> 10 <sup>51</sup> 24 <sup>40</sup> 23 <sup>55</sup> ; F ESE 15 <sup>45</sup> 23 <sup>42</sup>	
15	8	10	10	10	10.0	CC.0	00.0	08.7	.	* 0 <sup>04520</sup> 21 <sup>42</sup>	
16	7	10	10	10	10.0	00.0	00.6	01.1	.	0 <sup>320</sup> 8 <sup>20</sup> 11 <sup>44</sup> 21 <sup>45</sup> 24i, ♀ 10 <sup>30</sup> 10 <sup>57</sup> i, F ESE 21 <sup>58</sup>	
17	7	10	10	10	10.0	CC.0	00.0	09.5	.	● 0 <sup>1224</sup> 24i, F ESE 16 <sup>54</sup>	
18	6	10	10	10	10.0	00.0	00.0	05.6	.	● 0 <sup>6224</sup> 24i	
19	7	10	10	10	10.0	03.1	05.0	.	.	● 0 <sup>0224</sup> 24i = 0 <sup>1245</sup> 11 <sup>46</sup> F Nw 11 <sup>46</sup> 16 <sup>20</sup> i	
20	8	000	040	00	01.3	09.5	.	.	.	● 0 <sup>22024</sup>	
21	7	C9	090	04	07.3	02.8	.	.	.	● 0 <sup>2070</sup> 0 <sup>1445</sup> 16 <sup>05</sup> i, ♀ 0 <sup>1443</sup> 14 <sup>47</sup>	
22	8	050	050	05	05.0	08.6	01.5	.	.	● 0 <sup>4436</sup> 16 <sup>56</sup> 18 <sup>40</sup> i, 0 <sup>01620</sup> 16 <sup>40</sup> i	
23	8	000	070	00	02.3	08.2	00.0	.	.	● 0 <sup>02039</sup> 9 <sup>50</sup>	
24	8	000	050	07	04.0	12.1	01.1	.	.	● 0 <sup>02848</sup> i, 0 <sup>01524</sup> i	
25	6	09	10	10	09.7	00.0	.	.	.	● 0 <sup>075144</sup> 16 <sup>05</sup> i, F w 14 <sup>40</sup> 14 <sup>56</sup> i, 18 <sup>45</sup> 15 <sup>35</sup> ♀ 20 <sup>42</sup> 20 <sup>40</sup>	
26	8	10	050	09	08.0	05.7	06.1	.	.	● 0 <sup>0744</sup> 14 <sup>40</sup> 16 <sup>05</sup> i, F w 14 <sup>40</sup> 14 <sup>56</sup> i, 18 <sup>45</sup> 15 <sup>35</sup> ♀ 20 <sup>42</sup> 20 <sup>40</sup>	
27	8	08	090	09	08.7	08.2	04.4	.	.	● 0 <sup>0744</sup> 24	
28	8	040	080	10	07.3	08.6	.	.	.	● 0 <sup>0080</sup> 8 <sup>45</sup> 24 <sup>40</sup> 21 <sup>45</sup> i, 0 <sup>01645</sup> 18 <sup>45</sup> i, 20 <sup>45</sup> 20 <sup>45</sup> i	
29	8	10	060	08	08.0	06.0	00.5	.	.	F ESE -SE 0-3 <sup>74</sup> 7 <sup>45</sup> , 0 <sup>0545</sup> 7 <sup>05</sup>	
30	8	06	090	10	08.3	06.5	00.0	.	.	● 0 <sup>1643</sup> 21 <sup>40</sup> 18 <sup>40</sup> 21 <sup>40</sup> i, ♀ 0 <sup>1440</sup> 21 <sup>40</sup> 21 <sup>40</sup> i	
MES. WRED.			06.3	06.7	06.1	06.4	169.9	46.0			

$\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1h\ 22\ min.$ 

BR. ST. 173

E O	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	732.4	732.1	733.2	13.8	20.1	14.0	15.5	20.4	10.6	05.7	07.3	06.8	07.5	62	39	63	55	SE	2	S	2	SSW 1
2	734.7	738.2	741.1	11.9	11.8	11.2	11.5	14.0	11.0	04.8	10.0	09.7	09.3	95	93	93	94	W	3	W	2	W 3
3	743.6	743.9	744.6	10.6	18.7	15.2	14.9	19.7	09.4	07.2	08.1	08.4	09.3	85	52	72	70	WSW	2	WSW	3	SSE 2
4	743.7	742.2	741.9	14.8	19.9	13.4	15.4	20.4	12.8	10.4	07.4	07.9	08.6	58	45	75	59	SSE	2	SE	2	S 3
5	741.6	739.6	740.9	13.4	20.4	11.2	14.1	20.8	09.5	05.8	07.3	06.6	08.9	63	36	89	63	S	2	SSE	2	NNE 2
6	742.2	742.8	746.2	13.2	17.2	11.5	13.4	19.7	09.1	05.4	06.7	07.2	08.9	55	49	88	65	S	2	S	2	WSW 2
7	749.3	750.3	750.6	10.4	15.1	12.6	12.7	15.8	10.0	08.5	07.0	07.7	08.1	75	60	74	70	NNE	1	NE	2	SSE 2
8	751.7	751.2	749.5	11.6	14.8	12.0	12.6	15.8	10.2	09.2	09.5	08.8	08.2	93	69	78	80	NNW	1	NNW	2	NW 1
9	747.2	746.9	747.3	09.1	16.3	12.0	12.4	16.8	08.7	07.6	06.4	05.7	06.6	73	41	63	59	NW	2	NNW	3	NW 2
10	748.0	747.8	748.2	09.9	18.2	12.4	13.2	19.1	07.4	04.4	06.8	06.1	07.0	74	39	65	59	W	2	NW	2	SSE 1
11	748.9	749.2	749.5	13.5	23.3	16.6	17.5	23.4	09.2	03.8	06.8	07.0	06.6	59	32	49	47	SE	2	NNW	2	SF 2
12	749.5	751.9	752.5	16.6	16.2	14.6	15.5	19.1	12.9	07.2	08.2	10.4	10.9	58	75	88	74	-	0	E	2	- 0
13	754.6	755.1	755.0	12.7	19.5	14.6	15.4	20.1	11.8	11.6	10.0	08.8	09.3	91	52	75	73	W	1	NW	2	SF 1
14	753.4	751.3	749.6	15.4	22.9	16.3	17.7	23.1	10.4	06.0	09.2	08.3	09.1	70	40	65	58	SE	1	NW	2	WSW 1
15	751.4	750.3	749.2	10.2	10.3	09.2	09.7	16.3	09.1	09.3	08.8	08.3	08.2	94	88	94	92	W	2	NNW	1	SW 1
16	746.5	746.5	747.4	09.4	11.5	11.7	11.1	12.9	08.2	08.0	08.0	09.1	09.2	90	90	89	90	WSW	2	W	2	SW 3
17	749.1	750.1	751.7	11.0	16.2	10.6	12.1	17.2	10.5	08.6	07.9	07.4	08.9	81	53	93	76	WSW	2	W	1	NW 1
18	752.5	753.0	753.0	10.0	14.9	13.4	13.1	16.8	09.9	09.7	08.9	10.5	10.4	93	83	90	89	W	2	NNW	2	NNW 2
19	752.0	751.6	751.1	12.0	20.6	16.2	21.7	11.5	11.0	09.2	10.4	10.2	88	57	74	73	NNW	2	NW	2	- 0	
20	751.2	750.0	749.3	15.0	24.5	17.0	18.4	24.7	10.2	06.5	09.5	09.0	10.2	74	39	70	61	WSW	1	NW	2	- 0
21	750.0	750.9	751.0	14.4	20.2	15.0	16.2	21.2	13.3	09.0	10.3	11.0	10.7	84	62	84	77	NNW	2	WSW	2	WSW 2
22	749.8	745.6	743.8	13.2	21.7	11.5	14.5	21.7	11.5	09.0	09.3	09.3	09.7	82	48	95	75	WSW	1	SSW	2	NNE 3
23	743.0	742.6	742.9	11.6	16.1	11.0	12.4	16.9	11.0	10.4	06.4	06.5	06.8	82	47	90	73	NNW	2	NW	3	SSW 1
24	743.6	744.0	742.9	11.0	18.6	15.5	15.3	19.6	07.5	05.5	07.8	07.6	09.7	77	47	74	66	S	1	SE	2	ESE 3
25	745.7	747.0	749.7	12.3	19.4	15.2	15.5	19.6	11.6	08.4	09.9	09.2	08.8	92	54	68	71	W	2	NNW	2	NNW 2
MES.	VRED.	747.5	747.3	747.5	12.0	19.1	14.2	15.2	20.1	10.8	08.2	08.7	08.5	09.3	77	53	77	69	1.7	2.1	1.5	

## 1974 JUN

## RECGRAD

1	748.5	748.8	750.2	21.4	22.8	17.4	19.8	24.4	17.3	15.4	13.6	12.5	14.2	71	60	95	75	NNW	1	W	3	WNW 2
2	751.6	753.0	754.0	14.9	13.9	13.4	13.9	17.4	13.0	13.5	10.8	11.5	11.0	85	97	96	93	WNW	2	WNW	2	F 2
3	754.3	755.1	754.6	13.8	16.7	15.4	15.3	18.1	13.2	12.3	08.0	09.4	11.3	67	66	86	73	NW	2	S	1	
4	754.6	753.6	752.9	16.4	24.0	18.6	19.4	25.2	11.7	09.2	10.2	10.1	12.1	73	45	75	64	SSE	1	NW	2	SSW 1
5	752.9	751.5	750.3	18.4	26.0	21.0	21.6	26.6	14.3	11.5	11.5	13.1	12.1	72	52	65	63	WSW	1	NNE	2	E
6	748.6	747.5	747.4	21.5	28.0	17.8	21.3	29.5	17.5	13.9	13.6	15.2	14.1	71	53	92	72	SE	2	SSW	2	NW 1
7	747.6	749.2	752.0	17.5	15.4	14.4	15.4	18.0	14.4	15.8	13.4	11.5	09.8	90	88	80	86	W	2	NNW	3	NNW 2
8	754.7	744.9	743.3	12.6	18.5	13.8	14.7	19.6	09.6	07.1	07.7	06.6	07.9	70	41	67	59	NNW	2	ESE	2	
9	748.4	746.5	744.7	15.3	24.9	20.6	20.4	25.6	11.6	08.4	08.0	10.7	12.0	62	45	66	58	ESE	3	SSE	3	SE 3
10	745.2	743.3	743.5	15.0	25.6	18.2	19.2	27.1	14.6	12.5	12.0	13.8	11.8	94	56	76	75	SSW	2	NNE	2	NNW 2
11	742.1	742.6	744.0	13.2	12.0	11.2	11.9	18.2	11.2	10.9	10.9	09.7	09.5	96	92	95	94	W	3	NNW	3	WNW 3
12	744.5	743.1	743.8	11.9	18.2	12.0	13.5	18.2	12.0	07.4	07.3	06.6	08.7	69	42	82	64	WNW	3	W	2	W 2
13	743.5	743.2	744.4	11.9	17.0	12.5	13.5	17.2	08.7	07.2	06.9	06.5	08.0	66	45	73	61	W	3	NNE	1	
14	744.8	745.5	746.7	13.0	17.7	14.6	15.0	18.7	11.5	10.5	08.6	08.3	10.8	77	54	87	73	SW	1	WSW	3	SW 1
15	749.5	749.5	747.7	14.0	21.5	17.0	17.4	22.7	13.5	12.8	11.4	09.8	13.1	95	51	90	79	W	2	NNW	2	ESE 1
16	748.4	747.9	746.8	15.0	18.1	17.4	17.0	22.6	13.2	12.1	11.4	12.9	12.7	89	82	85	86	WSW	1	E	1	NF 1
17	747.1	746.8	746.8	16.5	19.5	17.8	17.9	24.0	12.9	10.6	12.4	13.0	12.5	88	76	82	82	S	1	SE	1	- 0
18	747.1	746.7	747.0	18.7	25.6	20.0	21.1	26.3	14.1	11.4	12.3	09.7	09.8	76	39	56	57	SSE	1	WNW	2	NNH 1
19	748.9	748.9	750.9	17.8	24.2	15.7	18.4	24.6	15.7	13.3	12.6	13.6	13.0	82	60	97	80	W	2	NW	3	W 2
20	751.4	751.1	751.0	14.4	21.2	16.0	16.9	22.2	14.2	13.8	11.0	10.2</										

BR. ST. 173

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_f = 1.2 \text{ m}$$

Dan	Veličina 0-9	Oblačnost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	9	050	070	08	06.7	06.4	06.4	.	.	0° 12° 13° 13° 13° 13° 13° 13° 13° 13° 24
2	6	100	100	100	10.0	00.0	06.7	.	.	0° 20° 22° 22° 22° 22° 22° 22° 22° 22° 24
3	7	000	060	09	05.0	10.5	C3.4	.	.	= 0° 6° 10° 10° 10° 10° 10° 10° 10° 10° 24
4	8	09	10	08	09.0	01.2	00.0	.	.	0° 0° 15° 14.5° 13.5° 13.5° 13.5° 13.5° 13.5° 13.5° 24
5	8	060	070	07	06.7	08.2	C1.8	.	.	0° 15° 15° 19.5° 19.5° 19.5° 19.5° 19.5° 19.5° 19.5° 24
6	8	010	080	C7	05.3	08.0	04.4	.	.	0° 11° 11° 13° 16° 14° 14° 14° 14° 14° 24
7	7	10	090	C8	C9.0	C3.5	C4.6	.	.	0° 2° 0° 5° 10° 8° 4° 9° 6° 21° 24
8	7	10	080	09	09.0	01.8	C4.1	.	.	0° 2° 0° 4° 14° 14° 14° 14° 14° 14° 24
9	8	060	060	C2	C4.7	10.3	.	.	.	= 0° 0° 9.5° 20° 20° 24°; F <sub>NNW</sub> 12° 15.5°
10	8	000	07	00	C2.2	11.6	.	.	.	0° 0° 0° 0° 20° 24°
11	8	000	030	00	C1.0	11.3	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
12	8	060	080	100	08.0	05.7	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
13	7	10	060	04	06.7	04.4	C1.6	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
14	7	060	080	03	05.7	C9.0	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
15	6	100	100	1C	10.0	00.0	03.3	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
16	7	10	10	06	08.7	00.0	12.4	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
17	8	100	060	100	08.7	02.1	C2.2	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
18	7	100	09	10	09.7	C1.5	03.8	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
19	7	08	060	00	04.7	09.1	01.1	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
20	8	000	060	05	03.7	11.4	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
21	7	09	040	1C0	07.7	03.6	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
22	7	010	09	100	06.7	04.7	07.1	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
23	8	C20	060	00	C2.7	07.1	C9.5	.	.	F <sub>NNW</sub> 8° 14° 14° 14° 14° 14° 14° 14° 14° 14° 24
24	8	09	050	05	06.7	06.1	C1.2	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
25	7	10	050	04	06.3	06.7	04.8	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
26	8	000	050	00	C1.7	12.3	01.2	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
27	8	000	060	00	02.0	12.4	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
28	8	060	040	06	05.3	11.4	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
29	8	10	090	10	09.7	02.2	00.4	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
30	7	C90	050	02	05.3	09.5	C0.2	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24
31	8	040	050	06	05.0	09.7	.	.	.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 24

PES.  
WRED.

1	8	09	09	10•	C6.3	C3.5	CC.1	.	• <sup>0</sup> -0 <sup>15</sup> i, 19 <sup>20</sup> 21 <sup>50</sup> , ♦ <sup>0</sup> 17 <sup>50</sup> 8 <sup>10</sup> 44 <sup>20</sup> 14 <sup>50</sup> , 17 <sup>35</sup> 18 <sup>40</sup>
2	3	10	10•	10•	10.0	00.0	06.3	.	• <sup>0</sup> -8 <sup>00</sup> 23 <sup>50</sup> i, ♦ <sup>0</sup> -14 <sup>45</sup> 10 <sup>45</sup> i
3	7	10	10	05	C6.3	CC.0	14.1	.	• <sup>0</sup> 2 <sup>45</sup> 3 <sup>50</sup> , ♦ <sup>0</sup> 20 <sup>20</sup> 24
4	8	00①	04①	00	C1.3	13.4	.	.	• <sup>0</sup> 4 <sup>20</sup> 0 <sup>90</sup> 20 <sup>30</sup> 24
5	8	09	05①	CC	04.7	10.2	.	.	• <sup>0</sup> 2 <sup>0</sup> 0 <sup>80</sup> 19 <sup>40</sup> 24
6	8	01①	08①	10•④	06.3	09.5	.	.	• <sup>0</sup> 0-8 <sup>15</sup> 14 <sup>00</sup> 14 <sup>50</sup> 19 <sup>00</sup> 21 <sup>30</sup> F <sub>sw</sub> 19 <sup>50</sup> 19 <sup>40</sup> , ♦ <sup>0</sup> 19 <sup>20</sup> 20 <sup>10</sup> , • <sup>0</sup> -20 <sup>40</sup> 21 <sup>40</sup>
7	7	10	10	04	C8.0	00.0	10.9	.	• <sup>0</sup> 17 <sup>50</sup> 12 <sup>50</sup> i, ♦ <sup>0</sup> 10 <sup>50</sup> 10 <sup>40</sup> , F <sub>sw</sub> 10 <sup>30</sup>
8	8	03①	02①	00	C1.7	13.6	CC.0	.	.
9	8	00①	08①	05	04.3	10.8	.	.	= <sup>0</sup> 4 <sup>15</sup> 11 <sup>45</sup> , ♦ <sup>0</sup> -14 <sup>45</sup> 15 <sup>40</sup> , 20 <sup>40</sup>
10	7	10	07①	CC	08.7	C8.8	.	.	.
11	8	10•	10•	10•	10.0	00.0	04.6	.	• <sup>0</sup> -2 <sup>55</sup> 6 <sup>50</sup> i, 13 <sup>40</sup> 13 <sup>20</sup> , ♦ <sup>0</sup> 6 <sup>40</sup> 10 <sup>10</sup> 12 <sup>45</sup> 23 <sup>25</sup> i, F <sub>w</sub> 15 <sup>50</sup> 21 <sup>40</sup>
12	7	00①	07①	05	04.0	07.7	18.9	.	F <sub>ww</sub> 7 <sup>20</sup> 16 <sup>50</sup> i, ♦ <sup>0</sup> -17 <sup>50</sup> 11 <sup>40</sup> 16 <sup>40</sup> 10 <sup>20</sup> , ▲ <sup>0</sup> 12 <sup>10</sup> 12 <sup>24</sup>
13	e	08	05	09	06.7	01.0	01.2	.	• <sup>0</sup> 7 <sup>50</sup> 7 <sup>40</sup> , ♦ <sup>0</sup> 10 <sup>55</sup> 15 <sup>05</sup> , 15 <sup>25</sup> 22 <sup>20</sup> , 24
14	8	10	10	10•	10.0	01.0	00.2	.	• <sup>0</sup> -0 <sup>36</sup> 7 <sup>40</sup> 44 <sup>50</sup> , 18 <sup>10</sup> 24 <sup>40</sup>
15	8	10	05①	10	08.3	09.2	01.1	.	• <sup>0</sup> 2 <sup>0</sup> -0 <sup>16</sup> i, 19 <sup>50</sup> 24 <sup>40</sup> , ♦ <sup>0</sup> 19 <sup>40</sup> 19 <sup>50</sup>
16	8	00①	08①	03	03.7	C9.6	C5.8	.	• <sup>0</sup> 0-0 <sup>16</sup> 12 <sup>50</sup> 13 <sup>45</sup> , ♦ <sup>0</sup> -1 12 <sup>20</sup> 12 <sup>07</sup> i
17	8	00①	06①	00	02.0	10.8	CC.2	.	= <sup>0</sup> 3 <sup>45</sup> 6 <sup>50</sup> , ♦ <sup>0</sup> 11 <sup>45</sup> 13 <sup>40</sup> , 18 <sup>10</sup> 12-12 <sup>45</sup> , ♦ <sup>0</sup> -1 12 <sup>02</sup> 12 <sup>30</sup> i, □ <sup>0</sup> 20-24
18	8	00①	02①	02	C1.3	13.0	C1.5	.	• <sup>0</sup> -2 <sup>0</sup> -0 <sup>16</sup> 10 <sup>20</sup> 24
19	8	06①	05①	10•④	07.0	08.4	.	.	• <sup>0</sup> 2 <sup>0</sup> -0 <sup>8</sup> 15 <sup>10</sup> 15 <sup>20</sup> 21 <sup>40</sup> , ♦ <sup>0</sup> -1 16 <sup>20</sup> 17 <sup>50</sup> i, 21 <sup>25</sup> 22 <sup>10</sup> , ♦ <sup>0</sup> 2 <sup>0</sup> 17 <sup>50</sup> 21 <sup>40</sup>
20	7	10	08	00	C6.0	03.1	38.3	.	= <sup>0</sup> 5 <sup>30</sup> 8 <sup>45</sup> , □ <sup>0</sup> 20 <sup>30</sup> 24
21	7	02①	05①	10	05.7	10.9	.	.	• <sup>0</sup> -2 <sup>0</sup> -0 <sup>9</sup> , 19 <sup>30</sup> 24
22	7	00①	05①	00	01.7	10.7	.	.	• <sup>0</sup> -2 <sup>0</sup> -0 <sup>9</sup> 16 <sup>10</sup> 16 <sup>50</sup> , ♦ <sup>0</sup> 16 <sup>52</sup> 17 <sup>45</sup> , ♦ <sup>0</sup> -1 22 <sup>45</sup> 24, ▲ <sup>0</sup> 23 <sup>50</sup> 24
23	7	00①	08①	05	04.3	09.7	.	.	• <sup>0</sup> -10 <sup>30</sup> 17 <sup>05</sup> 11 <sup>45</sup> i, 10 <sup>10</sup> 0 <sup>10</sup> , ♦ <sup>0</sup> -2 <sup>0</sup> 0 <sup>65</sup> 0 <sup>15</sup> , 15 <sup>30</sup> 15 <sup>52</sup> , 18 <sup>02</sup> 15 <sup>25</sup> 16 <sup>10</sup> , F <sub>15<sup>22</sup></sub> 15 <sup>46</sup>
24	8	10	06①	07	C7.7	C3.2	CC.0	.	• <sup>0</sup> 5 <sup>10</sup> 10 <sup>30</sup> i, □ <sup>0</sup> 20 <sup>30</sup> 24
25	7	10•	06①	00	05.3	06.9	12.6	.	.
26	8	02①	04①	04	C3.7	12.8	C1.1	.	• <sup>0</sup> -2 <sup>0</sup> -0 <sup>9</sup> 20 <sup>30</sup> 24
27	8	07	06①	02	05.0	03.7	.	.	• <sup>0</sup> -10 <sup>10</sup> 7 <sup>10</sup> , F <sub>SESE-SE</sub> 6, 9 <sup>40</sup>
28	8	10•	05	09	05.3	02.3	CC.0	.	• <sup>0</sup> 5 <sup>00</sup> 17 <sup>30</sup> , 14 <sup>50</sup> , 14 <sup>50</sup> i
29	8	10•	08①	10•④	05.3	C1.8	CC.0	.	• <sup>0</sup> -16 <sup>30</sup> 9 <sup>45</sup> , 15 <sup>20</sup> 24 <sup>40</sup> , ♦ <sup>0</sup> -2 <sup>0</sup> 16 <sup>02</sup> 16 <sup>22</sup> 19 <sup>40</sup> 21 <sup>20</sup> i, ▲ <sup>0</sup> 19 <sup>30</sup> 21 <sup>45</sup>
30	6	10•	10•	06	08.7	00.9	<u>43.8</u>	.	• <sup>0</sup> -2 <sup>0</sup> -0 <sup>15</sup> 3 <sup>40</sup> 14 <sup>45</sup> , F <sub>sww-NW</sub> 3, ▲ <sup>0</sup> 14 <sup>40</sup> , = <sup>0</sup> 14 <sup>45</sup> 16 <sup>30</sup>

MES.  
MAYER

1974 JUL

BEDOGRAD

 $\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1h\ 22\ min.$ 

BR. ST. 173

D DN	Vozdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost % %			Pravac i jačina vetro D, I (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	749.0	749.4	749.8	15.6	22.7	19.0	16.1	24.1	13.0	10.2	11.4	10.8	12.0	86	52	75	72	W	2	NNW	2	SW	1
2	752.7	754.5	754.0	17.6	20.2	16.6	17.8	21.7	16.6	12.6	11.6	11.0	11.6	77	62	62	74	N	2	NNW	2	SW	1
3	754.2	750.9	747.2	16.0	24.7	19.8	20.1	25.4	11.3	07.7	09.7	08.1	10.8	71	35	62	56	WSW	1	SSE	2	W	3
4	749.8	750.8	751.1	16.8	24.2	19.4	20.0	24.6	16.0	14.8	13.6	09.5	09.2	95	42	54	64	NNW	2	N	2	NNE	2
5	752.0	752.3	751.8	18.0	25.0	19.8	20.6	25.8	14.5	11.3	09.6	10.0	11.5	62	42	66	57	E	2	NNE	2	SE	1
6	750.7	749.0	747.0	20.1	29.9	23.6	24.3	31.0	16.4	12.3	11.2	15.2	15.3	63	46	70	60	SE	2	NNW	2	SSE	1
7	747.4	751.2	749.0	10.5	15.8	14.6	16.1	23.6	14.6	17.0	13.4	09.6	09.9	79	71	80	77	NW	3	NNW	3	NNW	2
8	751.4	750.8	751.9	13.6	20.8	16.0	16.6	21.3	10.8	08.7	09.5	08.6	07.5	82	47	55	61	NNW	2	NN	3	NNW	3
9	753.3	751.8	750.6	14.0	22.6	19.0	14.2	23.2	10.7	08.0	08.3	08.6	08.0	70	42	59	57	N	2	NNW	3	NNW	2
10	750.1	750.7	751.9	15.7	23.5	18.8	19.7	22.8	15.4	13.3	12.2	11.1	11.8	91	51	82	75	S	1	NNW	3	NNW	1
11	753.1	752.9	752.0	15.7	24.4	21.2	20.6	25.2	12.1	08.5	09.4	08.5	10.5	70	37	56	54	WSW	1	NW	2	SSE	1
12	751.6	750.7	751.1	20.0	29.8	23.2	24.0	31.0	16.0	13.0	12.2	12.0	15.0	69	38	70	59	ESE	2	NNW	2	ENE	1
13	751.0	750.0	748.9	22.5	32.5	26.2	26.8	32.8	19.0	16.1	14.9	13.9	15.9	73	38	62	59	-	0	SE	2	SE	2
14	749.3	748.4	747.3	25.1	31.6	24.0	27.7	34.4	21.0	16.0	13.1	10.6	15.2	55	27	60	47	SSE	2	NNW	2	SE	1
15	750.9	751.9	751.1	24.0	31.4	26.8	27.2	31.7	21.3	16.7	15.8	14.1	15.3	71	41	58	57	NNW	1	NW	1	NNF	2
16	751.9	750.3	749.4	19.8	19.6	25.0	25.4	31.1	17.8	16.3	12.0	14.5	15.1	75	46	60	60	W	1	NF	2	ESE	2
17	747.7	745.4	743.6	24.	23.3	28.5	28.9	34.9	22.7	19.0	16.3	16.5	16.1	72	46	62	60	SE	4	SE	3	SSE	2
18	742.9	752.9	745.4	26.	26.6	22.4	25.6	35.2	21.1	16.6	14.1	15.2	14.2	56	49	61	55	SE	1	NNW	4	NW	1
19	746.1	747.5	746.0	16.8	17.1	16.8	17.8	23.4	16.6	15.7	14.2	12.0	12.9	85	62	90	86	N	2	NNW	2	NNW	2
20	746.4	748.0	747.6	14.5	14.8	17.1	14.9	16.7	14.5	14.3	11.6	10.6	16.4	94	64	81	86	NNF	2	W	2	W	2
21	746.2	745.1	744.6	16.3	19.1	12.8	15.0	19.8	12.7	09.7	09.7	10.3	10.6	80	66	89	78	NNW	2	W	4	W	2
22	747.5	747.7	747.6	14.1	17.6	15.2	15.6	17.8	13.6	13.0	10.9	10.7	10.9	91	71	84	82	NNW	3	NNW	3	W	3
23	745.8	747.7	746.3	13.7	15.0	15.9	15.3	16.7	13.6	13.5	11.4	12.6	12.5	97	94	92	94	W	3	W	3	NNW	3
24	749.0	749.5	749.0	17.0	27.7	20.4	21.2	28.0	13.2	16.2	11.3	12.3	13.1	77	49	72	67	SE	1	NW	2	SE	2
25	742.6	747.6	751.8	21.0	29.5	16.5	21.5	30.0	16.8	12.9	11.9	11.1	11.2	57	36	78	57	SSE	1	S	2	N	2
26	754.5	754.0	754.0	14.8	21.8	16.8	17.6	22.7	14.2	13.9	11.3	09.6	10.0	90	49	65	65	W	2	NW	2	E	1
27	754.2	753.6	752.7	15.9	24.4	17.8	18.5	25.0	11.6	08.1	09.4	09.1	11.6	71	40	76	62	NNF	1	ESE	2	ESE	1
28	753.3	753.2	753.2	16.2	28.4	21.3	22.8	28.9	15.1	10.5	11.1	11.0	11.3	66	41	60	56	ESE	2	ESE	2	SE	1
29	754.5	754.6	754.7	15.7	29.7	21.6	23.2	30.2	16.7	12.0	12.9	12.0	12.8	75	39	66	60	SW	1	E	2	ESE	2
30	753.7	751.5	750.0	20.0	31.0	22.6	24.3	31.5	16.8	15.1	12.6	11.9	12.9	68	35	68	57	ENE	1	SE	2	ESE	1
31	749.5	749.4	749.6	21.5	31.3	23.2	24.8	31.8	16.6	17.3	12.7	11.9	14.9	66	35	70	57	NW	1	NF	2	E	1
MFS.	WRFD.	750.4	750.1	749.4	18.4	25.2	20.1	20.9	26.6	15.6	12.8	11.9	11.5	12.4	75	50	70	65	1.7	2.4	1.7	1.7	1.7

1974 AVGUST

BEDOGRAD

1	750.1	749.7	748.7	22.4	32.2	24.0	25.7	32.6	18.8	15.0	14.6	13.7	13.5	71	38	60	56	ESE	1	F	1	ESE	2
2	749.8	749.4	749.6	22.7	33.4	24.6	26.0	33.4	19.5	15.4	15.9	14.6	13.4	77	36	60	58	-	0	ESE	1	SE	2
3	750.6	750.6	750.7	22.8	34.2	24.6	27.0	34.3	19.8	15.9	14.8	14.4	13.7	67	38	58	54	SE	1	ESE	2	ESE	2
4	751.3	751.6	750.1	24.3	34.0	27.0	28.5	34.9	21.2	16.5	13.7	12.2	15.2	60	30	54	48	ESE	3	SE	2	SE	3
5	750.6	750.3	749.7	27.1	33.2	27.8	29.0	33.8	23.6	17.8	15.4	16.0	15.7	57	42	56	52	SE	1	NW	2	NL	2
6	751.7	754.2	754.0	21.8	22.8	19.6	21.2	27.8	19.6	14.0	12.0	11.1	09.6	61	50	56	56	NNW	2	NW	2	NNW	2
7	751.6	752.4	750.1	15.9	24.4	18.4	19.3	25.1	14.0	12.2	10.5	08.8	09.8	79	38	62	60	NNW	2	NNW	2	NNW	1
8	749.0	747.3	744.0	18.7	25.4	23.6	23.8	30.0	13.4	10.1	09.6	10.5	12.1	60	34	55	50	E	2	SE	2	SE	2
9	749.1	745.5	748.2	19.4	21.7	16.7	18.6	24.2	16.5	06.1	14.3	14.2	12.9	95	74	90	93	S	1	NN	3	W	3
10	750.6	749.7	747.5	16.7	24.4	19.2	19.0	25.2	14.4	12.7	11.2	09.4	11.6	76	41	70	63	W	2	NNW	1	ESE	2
11	744.0	742.4	746.1	17.9	19.6	14.6	16.7	20.2	14.6	12.0	11.3	12.0	11.2	74	76	90	78	SE	2	SE	1	W	2
12	746.7	747.2	748.4	14.2	15.0	14.2	14.4	17.1	12.8	12.5	09.2	11.0	11.4	76	86	94	85	NNW	3	NNW	4	W	2
13	751.2	752.3	753.4	14.3	22.4	17.6	18.1	23.6	13.6	13.4	10.2	11.0	11.4	81	54	75	70	W	2	NNW	2	W	1
14	754.4	7																					

ER. ST. 173

$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

1	E	000	020	C2	01.3	12.2	.	.	Δ <sup>-2</sup> 0-8 <sup>38</sup> 20 <sup>16</sup> 24
2	E	000	000	CC	00.0	12.2	.	.	Δ <sup>-1</sup> 0 9 <sup>19</sup> 24
3	E	000	000	CC	00.0	12.3	.	.	Δ <sup>-2</sup> 0 8 <sup>54</sup> 20 <sup>15</sup> 24
4	E	000	000	CC	00.0	12.6	.	.	Δ <sup>0</sup> 0 8 <sup>50</sup> F <sub>EE</sub> 9 <sup>44</sup> 12 <sup>15</sup> 24
5	E	000	010	00	02.3	10.9	.	.	.
6	E	070	010	C2	02.7	09.9	.	.	Δ <sup>0</sup> 3 -7 <sup>35</sup> 20 <sup>30</sup> 24
7	E	000	010	CC	00.3	12.9	.	.	Δ <sup>0</sup> 0 9 <sup>05</sup> 8 <sup>23</sup> 20 <sup>35</sup> 24
8	E	000	000	CC	00.0	12.7	.	.	Δ <sup>0</sup> 0 -3 <sup>40</sup> 15 <sup>47</sup> 16 <sup>40</sup> ; Δ <sup>0</sup> 0 <sup>05</sup> 0 <sup>45</sup> 3 ; 3 <sup>0</sup> 12 <sup>21</sup> 12 <sup>18</sup> 16 <sup>12</sup> 17 <sup>05</sup> ; Δ <sup>0</sup> 4 <sup>40</sup> 12 <sup>40</sup> 17 <sup>10</sup> 17 <sup>05</sup> ; Δ <sup>0</sup> 4 <sup>40</sup> 12 <sup>40</sup> 17 <sup>10</sup> 17 <sup>05</sup>
9	E	10	10	•	10	10.0	03.3	12.6	.
10	E	040	030	00	02.3	11.0	03.8	.	Δ <sup>0</sup> 20 <sup>15</sup> 24
11	E	060	10	10	0E.7	00.5	.	.	Δ <sup>0</sup> 0 -4 <sup>30</sup> F <sub>SE-W</sub> 3 <sup>45</sup> 4 <sup>42</sup> 18 <sup>11</sup> 2 <sup>31</sup> ; Δ <sup>0</sup> 0 <sup>15</sup> 18 <sup>35</sup> ; Δ <sup>3</sup> 4 <sup>21</sup> 18 <sup>11</sup> 13 <sup>0</sup> 11 <sup>2</sup> 12 <sup>10</sup>
12	E	10	10	10	•	10.0	00.0	CP.7	.
13	E	10	060	00	05.3	08.1	17.4	.	Δ <sup>0</sup> 20 <sup>15</sup> 24
14	E	030	020	00	01.7	11.5	.	.	Δ <sup>0</sup> 0 0 20 <sup>30</sup> 24
15	E	040	050	00	02.0	11.4	.	.	Δ <sup>0</sup> 0 0 19 <sup>45</sup> 24
16	E	060	030	00	03.0	10.9	.	.	Δ <sup>0</sup> 20 <sup>15</sup> 19 <sup>30</sup> 24
17	E	000	030	CC	01.0	11.8	.	.	Δ <sup>0</sup> 0 0 19 <sup>30</sup> 24
18	E	000	000	00	00.0	12.1	.	.	Δ <sup>0</sup> 0 -7 <sup>45</sup> 19 <sup>15</sup> 24 ; F <sub>SE</sub> 11 <sup>08</sup> 12 <sup>46</sup>
19	E	000	000	00	00.0	11.6	.	.	Δ <sup>0</sup> 0 -8 <sup>15</sup> 19 <sup>15</sup> 24
20	E	000	000	00	00.0	11.2	.	.	Δ <sup>0</sup> 0 -10 19 <sup>15</sup> 24
21	E	050	020	C8	05.0	10.7	.	.	Δ <sup>-2</sup> 0-7 <sup>15</sup>
22	E	060	050	00	02.7	10.3	.	.	Δ <sup>0</sup> 2 3 <sup>42</sup> 18 <sup>34</sup> 17 <sup>35</sup> ; 17 <sup>35</sup> 17 <sup>58</sup> ; Δ <sup>0</sup> 3 <sup>50</sup> 4 <sup>05</sup> ; 17 <sup>18</sup> 18 <sup>20</sup> 22 <sup>45</sup> 23 <sup>30</sup> ; Δ <sup>0</sup> 0 7 <sup>15</sup> 17 <sup>35</sup> 24
23	E	10R	060	09	06.3	06.3	00.0	.	Δ <sup>0</sup> 20 <sup>15</sup> 24
24	E	060	09	05	06.7	06.6	12.2	.	Δ <sup>0</sup> 0 -10 8 <sup>35</sup> 20 <sup>30</sup> 24
25	E	050	020	06	04.3	10.4	.	.	Δ <sup>0</sup> 0 0 20 <sup>30</sup> 24
26	E	030	000	C5	02.7	11.0	.	.	Δ <sup>0</sup> 0 0 19 <sup>30</sup>
27	E	10	040	CC	C7.7	06.7	00.4	.	Δ <sup>0</sup> 0 0 25 Δ <sup>0</sup> 22 <sup>30</sup> 24
28	E	040	040	C4	04.0	10.8	.	.	Δ <sup>0</sup> 0 -7 <sup>20</sup> 20 <sup>30</sup> 24 ; F <sub>EE</sub> 9 <sup>32</sup> 16 <sup>30</sup>
29	E	000	020	CC	00.7	10.8	.	.	Δ <sup>0</sup> 0 0 45 F <sub>EE</sub> 0 <sup>15</sup> 15 <sup>15</sup>
30	E	080	060	10	08.0	03.5	.	.	Δ <sup>0</sup> 15 <sup>45</sup> 16 <sup>45</sup> 16 <sup>45</sup> 19 <sup>45</sup> ; 23 <sup>45</sup> 24
31	E	010	020	00	01.0	11.2	03.1	.	Δ <sup>0</sup> 0 0 10 Δ <sup>0</sup> 20 <sup>30</sup> 24

$\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1\text{h }22\text{ min.}$

BR. ST. 173

S 8	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	750.3	749.8	749.6	17.5	20.5	21.4	21.8	27.7	15.4	11.1	09.5	09.1	10.6	63	35	55	51	SE	2	ESE	2	SE	2
2	749.3	749.5	750.3	19.6	27.8	19.4	21.6	29.0	17.0	13.1	10.6	13.5	16.8	62	48	94	68	SE	2	W	2	WSW	2
3	710.1	749.5	749.3	19.7	28.1	23.7	23.4	29.7	17.1	14.4	14.4	11.9	12.9	89	42	59	63	-	0	WSW	1	ESE	2
4	748.3	742.2	750.8	21.5	29.5	16.6	21.1	30.2	16.6	17.4	13.1	13.9	13.1	68	45	92	68	ESE	2	ESE	2	N	4
5	754.2	753.6	752.6	13.6	21.0	15.4	16.4	21.6	12.5	10.8	10.0	10.3	11.6	85	55	90	77	W	2	NNW	2	ESE	1
6	749.9	746.4	743.9	14.5	24.7	19.8	19.7	25.8	11.7	05.0	11.0	10.7	11.7	89	46	6E	68	ESE	2	ESE	3	SE	3
7	741.7	742.6	745.0	16.6	23.3	17.7	19.8	23.3	15.7	14.3	10.9	12.0	11.8	77	56	78	70	SE	4	ESE	3	S	2
8	749.6	751.7	754.0	15.0	22.8	19.2	18.6	23.3	14.0	12.5	11.7	13.2	13.6	92	64	88	81	WSW	2	W	2	W	1
9	755.7	755.3	753.8	16.5	26.2	19.4	20.4	26.6	14.1	11.4	12.0	11.5	11.6	92	45	70	69	-	0	E	1	ESE	2
10	753.8	753.7	754.9	20.1	28.6	22.0	23.2	29.0	18.7	14.2	12.7	12.9	15.6	72	44	79	65	SE	2	NNW	1	N	2
11	759.0	759.1	758.7	13.6	17.4	15.6	15.6	22.0	13.4	12.4	10.2	10.9	11.3	87	73	85	82	W	2	NW	2	WSW	2
12	758.2	757.2	756.2	16.6	23.7	19.0	19.6	24.3	15.4	11.9	11.5	12.0	09.7	81	55	59	65	ESE	1	SE	3	ESE	3
13	755.6	754.6	756.4	15.4	25.4	17.5	19.2	25.7	14.2	11.0	09.4	13.1	13.5	72	54	88	71	ESE	1	NNW	2	SW	1
14	754.9	754.0	751.7	15.4	24.7	18.6	19.3	25.1	14.5	11.5	12.6	12.6	13.2	96	54	82	77	SW	1	NW	2	W	1
15	752.0	751.7	750.9	17.0	25.4	19.8	20.5	26.0	15.6	12.6	12.3	12.1	12.4	85	50	72	69	WSW	2	N	2	NNE	2
16	754.0	754.6	755.5	14.5	21.2	16.6	17.0	22.5	14.0	11.9	11.1	11.5	09.5	90	58	70	73	N	2	ESE	2	SE	2
17	755.9	754.5	753.9	12.3	23.8	17.7	18.1	23.8	13.2	11.2	04.1	05.7	04.4	71	44	55	57	ESE	4	SE	3	SE	3
18	753.6	752.8	752.6	16.3	25.0	17.9	18.2	25.2	15.2	12.8	07.8	10.2	08.0	56	43	52	50	SE	3	SF	2	SSE	2
19	752.8	752.0	751.0	16.2	24.0	16.2	18.2	24.8	15.4	12.6	09.1	11.7	12.0	56	52	87	68	SE	2	NE	2	ENE	2
20	749.9	747.7	746.7	16.4	26.5	20.0	20.8	27.0	13.6	10.0	04.3	04.6	08.2	66	33	47	49	SF	2	SE	3	SE	3
21	748.7	746.1	746.0	17.4	22.6	18.0	19.0	22.7	17.3	15.0	06.2	10.5	11.8	55	51	76	61	SE	2	SSE	2	SF	2
22	746.6	747.1	746.3	18.1	24.7	19.5	18.6	25.1	15.2	11.7	12.3	12.0	12.5	79	51	95	75	SSE	3	SSW	2	SE	1
23	743.4	742.7	742.6	16.2	19.0	15.4	16.5	20.0	15.2	12.1	13.0	13.7	11.7	94	83	89	89	-	0	W	2	WNW	2
24	746.4	744.1	742.6	15.2	25.7	20.4	20.4	26.6	14.0	11.0	11.3	10.5	08.8	87	42	49	59	ESE	2	SW	2	SSE	3
25	739.6	739.4	738.8	16.5	14.5	11.8	13.6	20.6	11.8	14.3	11.0	11.1	09.6	78	90	92	87	SE	3	W	3	SSE	1
26	734.7	733.1	733.4	11.4	13.0	09.5	10.8	14.8	08.9	05.8	04.0	10.5	08.6	89	92	96	93	ESE	2	ESF	1	NW	3
27	740.2	740.5	751.0	09.0	15.6	09.6	11.0	15.7	08.8	07.5	07.1	04.4	06.6	83	48	74	68	W	3	NW	3	W	2
28	750.5	748.1	747.6	06.9	20.2	12.0	12.8	20.6	05.5	02.2	06.7	07.6	08.9	91	43	84	73	SE	1	W	2	SE	2
29	746.6	747.1	746.0	11.4	24.1	19.1	18.5	25.6	10.0	05.5	08.2	07.8	10.2	50	35	62	59	SE	1	SW	1	SE	2
30	747.3	747.9	749.6	16.4	19.5	12.2	15.1	25.6	12.2	11.9	04.4	11.6	09.9	67	68	93	76	SE	3	W	2	NW	2
MES.	NRFD.	750.0	749.1	750.1	15.6	23.2	17.2	18.3	24.3	13.9	11.4	10.5	11.1	11.1	79	53	76	69	1.5	2.1	2.0	2.0	2.0

1974. OKTOBAR

BEOGRAD

1	749.0	749.8	750.6	11.0	12.2	10.9	11.2	13.6	10.7	10.5	09.5	09.8	09.3	97	92	95	95	NNE	1	NW	1	WSW	1
2	750.6	747.5	744.4	07.7	12.2	12.6	11.4	13.2	07.5	06.1	07.2	08.2	09.8	91	77	88	85	SW	1	E	2	SSE	3
3	750.9	753.5	753.5	07.2	14.0	09.3	10.0	07.1	07.0	06.8	06.5	07.1	89	55	81	75	WSW	4	W	2	SL	3	
4	752.3	751.7	751.5	08.8	21.0	12.7	13.8	21.0	07.6	02.8	06.6	05.5	08.8	78	30	80	63	FSE	2	S	2	SE	2
5	750.3	749.9	749.0	09.1	18.7	10.2	10.0	12.4	08.5	05.7	08.4	08.7	09.7	98	91	93	94	SSE	1	NNW	2	W	2
6	746.4	747.8	751.7	09.5	24.5	07.6	08.3	10.2	07.6	09.5	08.7	07.9	06.9	98	95	88	94	SW	2	WSW	3	W	2
7	750.2	747.0	744.7	06.5	10.0	04.6	08.9	10.6	05.2	02.3	06.9	07.4	08.4	94	60	94	89	ESE	1	ESE	2	ESE	2
8	743.4	741.9	745.8	09.4	17.4	11.1	12.2	17.6	08.8	05.3	08.6	10.7	09.4	98	72	95	88	ESE	2	ESE	2	SSE	2
9	746.6	747.1	748.6	09.9	15.4	10.2	11.2	15.6	06.8	02.6	08.0	08.6	08.9	94	65	95	85	SE	1	WNW	2	SE	2
10	750.7	752.2	753.1	08.3	13.5	07.0	09.0	14.1	07.0	03.7	07.7	06.8	07.1	94	55	95	83	WSW	2	W	2	SF	1
11	752.6	751.8	752.4	06.3	17.6	11.5	11.7	18.4	04.5	00.7	06.9	07.6	07.5	96	50	73	73	ESE	2	SE	2	ESE	3
12	752.8	751.5	749.7	10.1	18.7	15.0	14.7	19.2	06.0	03.6	07.3	08.1	06.4	79	50	66	65	ESE	2	ESE	3	ESE	3
13	748.0	748.4	750.2	13.7	14.0	08.2	11.0	15.7	08.0	12.0	10.9	11.4	07.9	93	95	97	95	ESE	3	ESE	3	WNW	2
14	748.7	749.3	750.7	07.2	09.1	07.4	09.2	07.2	07.0	07.4	07.5	07.4	97	86	96	93	WNW	2	W	2	WSW	2	
15	750.1	749.1	746.0	06.2	09.2	07.8	07.8	10.0	06.2	05.8													

PP. ST. 173

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vlажност 0-9	Облачност N (0-10)					Изолација брз салі	Падавина R mm	Снеžни покривач h cm	Развој времена			
		14	7	14	21	Сред Dies				7	7	w	
1	8	050	050	09	07.7	06.7	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} F_{SE} 8^{\circ} 14^{\circ} 6^{\circ} 10 \cdot 19^{\circ} 22^{\circ} 23^{\circ}$			
2	8	C7	020	10•R	06.3	07.4	00.0	.	.	$\Delta^{+2} 0 \cdot 20^{\circ} 20^{\circ} 8^{\circ} 20^{\circ} 20^{\circ} 20^{\circ} 20^{\circ} 21^{\circ}$			
3	8	000	080	00	02.7	09.4	08.6	.	.	$\Delta^{+2} 0 \cdot 13^{\circ} 9^{\circ} 20^{\circ} 24$			
4	8	050	010	10•R	05.3	08.0	.	.	.	$\Delta^{+2} 0 \cdot 6^{\circ} 0^{\circ} 9^{\circ} 17 \cdot 17^{\circ} 22^{\circ} 22^{\circ} 24^{\circ} F_{SE} 0 \cdot 2^{\circ} 17^{\circ} 22^{\circ} F_{NW} 1^{\circ} 2^{\circ} 2^{\circ}$			
5	7	010	050	00	02.0	11.6	25.0	.	.	$F_{WW} 0^{\circ} \Delta^{+2} 0 \cdot 14^{\circ} 24$			
6	8	000	000	00	00.0	11.5	.	.	.	$\Delta^{+2} 0 \cdot 10^{\circ} F_{SE} 11^{\circ} 12^{\circ} 18^{\circ} 24^{\circ}$			
7	8	C9	050	00	04.7	06.2	.	.	.	$F_{SE} 0 \cdot 14^{\circ} 13^{\circ} 2^{\circ} 20^{\circ} \Delta^{+2} 0^{\circ} 19^{\circ} 24$			
8	7	10	060	00	05.3	05.9	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 19^{\circ} 24$			
9	7	000	050	01	02.0	10.8	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} 18^{\circ} 24 = 0 \cdot 130 10^{\circ} 45$			
10	7	000	060	03	04.7	07.8	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} F_{NW} 2^{\circ} 4^{\circ}$			
11	7	09	10	00	06.3	00.5	11.6	.	.	$\Delta^{+2} 0 \cdot 0^{\circ} 0^{\circ} 0^{\circ} 45^{\circ} 3^{\circ} 30^{\circ} 2^{\circ} 45^{\circ} F_{SE} 0 \cdot 35^{\circ} 3^{\circ} 0^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$			
12	7	10	040	00	04.7	05.1	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} 18^{\circ} 24$			
13	8	000	010	00	00.3	10.0	.	.	.	$\Delta^{+2} 0 \cdot 20 \cdot 0^{\circ} 19^{\circ} 24$			
14	8	000	050	00	01.7	00.7	.	.	.	$\Delta^{+2} 0 \cdot 15^{\circ} 19^{\circ} 24 = 0 \cdot 15^{\circ} 10^{\circ} 30^{\circ}$			
15	7	000	040	00	01.3	01.8	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 0^{\circ}$			
16	7	000	040	00	01.3	00.3	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 0^{\circ} = 0 \cdot 13^{\circ} 13^{\circ}$			
17	7	000	000	00	00.0	05.6	.	.	.	$\Delta^{+2} 0 \cdot 30^{\circ} 30^{\circ} F_{SE} 3^{\circ} 3^{\circ} 12^{\circ} 18^{\circ} 21^{\circ} 0^{\circ}$			
18	8	06	030	05	04.7	07.0	.	.	.	$F_{SE} 6^{\circ} 0^{\circ} 0^{\circ}$			
19	8	04	040	03	03.7	06.5	.	.	.	$\Delta^{+2} 0 \cdot 18^{\circ} 0^{\circ} 0^{\circ}$			
20	8	05	020	09	05.3	07.3	.	.	.	$\Delta^{+2} 0 \cdot 7^{\circ} F_{SE} - SE 1^{\circ} 10^{\circ} 13^{\circ} 16^{\circ} 10^{\circ} 23^{\circ} 14^{\circ} 21^{\circ} 0^{\circ}$			
21	8	07	10	00	05.7	00.0	.	.	.	$\Delta^{+2} 0 \cdot 0^{\circ} 20^{\circ} 24$			
22	8	10	10	07	09.0	01.9	00.0	.	.	$\Delta^{+2} 0 \cdot 4^{\circ} 45^{\circ} 0^{\circ} 45^{\circ} 30^{\circ} F_{SE} 15^{\circ} 15^{\circ} F_{WW} 15^{\circ} 16^{\circ} 16^{\circ} 16^{\circ} 0^{\circ} 0^{\circ}$			
23	8	10	10	• 10	10.0	00.0	C5.4	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 10^{\circ} 15^{\circ} 13^{\circ} 24^{\circ}$			
24	7	050	060	08	05.3	08.2	00.0	.	.	$\Delta^{+2} 0 \cdot 30^{\circ} 30^{\circ} = 0 \cdot 45^{\circ} 6^{\circ} 0^{\circ}$			
25	7	10	10	• 10	10.0	00.1	C1.4	.	.	$\Delta^{+2} 0 \cdot 45^{\circ} 6^{\circ} 0^{\circ} 45^{\circ} 15^{\circ} 0^{\circ} F_{SE} 4^{\circ} 35^{\circ} 7^{\circ} 0^{\circ} 10^{\circ} 23^{\circ} 0^{\circ}$			
26	7	07	10	• 10	09.0	01.1	C3.4	.	.	$\Delta^{+2} 0 \cdot 11^{\circ} 23^{\circ} F_{N-NW} 16^{\circ} 23^{\circ} 6^{\circ} 10^{\circ} 48^{\circ} 20^{\circ}$			
27	7	10	060	00	05.3	10.6	<u>39.4</u>	.	.	$F_{WW} - NW 1^{\circ} 15^{\circ} 0^{\circ} 48^{\circ} 13^{\circ} 0^{\circ} 10^{\circ} 45^{\circ} F_{WW} 8^{\circ} 13^{\circ} 0^{\circ} \Delta^{+2} 0^{\circ} 19^{\circ} 24$			
28	8	000	000	00	00.0	10.6	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 15^{\circ} 18^{\circ} 22^{\circ}$			
29	8	000	040	05	04.3	09.5	.	.	.	$\Delta^{+2} 0 \cdot 20 \cdot 0^{\circ} 19^{\circ} 24$			
30	8	040	080	10	07.3	07.7	.	.	.	$\Delta^{+2} 0 \cdot 7^{\circ} 0^{\circ} 17^{\circ} 45^{\circ} 21^{\circ} 45^{\circ} F_{WW} 18^{\circ} 0^{\circ}$			

БЕОГРАД

1974 OKT (BAR)

1	7	10•	10	09	05.7	00.0	13.5	.	
2	7	060	10	10•	08.7	00.6	04.5	.	$\bullet 2^{\circ} 19^{\text{m}} 30^{\text{s}}$
3	7	10	C10	C2	04.3	05.9	08.4	.	$= 0^{\circ} 5^{\text{m}} 46^{\text{s}}$
4	8	06	020	05	04.3	07.9	.	.	$\bullet 0^{\circ} 1^{\text{m}} 23^{\text{s}}$
5	5	050	10	10	08.3	00.0	.	.	$\bullet 0^{\circ} 1^{\text{m}} 48^{\text{s}}$
6	6	10•	10•	10	10.0	00.0	C2.0	.	$= 0^{\circ} 0^{\text{m}} 18^{\text{s}}$
7	6	10	1C	1C	10.0	00.0	C2.7	.	$= 0^{\circ} 0^{\text{m}} 20^{\text{s}}$
8	7	10	10•	10	10.0	00.0	C2.5	.	$= 0^{\circ} 0^{\text{m}} 13^{\text{s}}$
9	8	070	020	09	06.0	06.0	02.3	.	$= 0^{\circ} 0^{\text{m}} 09^{\text{s}}$
10	8	060	040	00	03.3	07.0	C4.7	.	$= 0^{\circ} 0^{\text{m}} 07^{\text{s}}$
11	8	040	0C0	CC	01.3	09.4	00.0	.	$\bullet 0^{\circ} 0^{\text{m}} 02^{\text{s}}$
12	8	030	060	08	C5.7	04.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
13	7	10•	10•	1C	10.0	00.0	C2.5	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
14	6	10•	1C	1C	10.0	00.0	27.4	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
15	7	1C	10	10•	10.0	00.2	10.0	.	$= 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
16	7	09	1C	10	C5.7	04.1	20.2	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
17	8	000	030	01	01.3	08.9	03.5	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
18	8	00	0C0	00	0C.0	09.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
19	8	00	000	05	01.7	09.4	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
20	8	C5	1C	CC	08.0	04.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
21	7	10	10•	10	10.0	00.0	02.2	.	$F_{SE-W} 0^{\circ} 18^{\text{m}} 02^{\text{s}}$
22	8	C9	1C	10	09.7	02.8	C8.5	.	$= 0^{\circ} 0^{\text{m}} 44^{\text{s}}$
23	6	10•	10•	10•	10.0	00.0	C8.5	.	$= 0^{\circ} 0^{\text{m}} 13^{\text{s}}$
24	8	08	040	10	07.3	07.8	20.5	.	$= 0^{\circ} 0^{\text{m}} 34^{\text{s}}$
25	7	10	0C	00	06.3	02.5	00.0	.	$= 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
26	7	040	10•	10•	08.0	01.7	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
27	7	02	080	00	03.3	08.1	04.7	.	$\bullet 0^{\circ} 0^{\text{m}} 19^{\text{s}}$
28	8	05	060	05	05.3	05.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 10^{\text{s}}$
29	7	10•	10	10	10.0	00.0	C0.7	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
30	5	10*	10•	10•	10.0	00.0	16.8	03	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
31	7	00	10•	10	06.7	00.0	C7.2	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$

$\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1h\ 22\ min.$

BR. ST. 173

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %				Pravac i jačina vetrova D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	741.9	743.4	747.0	04.9	04.9	04.0	04.4	07.0	03.5	04.4	06.3	04.8	05.2	97	74	85	85	NNE	2	NNW	3	W	3
2	740.2	748.2	749.0	04.0	10.4	06.7	07.0	11.2	03.1	00.9	04.7	03.6	04.8	78	39	66	61	W	3	W	3	WSW	2
3	750.5	751.9	753.1	05.2	09.1	06.0	06.6	10.2	04.3	-00.5	05.1	04.7	04.9	77	54	70	67	W	3	NNW	3	W	1
4	752.8	751.7	751.8	03.4	12.8	09.6	08.8	13.6	02.0	-03.0	04.8	05.0	06.1	82	45	68	65	SE	2	E	1	ESE	2
5	752.1	752.9	754.8	07.5	15.2	09.8	10.6	15.3	06.5	02.4	05.3	04.6	05.1	68	37	56	54	ESE	3	SE	3	SE	3
6	757.2	757.3	758.2	05.6	10.8	06.3	07.2	11.5	05.4	03.0	06.5	06.8	06.7	96	71	93	87	NNW	1	NNW	1	WSW	1
7	758.1	756.3	755.5	05.4	09.5	08.2	07.8	09.7	05.2	02.0	06.5	07.1	07.4	97	80	91	89	-	0	NNE	2	SE	2
8	753.6	753.9	755.0	05.4	04.6	05.0	05.0	08.2	04.6	05.2	06.5	06.2	06.4	97	97	97	97	NNE	2	NNE	3	NNW	1
9	755.1	755.5	756.2	04.4	05.4	05.2	05.6	04.4	04.2	05.9	05.8	06.2	94	86	92	91	NW	1	NW	2	SW	1	
10	756.0	756.0	756.0	05.1	09.8	06.8	07.1	09.8	04.4	03.2	06.2	06.2	06.3	94	68	85	82	SSE	2	SE	2	ESE	2
11	755.8	756.0	756.2	03.5	07.6	03.2	04.4	08.5	03.1	00.8	05.3	06.1	05.7	91	78	98	89	ESE	2	WSW	2	-	0
12	752.7	754.0	753.3	01.5	04.6	05.5	04.3	05.7	01.5	04.1	05.0	06.0	06.4	98	94	94	95	-	0	NNW	1	ESE	2
13	753.3	744.0	755.4	02.8	14.6	06.5	07.6	15.5	01.5	-01.3	05.3	06.2	06.8	95	50	93	79	-	0	NNW	2	SW	1
14	755.7	755.3	756.6	04.6	14.7	09.4	09.5	16.0	04.4	-00.2	06.1	07.1	06.5	96	56	74	75	SF	1	NNE	1	ESE	2
15	755.0	755.5	756.6	06.4	09.4	10.4	16.7	06.3	03.5	06.2	06.6	06.7	86	47	76	70	SE	3	ESE	2	SE	3	
16	754.7	753.3	754.0	07.3	18.4	11.4	12.1	18.4	07.3	04.8	06.1	07.6	06.6	79	48	65	64	ESE	3	SE	3	SE	3
17	756.0	756.5	756.2	06.9	15.1	10.6	10.8	16.2	06.9	00.7	06.7	06.8	07.2	95	53	75	72	-	0	NNE	1	ESE	1
18	755.5	754.5	753.4	07.1	11.8	11.8	11.8	16.8	06.6	-00.4	06.1	07.5	06.4	80	52	63	65	SE	1	-	0	ESE	2
19	750.7	747.3	751.4	08.2	17.5	10.6	11.7	17.7	06.0	04.2	05.7	06.0	06.8	70	40	72	61	ESF	3	NNW	2	-	0
20	756.3	755.7	755.7	07.1	10.4	08.9	07.6	10.8	06.0	03.1	06.4	05.2	06.5	90	55	87	77	WSW	1	ESE	2	ESE	2
21	754.2	753.9	754.3	04.9	11.1	06.5	07.4	11.1	04.5	00.4	05.7	06.7	07.0	88	68	93	83	ESE	2	-	0	W	1
22	754.6	744.1	753.9	06.0	09.6	06.1	07.0	10.1	04.4	04.4	06.4	06.8	06.6	92	76	93	87	NNW	1	NNW	1	SE	1
23	753.9	753.5	753.1	04.4	09.2	04.0	07.4	10.0	03.7	00.0	06.0	07.1	07.3	96	82	91	90	-	0	NW	1	-	0
24	753.0	753.8	754.8	07.2	07.5	03.8	05.6	08.2	03.8	05.2	06.5	05.8	06.7	86	74	79	80	ESE	2	ESF	3	SE	3
25	753.1	750.8	748.1	03.8	09.0	06.4	05.4	09.2	03.1	01.7	04.5	05.8	06.3	75	67	78	77	SE	5	SE	4	SE	4
26	746.5	748.6	746.3	07.2	C6.0	04.2	05.4	07.7	04.1	04.2	07.2	06.2	05.6	95	89	90	91	SSW	2	WSW	2	SSW	2
27	745.0	746.0	747.5	07.4	06.2	04.0	04.2	07.2	01.9	-02.0	04.7	05.0	05.8	87	70	95	84	SE	2	NW	2	WSW	2
28	739.3	736.0	731.6	02.8	10.4	01.0	03.8	11.8	01.0	-01.5	05.0	06.1	04.7	89	65	93	83	SE	2	NNW	3	-	0
29	739.4	740.7	742.1	01.2	C6.8	07.3	03.6	07.5	00.5	-00.5	04.7	04.6	04.1	95	62	71	76	SW	2	S	2	SE	2
30	747.3	749.8	752.0	00.9	07.1	02.4	03.2	07.8	00.5	-00.3	04.3	04.6	04.4	88	61	81	77	SSW	2	WSW	2	SE	2
MES.	VRED.			752.0	751.9	752.4	04.9	10.4	06.6	07.1	11.1	04.1	01.6	C5.7	06.0	06.0	88	65	82	78	1.8	2.0	1.9

## 1974 DECEMBAR

BEOGRAD

1	750.8	752.4	755.9	02.1	C8.6	06.1	05.7	08.8	01.5	-04.2	03.8	03.8	04.8	71	45	68	61	SE	2	SSW	2	NNW	2	
2	754.2	756.9	758.7	06.4	08.0	06.7	07.0	08.1	06.0	C2.6	05.2	06.1	06.6	72	76	89	79	NW	2	WSW	3	W	2	
3	749.6	750.7	750.3	06.6	08.8	08.6	08.2	08.8	06.2	05.6	07.1	07.4	07.6	97	88	91	92	W	2	WSW	2	-	0	
4	758.7	757.2	755.2	07.4	05.0	06.9	07.6	10.2	06.9	05.6	07.0	07.4	07.3	91	86	97	91	WNW	2	NW	1	ESE	1	
5	751.2	750.2	750.8	06.2	07.9	06.9	07.0	08.2	05.5	01.6	07.0	07.3	05.4	97	92	72	87	SF	2	-	0	N	2	
6	751.5	751.6	752.0	02.8	05.6	02.4	03.3	07.5	01.4	C2.2	05.4	04.6	04.0	97	67	74	79	WSW	2	W	2	SSE	1	
7	751.2	748.8	749.0	02.4	04.4	05.7	04.6	05.7	01.7	-00.9	05.1	05.9	06.5	94	94	94	94	SSW	2	WSW	3	NNW	2	
8	746.4	745.8	747.8	05.6	06.1	07.8	06.8	07.8	05.1	04.2	06.2	06.8	07.0	91	96	88	83	SSE	1	WSW	2	NNW	2	
9	752.5	753.6	755.7	02.4	04.2	02.0	02.6	07.8	01.5	01.0	04.6	04.6	04.7	84	75	88	82	N	1	NNE	1	ESE	2	
10	755.5	754.4	753.9	01.2	08.0	03.8	04.2	08.1	01.0	-02.8	04.3	05.7	04.2	86	71	70	76	SE	2	ESE	3	SÉ	3	
11	754.5	751.2	746.8	03.4	04.5	08.6	06.8	08.6	01.0	02.4	05.8	06.2	05.3	98	85	63	82	SSW	1	ESE	1	ESE	3	
12	743.9	747.1	746.8	06.9	C3.1	01.4	03.2	08.6	01.1	05.0	05.1	04.9	04.8	68	86	95	83	ESE	3	N	2	W	2	
13	742.0	742.7	745.8	01.1	01.0	01.2	01.1	02.4	01.0	00.6	04.8	04.7	04.5	97	95	90	94	WSW	2	WSW	2	W	2	
14	750.3	750.5	751.4	01.2	08.8	00.8	00.3	00.6	01.4	00.2	00.5	04.6	04.4	04.5	91	90	96	92	NW	2	NNW	3	W	2
15	750.5	750.4	750.8	-00.3	-00.3	-00.7																		

BR. ST. 173

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijeme O. 9	Oblačnost N (0-10)					Instalacija broj seti	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10•	10	07	09.0	CC.C	05.E	.	• <sup>0-12</sup> 10 <sup>15</sup> E <sub>NW</sub> 9 <sup>13</sup> 20 <sup>00</sup>	
2	8	10	01•	06	05.7	07.3	07.E	.	F <sub>w-wNW</sub> 10 <sup>13</sup> 12-14 <sup>45</sup>	
3	8	09	05	04	07.3	02.4	.	.	F <sub>WW</sub> 9 <sup>05</sup> 15 <sup>04</sup> , $\sqcup$ 23 <sup>00</sup> 24	
4	8	06	07•	06	06.3	05.1	.	.	$\sqcup$ 0-7 <sup>30</sup> F <sub>EE</sub> 6 <sup>14</sup> 14 <sup>24</sup> , 21 <sup>24</sup>	
5	8	05	07•	09	07.0	04.3	.	.	Δ <sup>0-20</sup> 7 <sup>45</sup> F <sub>EE</sub> 6 <sup>14</sup> 14 <sup>24</sup> , 21 <sup>24</sup>	
6	5	06	06	02	04.7	01.1	.	.	F <sub>SE</sub> 0-0 <sup>45</sup> $\sqcup$ 0-6 <sup>45</sup> 8 <sup>15</sup> 19 <sup>30</sup> 24, $\sqcup$ 0-2 6 <sup>45</sup> 24, $\equiv$ 0-2 6 <sup>45</sup> 10 <sup>30</sup>	
7	5	09	10	10•	09.7	CC.C	.	.	$\Delta$ 0-6 <sup>30</sup> $\sqcup$ 0-6 <sup>30</sup> 10 <sup>30</sup> 24, $\equiv$ 0-6 <sup>30</sup> 10 <sup>30</sup> 24	
8	5	10•	10•	10•	10.0	00.0	11.E	.	• <sup>0-10</sup> 24	
9	6	10	10	10	10.C	00.C	09.4	.	• <sup>0-4</sup> 45 $\equiv$ 0-4 20 24, 9 <sup>09</sup> 16 11 <sup>45</sup>	
10	7	10	07	04	07.0	CC.7	00.0	.	$\equiv$ 0-4 0-11 <sup>45</sup> 17 <sup>30</sup> 24, $\sqcup$ 21 <sup>30</sup> 24	
11	7	00	03•	10	04.3	06.5	.	.	$\equiv$ 0-10-8 <sup>45</sup> $\equiv$ 0-0-9 <sup>45</sup> F <sub>SE</sub> 1 <sup>13</sup> 24, $\equiv$ 21 <sup>30</sup> 24	
12	2	10	00	00	00	C3.3	01.6	.	$\equiv$ 0-2 <sup>30</sup> 6 <sup>30</sup> 14 <sup>45</sup> $\equiv$ 2 <sup>30</sup> 6 <sup>30</sup> 19 <sup>45</sup> , $\sqcup$ 4 <sup>45</sup> 7 <sup>45</sup> 18 <sup>30</sup> 24	
13	6	04	02	00	02.0	02.0	06.8	.	$\sqcup$ 0-8 <sup>45</sup> 22 <sup>15</sup> 24, $\equiv$ 0-5 <sup>15</sup> 19 <sup>45</sup> , $\equiv$ 6 <sup>30</sup> 7 <sup>45</sup> , $\Delta$ 19 <sup>45</sup> 23 <sup>30</sup>	
14	5	00	00	00	00.0	CC.0	08.3	.	$\sqcup$ 10 <sup>30</sup> 19 <sup>45</sup> 24, $\Delta$ 1-17 <sup>30</sup> 24	
15	6	00	00	00	00.0	CC.0	08.3	.	$\Delta$ 0-8 <sup>45</sup> 19 <sup>45</sup> 24	
16	8	00	00	00	00.0	CC.0	08.3	.	$\Delta$ 0-10-3 <sup>45</sup> 21 <sup>30</sup> 24	
17	6	05	04	00	03.0	C3.0	.	.	$\Delta$ 0-10 <sup>30</sup> 18 <sup>45</sup> 24, $\equiv$ 0-4 <sup>30</sup> 20 <sup>45</sup>	
18	5	03	03	00	02.0	C2.0	06.3	.	$\Delta$ 0-10 <sup>30</sup> 18 <sup>45</sup> 24, $\equiv$ 0-4 <sup>30</sup> 20 <sup>45</sup>	
19	8	03	05	00	10•	C6.0	02.9	.	$\Delta$ 0-19 <sup>45</sup> 24	
20	7	08	00	00	02.7	C2.7	05.7	01.8	.	
21	8	03	1C	1C	C7.7	01.7	.	.	$\Delta$ 0-10-9 <sup>45</sup> 20 <sup>15</sup> 22 <sup>30</sup> , $\sqcup$ 0-6 <sup>45</sup> 8, $\equiv$ 22 <sup>30</sup> 23 <sup>30</sup>	
22	7	09	04	00	04.3	C5.6	00.0	.	$\Delta$ 0-18 <sup>30</sup> 24	
23	5	07	10	10	05.0	00.0	.	.	$\equiv$ 0-5 <sup>30</sup> 12 <sup>45</sup> 30 <sup>00</sup> , F <sub>ESE</sub> 9 <sup>45</sup> , 12 <sup>45</sup> 22 <sup>32</sup> , F <sub>SE</sub> 22 <sup>42</sup> -24	
24	7	10	1C	08	09.3	C0.1	00.0	.	F <sub>SE</sub> 0-10 <sup>30</sup> 6 <sup>45</sup> 9 <sup>30</sup> , F <sub>SE</sub> 1 <sup>00</sup> 24, $\equiv$ 0-4 <sup>30</sup> 22 <sup>30</sup>	
25	7	04	10	10•	08.0	00.2	.	.		
26	7	1C•	10•	08	09.7	CC.C	05.7	.	F <sub>SE</sub> 0-7 <sup>30</sup> , $\equiv$ 11 <sup>45</sup> 9 <sup>45</sup> 12 <sup>45</sup> 18 <sup>00</sup>	
27	8	05	10	10	08.3	00.0	02.9	.	$\sqcup$ 1-8 <sup>30</sup> , $\equiv$ 0-14 <sup>30</sup> 18 <sup>00</sup>	
28	6	04	10	1C*	08.0	CC.4	C2.0	.	$\sqcup$ 3-8 <sup>30</sup> , F <sub>SE</sub> 8 <sup>45</sup> 7 <sup>25</sup> , 15 <sup>30</sup> 21 <sup>45</sup> , $\equiv$ 0-17 <sup>30</sup> 22 <sup>45</sup> , $\equiv$ 0-19 <sup>30</sup> 24 <sup>45</sup> , $\boxed{X}$	
29	8	08	06	05	06.3	05.8	16.0	01	* $0-20$ 24, * $0-0$ 0 <sup>30</sup> , $\boxed{X}$	
30	8	06	01	00	02.3	C2.3	06.5	.	$\sqcup$ 2 <sup>15</sup> 9 <sup>45</sup>	
MES.					06.1	05.8	05.3	05.8	96.4	63.0

BEOGRAD

1974 DECEMBAR

1	8	C9	10	07	08.7	00.7	.	.	$\sqcup$ 0-4 <sup>30</sup> 9 <sup>10</sup>	
2	7	1C•	1C	10	10.C	00.C	00.0	.	• <sup>0-5</sup> 45 10 <sup>45</sup> , 12 <sup>45</sup> 16 <sup>45</sup>	
3	6	10•	10	10	10.0	00.C	00.P	.	$\equiv$ 0-2 <sup>30</sup> 7 <sup>30</sup> , 16 <sup>30</sup> 17 <sup>30</sup> , $\equiv$ 0-15-24	
4	7	10	10	09	05.7	CC.C	CC.1	.	$\equiv$ 0-18 <sup>30</sup> 23 <sup>45</sup> , $\equiv$ 0-18 <sup>30</sup> 23 <sup>45</sup> , $\equiv$ 0-23 <sup>15</sup> 24	
5	5	04	05	10•	06.3	01.3	.	.	$\equiv$ 0-0-0, $\equiv$ 0-0 <sup>30</sup> , 10 <sup>45</sup> , 12 <sup>45</sup> , $\equiv$ 0-3 <sup>45</sup> 19 <sup>05</sup> , $\equiv$ 0-19 <sup>45</sup> 24, F <sub>N</sub> 21 <sup>45</sup> 21 <sup>50</sup>	
6	8	1C	04	05	06.3	C3.4	05.1	.	* <sup>0-2</sup> 15, $\equiv$ 3 <sup>30</sup> 6 <sup>30</sup> , F <sub>w</sub> 11 <sup>50</sup> , $\sqcup$ 20 <sup>45</sup> 24	
7	7	10	10•	10•	10.0	00.C	00.8	.	$\sqcup$ 0-0-0, $\equiv$ 0-0 <sup>30</sup> , 10 <sup>45</sup> , 12 <sup>45</sup> , $\equiv$ 0-20 <sup>45</sup> 24, F <sub>MSW</sub> 12 <sup>45</sup> 12 <sup>50</sup>	
8	6	10•	10•	10	10.C	00.C	C8.4	.	* <sup>0-1</sup> 17 <sup>45</sup> , $\equiv$ 21 <sup>45</sup> 21 <sup>45</sup> , F <sub>WW</sub> 12 <sup>45</sup> 15 <sup>05</sup> , $\equiv$ 0-16 <sup>30</sup>	
9	6	10	09	09	05.3	00.0	13.4	.	$\equiv$ 0-19 <sup>30</sup> 16 <sup>45</sup> , $\equiv$ 0-19 <sup>30</sup> 16 <sup>45</sup>	
10	7	00	00	02	00.7	07.5	.	.	$\sqcup$ 0-13 <sup>45</sup> 9 <sup>45</sup>	
11	6	10	08	09	09.0	01.4	.	.	$\equiv$ 1-2 <sup>45</sup> 3 <sup>30</sup> , 11 <sup>15</sup> 17 <sup>30</sup> , $\equiv$ 0-13 <sup>30</sup> 17 <sup>45</sup> , $\equiv$ 17 <sup>45</sup> 11 <sup>45</sup> , $\equiv$ 0-7 <sup>30</sup> 10 <sup>45</sup>	
12	7	1C	1C	10	10.C	00.C	00.C	.	$\equiv$ 0-4 <sup>5</sup> 5 <sup>15</sup> , $\equiv$ 14 <sup>30</sup> 17 <sup>30</sup> , $\equiv$ 0-20 <sup>45</sup> 24, F <sub>ESE</sub> 4 <sup>45</sup> 5 <sup>34</sup> , $\equiv$ 0-6 <sup>30</sup> 8 <sup>30</sup> , $\equiv$ 0-17 <sup>30</sup> 20 <sup>45</sup>	
13	6	10*	10	10	10.C	00.C	01.9	.	$\equiv$ 0-2 <sup>30</sup> 3 <sup>30</sup> , $\equiv$ 0-20 <sup>45</sup> 7 <sup>15</sup> , $\equiv$ 0-17 <sup>30</sup> 10 <sup>45</sup> , $\equiv$ 0-12 <sup>45</sup> 20 <sup>45</sup>	
14	6	10	1C*	1C*	10.C	00.C	00.C	.	* <sup>0-17</sup> 45, $\equiv$ 24 <sup>45</sup> , F <sub>WW</sub> 11 <sup>30</sup> 15 <sup>45</sup> , $\boxed{X}$	
15	5	1C*	10*	10*	1C.0	00.C	21.C	16	* <sup>0-10</sup> 24, $\boxed{X}$	
16	7	1C*	10	10	1C.0	00.C	22.5	26	* <sup>0-9</sup> 15, $\boxed{X}$	
17	7	00	09	10	06.3	05.3	00.4	20	* <sup>0-18</sup> 45, $\equiv$ 15 <sup>30</sup> , $\equiv$ 15 <sup>45</sup> 22 <sup>30</sup> , $\boxed{X}$	
18	6	10	10•	04	08.0	00.C	.	15	$\equiv$ 0-2 <sup>30</sup> 3 <sup>30</sup> , $\equiv$ 0-20 <sup>45</sup> 10, $\equiv$ 0-3 <sup>45</sup> 5 <sup>30</sup> , * <sup>0</sup> 9 <sup>30</sup> 11 <sup>50</sup> , $\boxed{X}$	
19	7	07	07	10	08.0	02.8	07.C	12	$\equiv$ 0-11 <sup>30</sup> 29 <sup>30</sup> , $\boxed{X}$	
20	6	10	10	05	08.3	01.1	00.0	11		
21	7	03	09	00	04.0	00.7	.	787	$\boxed{X}$	
22	7	03	00	00	01.0	C7.3	.	06	$\sqcup$ 1-2 <sup>45</sup> 9 <sup>30</sup> , $\equiv$ 0-2 <sup>30</sup> 3 <sup>30</sup> , $\equiv$ 17 <sup>45</sup> , $\equiv$ 0-2 17 <sup>45</sup> 18 <sup>45</sup> , $\equiv$ 2 18 <sup>45</sup> 24, $\boxed{X}$	
23	4	00	00	10	03.3	05.5	.	04	$\equiv$ 0-18 <sup>30</sup> 10 <sup>45</sup> , $\equiv$ 0-18 <sup>30</sup> 24, * <sup>0</sup> 13 <sup>45</sup> , $\equiv$ 0-18 <sup>30</sup> 18 <sup>45</sup> , $\equiv$ 2 18 <sup>45</sup> 24, $\boxed{X}$	
24	2	10	10	10	10.0	00.0	.	04	V <sup>0-11</sup> 15 <sup>45</sup> , $\equiv$ 0-20-24, $\boxed{X}$	
25	5	00	10	04	04.7	00.5	CC.C	04	$\equiv$ 0-6 <sup>45</sup> V <sup>0-2<sup>30</sup> 8</sup> , * <sup>0</sup> 21 <sup>45</sup> , $\boxed{X}$	
26	7	02	10	09	07.0	01.9	.	04	* <sup>0-3</sup> 45 10 <sup>45</sup> , $\boxed{X}$	
27	7	09	05	06	06.7	04.2	CC.1	02	$\boxed{X}$	
28	7	07	05	10	07.3	05.9	02.2	-	$\boxed{X}$	
29	7	10	09	00	06.3	01.3	.	.	* <sup>0-8</sup> 45 14 <sup>45</sup>	
30	7	10•	10	05	08.3	00.C	02.5	.	* <sup>0-14</sup> 45 9 <sup>00</sup> , 12 <sup>50</sup> 14 <sup>05</sup> , F <sub>WW</sub> 10 <sup>55</sup> 17 <sup>45</sup>	
31	7	10	09	00	06.3	CC.6	04.C	.		
MES.					07.5	08.0	07.2	07.6	51.8	90.2

$\varphi = 42^{\circ}26'$ ,  $N \lambda = 19^{\circ}17'$ , E Gr.  $\Delta G = +1h\ 17\ min.$ 

BR. ST. 248

E D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21		
1	761.5	760.6	761.5	07.9	09.6	09.6	09.2	09.6	07.3	05.9	07.7	08.9	08.7	96	98	98	97	-	0	-	C - C	
2	761.0	760.7	760.7	08.9	10.3	09.7	09.6	10.6	08.4	07.6	08.1	09.0	08.8	95	95	98	96	-	0	S - 2	- 0	
3	760.5	760.3	762.1	08.5	10.8	08.8	09.2	12.0	08.4	07.8	07.5	07.3	07.6	90	75	90	85	-	0	-	C NE 1	
4	763.6	763.1	765.0	07.0	09.5	05.8	08.3	15.0	05.8	05.1	07.3	09.7	06.7	97	70	97	88	-	0	SSW 1	- 0	
5	764.8	763.7	764.0	02.8	11.4	05.0	06.0	11.8	02.5	00.0	05.4	07.1	06.3	97	70	96	88	-	0	-	C - 0	
6	762.0	759.8	758.7	06.0	09.1	07.4	07.5	09.3	04.6	02.6	06.3	07.3	07.0	90	84	91	88	-	0	-	0 - 0	
7	758.9	759.6	760.9	07.2	09.1	06.7	07.4	09.5	06.1	06.2	07.4	08.1	07.3	97	94	99	97	NNE 1	-	C - 0	- 0	
8	760.9	760.3	761.2	04.2	07.9	03.6	04.8	08.0	02.9	01.0	06.0	06.7	05.7	97	63	95	92	ESE 1	-	0 - 0	- 0	
9	762.0	761.8	761.8	-00.2	09.8	02.7	03.8	10.3	-00.2	-01.9	04.3	04.5	05.1	95	50	92	79	-	0	WSW 1	- 0	
10	758.4	757.5	759.2	03.8	06.0	05.7	05.3	06.0	02.4	00.0	05.7	06.7	06.6	95	96	96	96	-	0	-	0 - 0	
11	761.3	762.7	765.7	05.5	11.2	04.4	06.4	11.3	04.0	03.6	06.5	07.3	05.7	96	73	91	87	N 1	S 2	- 0	- 0	
12	766.1	764.6	765.0	00.5	11.9	08.8	07.5	12.3	00.4	-01.5	04.7	06.5	04.3	98	62	50	70	-	0	SSW 2	NNE 3	
13	763.7	762.2	763.9	07.6	11.0	06.0	07.6	11.6	06.0	05.2	03.1	03.5	02.9	40	36	41	39	NE 4	NE 6	ENE 5	- 0	
14	764.6	763.8	764.4	03.0	10.2	01.4	04.0	10.2	01.0	-00.3	03.3	04.7	04.3	57	51	85	64	ENE 3	-	0 - 0	- 0	
15	764.9	763.9	764.1	-01.7	09.4	00.9	02.4	09.7	-02.1	-04.7	03.6	03.4	04.3	89	38	88	72	-	0	SSE 2	SSW 1	
16	764.8	763.9	763.7	-00.2	08.8	04.2	04.2	10.4	-00.8	-03.1	04.2	04.5	04.9	93	54	79	75	-	0	SW 2	- 0	
17	761.8	760.2	757.6	-00.4	04.5	04.4	03.2	05.1	-00.5	-03.0	04.1	04.8	05.9	93	77	94	88	-	0	C NNE 3	- 0	
18	758.8	758.5	759.6	07.2	10.2	02.4	05.6	10.6	02.3	03.8	04.3	03.9	04.1	57	42	74	58	N 2	ENE 5	NNF 2	- 0	
19	759.8	759.6	760.1	06.5	11.2	04.3	06.6	11.2	02.0	-02.0	03.4	04.0	04.3	47	40	69	52	NE 6	NE 5	- 0	- 0	
20	758.7	767.9	759.7	01.8	10.4	11.4	08.8	12.4	01.0	-01.6	04.5	05.3	05.8	87	56	58	67	-	0	ENE 5	- 0	
21	760.4	760.8	762.6	10.7	14.2	10.2	11.3	14.5	09.0	-01.8	04.4	04.4	03.9	45	36	42	41	NE 5	NE 6	NE 4	- 0	
22	763.7	763.2	763.7	03.5	14.5	04.9	07.0	14.6	03.0	00.0	04.7	06.2	04.7	80	50	73	68	-	0	SSW 2	- 0	
23	764.8	764.0	762.1	00.9	08.7	06.4	05.5	12.6	00.6	-02.6	04.6	06.2	06.0	95	75	84	85	-	0	S 2	- 0	
24	760.6	760.3	761.0	08.8	13.6	05.5	08.4	13.7	05.2	04.6	04.8	04.7	05.0	57	40	74	57	NE 5	ENE 6	FNE 3	- 0	
25	760.7	760.0	760.2	00.9	08.4	04.8	04.7	10.2	00.4	-02.8	03.9	04.1	05.4	79	46	84	71	-	0	S 1	- 0	
26	761.8	761.2	762.1	00.1	12.7	03.2	04.8	12.7	-00.2	-02.8	04.4	05.7	04.7	95	52	81	76	-	0	SSW 2	- 0	
27	761.8	759.9	760.1	01.4	12.4	05.6	06.3	12.7	01.0	-02.4	03.9	04.7	05.6	77	43	82	67	-	0	S 2	- 0	
28	759.9	759.7	760.8	02.8	12.8	08.0	07.9	13.4	02.5	-00.7	04.7	06.1	04.8	84	55	59	66	-	0	S 2	SSW 3	
29	761.8	761.4	762.8	01.9	13.9	03.6	05.7	13.9	01.0	-02.3	04.2	05.9	05.1	80	50	86	72	-	0	SW 2	- 0	
30	764.8	764.3	765.6	01.8	14.3	03.8	05.9	14.3	01.2	-02.0	04.4	06.3	05.1	85	51	85	74	-	0	SW 2	- 0	
31	766.9	766.5	766.7	03.0	12.4	03.6	05.6	12.8	01.9	-01.8	04.4	04.7	05.0	78	44	85	69	-	0	WSW 1	- 0	
MES.	VRED.	762.1	761.8	762.1	03.9	10.8	05.6	06.5	11.4	02.8	00.5	05.0	05.0	05.5	83	61	81	75	0.9	1.8	1.0	

1	765.8	765.0	764.3	05.4	11.0	08.0	08.1	13.1	03.0	-00.7	05.3	06.2	04.6	79	66	82	76	-	0	SW 2	- 0
2	764.7	764.8	764.1	06.0	10.4	07.8	08.0	11.0	03.5	01.0	06.0	07.3	06.7	86	77	85	83	-	0	-	C - 0
3	763.6	762.1	760.0	06.7	09.6	08.2	08.2	11.2	05.6	03.0	06.7	08.2	08.1	91	90	99	93	-	0	-	C E 2
4	756.1	754.0	753.1	08.2	12.2	07.8	09.0	13.6	07.5	01.5	07.4	06.2	06.4	91	58	81	77	SSE 5	S 5	- 0	- 0
5	754.3	753.0	751.5	05.5	09.8	07.1	07.4	10.5	05.5	04.3	06.2	06.3	06.9	92	70	91	84	-	0	WSW 2	- 0
6	749.5	747.9	747.7	06.9	09.0	10.2	09.0	10.6	06.5	00.8	07.2	08.2	08.4	97	94	90	94	-	0	-	C S 6
7	736.0	738.0	741.7	09.5	09.2	05.6	07.5	12.0	05.0	03.0	07.8	07.6	06.4	87	87	94	89	NW 2	W 2	- 0	- 0
8	747.0	752.2	757.4	04.4	09.3	06.4	06.6	10.7	02.5	00.1	03.4	02.8	02.2	54	32	31	39	N 2	NE 6	NE 3	- 0
9	761.4	761.9	763.7	02.4	11.6	04.8	05.9	12.2	02.1	-01.8	03.8	04.4	04.2	70	43	66	60	NE 6	S 3	- 0	- 0
10	763.4	762.0	762.3	02.2	12.2	04.6	06.0	13.5	01.6	-01.5	03.7	04.9	05.2	70	46	81	66	-	0	SSE 4	- 0
11	761.5	759.5	758.8	02.4	13.8	05.0	06.6	14.0	02.2	-01.1	04.7	05.1	05.9	87	43	90	73	E 1	SSW 3	- 0	- 0
12	757.5	755.0	754.1	02.3	14.7	06.9	07.7	15.1	02.2	-00.7	05.1	07.1	05.7	93	57	76	75	E 1	SS 2	- 0	- 0
13	752.4	751.2	750.3	06.6	10.4	08.6	08.6	10.6	04.2	01.2	06.3	07.5	07.4	86	79	89	85	-	0	-	NF 2
14	748.6	751.4	751.2	07.6	08.4	08.0	08.1	10.3	07.4	06.2	07.2	06.6	07.0	92	78	87	86	ENE 2	NNE 2	NF 4	- 0
15	751.0	750.3	750.9	08.0	15.7	09.2	10.5	16.4	07.5	05.9	07.6	08.9	08.3	95	67	95	86	N 3	S 1		

RR. ST. 248

$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijednost O	Oblačnost N (0-10)					Insolascija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	10	10	10	10	10.0	00.C	05.5	.	$\bullet^{0-1} 14^{35} n$	
2	7	10•	10•	10	10	10.0	00.C	03.8	.	$\bullet^0 n-19^{25} s$	
3	8	10	10	10	10	10.0	00.4	04.8	.	$\bullet^0 n-51 s 14-20$	
4	8	10	020	00	00	04.0	05.6	03.5	.	$\Delta^{19^{35}} 24$	
5	8	00	06	02	02	02.7	03.5	.	.	$\Delta^{10-21} 18^{45} n$	
6	8	10	10	10	10	10.0	00.C	00.4	.	$\bullet^0 5-6 14^{20} 20^{30} l$	
7	7	10•	10•	08	08	09.3	00.C	02.8	.	$\bullet^0 02-20 l 10^{30} 14-50$	$\equiv 17^{45} n$
8	7	10	10	00	00	06.7	00.C	00.7	.	$\equiv 2n-545$	
9	8	04	04	04	04	05.3	04.5	.	.	$\Delta^{10-30} \equiv 2n-8^{30} \Delta^{19^{30} n}$	
10	6	10•	10•	10	10	10.0	00.C	01.2	.	$\bullet^0 n-18 l 20^{20} 23$	
11	8	10	040	00	00	04.7	03.2	17.4	.	$\bullet^0 2^{35} 4^{30} \Delta^{115} n$	
12	8	02	030	00	00	01.7	06.3	.	.	$\Delta^{2n-8^{20}} F_{NNE} 21^{35} 24 l$	
13	8	00	020	00	00	00.7	08.3	.	.	$F_{NNE} 0-0^{30} l$	
14	8	00	010	00	00	00.3	07.7	.	.	$F_{NEC} 2^{20} l$	
15	8	05	000	00	00	01.7	07.6	.	.	$\Delta^{2n-9} \Delta^{115-17} n$	
16	8	10	10	00	00	06.7	02.2	.	.	$\Delta^{2n-8^{30}}$	
17	7	03	10	10•	10	07.7	00.C	.	.	$\bullet^{16-2150} \Delta^{17-9} F_{NE} 22-23^{30}$	
18	8	02	040	02	02	07.7	07.8	06.3	.	$F_{NNE} 0^{35} 15 l$	
19	8	02	030	01	00	02.0	08.6	.	.	$F_{NE} 4^{30} 14^{30} l$	
20	8	08	070	02	02	05.7	03.7	.	.	$F_{NE} 20^{15} 20^{30} l$	
21	8	02	020	00	00	01.3	08.6	.	.	$F_{NNE}-NF-ENE 112-3^{30} 9^{30} 24 l$	
22	8	C1	000	00	00	00.3	08.8	.	.	$F_{N-NE} 0-2^{40} l$	
23	8	C1	05	10•	10	06.7	04.0	.	.	$\Delta^{2n-45} \Delta^{20^{40} 20^{30}}$	
24	8	04	01	00	00	01.7	08.4	00.6	.	$\bullet^{0225-320} F_{NNF-NE} 3^{30} 6^{42} 8^{34} 13^{38}$	
25	8	07	07	10	10	08.0	04.7	.	.	$\Delta^{1n-730}$	
26	8	00	000	00	00	00.0	08.6	.	.	$\Delta^{1n-8^{30}}$	
27	8	C7	C30	10	00	06.7	07.9	.	.	$\Delta^{1n-8^{30}}$	
28	8	C3	070	00	00	03.3	07.6	.	.	$\Delta^{2n-8^{20}}$	
29	8	00	000	00	00	00.0	08.1	.	.	$\Delta^{1n-8^{10}}$	
30	8	01	060	00	00	02.3	08.6	.	.	$\Delta^{1n-8^{30}}$	
31	8	08	070	00	00	05.0	07.1	.	.	$\Delta^{1n-8}$	
MES.	VRED.	05.2	05.5	03.5	04.7	154.2	47.0				

## TITOGRAD

1974 FEBRUS

1	8	08	060	09	07.7	03.1	.	.	$\bullet^{0-1} 12^{30} 13$		
2	8	10	10	10	10.0	00.5	.	.	$\bullet^{0-1} 12^{30} 24$		
3	7	10	10•	10•	10.0	00.C	00.1	.	$\bullet^{0-10} 15^{30} n F_{SSSE-S} 3^{30} 6^{35} 8^{40} 12; 8^{30} 6^{40} 15; 6^{30} 8^{30} 18^{35} 19^{30}; F_{SW} 6^{35} 6^{45}$		
4	8	10•	R	08	10•	09.3	00.0	17.2	.	$\bullet^{0-10} 16^{30} 14-15$	
5	8	10	10	10	10.0	01.5	34.6	.			
6	7	10•	10	10•	10.0	00.C	02.7	.	$\bullet^{0-15} 035 l 13^{35} 24 F_{E} 17^{45} 24$		
7	7	10•	10	08	09.3	00.C	52.6	.	$\bullet^{0-10} 10^{30} 14^{40} F_{SSW-N} 0-8^{30} l 14^{30} 16^{40} F_{SSW} 2-2^{30}$		
8	8	10	070	00	05.7	05.5	10.5	.	$E_{N} 10^{35} 16^{35} l$		
9	8	00	01	00	00	00.3	09.5	.	$F_{NE} 4^{05} 4^{15} l$		
10	8	04	000	00	01.3	09.5	.	.	$\Delta^{0n-710}$		
11	8	00	000	00	00.0	09.5	.	.	$\Delta^{0n-730}$		
12	8	02	000	00	00.7	09.8	.	.	$\Delta^{0n-740}$		
13	8	10•	10	10•	10.0	00.3	.	.	$\bullet^{0-625} 7^{30} 12^{40} 13^{30} 16^{35} 24 l$		
14	8	10	10	07	05.0	00.4	07.5	.	$\bullet^{0-640} 17-15 l 14^{32} 19^{30} F_{N} 12^{35} 12^{30}$		
15	8	10•	080	00	06.0	03.9	08.7	.	$\bullet^{0-12} 1725$		
16	8	04	03	07	04.7	09.5	01.4	.			
17	8	04	040	05	04.3	08.7	.	.			
18	8	08	10	10	05.3	01.9	.	.			
19	8	10	06	10	05.3	03.7	07.5	.	$\bullet^{13-5} 50 F_{S-SSW} 10^{05} 15^{34} l$		
20	8	09	08	03	06.7	05.0	.	.			
21	8	05	09	08	07.3	06.4	.	.	$F_{ENE} 0^{05} 2^{38} l \bullet^{0-810} 9^{35} 16^{50} 23^{50} l$		
22	8	10	10	10•	10.0	00.C	.	.	$F_{NE} 22^{30} 24 l$		
23	8	10	070	07	06.0	03.2	08.3	.	$F_{NE} 0-6^{30} F_{NE} 6^{30} 24$		
24	8	C5	080	03	05.3	06.6	.	.	$F_{NE} 0-17 F_{NE} 17-24$		
25	8	08	050	07	06.7	04.8	.	.			
26	8	08	070	10	08.3	03.6	.	.	$F_{NE} 0-6$		
27	8	02	00	00	00.7	09.7	.	.	$F_{NE} 3^{25} 10^{35} l$		
28	8	00	030	00	01.0	09.7	.	.	$F_{NE} 2^{50} 3^{50}$		
MES.	VRED.	07.0	06.5	05.8	06.5	126.9	151.5				

$\varphi = 42^{\circ}26'$ , N  $\lambda = 19^{\circ}17'$  E Gr.  $\Delta G = +1h\ 17\ min.$ 

RR. ST. 248

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	758.6	756.8	756.2	01.6	12.2	05.2	06.0	13.7	01.4	-02.0	04.1	04.3	04.6	80	40	72	64	-	0	NW 3	-	0		
2	755.6	754.0	753.5	01.0	11.0	07.6	07.2	12.1	01.1	-02.8	04.4	05.9	07.4	85	56	95	79	-	0	SW 1	-	0		
3	756.0	758.2	760.3	06.2	13.0	07.0	08.3	13.4	06.0	-00.8	06.8	05.5	06.5	96	49	87	77	-	0	S 2	-	0		
4	761.5	750.3	760.8	05.6	11.3	07.6	08.0	11.5	05.0	02.0	06.1	07.0	07.6	89	70	97	85	-	0	-	0	-	0	
5	757.7	755.3	752.9	07.8	09.8	09.1	09.0	10.0	07.5	06.0	07.6	08.4	08.3	96	95	96	96	-	0	NNW 1	NNW 2	-	0	
6	752.6	753.3	753.8	07.8	09.3	08.0	08.4	10.7	07.5	01.5	07.1	07.6	07.6	90	83	94	89	-	0	-	0	NNE 2	-	0
7	754.8	755.2	757.1	06.0	10.3	07.4	07.8	11.5	05.9	05.2	06.2	05.9	03.5	89	62	45	65	-	0	SW 2	NE 4	-	0	
8	757.0	758.0	759.0	06.0	06.8	04.6	05.5	04.6	04.5	04.4	04.8	06.0	06.0	69	81	94	81	-	0	S 3	NN 1	-	0	
9	759.2	760.2	760.9	04.4	08.0	06.0	06.1	08.3	04.0	03.5	04.3	06.0	06.5	93	75	93	87	N	1	N 2	2	-	0	
10	759.8	757.9	759.4	03.8	14.5	08.4	08.8	15.0	01.5	-00.6	05.3	05.0	05.7	88	40	63	66	N	7	SW 3	-	0		
11	760.8	760.8	762.6	03.2	14.5	10.2	09.1	15.0	02.3	-00.5	05.3	05.0	05.0	92	48	51	58	-	0	SW 4	13	-	0	
12	763.3	762.4	762.4	08.2	14.0	04.4	08.0	16.2	04.2	00.0	03.0	03.4	03.0	88	45	81	81	3	3	3	3	-	0	
13	760.5	756.0	754.1	02.4	14.8	06.2	07.4	15.3	01.6	-01.4	05.0	05.1	05.6	92	40	78	70	-	0	SW 2	-	0		
14	750.8	746.5	746.0	03.8	18.0	13.4	12.2	18.4	03.0	-00.2	05.1	04.5	04.0	85	42	35	54	-	0	S 5	2	-	0	
15	745.2	745.8	748.0	10.0	12.0	09.8	10.4	14.8	05.8	08.5	04.0	04.2	04.1	44	40	46	43	N	4	NE 5	5	-	0	
16	749.5	749.6	751.0	08.6	14.0	10.1	10.7	14.6	06.5	06.6	05.1	04.4	07.2	51	52	78	66	NNE 2	55W 4	-	0			
17	753.2	754.1	756.9	06.8	16.4	05.4	10.5	16.6	04.5	00.7	02.3	07.1	08.2	85	51	93	76	N	3	S 5	4	-	0	
18	759.3	759.6	760.6	06.2	18.2	10.4	11.3	18.9	05.2	01.7	06.5	06.2	06.8	92	40	72	69	-	0	S 4	6	-	0	
19	761.9	761.7	762.0	08.0	19.7	10.9	12.3	20.2	06.5	02.0	06.3	09.3	08.4	78	56	67	73	ESE 2	53	3	-	0		
20	763.1	761.9	762.2	07.9	22.0	11.7	13.3	22.5	05.4	01.2	06.4	08.4	07.7	90	42	75	66	-	0	S 3	3	-	0	
21	762.5	760.0	760.7	07.8	24.8	12.6	14.4	25.0	05.4	00.9	06.0	06.6	05.7	76	28	51	52	-	0	S 2	-	0		
22	760.5	758.8	759.0	10.0	25.0	15.6	16.9	26.0	07.6	02.7	06.6	07.5	09.0	72	70	67	56	-	0	SW 2	-	0		
23	759.5	758.5	759.6	10.2	23.1	13.3	15.0	23.4	09.2	04.9	08.1	08.7	09.5	97	41	83	70	-	0	SSW 2	-	0		
24	760.2	758.7	758.5	09.4	23.6	15.8	16.2	24.0	07.3	03.3	07.8	07.2	08.6	88	34	64	62	-	0	S 5	2	-	0	
25	759.0	758.6	758.3	11.0	20.6	14.2	15.2	22.5	10.1	05.5	08.4	08.7	08.9	80	48	74	67	-	0	-	0	-	0	
26	759.0	756.6	756.7	14.0	22.8	14.6	16.5	23.2	11.4	05.9	07.4	09.4	09.6	62	45	77	61	N	4	55W 4	-	0		
27	755.9	754.3	754.5	11.6	21.0	14.6	15.4	21.3	10.0	06.3	04.7	09.5	09.2	94	51	74	73	-	0	NNW 3	-	0		
28	756.0	755.0	757.1	10.8	21.8	15.2	15.8	22.0	08.7	04.0	05.1	06.9	09.3	94	45	72	67	-	0	SW 3	-	0		
29	758.8	757.6	756.6	12.2	22.3	15.4	16.5	23.0	09.7	04.4	06.2	09.0	09.5	77	45	70	64	-	0	SW 4	-	0		
30	760.0	758.5	759.2	13.8	20.8	15.4	16.4	21.5	12.3	08.0	07.8	08.6	08.3	56	47	64	59	E 1	2	S 1	-	0		
31	758.7	756.2	756.0	12.0	16.2	12.6	13.4	17.4	10.0	06.0	09.2	09.1	10.1	88	66	82	82	-	0	SW 3	3	-	0	
MES.	VRED.	757.7	756.8	757.3	07.6	16.6	10.6	11.4	17.3	06.4	02.8	06.4	07.0	07.2	81	51	75	69	0.7	2.4	1.0	-	-	0

1974 APRIL

TITOGRAD

1	754.3	753.3	754.5	10.7	19.0	14.6	14.7	20.4	10.3	05.7	08.5	08.0	08.5	88	48	68	68	-	0	NN 2	13	-	0
2	756.1	757.2	756.3	12.8	18.4	13.6	14.6	19.4	12.0	10.0	08.8	08.4	09.2	80	53	73	71	NE 2	S 1	NE 1	-	0	
3	759.8	759.2	759.3	12.3	18.6	13.4	14.4	20.2	12.0	08.5	08.1	07.2	09.7	75	45	94	66	-	0	SW 4	4	-	0
4	757.9	756.0	756.4	13.3	19.4	12.3	14.3	20.0	10.3	05.7	08.0	08.0	08.3	53	53	77	61	NNE 3	S 5	6	-	0	
5	756.4	756.8	760.0	10.0	17.4	12.2	13.0	17.8	05.5	05.5	08.3	06.6	08.7	90	45	81	72	N	3	S 6	-	0	
6	754.7	753.1	754.6	10.4	18.0	14.4	14.3	20.0	07.0	03.0	04.8	04.3	07.0	72	41	51	57	N	1	SW 1	-	0	
7	755.9	754.3	755.5	13.6	19.4	16.0	16.4	21.2	17.1	04.8	05.5	06.3	05.3	47	36	34	41	NE 4	NE 5	4	-	0	
8	754.3	754.0	754.7	10.8	18.0	12.6	13.6	19.5	05.8	03.0	06.0	05.9	04.7	63	37	43	48	-	0	NE 4	5	-	0
9	756.3	756.0	757.1	11.4	19.0	14.4	14.8	19.4	08.6	03.0	05.1	05.2	04.8	53	31	39	41	NE 2	NE 4	4	-	0	
10	759.1	755.7	755.5	11.8	18.8	12.3	13.8	19.3	08.0	02.1	06.0	06.4	08.5	58	39	72	59	-	0	SSW 4	-	0	-
11	751.7	751.0	750.0	10.8	13.4	12.3	12.2	15.2	10.8	06.2	08.9	08.6	08.3	92	75	77	81	-	0	S 1	NN 2	-	0
12	749.5	750.1	750.1	11.5	12.0	11.9	11.8	13.7	11.0	09.5	08.9	09.6	09.4	88	91	90	90	ENE 1	-	0	EE 1	-	0
13	751.2	751.8	750.7	11.2	15.7	13.6	13.5	18.2	08.9	05.6	09.7	11.4	10.2	98	85	87	90	-	0	SSW 4	NNE 2	-	0
14	745.8	743.8	744.7	12.6	12.4	10.6	11.6	19.8	10.5	08.0	09.7	09.1	09.4	85	84	98	91	-	0	W 4	5	-	0
15	743.																						

BR. ST. 248

$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijeme G-9	Oblačnost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8 04	020	00	02.0	09.8	.	.	✓ 0-8			
2	8 040	020	10	07.2	04.7	.	.	✓ 2-8 25	• 17 24		
3	8 080	040	05	05.7	07.7	06.2	.	• 0-4 20 25	✓ 21 50		
4	8 10	10	10	10.0	10.0	00.0	.	• 14 55	24		
5	8 100	100	100	10.0	00.0	14.7	.	• 0-0	24		
6	8 100	10	100	10.0	00.0	28.7	.	• 0-0 20	14 40 24		
7	8 10	10	10	10.0	00.1	08.2	.	• 0-0	5		
8	8 10	10	10	10.0	10.0	00.0	.	• 15 24			
9	8 100	00	07	05.7	00.0	06.8	.	• 0-11 25			
10	8 10	060	04	06.7	06.6	03.8	.	✓ 2-0 9			
11	8 01	000	00	00.3	10.7	.	.	✓ 1-2 0-9	FENE 18 40 21 00		
12	8 BBD	BBD	BB	BB	BB	.	.	✓ 0-0	750		
13	8 000	000	00	00.0	10.7	.	.	✓ 0-0-9			
14	8 10	080	00	06.0	06.0	06.8	.	•	FNE 18 05 24		
15	8 10	10	10	10.0	10.0	00.0	.	•	FENE 0-24		
16	8 10	05	05	06.7	06.0	.	.	•	FNE 0-2 24		
17	8 000	000	00	00.0	10.2	.	.	•	✓ 1-2 0-9		
18	8 040	000	00	01.3	10.4	.	.	✓ 1-2 0-9			
19	8 01	000	00	00.3	10.9	.	.	✓ 0-0-9			
20	8 060	060	00	04.0	09.3	.	.	✓ 0-0-8			
21	8 030	050	00	02.7	11.3	.	.	✓ 0-0-9			
22	8 000	000	00	00.0	10.5	.	.	✓ 0-0-9			
23	8 020	040	00	02.0	09.5	.	.	✓ 0-0-9			
24	8 000	000	02	00.7	10.7	.	.	✓ 0-0-9			
25	8 06	10	00	05.3	02.7	.	.	✓ 0-0-9			
26	8 040	070	06	05.7	09.0	.	.	•			
27	8 06	030	02	03.7	06.1	.	.	•			
28	8 000	030	00	01.0	10.7	.	.	•			
29	8 000	060	02	04.7	10.2	.	.	•			
30	8 10	10	08	09.3	01.6	.	.	•	• 10 40 15 30		
31	8 10	10	10	10.0	01.0	.	.	•			
MES.		05.4	05.1	04.1	04.0	200.7	68.0				
VRFD.											

## TITOGRAĐ

1974 APRIL

1	8 06	08	07	07.0	02.3	00.5	.	✓ 0-0-9	• 0-14 55 15 10			
2	8 10	080	10	09.3	02.2	00.0	.	• 0-7 10 8 50 15 50 15 50	FNE 15 35			
3	8 10	08	06	08.0	03.5	00.6	.	• 0-14 50 15 30				
4	8 07	060	04	05.7	09.0	00.3	.	✓ 0-0-8	FSE 17 50			
5	8 10	090	02	07.0	02.4	03.8	.	• 0-3 15 15 15	FNE 5 15			
6	8 07	10	10	09.0	05.4	.	.	✓ 0-0-8				
7	8 00	06	05	03.7	09.3	.	.	•	FNE 10-10 40			
8	8 030	030	00	02.0	06.4	.	.	•	FNE 10-24 30			
9	8 06	010	00	02.3	11.2	.	.	•	FNE 8 30 17 25			
10	8 020	10	10	07.3	07.0	.	.	•				
11	7 100	10	09	09.7	00.0	00.6	.	•	• 0-2 0-24 10 55			
12	7 10	100	10	10.0	00.0	00.4	.	•	• 0-19 50 19 40 21-24			
13	8 030	10	09	07.3	03.6	13.4	.	•	• 0-0-30 14 20 15 40			
14	7 09	100	100	09.7	02.2	01.2	.	•	• 0-2 30 14 20 17 30 18 10 18 10 13 25 FSE 13 05 13 10 10 22 FNE SE 13 10 14 20 18 45 14 45			
15	8 10	10	10	10.0	10.0	05.1	10.7	.	•	• 0-3 20 16 16 14 20 24		
16	7 100	100	10	10.0	00.0	16.6	.	•	• 0-2 0-24 L FNE 18 40 18 50 23 05 23 44			
17	7 100	100	10	10.0	00.1	42.0	.	•	• 0-16 45 14 20 15 50 15 50 15 45			
18	7 100	100	10	10.0	01.0	24.3	.	•	• 0-10-19 40			
19	8 020	10	03	05.0	08.2	06.2	.	•	FNE 5-23 45			
20	8 000	010	00	00.3	12.4	.	.	•	✓ 20-24			
21	8 060	030	00	03.0	11.4	.	.	•	• 0-0-5 30			
22	8 10	08	00	06.0	03.4	.	.	•	FNE 14 25 14 35 FNE 14 35 14 35	✓ 20-24		
23	8 000	010	00	00.3	10.7	.	.	•	✓ 0-0-7 30			
24	8 020	040	07	04.3	09.8	.	.	•	✓ 0-0-8 30			
25	7 10	100	100	10.0	00.0	.	.	•	• 0-13 20-24			
26	7 040	070	00	03.7	05.3	06.8	.	•	• 0-0-5 20 10 35 12 05 FSE 15 24			
27	8 040	060	06	05.3	09.5	01.6	.	•	✓ 0-0-8 30			
28	8 10	10	10	10.0	00.0	.	.	•				
29	8 050	02	00	02.3	10.3	21.5	.	•	• 2 2 05 6 35 FSE 9 05 13 40			
30	8 060	10	100	08.7	05.2	.	.	•	• 14-16 40 20 30 22 20 19 30 24 1 FSE 21-24 52			
MES.		06.4	07.4	05.0	06.6	159.3	150.5					
VRFD.												

$\varphi = 42^{\circ}26'$ ,  $N \lambda = 19^{\circ}17'$ , E Gr.  $\Delta G = +1h\ 17\ min.$ 

RR. ST. 248

D e n	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost v %				Pravac i jačina vjetra D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	741.6	741.3	742.1	11.0	11.2	10.6	10.8	17.4	10.3	09.3	09.3	09.7	08.9	94	98	93	95	S	7	7	5
2	745.6	748.0	749.5	11.2	11.0	13.0	13.0	15.4	10.0	09.5	08.9	09.6	10.0	90	75	89	85	-	0	0	0
3	752.6	753.8	754.8	12.4	17.4	13.9	14.4	17.6	12.0	11.2	09.7	09.0	07.2	90	61	60	70	-	0	SSW	3
4	753.7	753.0	750.7	13.0	12.6	12.2	12.5	14.5	11.0	07.8	08.2	09.5	09.8	73	87	92	84	NW	1	SSF	6
5	750.7	751.0	750.9	12.0	15.4	12.2	13.0	16.3	10.5	09.0	09.7	09.3	08.8	92	71	92	85	-	0	N	1
6	752.7	754.0	755.5	10.4	17.6	13.4	13.7	18.1	09.9	08.6	08.9	09.1	09.9	94	60	86	80	NE	1	SSW	4
7	757.7	758.6	759.3	12.0	16.7	14.5	14.5	18.5	11.0	10.6	09.6	10.0	10.0	91	79	81	84	-	0	S	3
8	758.8	756.4	755.1	13.2	19.4	12.0	14.2	19.5	11.5	10.8	09.9	08.5	10.0	87	50	95	77	-	0	SSW	3
9	754.0	752.7	753.5	11.6	16.8	13.6	13.9	18.2	10.4	09.7	08.4	09.6	07.4	82	67	63	71	-	0	S	4
10	754.3	754.2	756.2	15.2	20.1	13.4	15.5	21.3	13.2	10.8	06.8	08.2	08.6	53	46	75	58	N	5	SSE	4
11	758.0	757.6	758.6	14.4	21.6	14.0	16.0	22.2	06.3	05.5	06.6	06.9	05.3	70	36	77	61	-	0	0	0
12	758.9	758.0	760.5	15.4	22.8	15.8	17.4	23.0	10.7	07.0	08.8	07.6	08.6	67	36	64	56	-	0	SSE	4
13	760.8	760.2	761.1	15.4	22.2	17.2	18.0	23.7	10.1	07.5	08.8	10.7	12.0	67	53	81	67	-	0	SSE	2
14	761.0	758.8	758.5	16.9	24.2	18.2	19.4	24.7	11.5	08.3	08.1	10.9	11.2	57	48	71	59	-	0	S	4
15	757.3	754.1	752.1	13.8	17.6	12.3	13.0	18.0	11.4	12.6	11.0	10.9	07.0	93	94	65	84	N	1	NNW	1
16	753.8	754.0	755.6	14.7	16.4	14.8	15.2	19.3	10.5	06.9	07.9	10.0	09.7	63	72	77	71	-	0	NNW	2
17	757.2	757.0	758.9	13.8	21.2	14.0	15.8	21.3	05.5	06.5	08.4	08.4	11.2	71	44	94	70	-	0	S	4
18	759.0	756.6	757.7	14.7	21.8	16.6	17.4	22.8	10.8	08.0	07.5	06.8	06.6	60	35	46	47	NNW	3	NNE	6
19	756.3	755.4	756.6	17.5	23.4	19.0	19.7	24.0	15.2	09.4	08.9	09.1	07.7	59	42	53	51	N	7	N	4
20	756.8	755.2	756.6	20.2	25.7	20.6	21.8	28.2	15.2	10.3	09.0	08.8	07.8	51	35	43	43	-	0	NNE	2
21	756.2	755.6	756.8	20.1	19.6	18.6	19.2	27.4	17.0	14.5	09.6	13.2	12.1	54	77	75	69	SF	3	ESE	3
22	757.0	754.4	751.5	12.6	25.6	19.8	21.2	26.0	17.2	13.0	10.4	10.5	10.8	61	42	62	55	NN	2	SSW	3
23	749.0	749.1	748.5	11.0	19.0	15.6	15.3	21.4	10.5	09.3	08.3	10.8	11.1	84	65	83	77	NE	6	SSW	4
24	749.1	750.8	752.4	14.8	18.4	17.0	16.8	20.0	13.4	12.9	09.7	11.1	11.8	77	70	81	76	-	0	SW	3
25	754.8	756.1	757.3	15.5	16.8	16.5	16.3	19.2	14.5	14.0	12.1	13.2	13.4	92	92	95	93	S	2	-	0
26	758.0	757.6	757.7	17.2	25.0	17.6	19.4	25.3	13.5	11.5	10.4	07.8	09.4	71	33	62	55	-	0	SW	3
27	757.0	755.6	755.0	16.8	25.2	18.4	19.7	25.8	11.9	09.1	08.1	07.7	11.1	57	32	70	53	FNE	3	SSW	4
28	754.7	752.3	751.8	17.8	25.4	18.3	20.0	25.8	12.5	10.0	10.3	10.0	09.7	68	45	62	58	NE	2	S	4
29	751.7	752.5	753.6	15.6	19.6	14.4	16.0	20.3	14.0	09.5	10.4	12.1	11.3	78	71	92	80	NNE	4	ENE	2
30	756.5	756.5	758.0	16.8	25.8	18.6	20.0	26.1	11.5	09.8	10.6	10.1	12.9	74	41	80	65	-	0	SW	3
31	759.3	759.3	759.7	19.6	26.7	21.6	22.4	27.0	15.5	12.5	12.0	13.7	14.6	70	52	75	66	NNE	3	SW	3
MES.	VRF.D.	755.6	754.6	754.9	15.0	20.0	16.7	16.6	21.6	12.1	09.8	09.3	09.8	10.1	74	58	75	69	1.5	3.2	1.2

1	758.0	756.4	756.1	18.0	26.8	21.8	22.1	26.8	16.3	14.5	13.2	14.1	10.7	85	53	55	64	-	0	SW	3	SSE	2
2	756.6	757.2	758.8	21.6	24.6	19.8	21.4	25.8	16.3	13.2	10.8	05.3	07.1	56	40	41	46	NNE	3	NNE	7	NNE	3
3	758.7	759.7	759.1	19.3	21.4	19.4	19.9	22.5	18.5	15.5	08.0	07.8	08.7	47	41	51	46	NNF	5	NE	7	KNE	5
4	759.4	758.3	758.1	19.6	27.2	20.8	22.1	28.2	15.2	10.4	10.8	12.1	12.6	63	45	63	59	-	0	SSW	3	-	0
5	759.0	758.0	757.3	21.4	29.7	22.8	24.2	30.1	20.6	12.5	11.5	12.7	13.1	60	41	63	55	NE	2	S	3	NH	1
6	757.4	756.3	755.9	22.2	27.3	21.8	23.3	29.1	16.6	12.5	12.7	12.3	11.2	63	45	57	55	NNE	2	SW	2	SSE	2
7	754.9	755.4	755.4	20.0	22.8	19.3	20.4	24.5	17.7	13.5	13.0	14.9	14.2	74	72	85	77	-	0	NE	3	-	0
8	758.3	757.0	755.6	19.8	27.2	20.6	22.0	27.6	17.8	14.0	07.8	08.9	11.5	45	33	63	47	NE	5	SW	3	NE	2
9	755.9	754.5	754.5	20.7	27.9	21.6	23.0	28.3	16.4	12.3	11.6	10.7	10.8	62	38	56	52	NNE	2	SW	5	SSW	4
10	754.4	753.8	752.7	22.4	25.2	20.6	22.2	26.4	15.5	13.0	09.4	11.0	10.0	46	46	55	49	SSE	5	SSE	7	KSW	1
11	747.9	749.8	752.1	20.2	18.8	14.6	17.2	22.1	14.5	14.5	13.2	12.0	06.8	74	74	54	67	SSW	5	FNE	3	NE	1
12	753.3	751.4	751.8	16.7	21.6	13.6	16.4	22.7	05.6	07.0	07.5	07.9	09.4	52	41	80	58	N	2	S	4	NE	3
13	752.0	751.8	752.3	12.4	17.8	13.6	14.4	18.5	11.7	10.0	09.8	08.8	08.8	91	58	75	75	-	0	SW	3	NE	2
14	753.5	754.1	755.8	14.6	21.6	17.2	17.6	22.5	10.2	07.1	08.4	08.2	08.2	67	42	55	55	NNE	2	SSW	2	S	2
15	758.4	757.0	757.4	16.2	25.0	16.6	18.8	26.0	10.8	07.4	09.1	10.5	13.9	66	44	96	69	-	0	SW	4	-	0

BR. ST. 248

 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Den	Vrijnost C-g	Obločnost N (0-10)					Intensitet broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	10•	10•	10•	10•	10.0	00.0	23.6	.	• 0-10-23 <sup>30</sup> ; R 14 <sup>5</sup> 6 <sup>20</sup> F <sub>s</sub> 2 <sup>30</sup> 13 <sup>40</sup> ; 15-18 <sup>30</sup> ; F <sub>s</sub> 13 <sup>30</sup> 15
2	8	10•	10	10•	10•	10.0	00.0	31.0	.	• 0-6 <sup>35</sup> 10 <sup>30</sup> 16 <sup>05</sup> 17 <sup>40</sup> 20 <sup>30</sup> 23
3	8	10	10	10	10•	10.0	00.5	C3.0	.	• 0-15 <sup>30</sup> 6 <sup>20</sup> 16 <sup>05</sup>
4	8	10	10•	10•	10•	10.0	00.0	.	.	• 0-19 <sup>30</sup> 23 <sup>30</sup> ; F <sub>s</sub> 12 <sup>30</sup> 20 <sup>40</sup> ; R 6 19 <sup>35</sup> 19 <sup>55</sup>
5	8	09	10	07	08.7	08.7	02.0	19.4	.	F <sub>s</sub> 9 <sup>30</sup> 10 <sup>35</sup> ; • 0-10 <sup>30</sup> 14 <sup>30</sup> ; 22 <sup>30</sup> 23 <sup>40</sup>
6	8	10•	08	08	08.7	08.7	04.9	18.4	.	• 12-8 <sup>30</sup> ;
7	8	09	09	10•	C5.3	04.2	02.7	.	.	• 0-19 <sup>30</sup> 22 <sup>30</sup>
8	8	07•	10	10•	09.0	04.1	02.2	.	.	• 0-17 <sup>40</sup> 24 <sup>30</sup>
9	8	10	09	10	05.7	03.1	04.8	.	.	• 0-10-4 <sup>30</sup> 16-16 <sup>40</sup>
10	8	040	030	00	02.3	02.3	12.4	00.0	.	△ 20-7
11	8	000	010	00	00.3	13.3	.	.	.	△ 0-7 <sup>30</sup> 0-12 <sup>30</sup> 12 <sup>35</sup>
12	8	000	060	03	03.0	11.4	.	.	.	△ 0-7-6 <sup>30</sup>
13	8	010	04	03	C2.7	12.3	00.0	.	.	△ 17-6 <sup>30</sup>
14	8	000	030	00	01.0	11.3	.	.	.	△ 0-12 <sup>30</sup> 20 <sup>20</sup> ; F <sub>NW</sub> -N 16 <sup>48</sup> 17 <sup>10</sup> ; 20 <sup>26</sup> 21 <sup>08</sup> ; R 19 <sup>30</sup> 20 <sup>30</sup>
15	8	10•	10•	04	08.0	00.0	07.0	.	.	• 0-13-13 <sup>30</sup> ; R 13 <sup>30</sup> 13 <sup>20</sup>
16	8	020	07•	08	05.7	10.5	16.2	.	.	• 0-13-13 <sup>30</sup> ; R 13 <sup>30</sup> 13 <sup>20</sup>
17	8	000	04	10•	04.7	07.7	00.7	.	.	△ 0-7-6 <sup>30</sup> ; • 0-14-21 <sup>20</sup> ; F <sub>NW</sub> 14 <sup>36</sup> 14 <sup>40</sup>
18	8	030	040	04	03.7	12.5	C2.6	.	.	△ 0-17-7 <sup>30</sup> ; F <sub>NW</sub> 8 <sup>34</sup> 24 <sup>30</sup>
19	8	07	040	05	05.3	06.7	.	.	.	F <sub>N</sub> 10 <sup>40</sup> 18 <sup>30</sup>
20	8	000	040	00	C1.3	11.5	.	.	.	F <sub>NE</sub> 7 <sup>40</sup> 8 <sup>20</sup> ; F <sub>SE</sub> -UNW 12 <sup>04</sup> 15 <sup>30</sup>
21	8	040	06•	05	05.0	09.9	.	.	.	• 0-13-14 <sup>40</sup> ; R 13 <sup>20</sup> 13 <sup>30</sup> ; F <sub>NE</sub> 13 <sup>25</sup> 13 <sup>39</sup>
22	8	060	080	09	07.7	11.6	01.3	.	.	F <sub>s</sub> 17 <sup>54</sup>
23	8	10	030	07	06.7	08.3	06.8	.	.	F <sub>N</sub> -NE 2 <sup>20</sup> 7 <sup>20</sup> ; 8 <sup>30</sup> ; • 0-25 <sup>30</sup> 9 <sup>40</sup> ; 23 <sup>20</sup> 24; R 5 <sup>10</sup> 7 <sup>40</sup> ; △ 5 <sup>30</sup> 6 <sup>30</sup>
24	8	10	10	10	10.0	00.7	C5.9	.	.	• 0-10-2 <sup>20</sup> 10 <sup>45</sup> ; 10 <sup>58</sup> ; 18-21 <sup>10</sup> ; 23 <sup>30</sup> 24; F <sub>s</sub> 21 <sup>23</sup>
25	8	10•	10	10	10.0	00.3	19.0	.	.	• 0-2-0-12 <sup>30</sup>
26	8	08	020	00	C3.3	11.2	06.5	.	.	△ 0-7 <sup>30</sup>
27	8	000	020	00	00.7	13.7	.	.	.	△ 0-7-7 <sup>30</sup>
28	8	020	030	09	04.7	11.8	.	.	.	△ 0-13-3 <sup>30</sup> 6 <sup>30</sup> 11 <sup>30</sup> ; 16-16 <sup>30</sup> ; F <sub>N</sub> 7 <sup>35</sup> ; R 9 <sup>30</sup> 10 <sup>30</sup>
29	8	10	07	04	07.0	02.6	00.3	.	.	△ 0-17-7 <sup>30</sup>
30	8	000	050	03	C2.7	12.0	11.4	.	.	.
31	8	050	090	09	07.7	07.7	07.8	.	.	.
MES.										
MRD.		05.7	06.5	06.1	06.1	219.1	187.8			

1	8	10•	050	07	C7.3	C7.1	00.0	.	• 0-6 <sup>35</sup> 7 <sup>15</sup> ;	
2	8	020	060	02	03.3	11.6	00.1	.	F <sub>NE</sub> 8-23 <sup>45</sup> ;	
3	8	08	030	CC	C3.7	08.5	.	F <sub>NE</sub> 70 <sup>2</sup> 11 <sup>30</sup> 15 <sup>33</sup> 22 <sup>3</sup> ; F <sub>NE</sub> 11 <sup>30</sup> 15 <sup>33</sup>		
4	8	000	010	00	00.3	13.5	.	F <sub>NE</sub> 7		
5	8	020	020	CC	01.3	13.6	.	.		
6	8	040	07	04	05.0	11.1	.	.	• 0-10 <sup>05</sup> 12 <sup>50</sup> ;	
7	8	09	060	02	C5.7	02.2	.	.	• 0-17-7 <sup>30</sup>	
8	8	000	020	00	0C.7	13.7	C1.6	.	F <sub>NE</sub> 1/2-7 <sup>30</sup> ;	
9	8	050	060	00	03.7	12.5	.	.	F <sub>s</sub> 6 <sup>50</sup> -18 <sup>30</sup>	
10	8	08	080	03	06.3	11.7	.	.	F <sub>s</sub> 15 <sup>50</sup> 7 <sup>02</sup> 8 <sup>05</sup> ; 0-05 <sup>20</sup> 5 <sup>30</sup> 9 <sup>10</sup> 17 <sup>30</sup> 8 <sup>20</sup> ; R 7 <sup>40</sup> 8 <sup>45</sup> ; EN 8 <sup>35</sup> 0 <sup>10</sup> ; 0-19 <sup>50</sup> 16 <sup>20</sup>	
11	8	10	060	03	C6.3	04.2	00.0	.	F <sub>w</sub> 17 <sup>30</sup> 1/9 <sup>40</sup> ; 1/17 <sup>45</sup> 19 <sup>10</sup> ; F <sub>N</sub> 18 <sup>45</sup> 18 <sup>55</sup>	
12	8	010	070	02	03.3	10.3	10.7	.	F <sub>N</sub> 2 <sup>10</sup> 2 <sup>35</sup> ; 6 <sup>19</sup> 4 <sup>45</sup> 7 <sup>20</sup>	
13	8	10•	09	02	07.0	03.2	C2.0	.	△ 0-17-7 <sup>30</sup>	
14	8	000	070	05	04.0	10.1	C1.2	.	• 0-10-7 <sup>15</sup> ; 0-18 <sup>10</sup> 24 <sup>30</sup>	
15	8	010	030	10•	04.7	10.0	.	.	• 0-1-0-11 <sup>35</sup> 12, 15 <sup>40</sup> 19 <sup>0</sup> ; R 18 <sup>15</sup> 18 <sup>35</sup>	
16	8	060	080	10	08.0	05.1	07.4	.	△ 0-7-8 <sup>30</sup>	
17	8	030	080	03	04.7	11.7	04.0	.	△ 0-17-7 <sup>30</sup>	
18	8	010	060	00	C2.3	09.9	.	.	• 0-1-0-13 <sup>05</sup> 13 <sup>45</sup> 13 <sup>55</sup> 14 <sup>30</sup> ; 6 13 <sup>20</sup> 14 <sup>30</sup> ; 6 13 <sup>20</sup> 14 <sup>15</sup> ; F <sub>N</sub> 13 <sup>20</sup> 21 <sup>45</sup> ; 0-13 <sup>45</sup> 14 <sup>20</sup>	
19	8	070	090	06	07.3	03.5	.	.	F <sub>NE</sub> 7 <sup>35</sup> 13 <sup>40</sup> ; 15 <sup>02</sup> 22 <sup>40</sup>	
20	8	030	030	03	C3.0	12.4	06.7	.	• 22 <sup>30</sup> -22 <sup>45</sup>	
21	8	020	070	06	C5.0	11.2	.	.	.	
22	8	000	030	00	C1.0	13.4	.	.	.	
23	8	000	040	07	03.7	10.5	.	.	F <sub>s</sub> 9 <sup>20</sup> 14 <sup>45</sup>	
24	8	090	040	05	06.0	08.7	.	.	F <sub>s</sub> 13 <sup>40</sup> ; • 14 <sup>35</sup> 15 <sup>20</sup> 15 <sup>20</sup> R 14 <sup>35</sup> -14 <sup>50</sup>	
25	8	070	08	00	05.0	05.8	.	.	.	
26	8	040	030	00	C2.3	12.2	C1.1	.	△ 0-7-7 <sup>30</sup>	
27	8	09	060	03	06.0	09.0	.	.	F <sub>s</sub> 12 <sup>52</sup> 20 <sup>4</sup>	
28	8	09	050	03	05.7	C7.7	00.3	.	F <sub>s</sub> 8-10 <sup>15</sup> ; • 0-22 <sup>24</sup> 24 <sup>0</sup>	
29	8	08	060	10	08.0	07.7	.	.	• 0-10 <sup>25</sup> 1 <sup>00</sup> 8 <sup>20</sup> 9 <sup>25</sup> ; F <sub>NE</sub> -NW 9 <sup>35</sup> 14 <sup>5</sup> 14 <sup>23</sup> 15 <sup>07</sup>	
30	8	030	060	08	05.7	07.1	08.4	.	.	
MES.										
MRD.		04.7	05.5	03.5	04.5	279.7	43.5			

$\varphi = 42^{\circ}26'$ , N  $\lambda = 19^{\circ}17'$ , E Gr.  $\Delta G = +1h\ 17\ min.$

BR. ST. 248

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	755.4	755.6	756.8	22.8	30.0	24.6	25.5	30.5	18.0	13.0	08.9	10.7	10.7	42	34	46	41	N	3	NNF	4	NNF	3	
2	758.3	757.5	757.0	23.0	32.1	26.7	27.1	33.2	19.1	15.6	10.1	12.8	12.6	48	34	48	44	NNF	2	SSW	1	NE	7	
3	758.7	756.1	754.4	23.8	31.3	24.7	26.1	31.8	21.9	18.1	09.1	12.9	14.9	41	37	64	47	NNF	3	S	3	-	0	
4	754.2	753.9	754.3	23.0	32.3	25.2	26.6	32.9	20.3	16.2	13.6	13.4	14.0	64	36	58	53	NNF	3	S	4	-	0	
5	755.6	755.3	756.1	24.2	32.6	26.4	27.4	33.8	21.8	18.0	12.8	12.5	13.9	57	34	54	48	NE	1	SW	3	FNF	1	
6	757.4	756.0	754.7	24.8	34.0	25.7	27.6	34.4	21.7	18.5	13.0	12.2	13.1	55	30	53	46	NNE	2	WSW	3	-	0	
7	753.8	753.9	754.9	23.5	20.6	19.4	20.8	30.2	17.5	15.8	12.5	14.6	06.3	57	80	38	58	-	0	N	6	NNF	8	
8	756.7	756.3	757.3	19.3	23.5	19.0	20.2	24.5	17.2	14.4	07.5	07.9	07.9	44	36	48	43	NNF	6	NNE	6	N	3	
9	759.8	758.8	758.1	19.6	26.7	20.7	21.9	27.3	15.8	12.6	07.2	08.3	08.0	42	32	44	39	NE	4	NE	4	NE	2	
10	759.1	757.0	757.8	20.2	29.2	22.2	23.4	29.5	16.8	14.3	08.1	11.4	13.4	46	37	67	50	S	2	SW	3	-	0	
11	758.7	757.7	758.3	23.8	31.9	24.6	26.3	32.2	20.1	17.4	04.5	11.3	12.2	39	32	52	41	NNF	7	NNW	2	ENE	2	
12	759.5	758.7	758.8	23.4	33.0	25.0	26.6	33.5	19.8	15.8	11.9	12.7	15.0	55	34	63	51	NNE	3	SW	3	-	0	
13	759.1	757.0	756.0	24.0	35.2	25.4	27.5	35.9	20.0	16.3	13.4	10.6	13.7	60	25	56	47	N	2	S	3	-	0	
14	757.2	755.8	756.3	24.7	36.4	27.9	29.2	36.8	21.3	16.8	11.8	11.6	12.6	51	25	45	40	NNE	2	SSE	3	ENE	3	
15	757.8	756.5	757.2	25.9	37.7	25.5	30.6	38.3	22.1	18.4	10.8	12.7	14.7	43	26	48	39	N	3	SW	3	NF	2	
16	757.0	755.0	755.2	28.0	28.7	30.0	31.7	38.6	24.8	20.8	13.9	13.1	14.8	49	25	47	40	N	2	SW	4	-	0	
17	754.9	752.6	742.4	27.6	28.0	30.0	31.4	38.6	24.9	21.0	13.4	12.5	14.2	48	25	44	39	NNE	2	SSE	3	-	0	
18	752.3	751.6	751.4	26.5	34.1	27.5	28.9	35.5	22.0	18.9	14.4	12.3	15.4	56	31	56	48	ENF	2	S	6	-	0	
19	751.8	752.6	751.9	25.2	29.2	21.3	24.2	29.7	20.8	19.5	14.8	10.8	15.3	61	35	81	59	S	5	S	5	S	1	
20	750.9	750.1	750.9	20.6	27.2	26.6	22.2	28.4	18.1	16.7	12.7	10.9	08.9	70	40	49	53	N	1	SSW	4	NNE	6	
21	750.9	750.5	752.1	19.8	22.4	20.2	20.6	25.6	18.5	16.0	07.8	08.2	08.6	45	40	49	45	NE	6	NNE	6	N	2	
22	753.8	754.0	755.2	19.2	26.4	20.2	21.6	27.4	17.5	15.3	08.9	09.8	08.8	53	38	47	46	N	3	NE	3	N	5	
23	755.4	757.2	757.8	17.8	20.0	18.0	18.4	22.7	16.0	12.7	08.8	12.9	12.1	58	74	78	70	-	0	NE	2	-	0	
24	759.9	758.2	758.1	18.6	27.0	22.2	22.5	28.2	15.0	12.5	11.5	12.0	13.1	72	45	65	61	N	1	S	2	W	1	
25	758.1	755.7	755.8	20.6	30.2	24.2	24.8	31.0	16.6	12.4	11.9	12.4	12.4	65	39	55	53	NNE	1	S	3	-	0	
26	756.5	755.0	757.2	23.2	30.8	22.8	25.4	31.7	19.8	16.0	12.9	12.8	09.7	60	38	44	47	-	0	SSW	4	NNE	6	
27	758.6	757.2	758.0	22.4	31.2	24.2	25.5	32.4	19.9	18.0	11.0	15.2	14.3	54	45	63	54	Nw	2	W	3	-	0	
28	758.3	757.3	758.3	23.6	33.4	26.0	27.2	34.2	19.0	14.4	11.1	11.0	13.9	51	28	55	45	N	1	SSW	2	-	0	
29	759.1	757.7	758.3	24.1	35.8	30.6	30.3	36.1	19.2	16.5	13.9	13.3	14.2	62	30	43	45	-	0	SSW	3	NE	6	
30	758.3	755.4	755.4	27.2	36.0	29.6	30.6	36.0	25.8	23.4	16.1	12.7	14.0	59	28	45	44	N	2	SSW	4	-	0	
31	755.6	753.8	754.0	27.2	35.7	29.3	30.4	36.5	24.4	20.3	14.6	13.3	13.2	54	30	43	42	NNW	2	S	4	-	0	
MES.	VRED.	756.5	756.5	756.8	23.2	31.1	24.7	25.9	32.2	19.9	16.6	11.5	11.9	12.4	54	36	53	48	2.2	3.5	1.9			

1974 AVGUST

TITOGRAF

1	754.6	752.8	753.7	27.7	37.0	27.7	30.0	37.0	26.2	23.6	13.1	12.5	12.9	47	27	46	40	NW	4	SSE	4	-	0
2	754.5	753.7	753.7	28.1	37.0	28.6	30.6	37.8	26.0	23.3	12.7	11.0	13.6	45	23	46	38	N	3	S	4	-	0
3	756.2	755.3	756.1	28.0	37.0	28.6	30.6	38.0	26.2	22.5	10.2	07.9	13.9	36	17	47	33	NNW	4	SSE	4	-	0
4	757.6	756.1	755.8	28.2	38.3	29.4	31.3	38.4	26.3	21.6	14.1	11.7	12.7	49	23	41	38	NNW	3	SW	2	-	0
5	757.4	755.3	754.7	27.6	38.7	26.4	31.3	38.7	25.4	21.0	13.7	11.5	09.5	50	22	31	34	NNW	2	SSE	4	-	0
6	756.3	754.0	754.8	27.9	37.7	28.8	30.6	38.0	25.2	20.5	10.6	15.4	14.4	38	31	49	39	-	0	S	4	N	6
7	756.2	754.0	754.0	24.5	33.0	28.0	28.4	33.1	24.0	22.2	09.7	11.7	12.8	42	31	45	39	N	6	SSE	4	ESE	2
8	754.1	752.1	751.6	24.8	33.6	27.2	28.2	33.8	23.0	19.9	10.6	11.7	10.4	45	30	39	38	N	4	S	3	-	0
9	752.4	751.4	752.2	24.0	28.6	25.6	26.6	31.4	20.4	16.4	10.1	17.6	18.4	45	60	75	60	-	0	SSE	4	SE	2
10	755.4	753.8	753.0	24.2	31.7	24.6	26.3	32.6	23.2	20.6	12.1	08.3	14.0	53	24	60	46	N	4	SSE	4	-	0
11	751.5	750.6	751.3	22.7	26.8	22.6	23.7	28.8	20.5	19.6	10.7	14.5	14.4	52	55	70	59	-	0	S	6	NNW	2
12	754.1	753.9	756.2	21.0	27.2	22.2	23.2	28.2	18.5	15.0	06.5	06.7	06.6	35	25	33	31	N	4	NNE	4	NW	2
13	757.7	757.2	759.0	21.8	29.6	24.6	25.2	30.0	17.0	12.2	07.1	07.4	08.0	36	24	34	31	NW	5	NNE	4	NNE	4
14	760.9	759.6	760.3	21.8	33.0</td																		

BR. ST. 248

$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vyhřev 0-0	Oblačnost N (0-10)					Insolace sati breh	Podzvuk R mm	Snežní pokrývka h cm	Razový vývoj w
		14	7	14	21	Sred Dies				
1	8 030	040	00	02.3	13.8	00.3	.	FNE 9 <sup>2</sup> -14 <sup>22</sup> i	.	.
2	8 000	020	00	00.7	14.0	.	.	FNNNE 22 <sup>12</sup> -24i	.	.
3	8 000	020	00	00.7	12.9	.	.	FNNNE 0-3 <sup>04</sup> i	.	.
4	8 030	020	00	01.7	13.3	.	.	.	.	.
5	8 030	020	00	01.7	13.5	.	.	.	.	.
6	8 000	010	00	00.3	14.0	.	.	.	.	.
7	8 030	090	01	04.3	08.8	.	.	• 0-11 <sup>25</sup> -13 <sup>15</sup> , FNNNE 11 <sup>12</sup> -14 <sup>10</sup> i, R 11 <sup>50</sup> -13 <sup>20</sup> , FNNNE 14 <sup>10</sup> -24	.	.
8	8 010	030	03	02.3	13.8	06.8	.	F-FNNNE 0-16 <sup>10</sup> i	.	.
9	8 000	040	00	01.3	14.1	.	.	FNNNE 5 <sup>50</sup> -15 <sup>52</sup> i, FNNNE 9 <sup>50</sup>	.	.
10	8 030	030	00	02.0	12.7	.	.	.	.	.
11	8 10	030	04	05.7	10.3	.	.	FNNNE 9 <sup>30</sup> -10 <sup>33</sup> i	.	.
12	8 000	010	00	00.3	13.9	.	.	.	.	.
13	8 000	000	00	00.0	14.2	.	.	.	.	.
14	8 000	000	00	00.0	14.1	.	.	.	.	.
15	8 000	000	00	00.0	13.5	.	.	.	.	.
16	8 000	000	00	00.0	13.2	.	.	.	.	.
17	8 000	030	00	01.0	12.7	.	.	.	.	.
18	8 010	080	00	03.0	09.1	00.0	.	• 0-17 <sup>20</sup> -7 <sup>0</sup> , 09 <sup>40</sup> -9 <sup>20</sup> , FSSSE 12 <sup>04</sup> -14 <sup>15</sup> , FSSSE 12 <sup>34</sup>	.	.
19	8 070	020	09	06.0	09.1	00.0	.	FSSSE 14 <sup>35</sup> -18 <sup>05</sup> , 12 <sup>35</sup> , F <sub>3</sub> 18 <sup>05</sup> -19 <sup>16</sup> , 18 <sup>19</sup> -20 <sup>45</sup>	.	.
20	8 080	060	06	06.7	11.4	03.5	.	FNNNE 18 <sup>30</sup> -12 <sup>35</sup> , FNNNE 22 <sup>12</sup> -22 <sup>50</sup>	.	.
21	8 08	09	08	08.3	05.6	.	.	FNNNE 0-19i	.	.
22	8 040	050	02	02.7	C8.2	.	.	FNE 15 <sup>29</sup> -20 <sup>45</sup> i	.	.
23	8 09	10	10	05.7	02.1	.	.	• 0-10 <sup>20</sup> -10 <sup>36</sup> , 13 <sup>20</sup> -14 <sup>30</sup>	.	.
24	8 000	06	00	02.0	12.2	00.8	.	.	.	.
25	8 000	010	00	00.3	13.5	.	.	.	.	.
26	8 030	07	00	02.3	10.0	.	.	FNE 15 <sup>27</sup> -22 <sup>32</sup> , FNE 16 <sup>36</sup> -20 <sup>24</sup>	.	.
27	8 000	000	00	00.0	13.7	.	.	FN 040-140	.	.
28	8 000	000	00	00.0	13.8	.	.	.	.	.
29	8 050	030	05	04.3	12.6	.	.	.	.	.
30	8 000	030	08	03.7	11.9	.	.	FNNNE 0 <sup>30</sup>	.	.
31	8 000	030	06	03.0	12.7	.	.	.	.	.
MES.				02.3	03.3	02.0	02.5	368.7	11.4	
WRED.										

1	8 010	030	00	01.3	13.3	.	.	FNNW 15 <sup>25</sup> -17 <sup>25</sup> , FNNW 15 <sup>20</sup>	.	.
2	8 000	010	00	00.3	13.2	.	.	FNNW 14i	.	.
3	8 000	010	00	00.3	13.2	.	.	.	.	.
4	8 010	010	00	00.7	12.6	.	.	.	.	.
5	8 000	010	00	00.3	11.8	.	.	.	.	.
6	8 000	020	00	00.7	12.5	.	.	FN 17 <sup>35</sup> -24, FN 18 <sup>30</sup> -24	.	.
7	8 000	010	03	01.3	12.3	.	.	FN 0-10 <sup>30</sup> , FN 0 <sup>31</sup> -7 <sup>47</sup>	.	.
8	8 000	010	00	00.3	12.7	.	.	FSSSE 13 <sup>14</sup> -16 <sup>36</sup> i	.	.
9	8 070	08	03	06.0	06.9	.	.	FN 05 <sup>35</sup> -10 <sup>25</sup> i	.	.
10	8 010	010	00	00.7	13.3	.	.	• 09-9 <sup>10</sup> , F <sub>5</sub> 9 <sup>25</sup> -17 <sup>48</sup> i, 23 <sup>50</sup> -24, 0-11 <sup>22</sup> -12i	.	.
11	8 05	070	08	08.0	08.0	.	.	FN 0-19 <sup>49</sup> i, FN 0 <sup>50</sup> -10 <sup>48</sup> i	.	.
12	8 010	050	05	03.7	12.9	06.6	.	FNNNE 8-22 <sup>54</sup> i	.	.
13	8 000	050	03	02.7	12.0	.	.	FNNNE 11-12 <sup>55</sup> i	.	.
14	8 000	010	00	00.3	13.2	.	.	FNNNE 3 <sup>45</sup> -17 <sup>00</sup> i, FNNNE 12 <sup>40</sup>	.	.
15	8 000	070	03	03.3	12.8	.	.	.	.	.
16	8 030	040	00	02.3	12.4	.	.	FSSSE 12 <sup>13</sup>	.	.
17	8 000	060	00	02.0	12.3	.	.	FNNNE 8 <sup>30</sup> -23 <sup>48</sup>	.	.
18	8 000	000	00	00.0	12.8	.	.	FNNNE 14 <sup>15</sup> -14 <sup>45</sup>	.	.
19	8 000	010	00	00.3	12.4	.	.	FNNW 14 <sup>55</sup>	.	.
20	8 000	030	04	02.3	11.3	.	.	• 19 <sup>50</sup> -22 <sup>40</sup> , T 20 <sup>15</sup> -21 <sup>30</sup>	.	.
21	8 05	070	03	06.3	04.8	.	.	FSE 17 <sup>02</sup> -12 <sup>37</sup> , 6 19 <sup>30</sup> -20 <sup>45</sup> , T 20-20 <sup>40</sup>	.	.
22	8 000	050	03	02.7	11.6	.	.	FSE-N 0 <sup>49</sup> -10 <sup>22</sup> , 15 <sup>45</sup> -16 <sup>00</sup>	.	.
23	8 07	070	08	07.3	07.2	.	.	FSE-SE-NNW 9 <sup>10</sup> -14 <sup>50</sup> , 6 <sup>12</sup> -17 <sup>45</sup> -18 <sup>00</sup>	.	.
24	8 08	050	03	05.3	06.5	01.4	.	• 02 <sup>40</sup> -3 <sup>50</sup> , □ 20-20 <sup>20</sup> , ▲ 20 <sup>20</sup> -20 <sup>25</sup>	.	.
25	8 040	040	09	05.7	11.3	.	.	FSE 17 <sup>34</sup>	.	.
26	8 010	060	01	02.7	12.2	.	.	.	.	.
27	8 020	030	05	03.3	11.6	.	.	.	.	.
28	8 08	10 <sup>07</sup>	10	09.3	03.2	.	.	.	.	.
29	8 08	09	05	07.3	05.5	07.2	.	FNNNE-NE 6 <sup>08</sup> -8 <sup>28</sup> , 16 <sup>50</sup> -17 <sup>00</sup>	.	.
30	8 09	040	00	04.3	07.3	00.3	.	16 <sup>50</sup> -17 <sup>00</sup>	.	.
31	8 000	040	04	02.7	12.1	.	.	.	.	.
MES.				02.5	04.0	02.6	03.0	335.6	15.5	
WRED.										

$\varphi = 42^{\circ}26'$ , N  $\lambda = 19^{\circ}17'$ , E Gr.  $\Delta G = +1h\ 17\ min.$ 

BR. ST. 248

SD	Temperature (°C)			Humidity (%)						Wind (m/s)			Pressure (hPa)									
	7	14	21	7	14	21	Sred. Dries	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dries	7	14	21		
1	757.2	756.7	757.0	21.4	28.8	22.0	23.6	30.0	17.8	15.3	12.2	12.5	11.8	64	42	59	55	N	3	SSE 3	- 0	
2	757.3	757.2	758.1	22.4	30.4	23.2	24.6	31.2	20.6	16.8	11.8	11.1	17.2	58	34	R1	58	N	3	SSE 5	- 0	
3	758.3	756.8	757.3	22.9	32.6	24.8	26.3	32.8	21.0	18.8	13.5	14.5	14.4	64	39	61	55	N	3	SSE 4	- 0	
4	756.8	755.1	755.3	23.2	33.2	24.4	26.3	33.8	20.8	17.0	14.4	14.6	15.3	67	38	67	57	-	0	S 4	- 0	
5	757.3	755.3	756.3	24.2	32.4	24.5	26.4	32.5	22.7	19.8	12.5	11.7	11.6	55	32	50	46	NNW 3	SE 2	NE 2		
6	755.1	752.0	751.1	21.8	30.8	23.0	24.6	31.5	19.9	17.8	07.8	11.4	13.0	40	34	62	45	N	3	S 5	- 0	
7	748.1	749.2	750.3	20.8	18.2	17.6	18.6	23.0	16.8	14.5	11.8	14.5	14.2	64	93	94	84	N	2	SE 3	- 0	
8	753.7	755.0	758.1	16.6	29.2	24.6	23.8	29.6	14.4	13.4	12.5	12.0	11.0	88	39	47	58	-	0	NNE 5	NNW 3	
9	761.0	760.1	760.1	21.0	30.8	23.0	24.4	31.0	20.5	17.7	11.3	11.7	13.0	60	35	62	52	NW 1	SE 3	- 0		
10	760.9	759.2	759.7	21.4	31.2	24.7	25.5	32.4	20.0	16.6	12.9	14.4	14.9	68	42	64	58	N	2	SE 4	- 0	
11	760.8	759.8	761.0	25.0	31.4	25.0	26.6	31.4	23.5	19.6	11.4	10.4	11.1	48	30	47	42	N	6	NNE 5	NNE 5	
12	761.9	760.5	761.1	21.6	30.0	22.8	24.3	30.7	21.4	17.5	10.2	11.4	11.6	52	36	56	48	NW 1	SE 3	- 0		
13	761.2	759.0	759.4	21.0	31.0	23.4	24.7	31.4	20.0	15.5	11.4	12.4	11.3	61	37	52	50	N	3	SSE 3	- 0	
14	760.1	758.2	758.4	22.4	31.2	24.6	25.7	35.6	21.9	18.9	11.3	09.8	13.8	55	29	60	48	NNW 3	SSE 4	- 0		
15	758.0	756.1	756.7	22.7	30.0	23.8	25.1	30.5	21.7	18.5	10.3	11.9	11.1	50	37	50	46	NW 2	SE 4	- 0		
16	758.0	757.5	758.4	23.5	30.4	25.2	26.1	30.8	22.3	16.3	11.6	11.7	09.9	53	36	41	43	N	2	SSE 3	N 4	
17	760.3	759.9	760.2	20.9	29.0	22.8	23.9	29.5	20.8	17.5	10.0	11.2	15.2	54	37	73	55	SSW 3	ESE 2	- 0		
18	760.3	759.0	759.4	20.4	26.8	22.6	23.1	28.6	19.0	16.0	11.4	11.8	12.3	64	45	60	56	NNE 3	WSW 3	- 0		
19	759.4	757.4	757.6	20.0	27.3	22.4	23.0	29.3	18.5	15.0	12.8	12.3	11.6	73	45	57	58	-	0	ESE 1	NF 2	
20	756.2	754.3	754.2	19.4	28.8	23.5	23.8	29.0	18.4	14.3	10.2	10.7	16.8	60	36	77	58	NNE 4	SE 5	ESE 4		
21	754.4	755.5	755.0	18.5	18.0	18.7	18.5	24.0	16.3	17.5	14.9	14.5	14.8	94	93	92	93	-	0	-	0	
22	755.1	756.4	757.5	18.5	24.2	18.2	16.8	24.4	17.5	17.0	14.2	12.4	14.8	89	55	94	79	W 2	SE 5	-	0	
23	756.5	757.4	757.5	17.0	21.6	17.5	18.4	23.2	15.6	16.9	14.3	12.2	13.4	98	63	90	84	NW 2	-	0		
24	754.8	754.2	752.4	17.4	22.3	20.6	20.2	24.7	15.6	13.5	13.6	15.1	13.9	91	75	76	81	-	0	SE 2	SE 4	
25	749.9	747.6	747.3	15.4	13.7	13.0	13.8	22.0	12.8	14.5	12.6	10.9	10.6	96	93	95	95	-	0	NNNE 3	-	0
26	742.3	741.5	747.5	12.4	16.0	13.4	13.8	22.0	12.0	10.4	10.3	11.5	06.0	96	84	52	77	NW 2	-	0	NW 5	
27	754.3	756.2	758.3	10.6	21.0	12.6	14.2	21.2	07.5	04.5	07.3	05.7	06.4	76	30	58	55	-	0	NF 3	-	0
28	756.8	757.1	757.2	12.0	21.8	14.8	15.8	21.8	10.2	06.3	06.5	08.5	11.5	61	43	91	65	N	4	SSE 3	-	0
29	757.1	757.3	757.8	13.5	23.6	16.0	17.2	23.8	12.0	09.1	09.1	09.8	12.0	78	45	88	70	-	0	S 2	-	0
30	756.6	755.0	756.4	16.0	24.6	17.4	18.8	25.1	13.0	10.0	11.0	10.7	14.3	81	46	96	74	-	0	SE 5	-	0
MES.	VRRED. 756.7 755.8 756.6			19.5	26.7	21.0	22.0	28.2	17.8	15.2	11.5	11.8	12.6	69	47	68	62	1.9	3.2	1.0		

1	755.4	755.5	757.0	14.8	22.0	15.6	17.0	22.0	14.4	13.6	10.8	09.8	09.4	86	50	71	69	SE 1	SE 5	- 0		
2	756.6	756.4	752.5	12.6	19.0	15.0	14.2	17.6	11.0	08.4	08.1	10.5	09.7	74	87	76	79	-	0	WNW 2	SSW 5	
3	759.3	760.0	761.8	11.4	19.4	11.4	13.4	20.0	10.4	08.0	09.3	06.5	08.5	92	38	84	71	-	0	S 3	- 0	
4	761.3	760.0	760.1	10.7	20.4	12.0	13.8	21.8	09.2	05.3	06.7	05.1	08.4	69	29	80	59	-	0	-	0	
5	758.4	756.4	754.9	13.2	21.4	15.0	16.2	23.0	11.0	07.2	06.0	07.8	10.5	61	41	82	61	NNW 2	-	0	-	
6	752.0	753.1	754.3	13.6	21.7	16.0	16.8	22.5	13.6	11.9	10.2	10.8	10.9	87	55	80	74	NE 1	SE 4	NE 2		
7	751.5	752.2	757.5	13.2	14.7	17.7	15.8	17.8	12.8	13.0	10.6	12.0	11.4	94	96	75	88	-	0	-	SE 5	
8	753.0	752.2	754.1	15.6	17.0	14.0	15.2	21.2	13.5	14.2	12.5	11.7	10.7	94	80	90	88	-	0	SE 5	- 0	
9	755.2	755.3	755.5	11.8	20.6	15.2	15.7	21.4	10.5	07.5	09.3	07.4	09.9	90	41	76	69	-	0	SE 3	NW 1	
10	758.9	758.2	759.1	11.8	21.2	12.2	14.4	21.4	08.6	05.9	07.4	05.9	08.0	72	31	75	59	N	3	W 1	-	
11	759.4	759.2	760.4	10.5	20.4	13.8	14.6	20.8	09.6	05.5	06.4	06.3	07.3	67	35	62	55	N	4	SE 2	N 4	
12	759.9	758.3	757.9	11.8	20.5	14.7	15.4	22.2	10.2	05.7	07.2	07.5	11.3	69	41	90	67	NW 2	NW 2	NNW 3		
13	756.5	755.0	753.3	14.0	15.4	15.2	15.0	16.6	13.5	13.6	10.7	11.8	11.4	90	90	88	89	-	0	NW 3	- 0	
14	753.4	753.4	753.6	16.8	19.4	16.8	17.4	20.6	14.8	14.5	12.2	14.5	12.4	85	86	87	86	SE 4	SSE 1	- 0		
15	752.9	750.4	750.1	15.4	17.3	17.3	16.8	19.7	15.0	14.0	11.5	13.0	12.4	88	88	84	87	-	0	ESE 7		
16	755.3	757.7	758.8	13.2	19.6	12.6	14.5	21.2	12.6	10.4	09.7	06.7	09.0	85	39	83	69	-	0	S 3	- 0	
17	760.0	760.3	760.8	09.6	18.6	09.8	12.0	19.0	08.5	05.4	07.2	04.9	07.7	81	31	84	65	N	2	SE 3	- 0	
18	761.1	759.7	760.6	08.6	18.0</																	

BR. ST. 248

 $H_s = 49 \text{ m } H_D = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vremenski razdoblje	Oblikovanje					Srednja vjetrenost m/s	Podzemna vjetrenost m/s	Srednji vjetrenost h cm <sup>-1</sup>	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 050	070	03	05.0	09.7	.	.	.	.	.
2	8 060	090	04	06.3	09.7	.	.	.	.	.
3	8 040	020	00	02.0	10.6	.	.	.	.	.
4	8 020	020	03	02.3	11.2	.	.	.	.	.
5	8 020	040	00	02.0	12.0	.	.	.	.	.
6	8 000	000	00	00.0	12.0	.	.	.	.	.
7	8 100R	05	03	07.3	00.0	.	.	.	.	.
8	8 000	030	00	01.0	11.2	14.4	.	.	.	.
9	8 000	010	00	00.3	11.6	.	.	.	.	.
10	8 000	010	00	00.3	10.9	.	.	.	.	.
11	8 050	020	00	02.3	10.8	.	.	.	.	.
12	8 000	010	04	01.7	11.0	.	.	.	.	.
13	8 06	010	00	02.3	09.0	.	.	.	.	.
14	8 040	010	00	01.7	10.9	.	.	.	.	.
15	8 000	000	00	00.3	11.0	.	.	.	.	.
16	8 000	020	00	00.7	10.7	.	.	.	.	.
17	8 000	010	00	00.3	09.6	.	.	.	.	.
18	8 030	10	C6	06.3	05.3	.	.	.	.	.
19	8 030	08R	02	04.3	08.1	.	.	.	.	.
20	8 010	010	08R	03.3	09.7	00.0	.	.	.	.
21	8 100	060	080R	08.0	02.0	07.2	.	.	.	.
22	8 100R	07	100	05.0	01.7	45.7	.	.	.	.
23	8 100R	070	08	08.3	04.4	31.0	.	.	.	.
24	8 10	070	100	09.0	06.6	15.1	.	.	.	.
25	8 100R	100R	04	08.0	00.3	42.2	.	.	.	.
26	8 100R	09	C6	08.3	01.6	61.0	.	.	.	.
27	8 030	010	00	01.3	11.1	32.4	.	.	.	.
28	8 000	020	00	00.7	10.9	.	.	.	.	.
29	8 080	040	03	05.0	07.2	.	.	.	.	.
30	8 070	070	10	08.0	07.0	.	.	.	.	.
MES.	WRED.	04.3	04.2	03.1	03.8	247.9	245.0			

TITOGRAD

1974 OKTEBAR

1	8 10	050	09	08.0	08.0	40.2	.	$F_{ESE} 11^{\circ} 11^{\circ} 11^{\circ}$	$\Delta^{\circ} n-B^{\circ} 0^{\circ} 20^{\circ} 23^{\circ}$	$F_{ESE-SE} 14^{\circ} 14^{\circ} 10^{\circ} 17^{\circ} 21^{\circ} 18^{\circ} 17^{\circ}$
2	7 09	10	100R	05.7	C0.8	.	.	$\Delta^{\circ} 0^{\circ} 19^{\circ} 24$	$\Delta^{\circ} 0^{\circ} 6.0$	
3	8 08	040	00	04.0	C9.2	11.3	.			
4	8 C50	070	02	04.7	09.2	.	.			
5	8 080	090	06	07.7	C4.5	.	.			
6	8 100	060	10	C6.7	C5.7	25.3	.	$\bullet^{\circ} 1^{\circ} 2^{\circ} 0^{\circ} 0^{\circ} 7^{\circ} 3^{\circ}$	$\Delta^{\circ} n-6^{\circ}$	$F_{NW} 0^{\circ} 49$
7	8 100	100	10	10.0	00.0	06.4	.	$\bullet^{\circ} 1^{\circ} 0^{\circ} 18^{\circ} 18^{\circ} 18^{\circ}$	$\Delta^{\circ} 21-22^{\circ} 22^{\circ} 23^{\circ}$	$F_{SE} 20^{\circ} 20^{\circ} 23^{\circ}$
8	8 08	100	100	05.3	02.9	40.5	.	$F_{ESE-SE} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 14^{\circ} 14^{\circ} 14^{\circ} 14^{\circ} 14^{\circ} 14^{\circ}$	$F_{NW} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$
9	8 10	060	07	C7.7	C6.8	10.3	.	$\bullet^{\circ} 1^{\circ} 2^{\circ} 7^{\circ} 9^{\circ} 1^{\circ} 21-21^{\circ} 21^{\circ} 21^{\circ}$	$\Delta^{\circ} 17^{\circ} 17^{\circ} 17^{\circ} 17^{\circ} 17^{\circ} 17^{\circ}$	$F_{SW} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ}$
10	8 030	030	01	02.3	10.3	06.4	.	$\Delta^{\circ} 18-n$		
11	8 020	030	00	C1.7	10.4	.	.	$\Delta^{\circ} n-8^{\circ} 19^{\circ} n$		
12	8 040	10	10	08.0	06.3	.	.	$\bullet^{\circ} 1^{\circ} 10^{\circ} 13^{\circ} 20^{\circ} 20^{\circ} 20^{\circ}$		
13	8 100	10	100	10.0	00.0	C5.8	.	$\bullet^{\circ} n-10^{\circ} 10^{\circ} 10^{\circ} 10^{\circ} 10^{\circ} 10^{\circ}$	$\Delta^{\circ} 13^{\circ} 13^{\circ} 13^{\circ} 13^{\circ} 13^{\circ} 13^{\circ}$	$F_{SE} 34^{\circ} 40^{\circ} 18^{\circ} 10^{\circ} n$
14	7 100	090	08	09.0	01.0	36.4	.	$\bullet^{\circ} 0^{\circ} 2^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 16^{\circ} 16^{\circ} 17^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$
15	7 10	100	100	10.0	00.1	26.5	.	$\bullet^{\circ} 0^{\circ} 2^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ}$	$F_{SE} 16^{\circ} 16^{\circ} 17^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$
16	8 040	040	06	04.7	07.6	97.0	.	$\bullet^{\circ} 0^{\circ} 5^{\circ} 0^{\circ} 17^{\circ} 20^{\circ} 20^{\circ}$	$\Delta^{\circ} 22^{\circ} 22^{\circ} 22^{\circ} 22^{\circ} 22^{\circ} 22^{\circ}$	$F_{SE} 19^{\circ} 19^{\circ} 19^{\circ} 19^{\circ} 19^{\circ} 19^{\circ}$
17	8 03	040	00	02.3	10.1	00.6	.	$\Delta^{\circ} n-8^{\circ} 19^{\circ} n$		
18	8 06	080	00	04.7	07.2	.	.	$\Delta^{\circ} n-8^{\circ} 19^{\circ} 24$		
19	8 02	040	00	02.0	10.0	.	.	$\Delta^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$		
20	8 03	070	07	05.7	06.9	.	.	$\Delta^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$		
21	8 10	08	100R	09.3	C1.0	12.1	.	$\bullet^{\circ} 0^{\circ} 4^{\circ} 0^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 5.4^{\circ} 34^{\circ} 24^{\circ} 15^{\circ} n$
22	7 C8	100	100R	09.3	00.5	52.8	.	$\bullet^{\circ} 0^{\circ} 2^{\circ} 0^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 5.4^{\circ} 34^{\circ} 24^{\circ} 15^{\circ} n$
23	8 100	100	090	09.7	C0.1	26.0	.	$\bullet^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 10^{\circ} 10^{\circ} 10^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 5.4^{\circ} 34^{\circ} 24^{\circ} 15^{\circ} n$
24	8 09	060	03	06.0	02.9	46.5	.	$\bullet^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 10^{\circ} 10^{\circ} 10^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 5.4^{\circ} 34^{\circ} 24^{\circ} 15^{\circ} n$
25	8 07	030	00	03.3	09.1	.	.			
26	5 04	100	10	08.0	03.2	.	.	$\Delta^{\circ} 7^{\circ} 0^{\circ} 0^{\circ} 12^{\circ} 16^{\circ} 20^{\circ} n$	$\Delta^{\circ} 13^{\circ} 14^{\circ} 14^{\circ} 14^{\circ} 14^{\circ} 14^{\circ}$	$F_{SE} 0^{\circ} 22^{\circ} 23^{\circ}$
27	8 03	020	00	01.7	10.0	C0.8	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 20^{\circ} 20^{\circ} 20^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 23^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$
28	8 06	010	100	05.7	C9.7	.	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 10^{\circ} 10^{\circ} 10^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 0^{\circ} 1^{\circ} 0^{\circ} 10^{\circ} 10^{\circ} 10^{\circ}$
29	8 10	100	100	10.0	01.8	34.1	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$
30	7 100	100	07	09.0	00.2	32.5	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$
31	8 10	100	10	10.0	00.0	16.6	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$	$\Delta^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$	$F_{SE} 0^{\circ} 1^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}$
MES.	WRED.	07.2	07.1	06.3	06.8	157.1	523.4			

$\varphi = 42^{\circ}26'$ , N  $\lambda = 19^{\circ}17'$  E Gr.  $\Delta G = +1h\ 17\ min.$

BR. ST. 248

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0—12)						
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	748.4	749.9	753.8	04.6	10.2	08.6	08.5	12.4	06.5	04.6	06.1	07.1	03.0	84	76	36	65	N	2	C	N	7	
2	750.3	750.2	750.3	04.6	12.6	05.6	07.1	13.0	04.2	-01.5	03.2	03.6	05.5	51	33	60	55	NW	3	SW	2	0	
3	760.9	761.3	761.7	05.6	12.6	08.2	08.6	12.8	04.5	00.2	05.9	05.1	06.7	86	47	82	72	-	0	SSE	2	-	
4	760.9	760.0	759.2	06.2	11.6	08.0	08.4	12.5	05.4	01.0	06.1	06.2	06.6	86	61	82	76	-	0	-	0	-	
5	759.9	760.4	762.4	08.6	12.6	10.0	10.3	14.6	06.2	03.4	06.3	06.4	07.7	75	58	83	72	N	2	N	3	-	
6	763.7	763.1	763.1	08.2	16.8	10.2	11.4	17.5	08.0	05.0	07.7	07.6	08.6	95	53	92	80	-	0	-	C	-	
7	760.1	758.0	758.0	05.2	11.5	10.2	10.3	12.5	09.2	07.2	07.7	08.7	08.2	88	85	88	87	-	0	-	C	-	
8	755.3	754.6	755.5	09.0	15.2	12.0	12.0	16.6	08.1	05.0	05.5	04.4	04.0	64	34	38	45	NW	3	NNE	7	NNE	7
9	755.7	756.1	758.9	11.7	14.2	11.4	12.2	15.5	11.2	08.4	03.8	04.3	04.1	37	36	41	38	NNE	7	NNE	8	N	7
10	760.1	759.8	761.1	05.6	15.6	07.2	08.9	16.0	05.3	00.5	05.5	05.5	06.4	80	42	84	69	-	0	SW	2	-	0
11	763.1	762.3	763.1	05.0	16.6	07.0	08.6	17.0	04.7	-00.4	05.4	05.7	06.5	83	40	87	70	N	3	SSE	2	-	0
12	763.0	761.7	761.7	06.2	14.2	08.6	09.4	16.5	04.7	-00.4	05.6	06.2	07.3	78	51	87	72	NNE	2	SE	1	-	0
13	761.6	762.1	763.5	07.5	15.0	08.5	09.9	15.4	07.0	03.5	07.1	06.7	07.5	91	52	90	78	-	0	-	C	-	0
14	764.4	763.7	764.0	07.4	16.7	07.6	08.6	17.5	06.9	03.0	07.3	06.8	07.2	95	47	92	78	-	0	SE	1	-	0
15	764.9	763.9	764.6	06.4	14.2	07.6	09.4	17.0	06.4	02.0	06.0	06.1	06.7	84	44	86	71	-	0	SSE	2	-	0
16	764.2	762.6	764.0	05.2	17.4	08.0	08.6	19.0	05.0	01.3	06.1	07.3	07.4	91	49	92	77	-	0	SE	2	NF	1
17	764.4	763.3	764.1	05.2	18.4	08.2	10.0	18.5	04.8	01.2	06.1	07.3	07.5	91	46	92	76	-	0	SF	2	-	0
18	764.6	763.4	763.5	04.4	17.2	08.2	09.5	17.4	04.4	00.6	05.5	06.1	06.7	88	41	82	70	-	0	SSE	3	-	0
19	767.5	760.2	759.7	05.4	16.0	11.2	11.0	16.9	05.3	01.5	06.2	06.4	06.3	91	50	93	78	-	0	-	C	W	2
20	761.6	761.1	762.5	10.4	15.0	09.8	12.4	19.1	09.5	06.5	08.4	08.2	08.4	86	50	93	76	N	2	SSE	2	-	0
21	761.7	761.0	759.8	08.0	12.6	05.6	10.0	14.0	07.9	05.0	06.6	07.9	07.9	82	72	88	81	-	0	-	C	-	0
22	759.8	754.7	761.0	08.2	15.8	07.6	09.9	16.2	07.7	06.6	06.9	06.8	07.1	85	50	90	75	-	0	SE	2	-	0
23	761.7	759.9	760.2	05.2	15.2	09.2	09.7	15.4	04.8	01.8	06.0	06.6	07.9	90	51	90	77	-	0	SE	2	-	0
24	759.8	759.8	760.5	05.0	11.8	08.2	08.3	12.0	05.0	01.5	05.9	07.2	07.5	90	69	92	84	-	0	-	O	-	0
25	761.1	760.1	758.1	07.4	09.6	09.4	09.0	10.8	06.8	02.5	07.1	07.2	08.3	92	81	94	85	-	0	-	C	NE	1
26	753.4	753.2	755.1	11.2	11.6	07.0	09.2	14.8	07.0	08.3	09.3	08.6	08.6	93	84	92	90	NE	2	KNE	3	-	0
27	754.3	751.9	752.5	05.8	08.2	08.6	07.9	09.2	05.0	02.5	06.3	07.1	07.3	92	87	87	89	-	0	NNW	2	N	4
28	750.6	747.3	741.0	08.9	10.4	14.6	12.1	14.7	08.1	05.7	07.1	08.0	09.2	83	85	74	81	-	0	-	0	SSE	6
29	747.0	748.3	752.1	06.2	14.0	06.8	08.4	15.6	05.5	02.5	03.7	03.6	06.5	52	30	88	57	N	3	S	2	-	0
30	753.6	756.8	759.4	04.5	12.2	07.3	07.6	12.6	04.0	00.6	05.1	04.7	03.2	81	44	41	55	N	2	S	1	NNW	4
MES.	759.4	758.8	750.4	07.0	14.0	08.6	09.7	15.1	06.3	03.0	06.2	06.5	06.9	82	55	81	73	1.0	1.7	1.3			
VRFD.	750.4	750.8	760.4	03.5	11.0	05.7	06.6	12.2	02.5	-00.4	04.5	04.7	04.7	82	55	81	73	1.0	1.7	2.2	2.0		

1	760.1	762.6	764.3	03.4	06.0	03.0	03.8	09.0	02.5	-02.0	04.0	06.0	05.3	68	86	94	83	NW	3	-	C	-	0
2	764.7	764.6	765.0	00.8	10.0	05.6	05.5	10.6	00.5	-02.5	04.5	05.0	05.6	93	54	82	76	-	0	-	C	-	0
3	765.8	764.9	765.3	05.8	14.4	09.8	10.0	15.6	05.5	03.5	05.8	05.9	06.1	83	48	67	66	NNE	1	SSE	2	-	0
4	764.2	762.2	761.0	05.8	17.5	10.2	10.9	18.2	05.0	01.7	06.1	05.7	05.1	89	38	55	61	-	0	NNE	4	-	0
5	759.0	756.5	756.1	04.4	14.8	06.0	07.8	15.0	03.3	-01.0	05.2	04.6	06.2	82	37	89	69	-	0	SE	1	-	0
6	755.7	756.7	758.8	05.6	12.4	06.8	07.9	13.0	05.0	01.8	06.2	03.6	02.7	92	34	37	54	-	0	N	6	N	3
7	759.4	757.9	758.3	00.0	09.2	05.4	05.0	10.5	-00.4	-04.2	03.9	03.9	04.8	96	44	72	67	-	0	-	C	NE	2
8	757.9	756.8	756.4	04.6	08.0	06.4	06.4	08.4	03.8	-00.6	05.4	06.6	06.7	85	82	83	87	-	0	-	O	-	0
9	757.3	757.6	760.1	03.8	14.0	11.2	10.0	16.0	02.6	-00.4	05.3	05.0	04.6	88	42	46	59	WNW	1	NNW	2	N	3
10	761.4	761.3	762.2	02.4	14.4	04.8	06.6	14.7	02.0	-01.1	04.9	05.6	05.9	90	45	91	75	-	0	-	O	-	0
11	762.5	759.9	757.6	02.2	11.2	07.8	07.2	12.3	01.8	-01.3	04.8	05.4	06.7	90	54	85	76	-	0	-	C	-	0
12	753.5	752.4	750.9	09.8	10.0	10.8	10.4	12.0	07.0	07.0	07.6	07.7	07.6	83	83	78	81	SE	6	SE	5	SE	6
13	748.4	748.1	749.2	08.8	10.0	06.7	08.0	11.7	06.7	08.0	07.6	07.5	06.7	90	81	91	87	SE	3	SE	2	E	4
14	750.0	751.0	751.6	07.4	07.6	06.4	07.0	10.4	06.2	04.5	03.3	03.0	02.7	43	39	37							

BR. ST. 248

$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vremenska interv.	Oblačnost N (0—10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	09	07	08.7	01.8	24.0	.	17-8 <sup>30</sup> 0-1 <sup>20</sup> 8 <sup>10</sup> 13 <sup>10</sup> 14 <sup>20</sup> FN 16 <sup>44</sup> 24 <sup>44</sup> 17 <sup>20</sup> 20, F 18 <sup>40</sup> 21 <sup>05</sup> , D 21.21 <sup>45</sup>	
2	9	03	00	06	03.0	02.8	21.2	.	F <sub>N</sub> 0-1 <sup>30</sup>	
3	8	10	07	10	09.0	03.6	00.4	.	0-1 <sup>20</sup> 3 <sup>10</sup>	
4	8	07	10	04	07.0	02.1	.	.	0-1 <sup>10</sup> 8	
5	7	09	10	10	05.7	01.8	.	.	.	
6	8	08	08	10	08.7	03.5	00.3	.	0-2 <sup>10</sup> 2 <sup>40</sup>	
7	7	10	10	10	10.0	00.0	.	.	0-1 <sup>8</sup> 14 <sup>10</sup> , 18-24 <sup>10</sup>	
8	9	06	07	00	04.3	09.4	04.5	.	0-1, F <sub>NNE</sub> 8 <sup>45</sup> 24, F <sub>NNNE</sub> 11-23 <sup>49</sup>	
9	8	06	04	00	03.3	08.3	.	.	F <sub>NNNE</sub> 0-23 <sup>40</sup> , F <sub>NNNE</sub> 0-08 20 <sup>08</sup>	
10	9	00	00	00	00.0	09.4	.	.	0-1 <sup>10</sup> 24	
11	8	00	00	00	00.0	09.1	.	.	0-1 <sup>0</sup> 8, 19 <sup>30</sup> 24	
12	9	02	07	05	05.3	06.9	.	.	0-1 <sup>0</sup> 8, 19 <sup>30</sup> 24	
13	8	05	08	02	05.0	01.7	.	.	0-1 <sup>0</sup> 8, 19 <sup>30</sup> 24	
14	9	03	02	00	01.7	09.0	.	.	0-1 <sup>0</sup> 8, 19 <sup>30</sup> 24	
15	8	00	00	00	00.0	08.8	.	.	0-1 <sup>0</sup> 8, 19 <sup>30</sup> 24	
16	9	00	00	00	00.0	09.1	.	.	0-1 <sup>0</sup> 7 <sup>30</sup> 19 <sup>30</sup> 24	
17	9	05	06	03	04.7	08.9	.	.	0-1 <sup>0</sup> 7 <sup>30</sup> 19 <sup>30</sup> 24	
18	8	02	07	00	03.0	08.7	.	.	0-1 <sup>0</sup> 6-17 <sup>30</sup> 20-24, D 17 <sup>45</sup> 18	
19	9	08	08	10	08.7	04.1	.	.	0-1 <sup>0</sup> 8, 0-11 <sup>50</sup> 16 <sup>40</sup> , 0-13 <sup>0</sup> 14 <sup>20</sup> , 21 <sup>00</sup> 24	
20	9	10	04	03	05.7	06.3	01.1	.	0-1 <sup>0</sup> 20 <sup>10</sup> 24	
21	6	07	10	10	09.0	00.9	.	.	0-1 <sup>0</sup> -8, 0-1 <sup>50</sup> 16 <sup>40</sup> , 0-13 <sup>0</sup> 14 <sup>20</sup> , 21 <sup>00</sup> 24	
22	8	07	06	04	05.7	07.2	18.6	.	0-1 <sup>0</sup> -6 <sup>10</sup> , 0-1 <sup>30</sup> 24	
23	9	03	03	04	03.3	08.0	.	.	0-1 <sup>0</sup> -7 <sup>30</sup> 20 <sup>00</sup> 24	
24	9	03	04	04	05.3	00.5	.	.	0-1 <sup>0</sup> -7 <sup>30</sup> 19 <sup>30</sup> 24	
25	8	10	10	10	10.0	00.0	00.4	.	0-0 <sup>00</sup> 2, 0-0 <sup>00</sup> 24, F <sub>ESE</sub> 22 <sup>30</sup> 23 <sup>40</sup> , 23 <sup>37</sup>	
26	6	10	10	10	06	08.7	00.5	62.2	.	
27	6	10	10	10	10.0	00.0	06.3	.	0-1 <sup>0</sup> -7 <sup>30</sup> 22 <sup>05</sup> 22 <sup>09</sup>	
28	8	10	10	10	10.0	00.0	23.7	.	0-1 <sup>0</sup> -7 <sup>30</sup> 18 <sup>45</sup> , S 20 <sup>55</sup> 22 <sup>32</sup>	
29	8	02	01	10	04.3	08.1	12.9	.	0-1 <sup>0</sup> -7 <sup>30</sup> 19 <sup>05</sup> 22 <sup>00</sup> , F <sub>N-S</sub> WNW 0 <sup>34</sup> 2 <sup>54</sup> , 19 <sup>14</sup> 19 <sup>40</sup>	
30	8	08	00	00	02.7	03.6	00.9	.	0-1 <sup>0</sup> -6 <sup>30</sup> , 0-1 <sup>48</sup> 24	
MES. VRED.		05.8	05.9	05.0	05.6	150.4	156.6			

TITOGRAĐ

1974 DECEMBER

1	8	08	10	05	07.7	00.0	.	.	0-1 <sup>50</sup> 12 <sup>30</sup>
2	8	05	03	07	05.0	02.6	01.1	.	0-1 <sup>0</sup> 7 <sup>10</sup>
3	8	08	05	10	07.7	05.5	00.2	.	F <sub>N</sub> 15 <sup>10</sup> 15 <sup>55</sup> L
4	9	04	06	00	03.3	05.7	.	.	F <sub>N</sub> 10 <sup>40</sup> 11 <sup>48</sup> L
5	9	04	02	00	02.0	08.6	.	.	.
6	8	10	05	00	05.0	04.0	.	.	0-1 <sup>0</sup> -7 <sup>30</sup> , 0-1 <sup>45</sup> 8 <sup>40</sup> F <sub>N</sub> 8 <sup>20</sup> 14 <sup>50</sup> , F <sub>N</sub> 8 <sup>56</sup>
7	9	07	08	00	05.0	04.0	01.1	.	0-12 <sup>35</sup> 18 <sup>40</sup>
8	7	07	10	05	07.3	00.0	.	.	0-19 <sup>-</sup> n
9	8	03	08	04	05.0	05.9	00.4	.	0-19 <sup>-</sup> n
10	9	00	00	00	00.0	00.0	08.5	.	.
11	7	00	09	10	06.3	04.1	.	.	0-1 <sup>0</sup> -8, 0-2 <sup>20</sup> 18 <sup>00</sup> L, n-7 <sup>30</sup> F <sub>ESE</sub> 5 <sup>53</sup> 24, 10 <sup>40</sup> 15 <sup>30</sup> F <sub>ESE</sub> 22 <sup>50</sup> 23 <sup>29</sup>
12	5	10	10	08	05.3	00.0	17.6	.	F <sub>ESE</sub> 0-1 <sup>40</sup> 12 <sup>00</sup> L, F <sub>ESE</sub> 12 <sup>00</sup> 24, 0-1 <sup>0</sup> 10 <sup>20</sup> 21 <sup>30</sup> L, n-14 <sup>45</sup> 15
13	8	10	10	10	10.0	00.5	24.2	.	F <sub>N</sub> 12 <sup>20</sup> 20 <sup>05</sup> L, F <sub>N</sub> 20 <sup>05</sup> 24, F <sub>N</sub> 0-23 <sup>40</sup> L, F <sub>N</sub> 20 <sup>05</sup> 24
14	9	10	07	03	06.7	00.0	07.3	.	.
15	8	09	05	03	05.7	03.6	.	.	F <sub>N</sub> 0-23 <sup>40</sup> L, F <sub>N</sub> 20 <sup>05</sup> 24
16	9	04	04	00	02.7	07.6	.	.	F <sub>N</sub> 0-23 <sup>40</sup> L, F <sub>N</sub> 6 <sup>44</sup> 17 <sup>25</sup>
17	9	00	05	08	04.3	07.5	.	.	0-2 <sup>0</sup> 6 <sup>50</sup> 20 <sup>00</sup> L, 0-12 <sup>30</sup> n, F <sub>NW</sub> 18 <sup>50</sup> 20 <sup>34</sup>
18	6	10	10	08	05.3	00.0	23.3	.	n-8 <sup>30</sup> , F <sub>N</sub> 8 <sup>20</sup> 12 <sup>30</sup> L, F <sub>N</sub> 17 <sup>30</sup> n, F <sub>NW</sub> 18 <sup>50</sup> 20 <sup>34</sup>
19	9	03	03	00	02.0	08.5	23.3	.	.
20	8	00	04	00	01.3	07.2	.	.	.
21	8	03	03	00	02.0	08.5	.	.	0-1 <sup>0</sup> -7 <sup>30</sup>
22	9	00	00	00	00.0	08.3	.	.	0-1 <sup>0</sup> -8 <sup>30</sup>
23	8	00	00	00	00.0	08.6	.	.	0-1 <sup>0</sup> -8 <sup>30</sup> 22 <sup>40</sup>
24	8	02	00	00	00.7	08.5	.	.	0-1 <sup>0</sup> -10 <sup>20</sup> 20 <sup>40</sup>
25	9	00	06	08	04.7	07.6	.	.	0-1 <sup>0</sup> -10 <sup>20</sup> 20 <sup>40</sup>
26	9	03	02	08	04.3	07.7	.	.	0-1 <sup>0</sup> -8 <sup>30</sup> 22 <sup>40</sup> , F <sub>N</sub> 20 <sup>10</sup> 21 <sup>45</sup>
27	8	10	00	08	06.0	07.6	.	.	F <sub>N</sub> 14 <sup>40</sup> 17 <sup>48</sup> L, F <sub>N</sub> 21 <sup>30</sup> 22 <sup>40</sup>
28	9	08	02	05	05.0	05.2	.	.	0-1 <sup>0</sup> -8, 19 <sup>-</sup> n
29	8	03	06	02	03.7	04.0	.	.	0-1 <sup>0</sup> -7 <sup>30</sup> 14 <sup>45</sup> 14 <sup>45</sup> F <sub>N</sub> 14 <sup>45</sup> 24, 0-17 <sup>05</sup> 18 <sup>40</sup>
30	9	02	06	10	06.0	04.1	.	.	0-1 <sup>0</sup> -7 <sup>30</sup> 14 <sup>45</sup> 14 <sup>45</sup> F <sub>N</sub> 14 <sup>45</sup> 24, 0-17 <sup>05</sup> 18 <sup>40</sup>
31	7	10	10	05	08.3	00.0	00.0	.	F <sub>N</sub> 0-23 <sup>40</sup>
MES. VRED.		04.9	05.1	04.1	04.7	153.9	75.2		

$\varphi = 41^{\circ}57'$  N  $\lambda = 21^{\circ}38'$  E Gr.  $\Delta G = +1h\ 27\ min.$

BR. ST. 268

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min S cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	748.0	747.5	747.6	04.2	05.8	05.6	05.3	06.1	04.0	03.9	06.1	06.7	06.6	98	97	97	97	-	0	-	C	-	0	
2	747.0	746.7	747.1	05.7	08.2	06.4	06.7	08.5	05.4	05.3	06.7	07.3	06.6	97	90	92	93	ENE	1	SSE	2	SSE	2	0
3	746.6	745.7	747.3	06.4	06.8	07.0	07.3	09.5	06.1	05.6	06.0	06.4	05.9	84	75	79	79	SSE	3	S	2	SSF	2	0
4	748.5	749.0	750.4	05.4	08.0	05.8	06.2	08.0	05.2	05.0	06.2	05.4	05.7	91	67	P2	80	SE	1	ESE	2	ENE	1	0
5	749.9	748.7	749.7	04.4	07.2	07.2	04.0	07.4	01.5	03.8	05.4	04.9	04.8	85	64	R9	79	NNE	1	-	0	-	0	0
6	746.7	744.0	744.0	-00.2	04.9	03.6	03.0	05.1	-02.2	-04.1	04.4	05.1	05.6	96	78	94	89	-	0	-	0	-	0	0
7	743.8	743.8	745.6	03.4	06.4	04.2	04.6	06.6	03.4	02.1	05.7	05.9	05.3	97	81	85	68	-	0	SSE	2	NNE	3	0
8	745.7	745.0	745.7	02.4	05.8	02.6	03.4	05.8	02.3	02.1	04.4	04.6	05.2	81	66	94	80	ENE	2	NNE	2	NW	1	0
9	747.1	747.3	746.7	01.8	04.4	03.4	03.2	05.0	01.4	01.4	04.5	04.4	04.9	87	71	85	81	NE	2	NNE	1	SSE	2	0
10	745.3	745.5	746.7	02.6	02.6	02.4	02.5	03.4	02.4	02.5	04.8	04.9	04.8	87	89	89	88	SSE	3	S	3	S	1	0
11	748.2	749.1	751.1	01.0	04.0	02.8	02.4	05.0	00.5	00.2	04.6	05.0	05.2	93	82	94	90	SE	2	SSE	2	-	0	0
12	751.5	750.2	749.9	02.2	04.4	00.2	01.8	04.6	-06.2	01.6	05.0	04.0	04.3	93	74	93	87	-	0	NW	2	WNW	2	0
13	748.8	747.4	749.1	03.0	04.6	-01.5	01.2	05.3	-01.5	-01.4	04.1	03.8	03.1	72	60	75	69	N	5	N	7	E	1	0
14	750.7	749.9	749.9	-03.8	02.2	-03.2	-02.0	02.9	-05.4	-07.2	02.6	02.0	02.9	74	48	81	68	NNE	2	W	1	NE	2	0
15	750.2	749.4	749.5	-06.8	01.4	-04.1	-03.4	02.6	-07.7	-09.6	02.5	03.8	02.9	91	75	86	84	E	1	W	1	SE	1	0
16	749.9	748.6	747.9	-06.7	01.4	00.0	-01.3	03.0	-07.0	-10.6	02.6	03.4	03.8	92	67	82	80	SE	2	-	0	-	0	0
17	744.7	742.5	742.4	-05.0	04.7	01.4	00.6	05.7	-05.0	-07.2	02.7	03.6	04.2	87	56	83	75	-	0	NW	1	N	2	0
18	742.1	741.1	742.1	03.4	03.6	02.2	02.8	06.5	00.6	00.0	04.8	04.4	03.8	82	74	71	76	NNW	3	N	6	NNW	3	0
19	743.5	743.8	744.2	02.2	04.6	01.1	02.2	06.1	01.0	01.5	03.5	04.3	03.9	65	67	78	70	NW	3	NW	4	NE	4	0
20	741.3	740.3	742.0	00.6	08.0	07.8	06.0	09.4	00.1	-01.0	04.5	05.8	05.5	93	72	70	78	-	0	NNE	2	NNW	5	0
21	744.2	744.8	746.8	06.6	07.3	05.4	06.3	08.2	05.3	04.3	04.8	04.8	05.0	66	60	75	67	N	4	NNW	3	NNE	2	0
22	747.7	748.1	749.5	06.4	09.2	06.6	04.2	10.1	06.6	03.9	04.5	04.6	04.3	63	53	89	68	WNW	2	NNW	1	-	0	0
23	749.6	747.7	746.7	-05.0	05.4	00.8	00.5	06.8	-05.4	-07.9	02.7	04.8	04.4	87	72	90	83	-	0	N	2	E	2	0
24	745.9	745.6	745.9	00.4	04.7	01.9	02.2	05.3	00.1	-01.0	04.6	04.5	04.5	96	70	85	84	NNW	1	NNW	3	N	3	0
25	745.5	744.0	745.4	-04.4	03.7	-01.4	-00.9	05.2	-04.8	-07.0	03.2	04.4	03.7	96	74	90	87	-	0	ESE	1	ESE	1	0
26	746.3	746.3	747.0	-01.6	07.1	-00.6	01.1	08.5	-02.0	-03.5	03.9	04.5	04.0	96	59	91	82	ESE	1	SE	1	-	0	0
27	747.0	744.5	744.7	-05.0	06.2	-02.6	-01.0	07.4	-06.0	-08.3	02.9	04.6	03.6	93	65	96	85	E	1	W	1	-	0	0
28	745.6	745.0	745.9	-05.3	05.4	-00.5	-00.4	07.6	-06.5	-08.6	02.9	04.5	03.9	95	67	90	84	S	1	-	0	-	0	0
29	747.2	746.0	746.9	-04.4	08.4	-02.0	00.0	09.6	-05.6	-07.4	03.0	05.0	03.6	92	61	92	82	-	0	WSW	1	S	1	0
30	749.4	749.8	751.3	-05.0	07.0	-00.2	00.4	09.0	-06.0	-08.0	03.2	04.4	04.2	100	65	93	86	-	0	WSW	1	SSE	1	0
31	752.6	751.1	751.3	-00.5	08.1	00.0	C1.9	08.7	-02.4	-05.7	04.1	04.8	03.9	93	59	86	79	-	0	SSW	2	SE	1	0
MES.	WRED. 747.1 746.4 747.1 00.3 05.6 01.6 02.3 06.5 -00.9 -01.8 04.2 04.8 04.5 86 70 86 81 1.3 1.8 1.4																							

## 1974 FEBRVAR

## SKOPJE - PETROVAC

1	750.5	748.0	748.3	-04.0	07.2	-01.4	06.1	09.4	-05.7	-08.2	03.1	04.3	03.8	92	57	91	80	SE	1	W	1	-	0
2	749.0	747.2	748.1	-04.8	07.2	-02.2	-00.5	09.2	-06.5	-08.6	02.9	04.3	03.7	91	57	96	81	-	0	WNW	1	E	1
3	748.8	746.8	746.2	-05.1	09.2	04.5	03.3	10.6	-05.8	-07.9	03.0	05.4	05.3	95	62	84	80	-	0	WNW	1	N	2
4	743.0	740.6	738.3	06.0	05.6	05.4	05.6	10.6	00.9	-00.7	06.0	06.2	05.8	86	92	86	88	SSE	1	NNW	2	SSE	4
5	737.5	737.1	736.1	02.0	05.4	03.7	03.7	06.0	00.7	-00.6	05.1	06.0	05.7	97	85	95	94	-	0	-	0	-	0
6	733.8	730.4	727.5	03.0	09.2	05.4	07.8	10.7	02.8	02.8	05.5	06.8	05.2	97	78	59	78	-	0	WNW	1	SSE	3
7	720.8	720.8	724.5	10.4	09.2	04.0	C6.9	13.0	04.0	07.5	05.8	06.0	05.0	61	69	82	71	S	5	WNW	5	NNE	2
8	730.5	735.5	741.5	03.2	06.4	02.0	C3.0	08.8	04.5	-00.1	04.6	04.0	04.2	80	55	75	70	NNE	4	N	5	N	2
9	745.4	745.5	746.1	-02.8	08.3	-00.4	01.2	09.8	-03.3	-06.0	03.1	03.4	03.8	83	41	85	70	NE	2	NNW	2	-	0
10	746.1	744.9	745.6	-03.1	10.7	00.8	02.2	12.0	-04.6	-07.3	03.3	04.2	04.1	91	45	P4	73	SE	1	-	0	-	0
11	745.4	742.4	741.4	-03.1	12.8	00.4	02.6	14.6	-03.6	-06.7	03.3	04.6	03.9	91	42	82	72	-	0	SW	1	-	0
12	741.2	738.4	738.0	-03.2	12.4	C1.9	03.2	14.3	-04.0	-07.0	03.4	06.2	04.6	93	57	87	79	SE	1	NNW	1	-	0
13	737.7	736.1	736.6	00.3	11.0	0																	

BR. ST. 268

$$H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$$

Dan	Vjetrost 0-9	Oblačnost N (0-10)					Intencija broj sat	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	3	10≡	10≡	10•	10.0	CC.0	C3.0	.	.	$\equiv^{0-10-4^0} \equiv^{0-14^0} 24, \equiv^{0-4^0} 8^0 24, \equiv^{0-18^0} 10^0 19^0 20^0$
2	7	10	10•	09	05.7	CC.0	C2.1	.	.	$\equiv^{0-9^0} \equiv^{0-17^0} 24, \equiv^{0-10^0} 3^0 24$
3	7	10	06	09	C9.3	CC.6	C1.6	.	.	.
4	7	10	10	10	10.0	00.0	.	.	.	$\equiv^{7^0} 15, 21^0 24, \square^{0-17^0} 20^0$
5	6	10	10	04	CC.0	CC.0	.	.	.	.
6	6	10	08	10	05.3	00.0	.	.	.	$\equiv^{0-24} \equiv^{0-10} 10, \equiv^{0-10^0} 4^0 24$
7	6	10•	10	10•	10.0	CC.0	C0.1	.	.	$\equiv^{0-16^0} 24, \equiv^{0-15^0} 21^0$
8	7	10	10	10•	10.0	00.0	01.8	.	.	.
9	6	10	10	10	10.0	00.5	04.3	.	.	$\equiv^{0-10^0} 18^0, \equiv^{0-17^0} 8^0 24, \equiv^{0-20^0} 20^0, \equiv^{0-19^0} 24^0$
10	6	10	10•	10•	10.0	CC.0	.	.	.	.
11	7	10•	10	10	10.0	CC.8	C5.0	.	.	$\equiv^{0-10-10^0} 24, \equiv^{0-12^0} 3^0 24, \equiv^{0-13^0} 4^0, \equiv^{0-14^0} 24$
12	7	10	10	10	10.0	00.0	00.2	.	.	$\equiv^{0-12^0} K^{20^0} 17^0 24, F_N 21^0 24^0$
13	7	10	06	00	05.3	01.6	.	.	.	$F_N 6^0 10^0 14^0 24, \equiv^{0-12^0} 24$
14	7	00	00	00	00.0	00.0	07.8	.	.	$\equiv^{0-12^0} 10^0 22^0 24, \equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24$
15	6	02	03	03	02.7	06.7	.	.	.	.
16	6	03	10	10	07.7	05.0	.	.	.	$\equiv^{0-24} \equiv^{0-10-12^0}$
17	7	00	09	10*	06.3	03.2	.	.	.	$\equiv^{0-12^0} 18^0 24, \equiv^{0-10^0} 24, \equiv^{0-13^0} 24, \equiv^{0-14^0} 24$
18	7	10	08*	06	08.0	C1.1	C1.8	.	.	$\equiv^{0-3^0} 4^0 11^0 12^0 24, \equiv^{0-13^0} 14^0 24, \equiv^{0-14^0} 24$
19	7	08	09	C7	08.0	02.1	00.0	.	.	$\equiv^{0-6^0} 5^0 13^0 15^0 24, \equiv^{0-17^0} 11^0 16^0 17^0, \equiv^{0-18^0} 22^0$
20	8	10•	09	07	08.7	00.1	00.0	.	.	.
21	8	08	10	10	05.3	CC.0	CC.1	.	.	$\equiv^{0-10^0} 25^0, \equiv^{0-15^0} 13^0 F_{NNE} 3^0 4^0 6^0, \equiv^{0-13^0} 10^0$
22	7	09	09	00	06.0	CC.9	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-12^0} 15^0 24, \equiv^{0-14^0} 24$
23	7	06	08	10	08.0	01.4	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-12^0} 15^0 24, \equiv^{0-14^0} 24$
24	7	10*	05.0	C7	07.3	C1.5	15.8	04	.	.
25	6	01	06.0	02	03.0	04.5	CC.0	.	.	$\equiv^{0-20^0} 25^0, \equiv^{0-22^0} 24, \equiv^{0-24^0} 24$
26	6	06	03.0	00	C3.0	C3.5	.	.	.	$\equiv^{0-4^0} \equiv^{0-9^0} 20^0 24$
27	7	02	00.0	00	CC.7	C7.5	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
28	6	01	02.0	00	C1.0	C5.9	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
29	6	08	01.0	00	03.0	07.5	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
30	6	00	02.0	00	C0.7	C6.6	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
31	6	09	05.0	08	07.3	05.4	.	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
MES. WRED.		07.2	07.2	06.2	06.9	75.4	25.9			

## SKOPJE - PETROVAC

1974 FEBRUAR

1	6	02	02.0	00	01.3	C7.3	.	.	$\equiv^{0-10-9^0} 24, \equiv^{0-16^0} 20^0 24$
2	5	02	02.0	00	01.3	C6.7	.	.	$\equiv^{0-10^0} \equiv^{0-24^0} \equiv^{0-12^0}$
3	6	00≡	01.0	06	C2.3	C5.5	.	.	$\equiv^{0-6^0} 6^0 10^0 12^0 24, \equiv^{0-19^0} 10^0 16^0 24$
4	6	10	10•	08	C9.3	C1.0	.	.	$\equiv^{0-11^0} 12^0 \equiv^{0-3^0} 24, \equiv^{0-13^0} 24, \equiv^{0-14^0} 24$
5	6	10≡	10	10	CC.0	00.0	08.8	.	.
6	6	10≡	03	10	07.7	03.4	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
7	7	10	10•	06	08.7	00.0	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
8	8	09	09•	05	07.7	C5.5	C3.5	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
9	8	01	01.0	02	01.3	C9.2	00.0	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
10	7	08	07.0	00	05.0	C8.6	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
11	7	00	00.0	00	CC.0	C8.8	.	.	$\equiv^{0-10^0} 9^0 20^0 24$
12	7	00	01.0	00	CC.2	C8.2	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
13	6	10	08.0	10	09.3	01.9	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
14	7	10	10•	10	10.0	CC.3	00.0	02.1	.
15	7	10•	10•	10•	10.0	00.0	02.1	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
16	5	10≡	07	03	06.7	C2.0	38.2	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
17	7	05	08	05	06.0	C6.7	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
18	7	10	05	10	05.7	CC.7	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
19	7	10	09	10	05.7	01.0	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
20	6	10•	10•	08	C9.3	00.0	15.2	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
21	7	08	08	07	07.7	02.4	12.0	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
22	7	10	06	10	C9.7	C2.5	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
23	7	10	05	08	CC.0	01.0	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
24	7	10	09	10	10.0	CC.1	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
25	7	10	10	10	CC.0	CC.2	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
26	7	10	06	10•	05.7	00.1	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
27	8	10	06	C5	08.0	03.1	00.0	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
28	7	C9	01.0	00	C3.3	C8.6	.	.	$\equiv^{0-10^0} 10^0 24, \equiv^{0-13^0} 24, \equiv^{0-16^0} 24$
MES. WRED.		07.6	06.8	C6.2	06.9	96.5	79.4		

$\varphi = 41^{\circ}57'$ , N  $\lambda = 21^{\circ}38'$ , E Gr.  $\Delta G = +1h\ 27\ min.$ 

BR. ST. 268

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)							
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	744.9	742.5	742.4	-05.0	07.0	-00.8	00.1	08.6	-05.4	-08.6	03.0	03.0	03.4	95	40	78	71	-	0	ENE 1	-	0		
2	741.5	739.2	739.6	-05.0	08.4	04.6	03.2	09.6	-05.0	-08.0	02.9	03.4	02.8	91	41	60	64	-	0	S 1	SSE 1			
3	741.7	743.9	746.7	-03.7	06.6	04.6	04.9	07.1	03.6	01.4	04.4	05.4	05.0	74	73	76	75	SSE 2	SSF 4	SSF 2				
4	748.5	748.3	748.3	02.6	07.7	05.2	05.2	08.2	06.3	-01.7	05.0	05.4	05.9	90	68	64	82	-	0	SSE 3	SSE 3			
5	746.4	744.5	742.9	05.0	07.0	05.0	05.4	07.0	04.8	04.2	05.8	05.8	05.7	86	75	87	85	SE 3	SE 4	SE 4	SSE 4			
6	739.6	736.6	739.5	05.0	04.4	03.6	04.2	05.7	03.6	04.5	05.8	05.5	06.4	86	84	91	88	SE 2	NNE 3	NF	2			
7	739.0	740.4	742.0	03.2	04.0	02.4	03.0	04.6	02.4	-02.4	05.2	05.0	04.1	91	82	74	82	N 1	NNE 4	NNE 4				
8	742.9	743.0	743.4	01.4	03.4	00.8	01.6	04.3	04.8	-00.2	04.2	04.9	04.6	83	85	95	88	NNE 2	-	0	ESE 1			
9	743.7	743.6	745.1	01.6	05.2	06.0	04.9	07.0	00.4	00.2	05.0	05.8	06.3	97	83	90	90	-	0	NW 2	SE 2			
10	744.9	744.3	744.6	05.0	08.9	06.0	06.5	09.4	04.4	04.1	05.8	05.4	05.1	88	63	73	75	E 2	SSE 2	NNE 3				
11	745.2	746.2	747.7	04.0	08.4	04.7	05.4	09.2	03.5	03.4	04.5	04.7	04.8	72	57	75	68	N 2	WW 2	NE 5				
12	748.9	747.7	747.1	02.8	09.7	01.4	03.7	09.4	01.4	02.8	04.4	05.2	04.4	78	60	87	75	NNE 4	WW 2	-	0			
13	745.7	745.2	740.9	-01.9	12.6	03.0	04.2	14.0	-02.4	-05.4	03.7	04.7	04.6	92	43	81	72	-	0	SW 2	E 1			
14	738.9	734.1	732.7	00.8	10.5	08.4	07.0	11.3	00.0	-02.0	04.4	05.1	04.3	90	53	52	65	ENE 1	NW 2	N 3				
15	731.3	732.1	733.6	03.8	06.8	05.0	05.2	08.4	02.7	03.6	05.6	05.4	05.9	92	72	90	85	NNW 1	WW 1	NNE 2				
16	734.2	734.9	736.4	03.8	07.8	04.4	05.1	08.7	03.8	03.5	05.1	04.8	05.2	85	60	82	76	NNE 3	NE 1	NNE 2				
17	737.2	736.9	739.7	-00.6	14.5	05.6	06.3	16.3	-01.7	-03.8	04.2	04.6	05.1	94	37	75	69	ENE 1	W 2	ESE 2				
18	742.6	740.9	741.9	00.9	18.6	11.8	10.8	21.1	-00.6	-03.0	04.3	05.8	05.9	88	36	57	60	-	0	S 1	SE 2			
19	745.3	743.5	744.7	02.1	20.6	14.0	12.8	23.0	01.7	-00.8	04.9	06.3	06.3	92	34	53	60	ESE 1	W 1	ESE 2				
20	747.1	744.9	745.6	04.6	22.6	10.8	12.2	24.2	03.0	00.0	05.8	06.4	07.0	91	31	72	65	-	0	NW 1	E 1			
21	747.1	744.7	745.6	06.7	23.6	11.2	13.2	25.2	04.6	01.7	06.3	06.9	06.9	85	32	65	62	-	0	WSW 1	-	0		
22	746.1	742.9	742.4	05.2	23.0	10.6	12.5	25.9	03.4	01.0	06.1	06.0	06.5	89	28	68	62	-	0	ESE 1	E 1			
23	743.9	741.7	742.2	06.0	23.2	14.1	14.4	25.2	04.6	01.9	06.2	05.4	06.6	89	28	55	57	-	0	SSW 1	ESE 1			
24	745.6	743.5	744.7	06.0	22.0	16.2	15.4	22.9	04.7	02.4	06.6	07.2	07.9	89	36	57	61	NE 1	S 3	SE 4				
25	746.0	744.2	742.9	07.9	19.0	13.0	13.2	19.9	06.2	04.2	07.1	07.0	07.3	89	43	65	65	NE 1	SSW 3	S 3				
26	746.1	742.4	741.7	05.8	17.6	10.6	11.6	18.7	06.9	04.1	07.0	07.6	07.1	83	50	74	65	SSF 2	S 2	SE 3				
27	740.5	737.2	736.8	06.4	16.6	13.4	13.0	20.2	06.4	05.1	07.2	08.0	06.3	87	56	81	75	SE 2	-	0	NE 3			
28	740.3	739.6	742.7	07.0	20.4	11.6	12.6	20.8	05.1	03.0	07.1	08.5	09.5	95	47	73	78	-	0	SSF 2	W 2			
29	744.7	745.0	745.2	10.4	14.4	09.2	10.8	15.7	09.2	08.8	07.5	07.0	06.8	79	57	78	71	SSE 2	SSF 3	SSE 3				
30	747.5	747.0	746.7	08.6	11.3	09.7	10.6	13.6	08.0	06.6	06.7	06.8	05.3	80	65	58	68	SSE 3	SSE 5	SSE 2				
31	745.9	745.3	745.3	07.2	14.2	09.2	10.0	16.0	06.6	04.5	06.5	06.7	06.2	85	38	71	65	SSE 2	N 2	ESE 2				
MES.	WRED.			741.3	742.0	742.3	03.9	12.0	07.6	08.0	14.2	02.8	01.3	05.4	0F.7	05.9	87	54	74	72	1.2	2.0	2.1	

15/4 APRIL

SKOPJE - PETROVAC

1	740.7	733.4	740.6	04.6	15.6	10.7	10.2	16.0	03.5	00.6	05.9	05.5	04.5	91	42	46	60	-	0	ESE 2	E 3		
2	742.1	741.7	744.0	06.1	15.8	08.0	09.6	15.9	04.0	01.5	05.1	05.9	04.3	73	44	52	57	ESE 1	SW 1	ENE 2			
3	744.1	743.9	743.9	03.4	14.0	05.0	06.6	16.0	00.3	-02.4	04.1	03.0	04.0	70	25	61	52	NE 3	SSE 2	SSE 1			
4	744.3	741.3	741.0	02.7	14.6	07.4	09.3	15.9	-01.8	04.4	04.3	05.4	04.8	80	43	62	62	SE 1	SE 2	E 1			
5	742.2	740.2	740.9	03.2	16.2	11.2	10.5	16.4	00.1	-01.7	04.9	05.9	06.1	84	43	61	63	-	0	SE 2	SSE 4		
6	742.0	740.7	740.3	05.0	13.1	09.0	09.6	13.2	03.6	02.0	06.6	07.0	06.5	82	62	76	73	NF 1	SSE 3	SE 2			
7	741.1	738.3	739.0	06.0	16.2	13.1	12.1	16.4	04.4	02.9	06.4	05.0	04.5	92	36	35	56	-	0	W 2	NW 3		
8	738.3	739.0	739.2	10.0	10.3	08.8	09.5	13.3	06.1	05.0	05.4	06.5	06.0	59	69	71	66	W 2	WW 2	WW 2			
9	737.8	740.7	742.2	05.8	12.4	05.8	07.4	14.7	04.0	01.8	05.4	04.8	05.2	78	45	75	66	NE 1	N 4	NNE 2			
10	743.0	740.2	739.0	03.9	17.8	12.1	11.5	18.0	01.0	-01.7	04.7	04.6	05.2	76	30	49	52	ENE 1	SSW 1	SSE 3			
11	737.7	737.4	736.5	05.6	10.2	07.4	08.6	13.6	07.4	05.4	05.8	05.9	06.3	65	63	82	70	SSE 2	SE 4	SE 2			
12	735.1	734.2	734.9	07.8	14.2	05.8	10.4	14.8	06.1	05.3	07.1	07.1	07.8	90	59	86	78	-	0	SSE 2	SE 2		
13	736.1	734.2	734.4	08.2	19.7	11.2	12.6	21.2	07.8	05.6	07.9	07.4	07.0	97	43	70	70	E 1	S 2	E 1			
14	732.7	728.3	729.3	11.1	16.0	09.8	11.7	18.7	08.0	06.4	08.3	08.5	07.8	84	62	85</td							

BR. ST. 268

 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vrijednost G-9	Oblačnost N (0-10)					Insolitacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7 03	C20	00	01.7	07.4	.	.	.	.	$\square^{0-1} 0-8^{30} 21^{30} 24_i = 8^{40} 11^{30} \square^{19^{30}} 21^{30}$
2	7 000	C30	10	04.3	07.2	.	.	.	.	$\square^{0-1} 0-8^{30} = 7^{40} 10^{15} \square^{18-21^{30}}$
3	7 10	05	10	05.7	01.1	00.0	.	.	.	$\bullet^0 6^{35} 11^{30}$
4	7 10	10	10	10.0	00.0	00.1	.	.	.	$\bullet^0 16^{30} 24_i$
5	7 100	100	10	10.0	00.0	00.2	.	.	.	$\bullet^0 0-22^{30}_i$
6	7 100	100	100	10.0	00.0	01.7	.	.	.	$\bullet^0 14^{10} 24_i, \bullet^0 17^{45} 8^{30} 22^{10} 23^{40}$
7	7 100	100	10	10.0	00.0	05.5	.	.	.	$\bullet^0 10-35^{30}_i, 10^{30} 18^{30} i, 10-18^{30} 10^{30}$
8	6 10	10	10*	10.0	00.0	00.3	.	.	.	$\times^0 16^{45} 11^{30} 20^{15} 23^{40}, 10^{30} 18^{30} 10^{30} 9^{15} 9^{15} 0-11^{30} 12^{10} 18^{12} 20^{15}, = 12^{10} 24$
9	5 100	100	10	10.0	00.0	06.1	.	.	.	$= 0-20^{30} \times^0 20^{30} 0-30 10^{30} 18^{30} i, \bullet^0 14^{35} 24^{30}_i$
10	7 10	090	10	05.3	00.4	00.7	.	.	.	$\bullet^0 10^{20} 10^{40}, \bullet^0 19^{30} 23^{30}$
11	7 10	05	10	05.7	00.0	00.1	.	.	.	$\bullet^0 10-35^{30} FNE 10^{30} 21^{30}_i$
12	7 10	05	00	06.0	02.9	.	.	.	.	$= 23^{30} 24$
13	7 000	020	00	00.7	08.8	.	.	.	.	$= 0-10^{30} 0-12^{30} 22-24$
14	6 10	10	100	10.0	00.2	.	.	.	.	$\square^{0-1} 0-7^{30} / 13^{30} 13^{40} 13^{30} FNE-NE 18^{30} 21^{32}_i, \bullet^0 21^{30} 24_i$
15	6 100	100	100	10.0	00.0	01.3	.	.	.	$\bullet^0 0-2-2 10^{30} 18^{30} 16^{25}_i$
16	7 100	10	09	05.7	00.0	01.8	.	.	.	$\bullet^0 0-13^{30} 10^{22} 13^{15}, 17^{30} 18^{10}, \bullet^0 14^{30} 21^{30} 17^{30}, \bullet^0 17^{30} 17^{30} 17^{30}$
17	7 09	020	00	03.7	08.4	00.0	.	.	.	$\square^{0-20^{30}} = 5^{30} 14^{30}$
18	7 030	030	00	02.0	19.2	.	.	.	.	$\triangle^0-5 24^{30} 24, \square^0 5-745$
19	8 050	010	00	02.0	09.9	.	.	.	.	$\triangle^0-2 0-8, 21^{30} 24$
20	8 000	040	02	02.3	09.3	.	.	.	.	$\triangle^0-4 0-8, 20^{30} 24$
21	9 070	010	00	02.7	10.8	.	.	.	.	$\triangle^0 0-8$
22	7 000	000	00	00.0	10.2	.	.	.	.	$\triangle^0 0-8^{45}$
23	7 010	010	01	01.0	10.4	.	.	.	.	$\triangle^0 0-20^{30} 24$
24	8 000	020	02	01.3	09.5	.	.	.	.	$\triangle^0 3-8^{45} FSE 21^{30} 20^{26}_i$
25	7 020	10	00	04.0	05.7	.	.	.	.	$\triangle^0 4-7^{30}$
26	7 10	010	01	04.0	07.6	.	.	.	.	$\triangle^0 3^{30} 13^{30} 21^{30} 24, \triangle^0 5^{30} 13^{20}$
27	6 10	030	100	07.7	05.4	.	.	.	.	$\triangle^0 0-10^{30} = 3^{30} 17^{23} 18^{30} T, 17^{23} 18^{30} T, 17^{23} 18^{30} 17^{33}, 17^{23} 18^{30} 17^{33}, 17^{23} 18^{30} 17^{33}, 17^{23} 18^{30} 17^{33}$
28	7 010	030	100	04.7	07.0	03.1	.	.	.	$= 5^{30} 17^{30}$
29	7 10	05	10	05.7	01.8	05.0	.	.	.	$FSE 12^{35} 14^{50}_i, \bullet^0 12-21^{10}$
30	7 10	10	10	10.0	00.0	00.2	.	.	.	$\bullet^0 6^{45} 8^{10}, 15-18^{30} i, FSE 14^{40} 16^{50}$
31	7 100	10	10	10.0	00.0	03.4	00.0	.	.	
MES.	VRED.	06.8	06.2	06.0	06.3	137.2	29.6			

## SKOPJE-PETROVAC

1974 APRIL

1	7 09	060	10	08.3	05.0	00.6	.	$\triangle^0 13^{30} 8^{30}$	
2	7 09	090	03	07.0	06.2	.	.	$\triangle^0 3^{20} 9^{30}$	
3	8 000	020	01	01.0	11.0	.	.	$\triangle^0 0-5 \square^0 5-6^{40}$	
4	7 07	08	00	05.0	09.1	.	.	$\square^0 2-4^{30} = 6^{30} 10^{45}, \bullet^0 10^{40} 16^{40}, FSE 18^{45} 20^{40}$	
5	7 000	09	09	06.0	07.5	.	.	$= 6^{30} 11^{30}, \bullet^0 19^{45} 23^{40}_i$	
6	7 10	10	100	10.0	00.2	.	.	$= 4^{30} 10^{40} FNE 10^{40} 10^{40}$	
7	7 09	09	10	05.3	05.4	00.4	.	$= 0-16^{20} 20^{40} 10^{35} 17^{45}_i, FNE 15^{30} 17^{30}$	
8	7 100	100	09	09.7	01.0	00.1	.	$FNE 8^{30} 16^{30}_i$	
9	8 06	06	03	05.0	06.2	01.9	.	$\triangle^0 3-6^{30}$	
10	8 000	070	10	05.7	08.0	.	.		
11	7 09	100	06	08.3	00.0	.	.	$\bullet^0 10^{10} 17^{40}$	
12	8 10	05	02	07.0	00.5	00.1	.	$= 6^{30} 8^{30} \bullet^0 44^{50} 17^{45}_i$	
13	7 08	08	00	05.3	06.8	00.8	.	$= 0-20^{30} FSE NNW 11^{10} 15^{40}_i, T, 13^{30} 14^{10} R, 14^{10} 15^{30}, \bullet^0 2-14^{20} 14^{33}, \bullet^0 14^{33} 17^{40}_i$	
14	7 050	10%	10	06.3	03.5	.	.	$\triangle^0 11^{20} 13^{35}, 18^{30} 19^{20}, FNE 17^{25} 18^{30} 19^{30}_i$	
15	7 100	100	10	10.0	00.0	16.4	.		
16	7 10	100	100	10.0	00.0	00.2	.	$\bullet^0 0-11^{40} 14^{40} 17^{25} 04_i$	
17	6 09	090	01	06.3	03.0	05.5	.	$= 4^{30} 11^{30} \bullet^0 14^{45} 16^{45}_i, 4^{30} 11^{30} 10^{40} 10^{40} 15^{40} 17^{45}_i, [T, 16^{45} 16^{45}, 19^{30} 21^{40}]$	
18	7 10	10	10	10.0	00.0	13.6	.	$= 4^{30} 10^{40} 12^{40}, 14^{30} 15^{40} FNE 16^{40} 17^{40}, \square^0 22^{30} 24$	
19	8 08	080	06	07.3	02.3	05.4	.	$\bullet^0 10^{45} 12^{40} 14^{40} 15^{40} 17^{40}_i$	
20	7 060	06	00	04.7	09.9	00.0	.	$\triangle^0 0-9^{30} 24_i, \triangle^0 10^{40} 10^{40}$	
21	7 08	050	04	05.7	07.9	.	.	$\triangle^0 0-4-1^{40} 17^{30} 10^{30}$	
22	7 10	06	10	08.7	04.8	00.0	.	$= 4^{30} 17^{30} \bullet^0 6^{45} 17^{30} 12^{40} 12^{40} 18^{45} 17^{45}_i, FNE 15^{30} 16^{40} 16^{40} 17^{40} 18^{40} 19^{40}_i$	
23	7 020	07	03	04.0	09.9	00.4	.	$= 1-10^{40} 18^{40}$	
24	7 040	040	10	06.0	09.6	.	.	$\triangle^0 5^{40} 24_i, FSE 14^{40} 15^{40}$	
25	7 10	100	100	10.0	00.0	00.0	.		
26	7 09	040	02	05.0	08.9	00.5	.	$\bullet^0 0-10^{40}$	
27	8 010	050	03	03.0	12.3	.	.	$\triangle^0 2-7^{20}$	
28	5 08	100	10	05.3	00.0	.	.	$\triangle^0 0-30^{40} \bullet^0-1-2 13^{30} 17^{45}_i$	
29	7 020	060	00	02.7	08.3	05.5	.	$= 4^{30} 5^{40} \triangle^0 10^{40} 12^{40}$	
30	7 020	10	06	06.0	07.5	.	.	$\triangle^0 0-7^{30} = 3^{30} 9^{40} FSE 9^{30} 20^{45}_i, \bullet^0 112^{10} 13^{30}, 18^{25} 19^{20}$	
MES.	VRED.	06.7	07.8	05.9	06.6	154.8	55.4		

$\varphi = 41^{\circ}57'$  N  $\lambda = 21^{\circ}38'$  E Gr.  $\Delta G = +1j 27$  min.

RR. ST. 268

D&T	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	727.1	726.8	727.2	11.2	15.4	11.4	12.4	15.8	05.2	07.5	07.3	07.3	06.6	73	56	85	71	SSE 2	S 5	ESE 1
2	728.5	729.0	731.7	10.0	19.2	14.6	14.6	20.1	08.3	06.5	08.3	07.6	06.5	90	46	68	68	SSF 1	WNW 1	NNE 4
3	734.0	735.4	736.6	12.4	20.4	12.6	14.5	21.4	08.6	05.5	06.5	06.8	07.7	78	38	70	62	-	0	N 1
4	737.7	735.6	736.8	11.6	21.2	16.0	16.2	23.0	08.3	05.8	08.6	06.6	07.3	84	35	54	56	SSW 1	SSE 4	NW 1
5	735.2	734.8	734.9	11.6	11.1	07.2	09.3	16.1	07.0	10.5	09.8	08.6	07.0	95	86	92	91	S 2	SE 3	NE 1
6	736.8	736.7	738.3	07.4	14.2	12.0	12.4	14.6	02.6	00.9	07.5	08.1	07.3	97	52	70	73	NE 1	SE 2	ENE 1
7	740.8	740.1	741.1	11.0	20.5	14.6	15.3	21.1	08.4	05.1	08.7	06.5	08.2	88	36	65	63	SE 1	ESE 1	NNW 3
8	742.7	740.2	738.8	10.6	18.6	12.4	13.5	19.4	06.1	03.0	08.0	06.5	08.7	84	40	80	68	S 1	S 2	SSF 3
9	737.2	736.6	737.7	11.0	19.6	11.6	12.2	17.0	08.6	05.7	08.9	06.2	06.8	91	47	69	66	NW 2	N 5	NNE 4
10	733.5	737.9	739.9	09.6	15.0	09.3	10.8	15.8	09.3	08.4	08.1	06.7	07.0	90	52	79	74	-	0	NNW 3
11	741.3	740.3	740.6	07.2	21.6	12.2	13.3	23.2	01.8	-00.6	07.0	05.7	07.4	91	30	70	64	-	0	W 2
12	743.1	740.8	741.7	10.4	25.2	17.2	17.5	25.8	05.2	02.0	07.7	07.8	06.3	81	33	63	59	-	0	SSE 3
13	744.4	744.5	745.8	14.0	21.4	14.2	16.0	22.0	09.4	06.8	10.0	07.5	08.2	83	39	68	63	SW 1	NNF 5	ENE 3
14	745.9	742.9	741.9	11.0	23.4	18.0	17.6	24.2	05.5	02.9	08.3	08.3	09.0	84	39	58	60	-	0	ESE 2
15	741.7	738.7	739.9	12.2	16.3	13.0	13.9	18.3	09.6	07.5	09.4	11.1	10.5	83	80	93	85	-	0	NE 2
16	732.1	737.6	740.3	10.6	14.0	08.2	10.8	16.4	06.6	04.4	08.0	07.6	07.7	84	56	95	78	-	0	NE 2
17	742.1	740.5	741.8	08.0	20.0	15.1	14.6	21.0	04.1	02.0	07.4	07.4	09.1	92	42	71	68	-	0	ESE 2
18	742.3	737.0	737.0	12.3	16.2	13.4	14.0	17.1	10.4	08.6	09.5	08.3	07.5	89	58	65	71	-	0	NNW 4
19	741.2	741.0	741.0	10.4	14.2	12.9	12.6	18.0	10.0	09.2	10.1	09.9	98	84	89	90	N 2	NNE 1	W 1	
20	741.7	740.1	739.9	11.1	20.8	17.6	14.6	21.8	10.5	09.5	09.9	10.4	10.0	93	57	90	80	5	1	-
21	741.0	740.0	741.0	12.4	14.4	14.6	14.5	23.6	08.4	06.4	09.8	10.8	10.2	91	77	82	82	-	0	SW 1
22	741.7	739.1	739.5	14.1	23.5	17.6	17.7	24.1	10.1	08.3	10.4	09.1	10.3	86	42	73	67	-	0	N 2
23	734.7	735.7	734.9	10.9	11.3	09.8	10.0	16.7	08.8	09.4	08.6	08.7	07.9	86	86	92	88	N 5	N 1	SSF 2
24	735.9	736.9	737.7	10.4	17.2	12.6	13.2	18.7	08.6	06.0	09.0	09.9	10.2	95	67	93	85	-	0	N 1
25	732.2	731.0	731.0	10.6	21.4	17.4	16.7	23.2	08.0	06.5	09.4	13.9	13.6	99	73	91	87	-	0	NW 2
26	742.4	742.6	742.3	15.6	20.0	14.0	14.6	21.7	12.5	08.8	08.4	08.3	67	47	70	61	KNE 5	K 2	NNE 1	
27	742.0	740.5	742.5	12.9	23.2	18.8	16.9	24.6	07.9	05.1	09.4	09.2	08.9	85	38	66	63	-	0	NW 2
28	739.9	736.0	735.7	15.0	24.4	19.4	19.6	25.2	09.0	07.0	09.3	09.9	10.1	72	39	60	57	-	0	S 2
29	732.6	730.4	731.6	16.4	17.2	14.0	14.6	23.0	12.6	09.5	10.3	11.7	10.0	73	79	83	75	W 2	NNW 2	NNE 3
30	740.7	741.4	742.8	15.2	25.7	17.7	18.6	25.4	13.0	12.5	10.9	11.7	12.5	84	51	82	72	NNE 1	NW 2	E 1
31	741.0	739.0	742.2	15.6	26.0	20.3	20.6	26.7	12.3	10.4	11.8	13.0	13.0	90	51	73	71	ESE 1	SE 2	ESE 2
MES.	739.4	738.6	739.0	11.0	19.2	13.9	14.7	21.0	08.5	06.7	09.0	08.7	09.0	86	53	76	72	0.9	2.2	1.7

1974 JUN

SKOPJE - PETROVAC

1	741.4	739.6	739.0	10.6	24.8	21.2	22.0	28.2	14.6	10.1	12.9	12.4	13.6	75	47	72	66	-	0	ESE 2
2	741.4	739.2	739.8	10.4	20.0	15.2	17.6	22.4	15.6	14.9	12.9	11.9	09.6	81	68	71	73	NF 2	N 5	NE 3
3	743.5	744.0	745.6	14.8	16.7	14.4	16.1	16.7	12.9	13.3	09.1	08.2	08.6	72	57	72	67	NF 3	NNE 5	-
4	742.3	741.3	743.5	14.9	24.9	18.8	19.2	26.0	09.2	07.4	10.0	12.2	11.4	82	52	70	68	-	0	KSW 2
5	744.3	742.3	741.2	17.0	27.2	17.4	19.8	28.7	10.8	08.6	11.8	11.2	11.6	81	36	74	65	N 1	SW 1	-
6	741.8	740.4	740.9	17.0	28.4	22.4	22.6	29.6	11.6	09.2	11.5	11.8	10.7	79	41	53	58	SE 1	SSE 1	ESE 1
7	742.8	740.8	740.2	19.6	22.9	16.5	19.0	27.0	15.6	14.6	13.0	13.2	12.0	76	63	84	74	-	0	ENE 1
8	744.2	742.9	742.3	16.2	21.2	15.0	16.3	22.0	13.9	12.4	09.9	09.7	09.3	72	51	72	65	NF 2	NE 2	ESE 1
9	742.4	741.6	738.7	14.0	25.3	20.4	20.0	26.3	06.9	06.9	09.5	12.7	11.4	79	53	64	65	-	0	SE 4
10	739.3	736.9	736.4	19.3	26.6	20.4	20.6	27.9	15.0	12.4	10.9	11.2	12.6	63	43	70	59	S 1	SSE 4	SSE 2
11	732.4	731.3	735.7	20.4	16.0	14.3	26.0	14.0	11.5	10.1	09.3	07.4	56	65	62	61	SSE 4	NNW 6	NW 3	
12	735.0	734.0	734.0	14.6	20.0	10.4	14.1	20.8	10.6	10.6	06.2	06.9	07.4	50	36	77	55	NW 4	NN 4	-
13	735.9	736.2	736.4	16.0	13.3	11.4	11.6	14.2	08.0	05.5	07.8	07.8	08.7	95	66	86	79	ESL 1	NNE 4	SE 1
14	737.6	737.5	738.6	13.4	22.5	13.6	15.8	23.6	09.8	07.7	08.9	07.0	08.1	77	34	65	60	-	0	E 2
15	741.6	740.2	739.1	12.7	24.4	16.8	17.9	26.6	05.2	03.2	06.1	07.9	10.2	73	32	71	59	E 1	S 2	E 1
16	739.5	738.1	738.4	17.1	25.4	17.0	19.1	25.6	14.4	12.5	11.2	11.5	13.7	77	47	94	73	ESF 2	SSW 2	SSW 1
17	739.3	737.2	738.2	16.6	24.3	15.4	19.4	25.0	16.0	15.3	13.3	11.5	13.3	94	50	79	74	NNW 1	N 3	

BR. ST. 268

 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 08	10	10	05.3	00.6	02.0	.	.	.	F SSE 8° 15° 10° i
2	8 07	06	10	07.7	05.9	.	.	.	.	20° 07° 12° 05° 12° 20° 21° 22° 25°
3	7 05	07	04	05.3	05.0	00.2	.	.	.	0° 05° 04°
4	7 04	10	10	08.0	07.0	.	.	.	.	F SSE 13° 23° 14° i 0° 13° 50° 14° 15° 18° 15° 19° 20°
5	7 10	08	02	07.0	01.7	03.0	.	.	.	0° 1° 18° 13° 10° 1° 19° 24°
6	8 09	06	03	06.0	09.5	04.2	.	.	.	12° 0° 4° 2° = 10° 8° 30° i = 10° 40° 1° 0° 14° 20° 5° 10° T 16° 25° 17° 20°
7	8 04	04	10	06.0	05.9	00.5	.	.	.	22° 29° 24°
8	7 03	10	09	07.3	02.5	.	.	.	.	2° 0° 0° 7° 30° F SSE 14° 46° 15° i 0° 14° 35° 20° 45°
9	7 10	09	10	05.7	01.7	00.7	.	.	.	0° 5° 40° 7° 30° EN 110° 20° 20°
10	7 10	08	10	05.7	01.7	00.1	.	.	.	0° 5° 40° 7° 30° i 0° 1° 19° 24°
11	7 00	010	00	00.2	11.6	00.0	.	.	.	1-2-0-1 20° 4° 24° = 0° 30° 0° 10° i = 24° 6° 30°
12	8 00	010	02	01.7	05.6	.	.	.	.	0-0-0 17° 50° 20° 24° T 11° 15° 16° 10°
13	8 07	05	01	04.3	06.7	.	.	.	.	0° 0° 7° 40° = 6° 15° 19° 10° 0° 9° 20° 40° 6° 10° EN 110° 18° 20°
14	7 00	07	01	02.7	12.3	00.0	.	.	.	12° 0° 0° 7° 40° 1° 19° 24° T 18° 20° 19° 20°
15	6 10	10	10	10.0	00.1	.	.	.	.	12° 0° 0° 7° 40° 1° 19° 24° T 18° 20° 19° 20°
16	8 03	10	00	04.3	06.6	25.8	.	.	.	1-2-0-1 0-0-5 F NW 0-0-5 18° 0-0-5 6-40° 0-0-5 140° 15° 16° i 0-1 20° 4° 24°
17	7 00	08	10	06.0	05.4	04.0	.	.	.	2-0-1 10° 14° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
18	7 10	05	04	07.3	00.6	00.4	.	.	.	0-0-1 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
19	7 10	10	09	09.7	00.7	08.5	.	.	.	0-0-0 12° 20° 20° 20° 20° 20° 20° 20° 20° 20° 20° 20°
20	7 09	08	08	05.7	05.7	12.6	.	.	.	= 3° 12° 12° 12° 12° 12° 12° 12° 12° 12° 12° 12°
21	7 03	10	08	07.0	05.1	01.8	.	.	.	12° 0° 8° 30° 22° 30° 24° = 10° 40° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
22	7 06	09	05	07.3	05.6	04.4	.	.	.	2-0-1 10° 20° 20° 24° = 4° 30° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
23	7 10	10	02	07.3	02.3	01.4	.	.	.	0-0-1 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
24	7 10	07	01	06.0	04.9	12.7	.	.	.	0-0-1 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
25	6 03	05	09	06.7	06.7	00.0	.	.	.	12° 0-10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
26	7 09	06	00	05.0	07.2	01.4	.	.	.	0-0-1 2° 15° F NNE 6° 15° 9° 2° i 10° 12° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
27	7 010	020	00	01.0	12.5	.	.	.	.	2-0-1 20° 20° 20° 24° = 4° 30° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
28	8 00	020	05	02.3	12.2	.	.	.	.	0-0-1 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
29	7 06	020	10	08.7	03.4	00.0	.	.	.	0-0-1 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
30	8 05	020	03	03.3	12.2	06.4	.	.	.	0-0-1 9° 20° 20° 24° = 1° 30° 9° 20°
31	7 04	08	06	06.0	06.9	.	.	.	.	12° 0-10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
MES.										
WRED.	05.7	07.2	06.6	06.0	105.0	91.5				

## SKOPJE - PETROVAC

1974 JUN.

1	7 05	040	02	05.0	05.3	.	.	.	.	$\Delta^+ 10-8-30-20-24 = 5-30-9-10-14-07-15-40-6-19-20-22-10$
2	7 06	09	10	06.3	02.7	00.6	.	.	.	$\Delta^+ 10-36-10-16-40-2$
3	7 10	10	05	05.7	00.0	01.5	.	.	.	$\Delta^+ 10-40-8-10 = 5-30-10-05$
4	7 03	06	01	03.3	11.9	.	.	.	.	$\Delta^+ 10-9-1 = 4-30-8-30$
5	7 00	01	00	02.3	12.9	.	.	.	.	$\Delta^+ 10-8-20-22-30-24-14-10-15-30-10-15-20-24$
6	7 02	03	02	02.3	11.9	.	.	.	.	$\Delta^+ 10-12-8-20-15-20-17-12-18-10-17-10-15-20-24$
7	7 06	09	04	04.3	04.7	00.1	.	.	.	$\Delta^+ 10-0-3-10-10-10-10-10-10-10-10-10-10-10-10$
8	7 02	04	00	02.0	10.5	14.4	.	.	.	$\Delta^+ 10-5-20-20-20-20-20-20-20-20-20-20-20-20-20$
9	7 00	06	03	03.0	12.0	.	.	.	.	$\Delta^+ 10-20-7-30-10-10-10-10-10-10-10-10-10-10-10$
10	7 02	07	01	03.3	09.6	.	.	.	.	$\Delta^+ 10-20-7-30-10-10-10-10-10-10-10-10-10-10-10$
11	8 040	10	05	07.7	05.9	00.0	.	.	.	$\Delta^+ 10-5-12-10-10-10-10-10-10-10-10-10-10-10-10$
12	8 05	040	01	04.3	05.8	00.2	.	.	.	$\Delta^+ 10-3-7-4-10-10-10-10-10-10-10-10-10-10-10$
13	7 10	09	10	05.7	00.4	.	.	.	.	$\Delta^+ 10-3-3-10-10-10-10-10-10-10-10-10-10-10-10$
14	8 020	04	01	02.3	11.7	00.0	.	.	.	$\Delta^+ 10-9-10-10-10-10-10-10-10-10-10-10-10-10-10$
15	8 010	030	08	04.0	12.9	.	.	.	.	$\Delta^+ 10-9-10-10-10-10-10-10-10-10-10-10-10-10-10$
16	8 10	07	10	09.0	05.4	00.1	.	.	.	$\Delta^+ 10-8-15-10-10-10-10-10-10-10-10-10-10-10-10$
17	8 10	030	08	07.0	07.8	06.1	.	.	.	$\Delta^+ 10-8-20-20-20-20-20-20-20-20-20-20-20-20-20$
18	7 06	040	10	06.7	09.5	00.3	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
19	6 09	10	10	05.7	00.9	04.6	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
20	7 07	08	07	07.3	03.6	03.4	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
21	6 06	060	10	07.3	06.1	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
22	6 010	020	02	01.7	12.3	00.1	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
23	7 000	010	08	03.0	12.0	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
24	8 020	040	01	02.3	11.8	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
25	8 030	070	04	04.7	10.9	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
26	8 000	030	00	01.0	12.5	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
27	8 020	090	09	06.7	08.2	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
28	7 090	060	05	06.7	08.2	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
29	8 020	060	09	06.3	11.9	.	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
30	8 09	09	08	08.7	01.9	12.6	.	.	.	$\Delta^+ 10-10-10-10-10-10-10-10-10-10-10-10-10-10-10$
MES.										
WRED.	04.7	05.9	05.4	05.3	248.2	44.6				

MES., WRED.

Σ = 41°57' N λ = 21°38' E Gr. Δ G = + 1h27 min.

BR. ST. 268

D	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost % .			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21	
1	738.0	739.4	741.0	19.3	26.0	18.6	20.4	25.7	12.9	10.5	09.0	09.3	10.2	52	35	62	52	NNW	2	NNW	5
2	744.2	742.5	743.4	17.4	28.6	20.0	21.5	29.7	10.8	09.2	12.0	10.9	10.3	80	37	59	59	-	0	N	2
3	745.2	742.0	749.9	18.2	25.6	17.9	19.9	26.8	14.1	11.7	10.7	09.1	11.2	68	37	73	59	-	0	N	2
4	740.1	739.6	740.6	16.4	26.9	21.1	21.5	28.9	10.4	08.9	10.8	12.5	11.9	77	42	64	61	SE	1	NE	3
5	742.3	741.3	742.1	20.0	28.4	23.6	23.9	29.7	14.8	11.6	11.6	12.7	13.0	56	44	59	56	-	0	E	1
6	744.1	740.6	739.6	20.4	26.6	23.6	24.5	31.8	15.2	12.5	13.2	13.5	14.5	74	41	66	60	-	0	SE	2
7	739.9	735.0	740.6	20.1	30.6	15.2	20.3	30.6	14.9	11.7	13.3	11.9	10.2	75	36	71	61	-	0	S	1
8	741.6	741.2	742.7	16.4	19.2	13.2	15.5	20.6	10.5	07.7	07.4	06.7	07.6	53	40	67	53	N	3	N	4
9	744.4	743.6	743.2	14.8	21.3	14.8	16.4	22.4	07.8	05.4	07.5	07.2	08.4	56	38	67	55	NW	1	N	3
10	744.1	741.7	745.2	12.4	24.8	18.6	18.7	26.8	06.9	04.8	09.1	09.2	08.8	85	39	54	59	-	0	NE	3
11	744.1	735.0	743.9	15.6	27.0	18.6	20.0	27.3	10.9	08.6	09.9	08.0	08.6	75	30	59	55	SSW	1	N	5
12	746.6	743.0	743.0	16.8	30.2	21.1	22.0	31.8	10.4	04.7	10.1	08.5	11.6	75	26	62	54	E	1	NNW	1
13	744.5	741.7	741.2	19.3	33.4	21.4	23.9	24.6	12.4	10.0	11.4	10.2	11.4	68	26	52	51	-	0	S	2
14	744.1	741.1	740.9	20.0	34.6	25.7	26.5	35.6	13.4	11.4	11.9	09.9	11.9	68	24	48	47	-	0	SSW	2
15	743.1	741.4	742.0	13.0	36.4	26.0	27.4	35.7	15.8	13.5	13.3	13.2	13.0	63	32	51	49	-	0	S	1
16	742.7	740.6	740.4	22.0	46.8	26.6	27.6	35.6	16.2	13.4	13.5	12.8	14.2	68	30	54	51	-	0	ESE	2
17	740.1	739.3	739.0	22.2	36.0	26.2	27.6	37.0	17.7	15.4	14.0	11.8	11.1	70	26	42	46	-	0	S	2
18	733.9	737.7	734.7	21.9	39.6	23.0	24.3	33.8	16.4	14.2	12.7	14.0	13.3	65	22	63	63	-	0	NW	1
19	736.6	734.8	735.0	19.8	32.6	23.4	24.8	34.0	14.7	12.0	12.6	08.9	10.1	73	24	42	46	SSE	1	SSW	1
20	735.6	735.6	735.3	20.0	26.9	18.0	20.7	27.3	16.0	15.6	11.9	12.2	11.4	68	46	74	63	NNW	3	N	5
21	735.8	730.6	730.0	16.6	19.0	16.8	17.4	20.1	15.4	14.0	08.5	08.5	08.6	56	51	60	57	N	5	N	4
22	737.4	730.4	740.0	14.2	23.0	17.1	17.6	23.0	13.6	11.9	10.4	07.9	05.8	86	37	67	62	-	0	NNW	4
23	732.9	730.2	741.2	14.0	21.4	19.0	17.8	23.3	11.5	09.7	10.5	01.8	10.0	87	46	65	66	E	1	NNE	5
24	742.4	741.7	741.5	16.4	27.0	20.5	21.2	28.0	14.2	11.5	10.5	09.8	10.8	75	37	59	57	-	0	NNW	2
25	740.4	740.0	740.4	17.4	30.8	24.6	24.4	31.9	11.7	09.6	11.3	11.2	10.2	76	34	49	51	-	0	WSW	1
26	742.0	741.3	740.4	20.0	24.4	19.3	20.9	25.2	16.7	14.4	11.1	10.8	08.6	61	47	51	52	NNW	5	N	6
27	745.5	741.3	740.1	16.6	26.8	21.4	21.6	29.0	11.5	08.2	08.7	05.4	11.5	61	35	60	52	NNE	1	SW	1
28	744.7	742.0	740.4	18.0	36.1	26.2	28.3	32.2	13.5	11.4	11.8	12.6	12.7	76	39	50	55	-	0	WSW	2
29	745.6	742.5	744.3	22.0	39.0	24.0	25.5	33.0	12.3	09.9	17.9	10.0	11.2	65	28	50	48	NNE	1	NNW	2
30	745.0	742.1	741.2	18.9	32.1	21.4	23.5	32.8	14.4	11.2	11.4	09.0	09.5	70	25	49	48	-	0	SE	1
31	741.0	739.4	739.3	17.4	32.7	22.2	23.5	33.6	13.0	10.4	10.2	09.0	11.7	68	25	56	50	-	0	WSW	1
MES.	741.0	740.1	740.0	18.3	26.4	20.5	22.2	26.6	13.3	10.8	11.1	10.5	10.8	70	36	58	56	0.8	2.4	1.7	
MES.	742.2	740.4	741.0	18.5	29.6	22.1	23.1	30.8	15.0	12.0	11.6	10.8	11.4	73	36	58	56	0.7	2.5	2.1	

1974 AVGVST

SKOPJE-PETROVAC

1	741.7	739.2	739.3	18.6	32.7	22.8	24.8	33.7	13.8	11.0	11.0	10.9	10.8	68	29	52	50	-	0	SSW	2
2	741.2	739.6	740.2	19.0	33.0	24.8	25.4	34.4	14.3	12.0	11.3	07.7	10.1	69	20	43	44	-	0	SE	2
3	747.5	741.6	742.1	19.6	34.0	23.6	25.7	34.8	14.1	11.2	10.8	07.2	11.8	63	16	54	45	-	0	SSW	2
4	744.0	742.6	741.7	19.4	35.1	22.8	25.0	35.7	14.3	12.2	11.4	08.4	09.4	67	20	45	44	-	0	E	1
5	744.3	740.8	740.6	19.0	35.3	25.2	26.2	36.2	15.3	12.5	10.8	09.0	11.0	65	21	48	44	-	0	NNW	1
6	742.0	739.7	742.2	21.2	34.8	24.4	26.0	34.1	16.8	14.2	12.4	15.7	11.1	61	40	48	51	-	0	NNF	4
7	742.9	740.4	740.3	21.1	28.0	23.6	24.1	29.0	18.4	17.4	09.5	10.5	10.7	50	37	49	45	N	4	N	2
8	740.6	737.7	737.4	17.6	31.0	25.0	24.6	32.0	14.9	11.9	12.6	11.7	13.5	63	35	57	58	SE	1	SSE	4
9	737.9	734.8	735.8	20.6	31.8	21.8	24.0	32.4	16.1	14.4	13.6	12.6	15.1	75	36	77	63	-	0	E	3
10	741.3	740.2	739.3	20.0	26.4	22.0	28.0	31.6	16.6	15.7	10.8	09.0	08.6	62	35	48	48	NNW	3	N	2
11	736.1	733.5	734.3	15.2	29.2	23.0	22.6	31.6	11.1	08.5	09.2	12.3	06.8	71	40	42	51	-	0	NW	2
12	738.9	737.7	740.2	17.8	24.4	18.3	19.7	25.6	15.1	13.4	09.3	07.6	07.6	61	33	48	47	KNE	3	N	5
13	741.0	742.1	744.2	17.4	23.0	16.8	18.5	24.4	12.8	10.9	08.4	09.6	08.8	56	46	62	55	NF	2	NE	1
14	745.9	745.3	745.3	17.7	27.4	22.4	22.5	29.0	11.0	09.1	08.9	09.6	10.4	54	35	51	48	NE	1	NNW	3
15	746.6	745.1	745.7	19.6	30.4	23.0	24.0	31.2	13.8	11.3	11.8	09.0	11.0	65	28	52	50	-	0	N	5
16	746.1	7																			

BR. ST. 268

$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

SKCP JF - PETROVAC

1974 AUGUST

1	8	000	010	00	00.3	12.9	.	.	$\Delta^0 0-7$	.
2	7	000	010	00	00.3	12.7	.	.	$\Delta^0 2-6^{*5}$	.
3	7	000	010	01	00.7	12.8	.	.		.
4	7	000	010	00	00.3	12.7	.	.		.
5	7	000	010	01	00.7	12.1	.	.		.
6	7	000	010	09	03.3	10.7	.	.	$F_{\text{E}} \text{ENE-NE} 12^{58} 24_i, \Delta 21^{45} 22^{45}$	
7	7	040	000	07	03.7	10.5	.	.	$F_{\text{ENE}} 0-1025_i$	
8	7	000	010	00	00.3	11.4	.	.	$\bullet 0^0 17-19_i; T 18-19^{45}, \Delta 0-19^{20} 18^{23} F_{\text{NNE}} 19-24_i, \Delta 19^{45} 21^{40}$	
9	7	000	070	04	03.7	05.4	.	.	$F_{\text{ENE}} 0-6^{*8}$	
10	8	010	020	00	01.0	11.6	00.1	.	$F_{\text{W}} 10^{50} 17^{34}$	
11	8	010	00	01	03.7	09.5	.	.	$F_{\text{ENE-NW}} 0^{*4} 925_i, 12^{48} 20^{45}_i, \bullet 226 3^{30}$	
12	8	030	030	07	04.3	10.6	00.2	.	$F_{\text{NW}} 7-1735_i$	
13	8	06	080	01	05.7	04.4	.	.	$F_{\text{NNE}} 15^{*2} 1943_i$	
14	8	030	040	00	02.3	12.1	.	.	$F_{\text{ENE}} 10^{*8} 17^{48}$	
15	8	000	070	00	02.3	11.1	.	.	$F_{\text{NNE}} 1458 1750_i$	
16	7	000	06	01	02.3	11.2	.	.	$F_{\text{NE}} 13^{*5} 17^{40}_i$	
17	7	09	040	00	04.3	09.7	.	.		
18	7	000	010	00	00.3	11.3	.	.		
19	7	000	020	02	01.3	11.8	.	.		
20	7	000	020	00	00.7	10.6	.	.	$F_{\text{N-NE}} 15-17^{40} 21^{45} 22^{45} T 16^{30} 18, \bullet 0^0 17^{40} 17^{45}_i$	
21	7	000	030	07	03.3	05.7	00.0	.	$T_{\text{N-SE}} 14^{30} 16^{30}, F_{\text{E}} \text{E} 15^{30} 17^{40}, \Delta 0^0 17^{40} 17^{40}_i$	
22	7	010	020	03	02.3	11.8	00.0	.	$T 13^{25} 15^{45}_i$	
23	7	010	07	02	03.3	07.4	.	.	$T 13^{20} 18^{40}_i, F_{\text{NNW-NW}} 14^{48} 16^{45}_i, \bullet 0^0 14^{42} 16^{42}_i, T 15^{40} 16^{40}_i$	
24	7	09	04	100B	07.7	04.6	00.1	.	$\Delta 0^0 20^{40}_i, \bullet 0^0 1725 1430 20-24_i, T 18^{45} 1935 F_{\text{NW}} 19^{25} 20^{20} 18, 19^{55} 2355 \Delta 0^0 2150 22^{40}$	
25	7	06	020	02	03.3	09.9	21.4	.	$\bullet 0^0 1-2^{40}_i, 17^{45} 18^{42}_i = 4^{40} 1540 T 15^{52} 18, \Delta 0^0 17^{40} 17^{45}_i, \Delta 19^{20} 26$	
26	7	000	03	03	02.0	10.5	03.1	.	$\Delta 0^0 10-8^{40} 23-24, T 12^{35} 18^{20}_i$	
27	7	000	060	02	02.7	09.0	.	.	$\Delta 1-2-8^{40} T 12^{35} 15^{45}_i$	
28	7	09	08	09	08.7	09.2	.	.	$\Delta 0^0 10-20^{40}_i, T 13^{40} 14^{40} 23^{40}, \bullet 0^0 13^{40} 14^{40} 22^{45} 24$	
29	7	09	10	10	05.7	00.4	02.1	.	$\bullet 0^0 10-20^{40}_i, 18^{52} M^{20}_i, T 18^{45} 19^{40}_i$	
30	6	10	070	00	05.7	C1.8	C1.9	.	$\bullet 3^{35} 6^{20}_i, 10^{52} 12^{40}_i = 5^{20} 13^{30} T 18^{45} 18^{40}_i$	
31	7	03	03	04	03.3	09.3	00.9	.	$\Delta 0^0 10-16^{45}_i, = 6^{30} 6^{30}, F_{\text{NNE}} 15^{40} 17^{23}$	
MES.	VRED.	02.5	03.8	02.8	03.0	302.7	29.8			

$$\varphi = 41^{\circ} 57', \quad N \quad \lambda = 21^{\circ} 38', \quad E \text{ Gr.} \quad \Delta G = + 1h\ 27\ \text{min.}$$

BR. ST. 268

D D D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %				Provac i jačina vetrova D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	743.5	742.1	742.0	13.2	26.0	16.2	17.9	27.6	10.2	07.9	09.7	07.0	09.9	85	28	72	62	SSE 2	NW 2	SE 2	
2	741.2	741.5	741.9	13.4	28.3	19.8	20.3	29.6	10.9	09.1	05.8	09.7	12.3	85	34	71	63	- 0	SSW 1	S 1	
3	743.5	741.4	741.4	14.8	30.2	20.2	21.4	31.3	12.0	10.5	11.3	11.2	12.7	90	35	71	65	- 0	WSW 2	- 0	
4	742.5	739.5	739.3	17.3	31.8	24.4	24.5	33.0	13.4	12.2	12.3	11.8	11.4	83	33	50	55	- 0	SE 1	SE 2	
5	743.0	742.7	742.7	15.4	28.6	18.6	20.3	26.1	17.4	14.0	12.2	09.7	08.9	77	39	56	57	NNE 5	NNE 5	NNE 4	
6	742.2	738.3	736.2	13.4	27.2	16.4	18.4	28.6	09.6	06.5	09.6	07.0	07.4	83	24	53	54	- 0	C - 0	- 0	
7	739.4	732.3	735.9	14.4	27.3	15.4	18.1	27.6	10.1	08.6	09.6	12.3	12.6	78	45	96	73	- 0	SSE 3	W 1	
8	739.1	741.1	743.6	15.8	23.8	21.4	20.6	25.2	15.0	14.6	12.8	13.8	12.9	95	62	68	75	NNW 1	WNW 2	- 0	
9	746.7	745.8	745.6	16.2	26.4	18.6	20.0	27.6	14.6	13.7	12.7	11.9	14.0	92	46	87	75	NE 1	- C	WSW 1	
10	746.8	744.3	744.5	15.6	28.6	15.0	20.6	29.1	13.9	12.4	12.2	13.2	13.5	92	45	82	73	- 0	WSW 2	- 0	
11	746.5	745.7	747.2	15.4	25.8	16.6	19.6	26.0	13.3	12.4	11.8	11.6	11.0	90	46	68	68	- 0	NNE 5	NNE 2	
12	749.4	746.6	746.6	15.6	26.0	17.4	19.1	27.7	13.5	12.2	10.9	11.8	11.6	82	47	78	69	NNE 2	WNW 2	- 0	
13	746.9	744.5	745.1	13.7	27.8	17.0	18.6	29.0	11.9	10.5	11.1	10.9	10.7	95	39	74	69	- 0	SW 1	W 1	
14	745.9	743.5	743.6	13.2	27.6	19.6	20.0	28.3	10.9	09.5	10.4	11.4	10.5	91	41	61	64	- 0	SSW 2	- 0	
15	744.0	741.8	742.6	14.6	26.4	18.6	19.6	27.1	12.4	10.5	10.9	11.0	11.1	88	43	69	67	- 0	WNW 2	- 0	
16	744.2	743.7	745.1	15.0	26.0	20.0	20.2	26.2	12.6	10.9	11.5	10.0	10.8	90	40	62	64	E 1	N 1	NNE 2	
17	746.8	745.7	745.6	16.4	23.7	17.9	19.0	24.3	14.4	12.2	11.8	11.5	10.6	85	52	69	69	- 0	SSE 5	SE 3	
18	746.1	744.6	744.2	15.4	23.4	18.6	19.0	25.0	13.4	11.8	10.8	11.9	12.6	82	55	78	72	- 0	E 2	- 0	
19	744.4	742.1	742.6	15.6	26.1	15.6	18.2	26.9	14.1	13.0	11.4	10.8	12.1	86	43	91	73	- 0	N 2	- 0	
20	742.7	740.0	739.6	12.1	25.4	19.4	19.1	25.8	10.4	09.3	10.2	10.6	11.1	97	44	66	69	- 0	SSE 2	SSF 2	
21	740.2	740.2	740.4	15.0	22.0	17.4	18.0	23.2	13.2	11.6	11.5	10.4	11.2	90	52	74	72	SE 1	SSE 4	SE 1	
22	741.7	740.1	741.7	14.8	25.4	17.4	18.8	26.2	13.8	11.2	11.3	10.9	14.3	90	45	66	77	ENE 1	S 1	- 0	
23	741.9	740.4	740.7	16.0	23.2	16.4	18.0	23.5	14.1	12.2	12.8	11.7	12.1	94	55	86	78	- 0	SSW 2	S 1	
24	741.0	737.5	737.1	10.6	26.2	15.4	16.9	27.1	05.4	08.4	09.4	09.9	09.5	98	39	73	70	SSE 1	SSE 3	S 1	
25	735.3	731.2	731.0	11.2	22.9	13.8	15.4	26.2	06.7	08.8	07.5	10.3	10.7	98	36	87	71	- 0	S 5	NNE 3	
26	729.7	725.7	728.3	10.0	14.8	14.3	13.4	16.7	07.5	05.2	09.0	10.8	10.7	98	46	60	81	E 1	S 2	NNE 5	
27	735.7	734.5	742.6	12.4	17.2	09.4	12.1	17.4	08.8	08.2	06.7	05.6	06.2	62	38	70	57	NNW 5	NNW 1	NE 1	
28	742.0	740.5	740.0	03.6	19.9	10.0	10.8	21.1	01.4	-00.5	05.6	05.0	07.3	94	29	79	67	SSE 1	NW 1	- 0	
29	741.0	740.4	741.7	05.6	22.4	12.4	13.2	23.6	03.7	01.7	06.6	06.7	08.9	97	33	83	71	- 0	SSW 1	SF 1	
30	742.2	740.3	740.0	09.0	24.9	19.0	17.7	26.2	06.4	04.4	07.6	08.7	09.0	95	37	59	62	- 0	S 4	NE 2	

1974 EKTCRAB

SKOPJE - PETROVAC

1	739.6	738.4	739.7	14.8	20.6	15.2	16.4	22.2	14.5	13.0	11.3	12.6	06.6	90	65	51	70	NW	3	E	1	NW	1	
2	741.5	739.6	737.6	07.8	20.6	18.0	16.1	22.3	04.9	02.1	06.9	06.9	08.5	87	38	55	60	-	0	WNW	1	NW	2	
3	740.2	742.4	744.2	14.6	21.9	13.6	15.9	22.8	11.2	06.4	07.1	05.1	06.3	57	26	54	46	N	2	SE	1	E	1	
4	745.6	743.1	743.3	05.7	21.8	10.4	12.1	22.6	03.5	00.8	06.2	05.9	07.3	90	30	77	66	E	1	SSE	2	-	0	
5	743.3	739.8	739.8	07.2	23.4	14.2	14.8	24.2	05.6	04.0	07.2	08.3	08.5	95	39	70	68	-	0	S	1	ESE	1	
6	737.9	736.6	738.5	08.6	23.2	15.6	15.8	24.6	08.1	05.9	07.7	09.2	09.4	92	43	71	69	ESE	1	ENE	1	E	2	
7	739.6	737.9	737.6	11.8	19.0	18.6	17.0	21.2	11.4	09.3	08.8	10.9	09.8	84	65	61	70	NNE	2	NW	1	SE	3	
8	738.2	735.4	737.7	12.8	25.4	20.9	20.0	25.7	10.6	07.6	09.2	08.9	06.8	83	37	52	-	0	S	4	SSE	2		
9	739.3	738.9	739.8	12.1	17.9	14.6	14.9	20.9	11.0	09.0	10.5	09.5	09.0	99	62	72	78	NNE	2	-	0	NE	2	
10	741.9	741.0	742.3	08.0	21.2	09.6	12.1	22.2	06.5	03.6	07.6	05.9	05.8	95	31	65	64	-	0	ESE	1	SE	1	
11	743.8	742.3	743.6	04.2	19.7	05.6	10.8	21.0	02.7	00.1	05.4	06.2	06.6	88	36	74	66	-	0	SSW	1	-	0	
12	745.6	743.2	742.8	04.7	22.4	15.0	14.3	23.2	03.6	01.0	05.9	08.8	09.3	93	43	72	69	-	0	SSE	3	SSE	1	
13	742.3	740.6	739.6	10.4	19.4	15.8	15.5	19.7	09.2	07.2	08.8	12.2	10.8	90	72	80	81	-	0	NNW	2	E	2	
14	737.9	737.5	738.5	18.0	23.2	16.4	18.5	24.8	15.4	13.0	10.5	11.4	12.5	66	54	89	70	SSE	4	SSE	3	-	0	
15	737.9	737.1	735.5	16.0	19.4	18.2	18.0	22.0	15.9	14.0	13.1	12.8	12.3	96	76	78	83	WSW	1	E	2	SSE	5	
16	737.8	738.8	741.0	15.2	21.2	16.8	17.5	22.7	14.6	12.1	09.9	08.9	05.4	76	47	37	53	SE	1	WNW	3	W	2	
17	743.2	743.0	743.7	09.0	18.9	10.0	12.0	19.8	06.5	03.4	06.7	06.6	07.0	76	40	77	65	ENE	1	WNW	1	N	1	
18	745.9	744.3	745.4	02.8	16.7	11.1	10.4	17.0	02.2	00.0	05.2	06.7	05.9	94	47	59	67	-	0	SW	1	-	0	
19	746.0	743.0	743.2	02.1	18.0	07.5	05.2	18.4	02.6	-00.4	05.1	05.9	06.6	89	38	82	70	-	0	S	2	SSE	7	
20	740.5	735.9	733.0	03.2	20.2	16.2	14.0	20.4	02.6	00.0	05.6	08.1	10.4	97	46	75	73	-	0	SSE	5	SE	5	
21	724.7	720.5	724.5	14.2	15.7	10.0	12.5	16.9	10.0	13.1	10.9	11.4	07.0	90	85	77	84	SSE	4	WNW	2	WSW	3	
22	731.4	734.6	736.0	05.2	15.0	07.2	08.6	16.2	04.8	02.9	06.3	06.9	07.0	94	54	92	80	-	0	SSW	3	SF	1	
23	735.3	735.0	735.6	06.8	25.6	21.4	18.8	25.8	06.6	05.1	07.2	09.4	08.8	97	38	46	60	NNE	1	SSW	3	SF	4	
24	737.3	737.3	740.7	17.0	25.1	13.0	17.0	25.1	12.4	14.8	10.0	09.4	06.3	65	35	56	55	-	0	WSW	5	W	2	
25	743.0	743.1	742.7	06.4	13.8	06.0	08.0	14.9	04.9	02.4	06.2	06.0	05.3	86	51	75	71	S	1	NNE	5	-	0	
26	741.3	737.0	736.1	-00.3	14.2	05.2	06.1	15.2	-00.6	-03.4	04.3	04.7	05.7	96	39	86	74	-	0	SSW	1	SSW	1	
27	736.4	736.7	738.0	05.6	08.0	01.4	04.1	10.0	01.0	01.6	06.1	04.7	04.2	89	58	83	77	W	2	NNE	6	NNE	3	
28	736.8	733.5	732.6	-03.4	10.9	01.0	02.4	11.4	-03.6	-07.0	03.3	04.0	04.3	93	41	86	73	SE	1	SE	2	ESF	2	
29	728.7	728.6	729.0	03.8	13.7	07.6	08.2	14.6	-01.8	-03.7	04.9	07.6	07.3	82	64	93	80	WNW	2	S	4	-	0	
30	726.1	728.0	734.0	06.8	15.0	08.0	09.4	15.2	06.2	04.3	07.3	06.5	05.0	99	51	63	71	SSE	2	SSE	3	WNW	3	
31	737.6	736.5	735.5	00.0	09.0	06.4	05.6	11.4	-00.4	-02.4	04.4	05.9	06.9	96	65	96	86	-	0	NW	3	N	1	
MES.	WRFD.	738.9	737.7	738.4	08.1	18.7	12.1	12.8	19.8	06.5	04.5	07.4	08.0	07.5	88	49	71	69	1-C	2.4	1.8			

ME 5-

Journal of Health Politics, Policy and Law, Vol. 35, No. 4, December 2010  
DOI 10.1215/03616878-35-4 © 2010 by the Southern Political Science Association

RR. ST. 268

$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

Dan	Vrijeme 0-9	Oblacnost N (0-10)					Insolacijia broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	000	06	02	02.7	09.9	.	.	.	$\Delta^{+1} 0-7, 22^{\circ} 24$
2	7	060	02	02	03.3	09.1	.	.	.	$\Delta^{+1} 0-7, 24^{\circ}, \bullet 0-11, 25, 11, 35$
3	8	010	020	00	01.0	11.0	00.0	.	.	$\Delta^{+1} 3, 730$
4	7	000	020	00	00.7	08.6	.	.	.	$\Delta^{+0} 0-6^{\circ}, T 14, 22, 16, 40^{\circ}, \Delta^{+1} 15, 0^{\circ}, 15, 0^{\circ}, R 15, 0^{\circ}, 15, 20^{\circ}, \Delta^{+1} 19, 20, 20, 40^{\circ}, 23, 40^{\circ}, 24$
5	8	07	020	00	03.0	08.1	03.0	.	.	$\Delta^{+0} 0-6^{\circ}, F_{NNW-NWW} 0-18^{\circ}, 20, 35^{\circ}, T 0-10^{\circ}, 3, 0^{\circ}, \Delta^{+0} 0-1, 100, 3, 10^{\circ}$
6	7	000	000	00	00.0	11.6	.	.	.	$\Delta^{+1} 0-7, 21^{\circ} 24$
7	7	09	10	10	09.7	04.4	.	.	.	$\Delta^{+1} 0-8^{\circ}, \bullet 0-14, 15, 19, 20^{\circ}, T 15, 20, 19, 20^{\circ}, R 15, 20, 19, 20^{\circ}, F_{NNW} 15, 45, 16, 40^{\circ}, \Delta^{+1} 15, 20, 19, 40^{\circ}$
8	6	10	080	09	09.0	02.6	49.6	.	.	$\Delta^{+4, 20, 30}$
9	7	000	010	00	00.3	09.6	.	.	.	$\Delta^{+0-1, 18, 0, 40, 18, 30} 24^{\circ}, = 4^{\circ}, 12, 30^{\circ}, 21, 24$
10	7	000	020	00	00.7	10.2	.	.	.	$\Delta^{+0-1, 2, 0-9, 30, 20, 30} 24^{\circ}, = 0-13, 40^{\circ}$
11	7	020	010	01	01.3	05.8	.	.	.	$\Delta^{+0-2, 0-9, 1, 6, 20, 9, 30} F_{NNW} 10, 40^{\circ}, 17, 50$
12	7	030	010	00	01.3	09.5	.	.	.	$\Delta^{+3, 730} 20, 24, = 5, 30, 10, 20$
13	7	000	010	00	00.3	09.8	.	.	.	$\Delta^{+1, 0-7, 21, 20, 24, = 5, 20, 11, 30}$
14	7	000	020	00	00.7	09.6	.	.	.	$\Delta^{+0-1, 0-7, 20, 30, 24, = 5, 10, 12, 30}$
15	7	000	020	00	00.7	09.0	.	.	.	$\Delta^{+0-1, 2, 0-8, 20, 24, 24, = 4, 30, 12, 30}$
16	7	010	020	08	03.7	09.4	.	.	.	$\Delta^{+2, 0-8, 30} = 0-9, 45$
17	7	09	010	00	02.3	05.1	.	.	.	$\Delta^{+4, 8, 30} = 4, 30, 8, 30$
18	7	09	08	10	09.0	03.2	.	.	.	$\Delta^{+7, 10, 9, 30} \leq 18, 40, 19, 50$
19	7	08	050	01	04.7	07.0	.	.	.	$\Delta^{+2, 30, 7, 40} = 6, 20, 12, 20, 23, 20, 24, T 14, 20, 14, 40^{\circ}, R 14, 40, 15, 0^{\circ}, \Delta^{+1, 2, 14, 50, 15, 02}$
20	7	000	010	00	00.3	08.5	04.0	.	.	$\Delta^{+0-10, 40}$
21	7	08	10	03	07.0	00.5	.	.	.	$\Delta^{+0, 3, 50} \bullet 0, 8, 20, 9, 40^{\circ}$
22	7	09	09	10	05.3	04.3	00.0	.	.	$\Delta^{+1, 0-7, 30} = 5, 10, 9, 40^{\circ}, T 15, 17, 20^{\circ}, \Delta^{+1, 15, 45, 16, 25, 19, 40^{\circ}, 19, 40^{\circ}, \Delta^{+1, 16, 40}}$
23	7	10	05	05	08.0	02.9	00.6	.	.	$\Delta^{+4, 30, 9, 45} T 13, 37, 14, 45, \Delta^{+1, 13, 42, 14, 35}$
24	7	000	04	00	01.3	05.0	00.6	.	.	$\Delta^{+0-2, 0-9, 45} = 3, 30, 7, 40^{\circ}$
25	7	030	09	09	07.0	05.0	.	.	.	$\Delta^{+0-10, 8, 30} F_{SSE-S} 10, 0^{\circ}, 14, 40^{\circ}, \bullet 0-12, 10, 12, 25, 16, 30, 18, 50$
26	7	08	06	10	08.0	02.4	00.5	.	.	$\Delta^{+5, 30, 6, 30} = 0-19, 30, 15, 20^{\circ}, 20, 30, 22, 20^{\circ}, F_{NNW} 19, 58, 21$
27	8	09	040	00	04.3	08.0	12.5	.	.	$\Delta^{+1, F_{NNW-NWW} 3, 40, 16, 05^{\circ}, \Delta^{+1, 19, 30, 24}}$
28	8	000	000	00	00.0	10.5	.	.	.	$\Delta^{+1, 2, 0, 0, 30, 20, 30, 24}$
29	8	00	00	00	00.0	10.0	.	.	.	$\Delta^{+0-2, 0-9, 20, 19, 40, 24}$
30	8	010	080	07	05.3	08.7	.	.	.	$\Delta^{+4, 2, 0-8, 20} F_{SSE} 18, 40, 18, 20, \bullet 0-21, 35, 22$

SKP-IE-PETROVAC

1974 EKTC 848

1	7	10●	08	05	07.7	C1.8	CC.3	.	• $\frac{2^{\circ} 9.30}{0-10.80} = \frac{8^{\circ} 10.20}{F_{SSE} 22.25 22.26}$
2	8	04○	05	04	04.3	C8.3	Cl.3	.	$\frac{F_{NNE} 7.7.30}{\Delta^{\circ} 0-10}$
3	8	01○	01○	00	CC.7	10.3	.	.	
4	8	01○	05○	04	03.3	C8.5	.	.	
5	7	05	04○	06	C5.0	CR.2	.	$\Delta^{\circ} 20-8.00 19.20 24$	
6	7	09	C5○	04	06.0	05.8	.	$\Delta^{\circ} 0-1.7$	
7	7	10●	09	04	C7.7	0C.3	CC.0	$F_{EN-NNE-SSE} 015.030 17.28 22.20 06.15.7.00 23.45.24$	
8	8	05○	04○	09	06.0	08.7	00.0	$\Delta^{\circ} 2-3.40 19.40 23.20 F_{SSE-C} 10.10 11.80 14.13 15.40$	
9	7	10	08	07●	08.3	C1.7	CC.4	$\bullet 0.032 10.7.15 12.45, 49.20-21.30$	
10	7	01○	06○	00	02.3	09.6	00.0	$\Delta^{\circ} 22.24$	
11	8	08	03○	00	C3.7	C8.6	.	$\Delta^{\circ} 0-1.0-8.30$	
12	7	04	02○	01	02.3	C8.4	.	$\Delta^{\circ} 3.30 8.20$	
13	7	09	09	08	08.7	00.1	.	$\Delta^{\circ} 3-8.00 = \frac{8.45 12.30 16.30 20.35 0.11.15 15.30}{F_{SE} 3.40.24 12.20 18.30 12.10.02 7.15.65 20.25.1} \Delta^{\circ} 20.25 22.40$	
14	7	C8	09●	09	08.7	04.3	00.2	$\Delta^{\circ} 2-4.10 0.3.5.50; 12.3.30; T.4.0.1.5.20 \Delta^{\circ} 4.38 4.38 4.38 4.38 10.38 = 6.25-11.40$	
15	7	09	10●	08●	09.0	C1.1	C1.7	$F_{SSE-W} 0-1.32 18.10.18.12 \bullet 0.10.45 11.05 6.20.30 21.15$	
16	8	03	05○	01	03.0	05.2	04.7	.	
17	8	03○	05	00	C4.0	C7.3	CC.0	$\Delta^{\circ} 1.0-5.4.5-7.40 \oplus 10.39.12$	
18	7	10	06	04	07.7	04.7	.	$\Delta^{\circ} 0-10.4.50 22.20.04 \Delta^{\circ} 0.4.30 6.20$	
19	7	00○	02○	00	00.7	C9.0	.	$\Delta^{\circ} 0-8.15 = 5.50.4.15 F_{SSE} 11.30 24.1$	
20	8	09	04○	04	05.7	C9.2	.	.	
21	7	10●	10●	08	09.3	00.6	05.5	$F_{SSE-W} 0-8.00 20-20.12 23.24 \bullet 0-10.45 11.25 20-20.20 \Delta^{\circ} 11.45 19.50 22.20 24$	
22	8	06○	03○	01	04.0	04.2	05.4	$\Delta^{\circ} 0-10 F_{SSE} 0-0.00 \bullet 0.1.20 3.05 \Delta^{\circ} 20-24$	
23	8	C3	05○	03	03.7	07.6	.	$\Delta^{\circ} 0-8 = 6.30.4.40 F_{SSE} 9.02 42.00 19.30 21.16$	
24	8	08	05○	09	07.3	06.1	.	$\Delta^{\circ} 0.45.2.1 \Delta^{\circ} 6.40.6.85 \bullet 0.7.05 8.10 F_{SSE-WWW} 11.20 18.16$	
25	8	02○	08	06	03.3	06.8	00.0	$\Delta^{\circ} 0-7.8, 19.24.1 F_{SSE} 10.02.04$	
26	7	04	C5○	06	05.0	08.1	.	$\Delta^{\circ} 10-0.30 \Delta^{\circ} 10.20 7.20 = 5.40 5.50 \Delta^{\circ} 17.30 21.30$	
27	7	10●	05	00	06.3	00.8	C1.9	$\bullet 0.3.45.4.50 F_{NNE-UWW} 5.3.1.5.6.9.0.1.15.4.1, \Delta^{\circ} 10-1.23-24$	
28	8	01○	07○	01	03.0	C7.9	00.0	$\Delta^{\circ} 1-2.0-7.45 20.40.24 \oplus 0.4.16.10$	
29	7	07	07	08	07.3	02.8	.	$\Delta^{\circ} 1-0-6.4.6-5.9.0.0 \bullet 0.7.05 8.2.2, 11.45-13.06, 16.20-17.8.2, 23.25 24, \sim 13.02-13.30$	
30	7	10	06	03	06.3	06.0	06.7	$\bullet 0-0-4.20.6.30.7.20 = 0.2.8.25$	
31	7	05	05	10	09.3	00.7	00.0	$\Delta^{\circ} 1-1.45.7.15 \bullet 0-1.25 24.1$	

$\varphi = 41^{\circ}57'$  N  $\lambda = 21^{\circ}38'$  E Gr.  $\Delta G = +1h\ 27\ min.$

BR. ST. 268

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pona e mm			Relativna vlažnost v%				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21		
1	730.0	731.7	737.6	06.4	11.0	04.2	06.4	12.2	04.2	05.5	07.0	06.8	05.2	97	69	84	83	SSW 1	-	C	NF 5	
2	741.3	741.0	742.5	03.2	11.3	00.2	03.8	11.8	00.3	00.5	04.2	03.6	04.0	72	36	86	65	N 1	NW 2	-	0	
3	743.5	743.0	744.2	-00.4	12.8	03.6	04.9	13.4	-01.6	-04.4	04.2	04.7	05.0	94	43	85	74	SE 1	SSE 1	S	1	
4	745.6	743.9	744.4	-01.1	12.6	02.0	03.9	14.0	-02.0	-04.6	04.0	04.7	04.8	94	43	90	76	S 1	SSE 2	-	0	
5	745.6	745.2	747.2	-01.2	14.4	07.8	07.2	15.2	-02.0	-04.4	04.0	05.7	06.6	96	46	83	75	-	0	NNW 1	SE 1	
6	749.3	747.8	748.6	02.2	16.4	11.0	10.2	16.6	02.0	-00.6	05.2	07.4	06.8	97	53	69	73	SE 1	WSW 1	E	1	
7	747.5	745.4	743.4	09.6	09.8	08.2	09.0	11.0	07.6	05.6	07.2	08.2	07.7	81	90	95	89	E 1	-	C	E 1	
8	740.5	739.9	741.1	07.8	08.2	07.0	07.5	09.1	07.0	07.4	07.7	07.1	06.1	97	87	81	88	-	0	NNW 2	NNW 2	
9	741.5	742.0	744.2	07.0	10.2	07.8	08.2	10.2	06.4	05.6	06.6	06.1	06.1	88	66	77	77	WWN 3	W 3	N	3	
10	745.4	745.7	746.6	05.9	10.2	08.0	08.0	10.2	05.8	04.9	06.1	05.9	06.6	89	63	82	78	NNE 2	NNW 1	SSW 1		
11	747.4	746.5	747.5	04.8	14.3	04.4	07.0	15.1	04.3	04.7	06.1	06.2	05.7	94	51	91	79	SSW 1	SSW 1	S	2	
12	748.0	746.0	746.0	-00.6	12.6	05.4	05.7	13.4	-01.0	-03.0	04.2	06.5	06.2	96	59	91	82	-	0	-	0	
13	745.9	745.9	747.0	04.6	13.0	04.6	06.7	13.6	02.4	00.4	06.2	07.5	06.2	97	67	97	87	-	0	WSW 2	NNW 1	
14	748.5	747.4	748.6	01.4	09.7	03.2	04.4	11.4	00.9	-01.0	05.1	07.1	05.6	100	79	97	92	-	0	-	0	
15	749.7	748.7	749.0	00.4	06.4	02.2	02.8	08.6	-00.4	-01.4	04.7	06.6	05.2	100	92	97	96	-	0	SE 1	-	0
16	749.0	747.5	748.1	01.8	09.6	03.0	04.4	10.6	-00.6	-01.6	05.0	06.8	05.5	97	76	97	90	-	0	NW 1	-	0
17	749.1	748.5	749.0	03.2	05.2	04.1	04.2	05.4	-00.9	-01.3	05.8	06.4	06.1	100	97	100	99	SSE 1	-	0	-	0
18	749.4	748.7	748.7	02.4	03.6	02.8	02.9	04.3	02.0	02.8	05.4	05.8	05.6	100	97	100	99	NE 1	-	C	-	0
19	747.9	745.4	745.3	02.0	05.0	05.2	04.4	06.0	02.0	02.5	05.3	06.4	06.3	100	97	94	97	-	0	-	0	W 2
20	746.0	746.0	747.1	05.4	12.0	03.8	06.2	12.7	03.4	05.0	06.3	07.1	05.9	94	68	98	87	-	0	-	C	ENE 1
21	746.9	745.8	745.4	04.0	06.8	07.1	06.2	07.5	01.4	-00.4	06.1	07.0	07.2	100	95	95	97	-	0	ENE 1	ENE 1	
22	744.4	743.7	745.0	06.8	11.2	07.6	08.3	12.2	06.4	06.4	07.2	07.5	06.4	97	75	82	85	-	0	-	C	NE 3
23	746.0	744.7	744.5	03.2	05.8	05.6	05.0	08.0	01.0	-01.5	05.6	06.1	06.3	97	89	93	93	NE 1	-	0	NE 1	
24	744.0	744.3	745.7	05.3	08.5	03.8	05.4	08.6	03.4	05.3	06.2	06.8	05.8	93	81	97	90	-	0	W 1	-	0
25	746.7	745.2	744.8	05.6	09.4	07.8	07.6	10.0	03.8	00.0	06.6	07.3	06.9	97	83	87	89	-	0	NW 2	SSE 4	
26	740.8	738.6	737.9	08.2	08.2	06.6	07.4	09.7	06.5	02.1	06.9	07.9	07.1	85	97	97	93	SE 4	S 2	NNE 1		
27	738.5	736.8	736.2	03.2	06.9	05.2	05.1	07.1	02.8	00.6	05.5	06.6	06.4	95	88	97	93	NF 1	-	0	NNE 1	
28	735.9	732.2	727.6	01.2	09.3	06.2	05.7	09.8	01.2	-01.1	04.8	06.9	06.4	97	78	90	88	S 1	-	0	NNW 1	
29	729.3	732.9	734.9	04.4	10.5	00.6	04.0	14.5	00.2	03.3	05.4	04.8	04.1	85	50	86	74	NW 3	-	0	-	0
30	737.4	739.2	743.2	-02.8	07.7	01.8	02.1	08.1	-03.4	-05.6	03.4	05.2	04.4	91	66	83	80	-	0	NNW 4	NE 3	

MFS.  
WRF0. 744.0 743.3 744.0 03.5 09.8 05.0 05.8 10.7 02.1 01.0 05.6 06.4 05.9 94 73 90 86 0.8 - 0.9 1.2

1	745.2	746.3	748.3	-04.4	04.0	01.4	00.6	04.5	-04.6	-07.6	03.0	04.5	04.7	92	73	92	86	-	0	NW 1	-	0	
2	749.0	748.5	749.2	-01.4	06.2	03.0	02.7	07.1	-01.9	-04.0	04.0	04.8	05.0	96	68	87	84	-	0	-	C	-	0
3	750.3	749.3	749.8	03.2	11.0	07.6	07.4	11.2	02.9	01.1	05.4	05.3	06.4	94	54	82	77	-	0	NNW 2	W 1		
4	748.9	746.9	745.8	08.0	11.0	08.4	09.0	11.9	06.4	05.4	06.8	07.4	06.4	85	75	78	79	NNE 2	-	0	NF 2		
5	743.3	741.2	740.4	00.6	12.0	06.4	06.4	12.4	00.0	-02.0	04.7	06.2	06.1	98	58	85	80	S 1	-	0	NF 1		
6	740.2	741.6	743.2	05.8	07.0	00.0	03.2	07.2	-00.6	00.3	04.5	04.7	03.7	65	62	80	69	N 5	-	0	NNE 2		
7	743.0	742.0	741.6	-04.0	05.1	01.8	01.2	06.0	-04.4	-07.0	03.2	03.6	04.4	94	54	85	78	ENE 1	SSW 1	NW 1			
8	740.9	738.3	739.6	00.0	07.4	04.3	04.0	07.6	-00.6	-03.4	04.3	05.1	06.0	93	65	97	85	NW 1	NNF 3	N	2		
9	740.5	742.6	745.7	02.9	09.4	03.4	04.8	09.4	01.3	-00.2	05.6	04.9	04.1	98	56	70	75	NW 3	NNE 4	NF 2			
10	747.4	746.7	747.4	-03.2	08.1	03.4	-00.5	09.1	-03.5	-06.2	03.4	04.6	03.2	93	57	89	80	-	0	-	C		
11	747.5	744.5	743.1	-05.6	06.6	-02.0	-00.8	07.4	-05.7	-08.3	02.8	03.9	03.3	92	53	83	76	-	0	-	0		
12	741.0	739.2	738.0	-02.4	04.2	00.4	00.6	04.6	-04.4	-06.9	03.5	04.2	04.2	90	68	89	82	-	0	-	C	E 1	
13	735.0	732.7	732.8	01.8	10.4	05.0	05.6	10.6	00.0	-01.6	04.7	06.0	05.8	90	64	88	81	N 1	W 2	NE 1			
14	735.9	737.2	736.2	02.6	01.6	00.2	01.2	05.6	00.2	02.0	05.0	04.5	04.5	90	87	96	91	W 2	NNW 2	NW 3			
15	736.8	737.2	738.6	00.9	01.8	00.4	00.9	02.4	00.0	00.0	03.8	04.2	04.4	78	80	93	84	NW 2	MSW 2	MSW 2			
16	740.1	740.8	742.5	00.2	02.0	01.6	01.4	02.3	-00.4	-00.6	04.0	04.3	04.3	86	80	83	83	NE 3	NNE 4	NNE 3			
17	743.4	741.5	741.1	02.0	05.1	-02.1	00.7	05.6	-02.2	-00.1	04.3	04.2	03.7	80	64	94	79						

BR. ST. 268

 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Den	Vreme	Obložnost N (0-10)					Instalacija levi seni	Podzemje R mm	Snežni pokriven. h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	7	10*	08	10*	08.3	02.7	09.6	.	.	$\bullet^{-1} 0^{-8} 30^i, 18^{35} 23^{30}_i = 5^{30} 7^{30}, F_{NE} 18^{40} 21^{40}$	
2	8	04	020	00	C2.0	08.8	03.1	.	.	$\Delta^{-1} 7^{40} 20^{30} \Delta^{-1} 28^{30} 24$	
3	8	04	030	01	C2.7	C8.2	.	.	.	$\square^{-1} 0^{-7} 30 22^{30} 24$	
4	8	06	020	00	02.7	07.8	.	.	.	$\square^{-1} 0^{-8} 30^i, 21^{30} 24$	
5	7	03	010	08	C4.0	C7.1	.	.	.	$\square^{-1} 0^{-8} 30^i = 6^{30} 7^{30}$	
6	7	04	060	09	04.3	04.1	.	.	.	$\equiv 5^{30} 12^{30}$	
7	7	10*	10*	10*	10.0	00.0	00.0	.	.	$\bullet^{-1} 6^{30} 24^i$	
8	6	10*	10*	10*	10.0	00.0	20.5	.	.	$\bullet^{-1} 0^{-7} 30^i, 21^{30} 22^{30} = 2^{-9} 30^i, \equiv^{-2} 6^{30} 7^{30}, 0^{-1} 12^{30} 14^{30}, 18^{40} 21^{40}$	
9	7	10	10	10	10.0	00.0	00.0	.	.	$\bullet^{-1} 4^{-6} 30$	
10	7	09	09	10	09.3	01.1	.	.	.	.	
11	7	09	010	00	03.3	C7.7	.	.	.	$\Delta^{-1} 20^{30} 24$	
12	7	10*	030	05	06.0	05.7	.	.	.	$\square^{-1} 0^{-8} 30^i, 45^{30} 5^{30} 7^{30} 12^{30} 16^{30} 24 = 5^{30} 7^{30}, \Delta^{-1} 20^{30} 24$	
13	6	09	09	10	09.3	04.6	.	.	.	$\Delta^{-1} 0^{-8} 30^i, 11^{30} 12^{30} = 12^{30} 10^{30} 11^{30} 24$	
14	6	10*	00	00	03.3	02.9	.	.	.	$\equiv 0^{-1} 0^{-8} 30^i, 12^{30} 11^{30} = 12^{30} 10^{30} 11^{30} 24$	
15	5	10*	020	00	04.0	02.1	.	.	.	$\equiv 0^{-1} 0^{-8} 30^i, 12^{30} 11^{30} = 12^{30} 10^{30} 11^{30} 24$	
16	6	10*	030	00	04.3	02.2	.	.	.	$\Delta^{-1} 0^{-5}, \equiv 0^{-1} 0^{-8} 30^i, 24^{30} 23^{30} = 0^{30} 8^{30} 23^{30} 24, \equiv 9^{30} 21^{30} 12^{30} 24$	
17	5	10**	10	10*	10.0	00.0	00.0	.	.	$\equiv 0^{-1} 0^{-8} 30^i, 16^{30} 20^{30} = 10^{30} 6^{30} 10^{30} 24, \equiv 10^{30} 7^{30} 15^{30} = 15^{30} 16^{30} 20^{30} 24$	
18	4	10**	10	10*	10.0	00.0	00.3	.	.	$\bullet^{-1} 6^{30} 6^{30} = 6^{30} 15^{30} 9^{30} 15^{30} = 15^{30} 24$	
19	3	10*	10*	10	10.0	00.0	00.0	.	.	$\equiv 0^{-2} 24^{30}, \equiv 0^{-1} 0^{-8} 30^i, 12^{30} 10^{30} 24$	
20	6	10	02	03	05.0	04.1	00.2	.	.	$\equiv 0^{-1} 0^{-8} 30^i, 12^{30} 10^{30} 24, \equiv 22^{30} 24$	
21	3	10*	10*	10	10.0	00.0	00.0	.	.	$\equiv 0^{-3} 0^{-9} 45^i, 4^{30} \Delta^{-1} 0^{-8} 30^i, \equiv 0^{-3} 0^{-9} 45^i, 9^{30} 11^{30} = 14^{30} 24$	
22	5	10*	020	08	06.7	01.2	00.6	.	.	$\equiv 0^{-1} 8^{30}, \bullet^{-1} 4^{30} 12^{30}$	
23	5	10	10	10	10.0	00.0	00.2	.	.	$\equiv 4^{30} 24$	
24	5	10	09	10	09.7	00.0	00.0	.	.	$\equiv 0^{-2} 24^{30}, \equiv 0^{-1} 0^{-8} 30^i, 20^{30} 24$	
25	6	10*	10	10	10.0	00.0	00.0	.	.	$\equiv 0^{-1} 6^{30}, \Delta^{-1} 0^{-8} 30^i, 12^{30} 10^{30} 24, \equiv 6^{30} 7^{30}$	
26	5	10	10*	05	08.3	00.0	.	.	.	$F_{SE} 2^{30} 5^{30}, \bullet^{-1} 9^{30} 14^{30} 16^{30} 17^{30} = 9^{30} 23^{30}, \equiv 21^{30} 22^{30}$	
27	6	10	10	10	10.0	00.0	00.0	.	.	$= 7^{30} 24^{30}, \equiv 7^{30} 7^{30}, \Delta^{-1} 18^{30} 19^{30}, \bullet^{-1} 21^{30} 22^{30}$	
28	7	07	09	09	08.3	01.5	00.0	.	.	$\equiv 0^{-1} 0^{-8} 30^i, F_{SE} 20^{30}, \Delta^{-1} 24^{30}$	
29	8	09	01	02	04.0	07.9	00.3	.	.	$F_{NNE} - 86^{\circ} E 0^{-9} 30^i, \bullet^{-1} 4^{30} 5^{30} \Delta^{-1} 0^{-8} 30^i, 19^{30} 24$	
30	7	08	09	02	06.3	01.8	.	.	.	$\Delta^{-1} 0^{-10} 0^{-8} 30^i, 24^{30}, \equiv 12^{30} 12^{30}$	
MES.											
VR ED.		08.7	06.4	06.4	07.2	R1.	47.7				

1	7	04	10	09	C7.7	CC.0	.	.	.	$\Delta^{-1} 0^{-10} 30^i$	
2	6	09	03	08	06.7	00.7	.	.	.	$\equiv 0^{30} 24, \Delta^{-1} 0^{-8} 30^i$	
3	6	09	080	08	08.3	02.4	.	.	.	$\equiv 0^{-1} 4^{30}, \bullet^{-1} 23^{30} 24$	
4	7	10	09	09	09.3	00.2	00.0	.	.	$\bullet^{-1} 0^{-8} 30^i, 6 = 4^{30} 5^{30}, 9^{30} 24, \equiv 5^{30} 9^{30}, \Delta^{-1} 6-7^{30}$	
5	6	03*	07	10	06.7	05.1	.	.	.	$= 0^{-5} 0^{-8} 30^i, \bullet^{-1} 7^{30} 9^{30}, 13^{30} 16^{30}, F_N 5^{30} 8^{30}, 15^{30} 17^{30}, \Delta^{-1} 0^{-8} 30^i$	
6	8	10	10	02	07.3	00.0	.	.	.	$\Delta^{-1} 0^{-9} 30^i, 7^{30} 10^{30}, \bullet^{-1} 8^{30} 8^{30}$	
7	7	04	05	05	04.7	03.3	00.0	.	.	$\bullet^{-1} 13^{30}, \Delta^{-1} 24^{30}$	
8	7	10	10*	10*	10.0	00.4	00.0	.	.	$\equiv 0^{-6} 30, \bullet^{-1} 15^{30}, \Delta^{-1} 24^{30}$	
9	7	09	06	09	08.0	00.8	01.7	.	.	$\Delta^{-1} 0^{-10} 30^i, 8^{30} 10^{30}, 24^{30}, \equiv 7^{30} 12^{30}, 16^{30} 24$	
10	7	02	000	00	00.7	07.5	.	.	.	$\Delta^{-1} 0^{-8} 30^i, 0^{-1} 9^{30} 24^{30}, \equiv 0^{-2} 24^{30} = 0^{-2} 24$	
11	6	00	010	00	00.3	06.4	.	.	.	$\Delta^{-1} 0^{-9} 30^i, 19^{30} 24, \equiv 0^{-2} 24^{30} = 0^{-2} 24$	
12	5	07	10	09	C6.7	00.2	.	.	.	$\Delta^{-1} 0^{-9} 30^i, 0^{-1} 24^{30}, \bullet^{-1} 24^{30} = 22^{30}$	
13	6	09	04	10	07.7	03.3	00.0	.	.	$\equiv 0^{-10} 30^i, F_{NNE} - www 2^{30} 4, 15^{30} 18^{30}, \bullet^{-1} 13^{30} 15^{30}, \Delta^{-1} 13^{30}, \Delta^{-1} 20^{30}$	
14	6	10*	10*	10*	10.0	00.0	06.4	.	.	$\bullet^{-1} 0^{-7} 30^i, 9^{30} 24^{30}, \bullet^{-1} 24^{30}, \equiv 24^{30}$	
15	6	10	10*	10*	10.0	00.0	14.2	07	.	$\bullet^{-1} 0^{-9} 30^i, \bullet^{-1} 12^{30}, \Delta^{-1} 24^{30}$	
16	7	10*	10	10	10.0	00.0	C2.8	08	.	$\bullet^{-1} 0^{-9} 30^i, \bullet^{-1} 12^{30}, \Delta^{-1} 24^{30}$	
17	7	10	000	02	04.0	06.5	00.0	04	.	$\Delta^{-1} 0^{-10} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
18	6	04	09	10*	C7.7	CC.5	.	.	.	$\equiv 0^{-10} 30^i, F_{NNE} - www 2^{30} 4, 15^{30} 18^{30}, \bullet^{-1} 13^{30} 15^{30}, \Delta^{-1} 13^{30}, \Delta^{-1} 20^{30}$	
19	1	10*	00*	09	06.3	01.0	C8.2	01	.	$\bullet^{-1} 0^{-8} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
20	7	08	06	06	CC.7	C1.4	.	.	.	$\Delta^{-1} 0^{-10} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
21	7	05	010	09	05.0	05.4	.	.	.	$\Delta^{-1} 0^{-9} 30^i, 23^{30} 24, \equiv 6-7^{30}, 16^{30} 24$	
22	6	00	020	00	0C.7	05.7	.	.	.	$\equiv 0^{-15} 30^i, \bullet^{-1} 10^{30}, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
23	5	00	000	00	00.0	06.6	.	.	.	$\Delta^{-1} 0^{-10} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
24	5	00	000	00	00.0	06.4	.	.	.	$\equiv 0^{-2} 24^{30}, \Delta^{-1} 0^{-8} 30^i, 17^{30} 24, \equiv 0^{-2} 24^{30} = 24^{30}$	
25	5	00	000	00	00.0	04.4	.	.	.	$\Delta^{-1} 0^{-10} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
26	6	00	030	03	02.0	05.9	.	.	.	$\Delta^{-1} 0^{-9} 30^i, 19^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
27	5	09	08	01	06.0	01.9	.	.	.	$\equiv 0^{-13} 30^i, 4^{30} 12^{30}, \bullet^{-1} 0^{-9} 30^i, 16^{30} 22^{30}, \equiv 2^{30} 3^{30} 6^{30} 12^{30} 17^{30}$	
28	4	10*	10	10*	10.0	00.0	C1.0	.	.	$\equiv 0^{-9} 30^i, 8^{30} 10^{30}, 18^{30}, \bullet^{-1} 24^{30} = 24^{30}$	
29	4	10	08	10*	09.3	00.0	00.0	.	.	$\equiv 0^{-7} 30^i, \bullet^{-1} 17^{30}, \bullet^{-1} 24^{30} = 24^{30}$	
30	3	10*	10	10*	10.0	00.0	00.0	.	.	$\equiv 0^{-9} 30^i, F_{NNE} 24^{30}, \bullet^{-1} 6^{30}, \Delta^{-1} 0^{-8} 30^i, 17^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
31	5	10*	10*	10*	10.0	00.0	C2.0	.	.	$\bullet^{-1} 0^{-10} 30^i, F_{NNE} 24^{30}, \bullet^{-1} 6^{30}, \Delta^{-1} 0^{-8} 30^i, 17^{30} 24, \bullet^{-1} 24^{30} = 24^{30}$	
MES.											
VR ED.		06.5	05.8	06.4	06.2	76.4	76.3	.	.		

**B) Mesecni i godišnji  
pregled**

1974

Mjesec	Vrednost pritisak Pn mm.	Temperatura vazduha °C								Čestina pravaca i srednja jačina vatra nD, Fm (0-12)																									
		Tm			Sred. (tides)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C								
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.							
SR SLOVENIJA																																			
$\varphi = 46^{\circ}20' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																																			
I	-	-06.6	04.5	C1.3	01.7	05.4	-01.0	12.3	20 -04.8	24 06	00.6	C4	01.2	C1	06.1	.	.	21	02.6	05	00.8	.	.	.	.	.	.	56							
II	-	C1.7	02.3	03.6	04.1	C6.2	04.9	12.7	21.20 -04.3	09 14	C1.8	10	03.5	C7	00.8	.	.	20	02.4	14	03.4	02	00.3	.	.	.	.	17							
III	-	03.2	11.8	06.0	06.7	12.6	02.0	23.8	22 -05.2	01 06	00.8	05	01.4	C7	01.2	.	.	33	03.9	23	04.0	01	00.2	.	.	.	.	18							
IV	-	05.5	13.3	08.4	08.9	14.2	03.4	19.7	12 -01.3	20 05	C6.6	16	05.4	11	C2.2	.	.	22	02.8	17	04.4	.	.	.	.	.	.	19							
V	-	09.9	16.8	11.4	12.4	17.6	07.5	24.3	21 02.6	15 04	C0.8	C2	00.5	17	C2.3	.	.	21	02.9	21	05.7	.	.	.	.	.	.	28							
VI	-	12.5	19.1	13.7	14.8	20.3	05.7	26.5	04 03.4	14 19	C3.3	C9	02.4	01	00.1	.	.	20	02.8	16	04.3	.	.	.	.	.	.	25							
VII	-	15.5	23.7	16.6	16.1	24.4	12.2	24.1	30 07.2	26 12	C1.4	C6	02.9	.	.	25	03.5	15	04.3	02	00.5	.	.	.	.	.	.	31							
VIII	-	15.4	25.8	17.8	19.3	26.5	13.5	32.7	16 05.2	13 04	C0.5	C1	00.4	C1	00.1	.	.	29	04.9	07	01.8	01	00.1	.	.	.	.	50							
IX	-	16.9	26.3	14.7	14.2	21.0	03.3	26.9	14 C1.6	27 03	C0.3	C1	00.8	.	.	.	.	23	03.7	10	02.4	04	C0.8	.	.	.	.	46							
X	-	03.3	09.8	04.7	05.6	10.6	C1.7	15.1	18 -03.1	30 31	C4.3	C9	01.8	06	01.7	.	.	21	02.7	05	01.4	03	00.5	.	.	.	.	22							
XI	-	03.0	09.1	04.1	05.1	04.8	01.3	12.9	08 -04.2	03 10	C1.3	C4	01.3	06	01.8	.	.	24	63.0	07	01.7	01	00.2	.	.	.	.	38							
XII	-	-01.0	05.7	00.5	01.4	06.5	-02.1	12.4	03 -07.1	15 10	C1.6	C5	01.4	12	C4.2	.	.	21	02.7	01	00.1	05	00.6	.	.	.	.	39							
GOD.	-	06.7	13.9	08.4	09.4	14.8	04.9	32.7	16W -07.1	15X	02.2	124	02.2	71	02.9	69	02.2	.	.	280	03.2	141	04.1	19	00.5	.	.	.	391						
VEDRIJAN																																			
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																																			
I	-	04.1	C7.9	C5.3	05.7	C9.2	C3.3	16.0	21 06.0	26.15	.	.	62	24.0	.	.	11	02.7	C2	00.4	09	C1.8	.	.	01	00.2	08								
II	-	05.8	09.4	C6.4	07.3	10.5	05.0	14.6	15 01.0	07	.	.	65	23.0	.	.	20	05.5	.	.	07	02.2	.	.	.	.	02								
III	-	07.1	12.9	08.7	05.4	14.0	06.2	25.0	22 00.5	11	.	.	48	22.8	.	.	12	03.0	01	00.2	25	05.9	.	.	03	C0.4	04								
IV	-	08.9	15.1	10.0	11.3	16.6	08.0	21.0	08 05.0	26.16	.	.	56	20.7	.	.	15	04.1	01	00.1	14	03.8	.	.	.	04	C1.6								
V	-	12.9	18.3	13.7	14.7	20.0	11.2	26.5	21 07.4	24	.	.	42	12.6	.	.	18	04.7	C3	00.4	22	05.8	.	.	05	C1.3	03								
VI	-	15.2	20.6	16.4	17.2	22.1	13.3	26.0	05 07.5	10	.	.	41	13.3	.	.	23	06.0	.	.	18	04.4	.	.	06	C1.3	02								
VII	-	18.7	25.1	20.1	21.0	26.4	16.4	31.5	31 11.2	19	.	.	45	16.4	.	.	21	05.1	.	.	25	06.4	.	.	01	C0.3	03								
VIII	-	20.1	27.3	22.2	23.0	26.5	18.8	34.0	16 11.4	11	.	.	59	22.5	.	.	11	02.5	.	.	18	04.6	.	.	03	C1.4	02								
IX	-	19.4	22.0	17.2	18.0	23.2	14.6	25.6	14 07.0	27	.	.	59	25.5	.	.	10	02.8	.	.	13	02.7	.	.	01	C0.5	07								
X	-	07.1	12.0	08.0	08.6	19.2	06.0	17.5	07 02.4	31	.	.	55	22.1	.	.	15	04.0	01	00.1	16	03.7	.	.	03	00.9	03								
XI	-	07.1	11.0	07.8	08.5	12.0	06.1	15.8	11 02.0	02	.	.	39	15.5	.	.	22	05.3	.	.	20	04.8	.	.	01	C0.2	08								
XII	-	04.4	08.7	09.5	06.0	09.6	C3.4	15.5	03 -00.6	15	.	.	46	13.6	.	.	20	04.3	01	00.1	13	03.1	.	.	04	C1.3	09								
GOD.	-	10.6	15.9	11.4	12.6	17.1	09.4	34.0	16W -00.6	15X	02.0	10.0	605	20.0	.	.	198	04.5	09	00.3	200	04.6	.	.	32	C1.1	51								
RATECE-PLANICA																																			
$\varphi = 46^{\circ}30' N \lambda = 13^{\circ}43' E$ Gr. AG = + 54 min.																																			
I	-	69C.7	-03.3	C2.8	-02.2	-01.2	03.3	-04.6	04.2	19 -07.8	27.24	.	.	07	01.6	.	.	01	00.1	05	00.7	02	C0.2	78											
II	-	683.9	-02.4	04.3	00.1	00.8	04.9	-01.9	C9.4	12 -05.4	09	.	.	66	00.9	C6	01.0	04	00.9	03	00.3	06	00.6	09	01.4	.	.	50							
III	-	687.3	-01.0	07.7	01.3	02.3	08.5	-02.0	15.3	22 -07.0	12	.	.	04	00.7	C6	01.4	01	00.2	25	05.9	.	.	03	C0.4	04									
IV	-	684.3	00.8	09.8	04.1	04.7	10.8	-01.0	17.0	12.09 -06.4	26	.	.	07	02.1	13	C3.2	03	00.4	04	00.6	03	00.4	02	C0.3	58									
V	-	685.1	06.9	15.0	08.4	09.7	15.8	03.5	22.2	22 00.0	25.24	.	.	03	00.7	C3	00.6	10	01.6	02	00.3	06	01.1	.	.	.	69								
VI	-	686.5	16.4	16.6	10.7	11.9	18.1	05.9	25.0	04 -01.4	12	.	.	02	00.7	C6	C1.3	06	02.0	07	01.9	02	C0.2	68											
VII	-	686.1	21.4	13.9	15.4	22.1	06.6	27.0	30 02.8	26	.	.	01	00.4	C16	C3.3	03	00.6	04	03.9	13	03.0	01	C0.2	56										
VIII	-	690.2	12.5	22.2	14.8	16.1	23.0	10.0	30.7	15 04.2	13	.	.	02	00.3	11	C2.5	06	00.9	04	00.7	06	00.7	01	.	68									
IX	-	688.2	C7.6	16.8	09.1	11.1	17.7	05.5	24.8	14 -02.4	27	.	.	0																					

Mesec	Oblačnost Nm (0-10)			Insolacije broj sati	Vlažnost vazduha		Padavine R mm		Broj dana na mesecu																										
					mm	7	14	21	Strelo	Min	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	△	■	≡	■				
	7	14	21	(Dnev.)	mm	7	14	21	Strelo	Min	Max	Dat.	≤	<	<	≥	IN	IN	IN	IN	≥	<	>	IN	IN	IN	IN	•	Δ	○	▲	△	■	≡	■
<b>BR. ST. 1</b>																																			
<b>SR SLOVENIJA</b>																																			
I	7.5	7.2	5.6	6.9	059.2	04.6	56	80	90	68	47	074	029.2	01	.	.	21	.	.	.	.	02	13	12	06	03	07	C6	01	.	.	09	17		
II	6.7	7.6	7.1	7.0	072.5	05.0	89	71	86	61	36	243	061.3	07	.	.	10	.	.	.	.	02	15	13	12	06	13	06	.	.	01	01			
III	5.3	6.7	5.1	5.7	137.0	05.5	87	98	78	74	19	134	077.9	05	.	.	10	.	.	.	.	07	09	11	11	01	06	04	.	.	01	03			
IV	5.5	7.4	5.8	6.2	141.0	05.6	83	53	66	68	27	204	066.1	30	.	.	02	.	.	.	.	03	11	09	06	06	05	.	.	.	02	.			
V	6.4	7.0	6.4	6.9	130.9	08.5	90	64	82	75	32	101	021.6	25	.	.	.	.	.	.	.	13	18	16	03	18	.	.	.	01	07	02			
VI	6.7	7.5	6.7	7.0	132.1	09.7	86	61	83	77	31	370	076.2	30	.	.	02	.	.	.	.	02	11	19	16	09	19	06	.	.	01	11	01		
VII	4.5	6.3	6.4	5.7	211.7	11.8	84	56	83	74	35	222	082.6	16	.	.	14	.	.	.	.	04	03	12	10	06	12	.	.	.	01	06	01		
VIII	4.4	5.5	3.7	4.5	215.4	13.2	91	58	82	78	24	120	037.6	11	.	.	17	12	.	.	.	10	05	10	07	10	.	.	.	01	07	.			
IX	4.6	5.6	4.5	5.0	172.5	11.0	95	73	94	88	51	277	085.6	25	.	.	05	.	.	.	.	08	07	15	12	06	15	.	.	.	01	06	.		
X	6.6	7.7	6.6	7.0	084.5	04.0	93	73	93	87	44	236	055.4	21	.	.	12	.	.	.	.	02	15	20	17	06	20	02	.	.	04	.			
XI	6.8	6.6	6.4	6.6	075.7	05.8	94	72	86	35	196	068.2	20	.	.	13	.	.	.	.	02	12	12	09	06	12	.	.	.	01	01	.			
XII	3.2	5.0	3.4	3.9	077.4	05.9	84	62	84	78	16	021	017.2	12	.	.	25	.	.	.	.	12	05	04	03	01	03	02	.	.	01	01	.		
GOD.	5.7	6.6	5.7	6.0	1510.5	07.6	89	65	84	79	18	2200	085.6	25IX	.	.	93	38	12	.	.	54	119	195	125	58	147	14	03	.	06	.	49	15	25
<b>VEDRIJAN</b>																																			
<b>BR. ST. 2</b>																																			
I	6.6	5.7	5.7	6.0	057.2	05.9	89	80	85	43	047	023.8	01	.	.	.	.	.	07	07	03	12	10	09	01	16	.	.	.	01	09				
II	6.0	6.7	5.5	6.2	091.7	06.5	87	78	86	84	43	162	037.4	01	.	.	.	.	06	07	03	11	12	12	05	12	01	01	.	01	05				
III	5.3	5.2	4.9	5.3	142.5	07.1	83	70	80	76	44	040	027.2	05	.	.	01	.	08	08	09	09	08	06	01	08	02	02	.	.	01	.			
IV	4.6	5.6	5.3	5.2	168.0	06.2	83	75	82	80	42	124	038.5	29	.	.	.	.	04	03	04	08	11	10	05	11	.	.	.	.	.				
V	5.6	6.5	6.1	6.1	175.5	10.6	86	76	85	83	37	131	033.6	25	.	.	04	.	03	02	01	12	14	13	04	14	.	.	.	02	.				
VI	6.0	6.9	6.6	6.5	168.0	12.8	88	81	86	85	59	224	035.1	30	.	.	07	.	02	02	03	12	17	16	08	17	.	.	.	02	.				
VII	3.6	4.5	5.7	5.7	282.6	15.7	85	78	84	82	48	122	048.9	26	.	.	28	03	02	03	03	03	07	07	03	07	.	.	.	04	.				
VIII	3.5	3.7	2.8	3.3	267.0	14.0	82	65	78	75	18	062	040.8	11	.	.	28	12	13	07	05	14	02	06	02	06	.	.	.	02	.				
IX	4.1	4.8	4.5	4.5	195.0	13.6	88	79	87	85	65	203	071.0	25	.	.	14	.	01	12	11	11	08	10	09	05	10	.	.	01	03				
X	7.1	6.5	6.1	6.5	095.2	07.5	88	81	88	86	51	202	047.4	21	.	.	.	.	08	07	02	09	16	14	07	16	.	.	01	01					
XI	7.3	6.7	5.8	6.6	073.2	07.4	90	82	89	87	50	097	018.1	06	.	.	04	03	02	13	10	09	04	10	.	.	.	06	.						
XII	9.8	9.3	9.2	9.4	102.2	06.1	88	82	86	85	49	023	013.9	12	.	.	01	.	05	09	04	04	01	04	.	.	.	06	.						
GOD.	5.5	5.7	5.4	5.5	1859.6	06.8	86	77	84	82	18	1443	071.0	25IX	.	.	01	76	15	16	67	58	65	108	125	115	46	125	03	03	.	02	17	27	
<b>RATEČE-PLANICA</b>																																			
<b>BR. ST. 3</b>																																			
I	7.4	6.3	5.9	6.9	074.2	03.7	95	75	92	87	42	024	016.0	01	.	04	30	.	.	01	03	11	06	03	01	01	06	.	.	01	08	31			
II	7.8	7.8	6.4	8.0	056.5	04.1	92	71	89	84	45	098	032.3	07	.	.	17	.	.	.	.	17	15	08	03	11	07	01	.	.	01	02	21		
III	8.3	8.3	7.2	6.5	113.8	04.4	96	61	88	82	29	115	053.3	05	.	01	23	.	.	.	03	15	10	07	03	03	07	.	.	01	01	23			
IV	6.4	7.7	6.2	6.8	141.4	04.6	92	53	78	74	24	093	027.1	29	.	.	17	.	.	.	.	03	11	08	06	04	07	03	.	.	01	.			
V	6.5	7.0	6.6	6.8	164.1	06.6	89	50	82	74	31	068	019.6	25	.	.	02	01	.	.	.	02	13	15	10	02	15	.	.	.	03	01			
VI	6.0	6.5	6.2	6.7	161.2	06.0	90	56	83	76	32	248	039.0	30	.	.	02	01	.	.	.	03	13	19	15	07	18	02	.	.	06	01			
VII	4.5	5.2	5.3	5.0	261.7	09.2	84	47	80	70	27	160	034.4																						

Mesec	Vrstdinski Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vatre ND, Pm (0-12)																
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.		
$\psi = 46^{\circ}23' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = + 55$ min.																												
I	561.0	-05>3	-04+1	-05+1	-04+9	-06+1	-07+5	03+4	22 -12.6	18 03	02+2	04	02+4	04	01+3	10	03+8	02	00+4	02	00+5	07	03+3	45	24+8	16		
II	554.9	-08+7	-06+8	-06+2	-06+0	-05+6	-10+1	02+6	11 -15.6	07 12	00+6	03	01+2	05	01+5	26	10+1	02	01+0	01	00+4	.	.	30	17+1	05		
III	558.8	-06+0	-04+1	-05+7	-05+4	-03+1	-07+5	05+4	21 -13.3	11 06	02+3	03	01+1	02	00+6	44	17+6	.	.	02	00+8	04	00+8	18	08+2	14		
IV	556.8	-0+6	-04+5	-05+9	-05+7	-03+4	-0d+1	01+4	12+10	-14.7	17 05	02+8	03	01+3	02	00+7	26	09+6	03	01+7	03	01+2	05	01+7	26	10+5	17	
V	559.5	-01+7	00+1	-01+1	01+4	-03+5	07+1	14 -0+2	24 16	06+7	01	00+4	06	02+3	12	04+0	01	00+4	01	00+2	02	00+7	38	14+1	16			
VI	561.6	00+8	02+3	01+3	01+5	04+2	-00+8	10+2	04 -0+2	13+08	18	07+7	01	00+4	09	01+6	13	04+7	01	00+4	.	04	01+6	35	14+6	13		
VII	565+2	04+5	06+4	05+1	05+3	08+0	02+6	13+3	30 -0+0	20 11	04+7	02	00+5	05	01+5	13	04+1	.	.	.	02	00+9	44	19+2	16			
VIII	566.9	06+0	08+7	07+1	07+4	10+0	05+3	16+6	15 -0+0	11 07	02+4	02	00+5	03	00+8	37	12+3	02	00+9	01	00+3	.	.	19	06+8	22		
IX	563.5	03+2	04+4	03+4	03+6	06+5	01+1	12+2	06 -0+6	27 16	06+9	07	00+4	04	01+4	27	08+2	02	00+7	.	.	02	01+0	13	06+6	24		
X	555+1	-07+5	-05+8	-07+0	-06+8	-04+2	-0+0	-0+6	25 -12.9	31 28	12+8	02	00+7	07	02+8	11	04+0	03	01+7	02	00+6	03	01+4	26	11+6	11		
XI	558+7	-0+6	-04+9	-05+5	-05+3	-02+8	-0+0	03+0	23 -14+2	01 33	20+8	05	02+5	02	01+1	16	06+0	01	00+4	.	.	03	01+7	19	11+0	11		
XII	560+3	-05+5	-04+4	-05+3	-05+2	-02+3	-0+2	05+1	22 -17+7	13 13	08+4	01	00+4	03	01+5	05	01+5	.	.	.	03	01+1	63	35+9	05			
GOD.	560.2	-02+6	-01+1	-02+3	-02+1	00+6	-04+5	16+6	15+M	-17+7	15+XII	168	10+1	29	01+3	48	01+6	240	09+6	17	01+0	12	00+7	35	01+7	376	18+7	170
$\psi = 46^{\circ}01' N \lambda = 13^{\circ}55' E$ Gr. $\Delta G = + 56$ min.																												
I	-	00+1	02+2	00+2	00+2	07+3	03+4	-02+6	11+7	20 -0+0	14	01	00+1	.	.	17	01+8	.	.	.	07	00+7	01	00+1	05	00+5	62	
II	-	00+2	02+2	00+8	01+0	03+1	-01+3	05+1	04 -0+3	28	.	.	.	.	27	03+2	.	.	.	07	01+0	05	00+6	04	00+4	41		
III	-	01+6	05+1	02+4	03+6	03+0	06+1	-00+4	17+0	22 -0+1	01	.	.	.	40	04+1	.	.	.	08	00+8	02	00+2	.	.	43		
IV	-	03+5	07+3	04+4	04+9	08+1	01+0	13+1	09 -0+0	14	.	.	03	00+6	33	03+8	.	.	.	02	00+2	02	00+3	.	.	50		
V	-	08+9	11+9	08+2	09+3	14+8	05+5	19+5	21 01+0	24	02	00+4	.	.	10	01+0	.	.	.	12	01+5	.	.	01	00+2	68		
VI	-	11+4	14+6	10+7	11+9	15+4	07+7	22+7	04 -0+5	10	.	.	.	.	15	04+7	.	.	.	17	02+0	.	.	01	00+2	57		
VII	-	14+5	18+4	14+0	15+3	19+7	10+3	25+0	30 05+5	20	02	00+2	.	.	17	01+8	.	.	.	16	01+7	14	01+4	01	00+5	43		
VIII	-	15+3	19+7	15+8	16+6	20+8	12+6	27+7	17 05+5	11	.	.	.	.	28	02+9	.	.	.	04	00+4	01	00+1	.	.	60		
IX	-	10+7	14+3	11+0	11+8	15+9	08+2	23+3	13 02+5	27	.	01	00+1	27	03+1	.	.	.	08	01+0	01	00+1	.	.	53			
X	-	01+6	04+3	02+2	02+6	05+7	-00+2	09+5	04 -0+0	31+30	02	00+2	.	.	24	02+4	.	.	.	06	00+7	02	00+3	04	00+5	55		
XI	-	01+7	04+0	02+1	02+5	04+9	-00+1	10+3	17 -0+1	30	.	.	10	01+0	.	.	.	11	01+9	03	00+3	01	00+1	65				
XII	-	00+9	03+0	01+0	01+5	04+3	-01+6	11+0	29 -0+0	15	01	00+1	05	01+2	03	00+3	.	.	07	00+7	05	00+5	06	00+9	66			
GOD.	-	05+9	08+9	06+1	06+8	10+0	03+3	27+7	17+M	-07+1	04+M	08	00+2	09	00+9	251	02+8	.	.	.	105	01+3	36	00+8	23	00+5	663	
$\psi = 46^{\circ}21' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = + 57$ min.																												
I	-	-01+2	03+2	00+4	00+7	03+7	-02+1	16+0	20 -0+4	23	18	02+7	13	02+6	.	.	06	01+4	10	01+2	01	00+1	.	.	10	01+9	35	
II	-	01+9	07+0	03+7	04+1	05+7	05+7	12+9	12 -0+0	09	11	01+4	16	03+3	.	.	11	02+5	07	01+0	04	00+6	.	.	07	01+3	28	
III	-	02+3	10+1	05+9	06+0	10+8	01+7	21+5	22 -0+0	11	11	01+2	17	03+6	.	.	13	03+4	04	00+6	03	00+4	.	.	04	00+5	40	
IV	-	04+6	12+1	08+4	08+4	13+3	02+3	19+1	10 -0+6	16	09	01+6	15	03+9	.	.	13	03+1	07	01+5	01	00+1	.	.	13	01+4	32	
V	-	10+3	17+1	12+2	13+0	18+3	07+2	24+4	21+20	03+2	10	10	01+3	08	02+1	.	.	10	01+9	07	01+0	06	00+9	.	.	11	01+9	41
VI	-	12+7	18+8	14+5	15+1	20+1	09+7	25+7	04 -0+3	12	07	01+5	12	03+1	.	.	07	01+9	05	01+1	10	01+7	.	.	02	00+3	47	
VII	-	14+4	22+8	17+4	18+0	23+8	11+7	28+4	30 08+0	26+09	08	01+2	06	01+4	.	.	05	01+2	09	01+0	03	00+7	.	.	05	00+8	56	
VIII	-	15+7	23+6	18+7	19+2	24+7	13+3	30+9	04 -0+7	12	09	01+6	11	02+4	.	.	17	03+8	05	00+9	02	00+5	.	.	07	01+0	42	
IX	-	11+0	18+3	13+2	13+7	17+9	10+3	23+6	14 -0+5	27	11	01+6	06	01+4	.	.	12	02+9	11	01+8	.	.	.	.	08	01+2	43	
X	-	02+7	08+6	04+2	04+6	07+9	02+0	14+8	25 -0+4	23	22	04+1	06	01+6	.	.	06	01+2	10	01+5	03	00+9	.	.	07	01+1	39	
XI	-	02+0	08+2	03+6	04+3	08+8	00+4	14+5	18 -0+0	30+09	17	01+6	07	01+2	.	.	11	02+2	09	01+6	01	00+4	.	.	11	02+3	39	
XII	-	-01+7	06+5	00+7	01+6	07+3	-03+0	11+9	04 -0+8	15	27	05+4	12	02+5	.	.	11	01+9	04	00+4	02	00+3	.	.	11	03+1	26	
GOD																												

Meseč	Oblačnost Nm (0-10)			Vlažnost vazduha %	Padavine R mm	Broj dana na mesečno																											
	Temperatura Istočnjak Broj sati					Um			Tx			Tn			Tx			Tn			F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	Δ	▲	□	■	☒
	7	14	21	Sred. (Dnev.)	mm	7	14	21	Spred. znač.	mm	Σ	Tx	Tx	Tn	Tn	Tn	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	Δ	▲	□	■	☒			
KNEĐARICA																																	
BR. ST. 6	II = 2514 m H <sub>b</sub> = 2519,0 m h = 2,0 m h = 1,0 m																																
I 6,2 5,9 4,7 5,5	109,1	02,0	71	66	69	69	13	C47	C14,1	01	06	23	31	•	•	•	20	11	C3	C6	13	11	01	•	13	•	•	•	13	31			
II 7,3 7,6 6,4 7,1	057,8	02,1	87	66	86	86	20	083	00,7	07	14	26	28	•	•	•	14	08	03	14	19	17	•	•	01	23	23	31					
III 6,0 7,4 7,3 7,0	117,9	02,5	80	82	85	P2	13	099	C24,1	05	12	25	30	•	•	•	09	02	03	15	12	08	04	01	11	02	02	24	31				
IV 6,3 7,9 7,2 7,2	108,0	02,5	84	E0	E6	F6	17	080	G15,6	29	06	47	30	•	•	•	C6	01	03	16	19	11	02	•	19	•	•	23	30				
V 6,3 8,2 6,4 7,0	142,5	03,4	81	84	82	20	094	C26,5	25	•	15	27	•	•	•	13	01	02	16	17	10	03	04	16	C2	03	•	•	03	24	31		
VI 7,3 8,4 6,8 7,5	125,8	03,4	83	84	82	B3	40	381	G9,0	30	•	14	17	•	•	•	12	04	01	15	16	11	12	18	01	01	02	05	01	10	23	30	
VII 4,6 7,5 5,5 5,9	232,5	03,1	71	78	80	76	36	200	03,6	25	•	11	09	•	•	•	13	03	01	05	14	06	07	11	07	03	•	02	05	14	03		
VIII 4,9 7,1 4,7 7,6	189,2	03,7	71	78	73	J4	15	200	07,4	24	•	•	04	•	•	•	06	02	03	10	15	13	04	15	2	•	04	04	19	19			
IX 4,8 8,4 4,7 5,3	172,7	04,3	75	78	72	75	17	240	C38,7	25	•	03	10	•	•	•	11	04	06	10	16	15	08	12	12	03	•	01	03	•	04	15	10
X 7,2 7,7 7,9 7,6	080,2	02,3	88	87	90	H3	37	210	D26,4	05	10	31	31	•	•	•	16	07	03	17	22	21	C9	•	22	•	•	02	24	31			
XI 6,8 6,4 5,7 6,3	109,1	02,4	77	75	73	75	20	104	E17,1	06	12	23	30	•	•	•	18	14	01	09	19	18	03	02	19	•	•	03	01	18	30		
XII 4,6 4,5 3,8 4,4	128,3	01,6	69	63	66	66	14	012	007,6	12	13	18	24	•	•	•	20	16	06	03	06	03	•	06	•	•	•	06	10	31			
GOD. 6,6 7,0 5,9 6,4	1571,1	03,2	78	78	78	78	13	1750	C96,0	261	73	196	274	•	•	•	160	74	35	136	194	154	53	56	164	05	07	04	17	01	37	232	286
VCJSKE																																	
BR. ST. 7	II = 1070 m H <sub>b</sub> = m h <sub>t</sub> = 2,0 m h = 1,0 m																																
I 7,2 6,6 5,0 6,3	-	-	-	-	-	-	-	075	039,6	01	•	04	27	•	•	•	04	11	09	07	02	07	06	C2	•	•	12	31					
II 8,0 8,3 7,7 8,0	-	-	-	-	-	-	-	202	D7,2	07	•	03	17	•	•	•	01	18	14	14	06	11	10	03	•	01	•	10	18	18			
III 7,5 7,8 6,7 7,4	-	-	-	-	-	-	-	100	C38,7	05	•	05	16	•	•	•	03	15	09	08	05	03	04	•	•	02	12	22					
IV 5,5 7,6 5,8 6,4	-	-	-	-	-	-	-	180	D80,0	29	•	•	07	•	•	•	04	10	11	10	06	10	04	•	•	01	C2	CS	01				
V 6,1 8,1 6,4 6,8	-	-	-	-	-	-	-	127	D28,5	25	•	•	•	•	•	•	02	13	20	17	03	20	01	•	•	02	05	05	•				
VI 7,2 7,7 5,5 6,9	-	-	-	-	-	-	-	260	D45,0	07	•	•	•	•	•	•	02	10	18	16	08	18	02	•	•	01	05	01	•				
VII 4,6 5,4 4,7 4,9	-	-	-	-	-	-	-	100	C44,6	26	•	•	•	01	•	•	05	04	10	09	02	10	•	•	02	02	02	•					
VIII 5,8 5,4 4,0 5,1	-	-	-	-	-	-	-	137	D51,0	29	•	•	•	06	•	•	05	04	09	05	04	•	•	01	04	06	•						
IX 6,1 6,2 4,9 5,7	-	-	-	-	-	-	-	415	A15,9	25	•	•	•	•	•	•	04	10	17	16	08	17	•	•	02	07	05	•					
X 7,9 6,1 7,4 7,8	-	-	-	-	-	-	-	396	D92,1	21	•	•	14	•	•	•	02	19	20	19	05	17	11	03	•	03	04	15	07				
XI 8,1 7,2 6,5 7,3	-	-	-	-	-	-	-	188	E51,3	20	•	•	17	•	•	•	04	16	12	10	06	11	05	•	•	02	01	04	15	15			
XII 4,9 5,3 4,0 4,8	-	-	-	-	-	-	-	044	D36,0	12	•	02	21	•	•	•	06	05	04	03	01	04	01	•	•	•	08	14	14				
GOD. 6,6 7,0 5,8 6,4	-	-	-	-	-	-	-	2224	A165,9	251X	•	18	119	07	•	•	•	42	140	153	138	61	137	46	08	•	13	•	43	54	108		
RACCUVLJICA																																	
BR. ST. 8	II = 495 m H <sub>b</sub> = m h <sub>t</sub> = 2,0 m h = 1,0 m																																
I 6,3 6,5 7,1 7,4	-	04,4	93	84	93	90	42	041	D26,0	01	•	02	25	•	•	•	02	16	08	05	01	04	05	•	•	12	18						
II 7,0 7,3 7,7 7,3	-	05,1	87	73	86	82	42	081	C46,0	07	•	03	17	•	•	•	03	15	15	06	02	12	04	•	•	05	02	02	30				
III 6,5 6,7 5,4 6,2	-	05,5	68	66	81	77	33	089	C59,1	05	•	•	14	•	•	•	05	13	09	07	01	05	05	•	•	02	02	02	30				
IV 5,8 6,8 6,0 6,0	-	06,5	88	70	79	76	36	101	D57,0	29	•	•	04	•	•	•	04	01	06	11	07	02	10	01	•	•	01	01	01	30			
V 5,5 6,5 5,9 6,0	-	10,2	85	69	83	87	45	070	D22,0	25	•	•	•	01	•	•	01	01	03	09	16	10	03	16	•	•	02	04	04	30			
VI 5,6 6,7 6,1 6,8	-	11,1	90	77	88	85	50	248	D72,1	30	•	•	01	•	•	•	03	07	16	14	06	17	16	16	•	•	02	03	03	30			
VII 4,6 4,9 5,4 4,8	-	12,0	51	61	82	78	29	183	D65,0	16	•	•	14	•	•	•	08	06	12	09	05	12	16	16	16	•	•	01	01	01	30		
VIII 4,9 4,8 4,5 4,8	-	13,3	91	61	88	80	33	092	D23,8	11	•	•	14	03	•	•	08	08	15	10	03	15	15	15	•	•	05	01	01	30			
IX 5,1 5,5 5,7 5,4	-	10,5	94	73	92	E6	48	213	D79,0	25	•	•	•	•	•	•	07	09	14	14	06	14	14	14	•	•	03	01	01	30			
X 7,6 7,1 6,4 7,1	-	05,8	95	76	91	87	49	207	D52,5	05	•	•	09	•	•	•	02	16	20	13	07	20	13	13	•	•	01	05	01	30			
XI 6,4 6,5 6,6 6,5	-	05,4	92	76	88	83	41	304	D47,2	10	•	•	08	•	•	•	06	09	05	13	10	02	13	13	13	•	•	04	01	01	30		
XII 5,2 5,3 5,2 5,1	-	11,4	85	68	77	77	46	112	D48,6	26	•	•	06	•	•	•	06	09	12	09	12	04	12	12	12	•	•	06	01	01	30		
XIII 5,2 4,3 4,0 4,7	-	13,1	89	70	80	82	47	175	D47,1	29	•	•	13	•	•	•	04	10	09	12	06	13	12	12	•	•	06	01	01	30			
IX 5,7 5,6 5,6 5,9	-	10,1	90	75	88	84	44	274	D108,5	25	•	•	•	02	01	05	12	15	12	08	05	10	10	06	15	15	15	•	•	04	05	05	30
X 6,1 6,0 5,8 6,0	-	05,6	92																														

Mesec	Vazdušni pritisak Pn mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																				
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dnes)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.			
$\varphi = 46^{\circ}13'$ N $\lambda = 14^{\circ}29'$ E Gr. $\Delta G = + 58$ min.																														
I	734.7	-01.1	02.6	01.3	00.5	03.4	-01.9	18.0	20	-07.5	22	04	00.5	03	00.4	13	01.6	C3	00.3	02	00.2	01	00.2	10	01.5	06	C1.0	51		
II	727.4	01.2	07.8	03.0	03.7	08.7	-06.3	13.1	12	-07.6	09	03	00.5	01	00.1	C9	01.5	10	01.7	C2	00.2	11	01.8	19	03.4	11	C1.9	18		
III	730.5	00.9	10.7	04.4	05.1	11.7	-00.3	23.8	22	-06.7	14	07	00.9	03	00.6	09	01.4	C4	00.9	05	00.6	09	01.2	16	02.5	07	C1.0	33		
IV	727.3	03.1	13.0	06.2	07.1	14.3	-06.2	19.4	10	-07.0	17	09	C1.6	04	00.9	11	02.6	11	02.0	04	00.7	04	00.6	14	02.3	08	C1.4	25		
V	727.6	06.8	17.5	10.7	12.2	19.0	05.0	25.2	20	-00.4	26	03	00.6	01	00.1	10	C1.9	C5	00.9	07	01.0	13	02.8	17	02.9	05	C1.0	32		
VI	726.4	12.1	19.5	13.4	14.6	21.1	08.1	27.4	04	-06.2	12	05	01.1	03	00.7	10	C2.0	04	00.7	08	01.6	10	01.8	08	01.5	04	00.9	37		
VII	730.5	14.5	23.5	16.3	17.7	24.9	09.8	30.7	20	07	01.7	01	00.1	14	C2.1	04	00.7	10	01.6	05	01.1	15	03.6	06	C1.2	31				
VIII	731.1	15.2	24.6	16.9	18.4	25.9	11.4	32.1	17.6	05.2	13	01	00.2	03	00.4	10	01.7	12	02.3	05	00.8	02	00.3	13	01.9	08	C1.5	39		
IX	730.1	10.3	19.0	12.2	13.4	20.4	07.6	25.6	14.0	-01.7	27	04	00.8	01	00.1	11	01.9	06	00.9	08	01.3	02	00.4	08	01.2	12	C1.7	38		
X	726.4	02.6	08.9	03.6	04.7	05.6	06.6	14.4	25	-05.7	30	*	*	01	00.1	11	C2.0	03	00.3	09	01.4	02	00.5	19	02.9	06	C1.3	42		
XI	730.9	01.1	08.1	02.6	03.6	09.2	-01.0	15.4	18	-07.2	09	02	03	00.3	C4	00.2	C1	00.1	06	00.6	04	00.5	04	00.9	15	02.2	08	C1.6	47	
XII	732.2	-03.3	04.5	-00.7	07	00.0	05.9	-04.7	16.7	29	-11.5	15	01	00.1	07	01.2	C8	01.1	02	00.4	02	00.5	08	01.1	21	03.2	05	C1.2	38	
GOD.	726.8	05.5	13.3	C7.4	08.4	14.5	02.9	32.1	17.6	VMM	-11.5	15	04	48	00.9	30	00.6	117	01.8	71	01.3	66	01.1	71	01.5	175	02.6	86	C1.4	431
$\varphi = 46^{\circ}21'$ N $\lambda = 14^{\circ}30'$ E Gr. $\Delta G = + 58$ min.																														
JEZERSKO																														
BR. ST.12																														
I	-	-01.6	C2.9	06.6	00.6	01.1	C3.4	-03.2	13.3	20	-07.6	15	*	*	14	02.5	C5	01.2	14	03.5	*	*	03	00.7	*	*	01	C0.2	56	
II	-	00.1	04.3	00.7	01.5	C5.6	C0.5	-01.6	07.9	16	-05.4	09	*	*	14	03.6	C7	01.8	C10	03.0	*	*	07	02.3	01	00.5	01	00.3	44	
III	-	-00.4	07.5	01.7	02.6	C6.4	-01.4	19.7	22	-08.4	11	*	*	26	05.2	C5	01.1	06	01.4	01	00.2	08	02.5	01	00.2	01	00.3	45		
IV	-	01.0	09.0	03.4	04.2	10.3	-03.5	16.1	12.9	-09.6	20	*	*	26	06.4	C7	01.8	05	01.0	*	*	10	02.4	01	00.2	02	00.5	39		
V	-	06.2	13.9	07.7	08.0	15.3	03.2	20.8	20	-00.8	26	*	*	15	02.5	C6	00.9	15	04.0	*	*	10	02.9	02	00.7	01	C0.1	44		
VI	-	09.5	15.6	05.8	11.2	17.3	05.3	24.1	04	-06.2	12	*	*	18	04.0	C3	00.8	14	03.3	*	*	07	02.1	02	00.5	03	00.8	43		
VII	-	12.0	19.7	13.4	14.6	21.2	09.4	27.0	30	04.2	26	*	*	11	02.5	C5	02.1	18	05.9	*	*	10	03.1	01	00.3	05	C1.6	40		
VIII	-	11.8	21.8	13.8	15.3	22.6	09.1	25.4	15	03.9	13	*	*	11	02.6	C5	01.2	14	03.6	*	*	09	02.4	02	00.5	01	00.2	51		
IX	-	07.3	16.3	09.2	10.5	17.7	05.9	24.8	14	-00.3	27	*	*	11	02.4	C5	01.0	13	03.5	*	*	07	02.0	02	00.6	*	*	52		
X	-	00.3	05.6	01.7	02.2	07.1	-01.0	12.6	25	-03.3	23	*	*	26	05.9	C2	00.3	14	04.9	*	*	06	02.2	*	*	*	*	45		
XI	-	00.4	04.8	01.3	01.9	06.1	-01.3	12.6	18	-06.1	29	*	*	08	01.6	C2	00.7	30	10.3	*	*	02	00.4	*	*	04	00.7	44		
XII	-	-02.1	02.9	-01.2	-00.4	C4.2	-03.0	11.4	08	-09.5	24	*	*	18	04.9	C1	00.3	13	03.9	*	*	01	00.5	*	*	03	00.6	57		
GOD.	-	03.7	10.4	05.1	06.1	11.6	C1.8	29.4	15	VMM	-09.5	24	*	*	198	04.2	56	01.3	166	05.0	01	00.2	80	02.3	12	00.5	22	C0.8	560	
LJUBLJANA-BEZIGRAD																														
BR. ST.13																														
I	744.7	00.1	C2.8	01.3	01.4	03.7	-04.4	11.3	20	-02.4	21	07	00.7	29	02.9	C8	00.8	13	C1.4	04	00.5	07	C1.2	30	C0.6	12	C1.2	07		
II	733.3	03.5	C0.5	04.5	05.7	09.3	02.8	15.0	19	-02.6	09	C7	00.9	23	03.8	10	01.6	12	01.8	02	00.2	14	03.5	05	01.2	26	C0.9	05		
III	730.3	03.4	11.4	07.4	07.4	12.4	03.0	24.4	22	-02.8	14	04	00.4	24	02.9	13	C2.2	17	02.9	05	00.8	17	04.0	08	01.0	04	00.7	01		
IV	733.1	05.3	13.9	09.4	09.5	14.8	03.8	26.3	09	-01.3	20	06	00.9	34	05.9	14	C2.4	17	02.8	03	00.8	11	02.6	01	00.1	03	C0.5	01		
V	-	733.3	10.7	18.5	13.4	14.0	19.7	06.7	26.1	20	D4.0	10	06	C1.0	21	02.9	13	01.6	07	00.8	01	00.1	28	06.1	08	C1.4	02			
VI	734.2	13.0	20.4	15.6	16.2	21.9	11.0	26.6	04	04.6	12	08	01.6	10	01.0	C8	01.1	11	01.6	16	C2.2	24	05.0	06	01.2	02				
VII	736.2	15.8	24.4	19.4	19.7	25.9	13.3	31.7	30	05.4	20	04	00.5																	

Mjesec	Oblačnost Nm (0-10)			Inzolacijska broj sati	Vlažnost vazduha		Padavine R mm		Broj dana na sata:																											
	7	14	21		Um t		Σ	Max	Min	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	Δ	▲	▲	■	T	≡										
					mm	7	14	21	Streš.	Min	≤	<	IV	IV	IV	IV	IV	IV	>	IV	IV	IV	IV	IV	IV											
<b>BR. ST.11 BRNIK-LETALISTE</b>																																				
I	9.4	8.5	8.0	8.6	032.0	04.4	58	88	94	93	24	037	021.2	01	.	C3	31	.	.	C1	.	01	23	12	07	01	10	08	02	01	01	.	.	21	14	
II	8.0	7.9	7.6	7.8	060.4	01.1	95	67	89	84	30	051	C29.5	07	.	16	.	.	01	.	01	17	13	07	01	13	01	01	.	.	02	07				
III	7.1	7.3	7.1	7.2	115.4	05.3	96	58	90	81	30	055	C20.1	05	.	20	.	.	01	.	03	14	08	06	03	04	08	03	.	.	01	10	08			
IV	5.7	7.9	6.3	6.6	153.8	05.4	91	47	79	72	21	059	C6.2	29	.	19	.	.	02	.	02	12	11	07	01	11	.	.	.	.	.	04	.			
V	5.5	7.0	6.4	6.3	197.3	08.1	90	55	86	77	23	080	C22.2	25	.	01	01	.	01	.	01	09	16	05	03	16	.	.	.	.	.	07	05			
VI	7.0	6.4	5.5	6.4	185.2	09.9	92	58	88	79	30	263	C52.2	30	.	01	03	.	03	.	02	08	17	15	08	17	.	.	.	.	.	12	06			
VII	4.9	4.9	4.5	4.8	285.4	11.4	89	52	86	76	35	123	C44.8	26	.	17	01	.	06	04	11	08	04	11	.	.	.	.	.	08	06					
VIII	5.6	6.6	5.3	5.2	246.5	13.1	95	59	94	82	30	122	C37.1	11	.	15	07	.	10	04	16	12	04	16	.	.	.	.	.	12	08					
IX	7.4	6.1	5.2	6.2	146.2	10.1	96	66	96	86	33	190	C73.1	25	.	02	02	.	01	.	03	10	14	11	05	14	.	.	.	.	01	07	15			
X	8.8	7.7	7.5	8.0	076.2	05.8	98	73	97	89	39	255	C69.5	05	.	14	.	01	.	01	19	20	17	08	20	.	.	.	.	.	05	16				
XI	7.6	6.9	7.0	7.2	079.1	05.4	96	72	95	88	30	080	C16.5	20	.	19	.	01	.	01	16	14	08	04	14	02	02	.	.	01	08					
XII	5.8	5.9	5.4	5.7	087.6	03.9	93	75	88	85	18	011	C01.5	12	04	.	28	.	05	.	04	06	06	01	01	01	01	.	.	01	14					
GOD.	6.8	6.8	6.2	6.6	1665.3	07.3	94	64	90	82	18	1326	C73.1	25IX	04	03	151	38	06	.	18	.	34	142	156	10E	43	148	20	09	01	01	.	01	56	120
<b>BR. ST.12 JEZERSKO</b>																																				
I	7.2	5.5	5.7	6.1	-	03.9	91	25	89	85	33	033	C23.8	01	.	02	26	.	01	.	04	10	06	04	01	04	05	.	.	.	.	08	20			
II	7.9	7.6	7.4	7.6	-	04.3	89	10	87	82	36	112	C68.5	07	.	01	17	.	02	.	02	17	15	10	02	12	06	.	.	.	.	02	10			
III	6.5	6.9	6.3	6.6	-	04.5	93	63	71	81	31	089	C55.9	05	.	01	19	.	04	12	10	07	03	02	08	.	01	.	.	02	19					
IV	5.6	7.0	6.1	6.4	-	04.6	88	56	82	75	30	100	C04.5	29	.	17	.	04	12	11	08	03	05	02	.	.	.	.	.	01						
V	6.0	7.2	5.4	6.2	-	06.6	91	57	84	77	28	096	C23.2	25	.	02	.	01	.	12	17	12	03	17	.	.	.	.	02	.	.	.				
VI	6.1	6.9	5.4	6.2	-	06.2	89	64	88	80	31	321	C101.7	30	.	01	.	01	.	03	09	20	17	09	20	02	C1	.	.	.	06	01				
VII	4.6	5.7	5.0	5.1	-	09.4	85	56	82	75	35	209	C64.4	26	.	02	.	01	.	04	05	13	12	06	12	.	.	.	05	01						
VIII	4.1	4.8	4.0	4.3	-	10.6	93	59	90	81	35	145	C032.1	11	.	13	.	08	06	15	09	04	15	.	.	.	.	06	.	.	.					
IX	4.6	5.5	4.6	4.9	-	08.3	95	67	93	85	42	283	C112.4	25	.	02	.	01	.	08	66	15	15	05	15	.	.	.	01	05	.	.				
X	6.8	7.3	6.6	6.9	-	04.8	95	74	92	87	40	298	C086.3	21	.	17	.	02	.	01	16	21	17	07	01	01	.	.	02	07						
XI	6.5	6.3	5.6	6.1	-	04.4	89	71	86	82	37	104	C049.7	20	.	21	.	01	.	01	08	12	09	03	12	06	04	.	.	07						
XII	5.1	5.4	3.1	4.5	-	03.5	85	67	83	78	36	020	C019.4	12	01	27	.	05	04	04	01	01	04	01	.	.	.	.	.	06	.	24	24			
GOD.	5.9	6.4	5.4	5.9	-	06.1	90	64	86	80	28	1810	C112.4	25IX	.	05	149	15	.	06	.	44	117	159	116	47	141	39	06	01	.	01	24	16	88	
<b>BR. ST.13 LJUBLJANA-BEŽIGRAD</b>																																				
I	9.5	8.8	8.0	8.8	019.3	04.6	95	67	92	91	52	045	C27.5	01	.	17	.	01	.	25	15	C7	01	11	06	02	01	03	.	.	01	23	05			
II	8.8	7.1	7.0	8.0	042.3	05.5	89	67	81	79	31	049	C22.2	07	.	05	.	01	.	16	11	08	01	11	01	.	.	.	01	07	01					
III	7.2	7.1	6.8	7.1	113.7	05.6	91	57	75	74	27	080	C17.4	05	.	06	.	02	.	02	15	16	07	02	07	07	01	.	03	.	02	10	06			
IV	6.1	7.5	6.1	6.5	161.9	05.6	83	46	66	65	23	056	C10.5	29	.	01	.	01	.	04	14	11	08	02	11	.	.	.	.	04	.	.				
V	6.5	6.7	6.5	6.6	207.4	08.1	87	51	72	70	29	109	C31.0	25	.	03	.	01	.	02	12	15	11	04	14	.	.	.	.	04	02					
VI	6.8	6.4	5.7	6.3	189.4	09.9	88	55	77	73	29	245	C49.0	30	.	06	.	01	.	02	08	17	15	09	17	.	.	.	.	12	04					
VII	5.3	5.4	4.6	4.8	287.4	11.6	85	51	71	69	34	086	C35.0	19	.	15	06	01	.	06	04	11	06	02	11	.	.	.	05	05						
VIII	5.3	4.3	3.2	4.7	243.8	13.7	94	54	82	77	29	168	C038.7	11	.	17	12	01	.	07	06	13	12	05	13	.	.	.	01	06	17					
IX	8.8	5.9	4.6	6.4	145.8	10.8	56	63	85	83	26	168	C42.2	07	.	07	.	01	.	01	11	17	13	05	16	.	.	.	.	05	14					
X	9.4	7.3	6.5	7.9	071.9	06.2	96	71	90	86	40	283	C058.8	05	.	03	.	01	.	02	17	19	09	21	01	01	.	.	.	05	17					
XI	8.3</																																			

Mesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, Fm (0-12)																	
		Tm				Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21	Sred. (Dies)							8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.		
$\varphi = 46^{\circ}04'$ , $N \lambda = 15^{\circ}11'$ , E Gr., $\Delta G = +1h\ 01\ min.$																													
I	-	60.4	64.2	61.6	62.0	59.1	-60.7	16.1	20	-03.4	18	03	60.6	.	.	12	02.3	01	00.1	.	.	.	09	02.1	01	00.3	67		
II	-	64.6	64.4	65.6	64.3	60.2	67.7	14.2	12	-01.6	08	16	64.4	.	.	16	04.7	02	00.5	.	.	.	16	04.2	06	02.7	28		
III	-	64.4	62.0	66.9	67.5	62.7	64.8	25.0	22	-02.2	14	22	64.3	.	.	16	03.8	02	00.5	09	01.5	01	00.4	17	03.4	04	02.0	22	
IV	-	65.9	64.2	66.0	69.5	15.5	63.5	21.6	10	-01.7	05	12	63.1	.	.	26	06.0	01	00.6	07	02.9	01	00.3	24	04.8	02	00.7	17	
V	-	11.2	16.6	12.6	13.9	20.4	08.1	27.5	20	03.9	10	09	11.4	.	.	19	04.8	.	02	00.4	01	00.4	30	05.6	02	00.5	30		
VI	-	13.7	21.0	15.9	16.2	27.6	10.4	27.2	12	04.2	12	06	11.5	01	00.3	15	03.1	01	00.3	01	01.5	.	.	24	04.9	03	00.8	29	
VII	-	16.0	24.5	17.6	18.4	26.2	12.7	31.8	14	05.4	09	11	01.1	.	.	12	02.8	01	00.3	07	01.4	.	.	30	05.8	02	00.9	30	
VIII	-	17.7	25.9	18.9	20.8	15.0	12.8	17.6	13	06.6	13	06	11.5	.	.	24	05.8	.	05	00.9	.	.	19	03.9	06	02.8	33		
IX	-	12.2	20.4	13.9	15.1	21.6	10.5	26.0	C4	06.7	27	03	01.3	.	.	11	01.8	.	08	01.3	.	.	19	03.4	06	02.0	38		
X	-	04.5	10.3	06.0	06.7	11.4	02.0	16.5	25	-01.6	30	19	14.3	.	.	C1	00.2	.	11	02.1	.	.	19	03.9	*	.	43		
XI	-	04.0	10.4	05.5	06.4	10.0	02.2	17.2	17	-01.2	07	27	14.4	.	.	C6	01.3	.	04	0.9	.	.	17	03.5	04	C1.8	32		
XII	-	31.2	67.5	63.1	63.7	66.5	-90.6	15.1	29	-06.6	16	25	65.3	.	.	C3	00.4	.	07	01.1	.	.	09	02.3	06	C1.8	43		
GOD.	-	C6.0	14.0	09.7	10.5	16.0	05.4	37.8	M7	VM -06.9	K4	166	04.2	01	00.3	161	04.0	08	00.4	49	01.6	03	0L.4	233	04.3	42	C1.9	412	
$\varphi = 46^{\circ}37'$ , $N \lambda = 15^{\circ}11'$ , E Gr., $\Delta G = +1h\ 01\ min.$																													
RADUJE CB DRAVI																													
I	-	-60.8	64.1	60.2	60.9	59.2	-02.6	15.5	20	-06.4	23	22	C1	00.1	C1	00.1	C1	00.1	C3	00.3	*	02	00.2	03	00.3	04	C0.4	78	
II	-	C1.9	C8.2	63.5	64.3	C9.4	60.3	15.0	12	-03.6	23	03	66.3	C3	00.6	*	05	00.6	02	00.3	08	01.2	03	00.3	06	C0.6	54		
III	-	02.9	11.4	14.7	15.6	15.3	06.3	12.1	01.7	24.2	22	-04.1	01	01	00.1	04	00.4	C2	00.2	04	00.5	05	00.6	07	01.0	01	00.1	56	
IV	-	04.0	13.4	17.4	18.0	19.0	01.0	21.5	10	-03.0	05	01	00.2	C1	00.1	C2	00.2	05	00.5	03	07	05	00.6	11	01.3	56			
V	-	10.1	18.3	11.9	13.1	19.8	07.1	25.5	27	06.5	10	01	66.1	.	.	C2	00.3	10	01.4	01	00.1	06	00.9	02	00.2	04	00.9	67	
VI	-	12.9	20.1	14.6	15.3	22.3	05.4	26.3	M7	05.0	04	02.6	12	03	C6.3	C1	00.1	C1	00.1	04	00.5	02	00.3	08	01.6	01	00.1	66	
VII	-	15.1	24.3	17.1	18.4	25.4	11.7	36.8	30	07.6	C9	.	.	04	04.4	05	00.7	02	00.3	05	06.6	06	00.8	65					
VIII	-	15.6	25.3	18.0	19.2	26.5	13.6	33.4	16	07.3	13	01	00.1	.	.	C1	00.1	02	00.2	01	00.1	03	00.3	05	04.6	03	00.3	77	
IX	-	11.6	19.6	13.3	14.4	20.8	05.8	27.9	14	03.0	28	05	05.5	.	.	C1	00.1	C3	00.3	03	00.4	04	00.4	05	00.6	05	C0.8	64	
X	-	03.0	10.0	06.8	05.9	11.1	02.6	15.2	07	-02.8	24	01	00.2	02	00.2	C2	00.2	C2	00.4	02	00.4	01	00.1	04	00.4	06	00.6	73	
XI	-	03.0	08.9	03.7	04.8	10.6	01.1	17.7	15	-02.4	04	01	00.1	.	.	C3	00.4	04	00.7	11	01.5	06	00.7	10	C1.3	55			
XII	-	-01.7	05.4	06.0	06.9	07.0	-03.4	11.0	09	-09.0	15	02	00.2	.	.	C7	00.2	C5	00.5	*	01	00.1	01	00.1	06	C0.8	76		
GOD.	-	C6.5	14.1	08.3	09.3	15.4	04.4	32.4	M7	VM -05.0	K5	15	00.3	12	00.3	18	00.2	51	00.7	25	00.5	61	01.0	47	C0.5	795			
$\varphi = 46^{\circ}15'$ , $N \lambda = 15^{\circ}11'$ , E Gr., $\Delta G = +1h\ 01\ min.$																													
CELJE-LEVEC																													
I	-	-60.7	64.2	60.5	61.4	64.6	-02.6	16.5	20	-06.5	24	02	00.2	24	02.4	C1	00.1	C4	00.4	*	.	.	12	01.6	*	03	C0.3	47	
II	-	C2.9	C8.7	63.0	64.7	65.0	05.6	06.6	12	-04.3	23	*	14	01.7	C1	00.1	C8	01.4	*	05	00.6	02	00.3	08	01.2	03	00.3	54	
III	-	02.1	10.9	09.6	06.1	11.7	00.5	23.5	21	-05.5	15	01	00.1	18	02.0	C1	00.1	C7	00.7	*	09	02.1	*	05	00.6	52			
IV	-	03.5	13.7	07.6	08.1	14.5	06.5	24.2	10	-05.2	05	01	00.2	C6.2	18	03.6	C1	00.2	00.9	01.0	02	00.2	13	01.5	06	C0.6	40		
V	-	10.4	18.6	13.6	13.5	19.6	06.6	25.8	20	-06.4	10	02	00.2	27	01.1	C1	00.1	14	02.4	*	.	.	28	03.9	*	09	C1.2	30	
VI	-	12.9	20.6	14.9	15.8	23.0	05.2	27.4	C4	01.5	12	03	03.3	13	01.7	*	07	00.9	*	.	.	27	04.1	01	00.1	10	C1.4	29	
VII	-	15.3	24.2	17.9	18.8	25.4	11.5	30.5	17	06.6	09	02	00.2	12	01.4	C1	00.1	17	02.2	*	.	.	24	04.0	02	00.2	13	01.6	22
VIII	-	15.8	25.3	18.8	19.7	26.2	12.4	34.5	17	06.0	14	06.0	03.2	16	02.2	C2	00.2	04.5	*	.	.	15	01.6	01	00.1	07	00.7	47	
IX	-	11.3	19.8	13.6	14.6	20.6	05.0	27.1	03																				

Mesec	Oblačnost Nm (0-10)				Insolacije broj sati (tjed.)	Vlažnost vazduha				Padavine R mm		Broj dana na sat																			
	7	14	21	Sred. (tjed.)		mm	7	14	21	Sred.	Mn	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(0-10)	R mm	●	★	▲	△	◆	▲	▼	■	
						mm	7	14	21	Sred.	Mn	Max	Dat.	30.00	0.0	0.250	0.020	0.6	8	2.0	8.0	0.1	1.0	0.0	●	★	▲	△	◆	▲	▼
<b>BR. ST-16</b>																															
<b>RAĐEĆE</b>																															
I 9.6 8.1 7.8 8.5	-	04.6 89 82 90 87 42	030 016.6	C1	.	.	.	.	.	.	.	.	.	.	.	.	.	.	21	10	06	01	06	02	.	.	.	.	11	04	
II 6.6 7.6 6.6 7.6	-	05.4 81 60 81 74 24	042 022.4	O7	.	.	.	.	.	.	.	.	.	.	.	.	.	02	15	11	08	01	01	.	.	.	.	07	01		
III 7.5 6.4 6.1 6.7	-	05.5 83 55 78 72 16	C74 027.2	O6	.	.	.	.	03	01	.	.	.	.	.	.	04	03	14	10	07	03	06	07	01	.	.	01	02	02	
IV 6.6 7.4 5.2 6.2	-	05.6 86 46 69 64 16	038 014.3	26	.	.	.	01	.	.	.	.	.	.	.	07	04	14	08	06	01	08	.	.	.	.	.	.	.	.	
V 4.6 7.3 6.9 6.6	-	08.6 85 52 82 73 30	170 038.3	25	.	.	.	.	04	.	.	.	.	.	.	02	04	11	17	15	05	17	.	.	.	.	.	03	.		
VI 7.1 7.3 6.2 6.9	-	10.3 86 55 83 74 36	211 056.2	O7	.	.	.	.	06	.	.	.	.	.	.	04	02	10	18	14	06	16	.	.	.	.	05	01			
VII 4.6 5.7 4.4 4.9	-	11.8 84 51 82 72 32	C98 047.5	26	.	.	.	.	21	05	.	.	.	.	.	08	06	07	06	04	07	.	.	.	.	04	03				
VIII 5.6 6.7 3.2 4.6	-	13.7 90 55 86 77 31	179 046.5	11	.	.	.	18	11	01	01	01	01	01	01	09	07	13	11	07	13	.	.	.	.	04	03				
IX 7.7 6.1 5.6 6.5	-	10.6 92 41 91 81 30	193 058.6	25	.	.	.	06	.	.	.	.	.	.	02	05	13	14	10	06	14	.	.	.	.	02	05				
X 9.4 7.7 7.4 8.2	-	06.2 93 70 90 84 42	303 069.3	O5	.	.	.	06	.	.	.	.	.	.	01	01	15	23	19	08	23	01	.	.	.	01	11				
XI 7.2 6.8 6.1 6.7	-	05.8 87 65 85 79 27	107 038.2	29	.	.	.	06	.	.	.	.	.	.	04	01	03	10	08	03	10	01	01	.	.	02	07				
XII 6.1 5.4 5.5 5.7	-	04.6 80 65 80 75 32	017 014.4	12	.	.	.	16	.	.	.	.	.	.	01	04	04	02	01	04	.	.	.	.	04	.					
GOD. 7.0 6.7 6.0 6.6	-	07.7 85 59 83 76 16	1462 069.3	53	.	.	.	53	55	16	01	15	02	45	146	145	112	46	138	12	02	.	.	.	.	22	62	07			
<b>BR. ST-17</b>																															
<b>RADLJE OB DRAVI</b>																															
I 9.7 6.6 7.4 8.0	-	04.3 95 71 93 86 47	034 015.2	02	.	.	.	30	.	.	.	.	.	.	.	17	04	04	01	02	03	01	.	.	.	.	06	18			
II 8.8 7.5 7.3 7.9	-	05.1 80 66 88 61 44	042 030.0	O7	.	.	.	14	.	.	.	.	.	.	.	15	06	07	01	07	03	.	.	.	.	06	04				
III 9.1 6.8 7.0 7.6	-	06.1 94 57 88 63 38	116 054.7	O7	.	.	.	10	.	.	.	.	.	.	02	15	10	08	03	05	07	.	.	.	.	04	15	11			
IV 7.8 7.2 6.3 7.1	-	06.0 89 57 79 75 28	024 010.6	26	.	.	.	11	.	.	.	.	.	.	02	12	05	03	01	05	.	.	.	.	05	.					
V 7.0 7.0 6.6 6.9	-	08.6 90 57 82 76 36	080 016.8	25	.	.	.	01	.	.	.	.	.	.	01	08	14	11	04	14	.	.	.	.	04	03					
VI 7.2 6.8 7.1 7.0	-	10.5 91 63 86 80 36	183 051.5	30	.	.	.	06	.	.	.	.	.	.	01	11	15	15	07	15	.	.	.	.	06	04					
VII 6.0 5.0 5.3 5.5	-	12.0 90 56 81 76 37	148 028.4	O7	.	.	.	20	02	.	.	.	.	.	04	05	11	11	05	11	.	.	.	.	06	03					
VIII 7.6 5.5 5.2 6.2	-	13.5 94 61 87 81 34	224 043.7	11	.	.	.	17	07	.	.	.	.	.	03	09	13	12	06	13	.	.	.	.	07	09					
IX 8.4 6.2 5.6 6.8	-	10.7 96 67 93 85 45	208 049.7	23	.	.	.	07	.	.	.	.	.	.	02	13	14	13	07	14	.	.	.	.	04	10					
X 9.5 6.6 7.5 8.0	-	06.1 96 71 92 86 38	201 050.5	21	.	.	.	06	.	.	.	.	.	.	01	16	12	17	07	16	.	.	.	.	01	01					
XI 8.2 6.5 6.7 7.1	-	05.4 88 68 89 62 36	C53 017.2	26	.	.	.	15	.	.	.	.	.	.	04	11	07	06	02	07	01	.	.	.	.	06	01				
XII 6.7 5.0 6.8 6.0	-	04.0 89 65 88 81 40	007 004.5	12	.	.	.	29	.	.	.	.	.	.	04	08	03	02	02	01	01	.	.	.	.	C9	01				
GOD. 8.0 6.5 6.6 7.0	-	07.7 91 64 87 81 28	1920 051.5	30	.	.	.	116	51	09	.	01	.	.	19	140	126	104	44	117	17	04	.	.	.	.	37	94	36		
<b>CELJE-LEVEC</b>																															
BR. ST-18																															
I 9.3 7.4 8.4 8.6	030.6	04.7 96 85 94 86 54	92 40	037 016.4	02	.	.	25	.	.	.	.	.	.	01	01	02	08	06	04	06	02	08	06	04	06	02	16	10		
II 6.6 7.5 7.4 7.8	050.7	05.6 91 69 88 62 43	040 026.6	O7	.	.	.	13	.	.	.	.	.	.	01	01	13	09	04	01	07	03	01	01	07	03	01	07	01		
III 8.2 6.7 6.7 7.2	105.0	05.7 94 65 85 61 41	085 026.2	O5	.	.	.	15	.	.	.	.	.	.	03	13	11	08	03	08	06	03	01	01	01	02	06	09			
IV 6.8 7.4 6.9 7.0	138.9	05.8 88 53 73 72 28	029 009.6	26	.	.	.	15	.	.	.	.	.	.	02	15	09	05	05	05	05	05	05	05	05	05	05	03			
V 6.2 7.3 7.5 7.0	171.9	08.9 91 59 81 77	32	074 018.8	05	.	.	01	02	.	.	.	.	.	01	01	01	10	10	16	02	16	.	.	.	.	04	.			
VI 6.8 7.0 7.0 6.9	172.0	11.1 93 64 86 61 41	236 026.5	30	.	.	.	04	.	.	.	.	.	.	02	01	01	15	19	15	05	15	.	.	.	.	10	04			
VII 5.3 5.7 5.4 5.5	255.9	13.1 92 65 80 79 37	086 025.6	26	.	.	.	19	04	.	.	.	.	.	02	04	04	12	08	04	12	.	.	.	.	02	02				
VIII 6.9 5.1 4.7 5.6	219.4	14.9 95 69 82 65 46	146 035.5	11	.	.	.	18	09	.	.	.	.	.	04	06	13	12	06	13	.	.	.	.	07	08					
IX 6.5 5.7 5.6 6.3	129.2	10.9 94 71 93 86 46	202 048.6	23	.	.	.	01	04	.	.	.	.	.	01	01	03	08	13	13	10	06	12	.	.	02	11				
X 8.5 7.6 7.5 8.0	046.7	06.0 95 71 90 85 45	215 066.7	05	.	.	.	09	.	.	.	.	.	.	01	17	21	15	06	21	.	.	.	.	01	13					
XI 7.7 6.8 6.7 7.1	047.6	05.4 88 64 86 80 40	C66 022.0	29	.	.	.	14	.	.	.	.	.	.	06	07	11	07	04	11	.	.	.	.	02	04					
XII 6.2 5.8 5.5 5.8	042.9	04.3 93 63 87 81 27	013 011.7	12	.	.	.	26	.	.	.	.	.	.	01																

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C							Čestina pravaca i srednja jačina vetrova nD, Fm (0-12)																							
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW							
		7	14	21							8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.						
$\varphi = 46^{\circ}24' N \lambda = 15^{\circ}39' E$ Gr. $\Delta G = + 1h 03 min.$																																
I	-	-00.5	04.5	06.8	01.4	04.9	-01.3	14.2	20	-05.0	22	.	.	06	00.8	*	*	04	00.6	*	*	21	02.8	01	00.1	05	C0.7	56				
II	-	03.1	09.0	04.7	05.4	09.5	01.8	15.3	12	-03.2	23	.	.	10	01.8	C4	00.6	10	01.4	*	*	30	08.0	01	00.2	03	00.7	26				
III	-	03.2	11.4	03.3	06.8	11.8	01.6	23.8	21	-02.5	01	.	.	19	04.3	10	01.4	02	00.3	*	*	18	04.8	03	00.3	*	*	41				
IV	-	05.5	14.1	09.1	09.0	14.8	02.6	22.0	10	-02.8	20.0	.	.	14	04.2	14	02.6	05	00.8	*	*	14	02.3	*	*	01	00.1	42				
V	-	11.0	18.5	12.1	13.4	19.5	07.6	26.0	20	01.7	10	.	.	C5	01.0	*	*	C3	00.6	*	*	32	06.0	*	*	*	*	48				
VI	-	14.0	20.7	14.5	16.0	21.9	10.0	27.0	04	05.0	12	.	.	C6	01.1	*	*	C4	00.7	*	*	21	04.2	02	00.3	06	01.2	53				
VII	-	15.9	23.9	17.6	18.8	25.2	12.4	31.2	31	07.8	20	.	.	C2	00.4	*	*	C4	00.7	*	*	25	05.2	01	00.2	07	01.2	54				
VIII	-	15.9	25.3	18.7	19.7	26.1	13.8	32.5	16	06.2	13	.	.	C3	00.6	*	*	C1	00.2	*	*	22	03.5	03	00.4	10	01.7	54				
IX	-	11.4	19.6	13.4	14.5	20.3	09.3	27.2	C3	01.2	27	.	.	C9	01.4	C2	00.2	C6	00.8	*	*	19	03.5	01	00.1	*	*	53				
X	-	03.8	10.0	05.6	06.2	10.6	01.1	16.0	25	-02.5	31.27	.	.	C6	01.1	*	*	C1	00.1	*	*	30	06.4	*	*	07	00.8	49				
XI	-	03.8	09.7	05.0	05.9	10.4	02.3	16.8	17	-04.6	09	.	.	C9	01.2	*	*	C1	00.2	*	*	27	05.5	*	*	11	01.7	32				
XII	-	06.2	07.5	02.4	03.1	08.0	-01.4	15.5	29	-02.0	15	04	C0.4	01	00.2	*	*	*	*	*	*	26	04.4	09	01.6	17	C1.9	36				
GOD.	-	07.3	14.5	09.1	10.0	15.3	05.1	32.5	KvM	-08.0	15 XII	04	00.4	64	02.4	34	01.6	56	01.4	*	*	285	05.0	21	00.8	67	C1.4	544				
$\varphi = 46^{\circ}38' N \lambda = 16^{\circ}11' E$ Gr. $\Delta G = + 1h 05 min.$																																
I	754.2	00.6	03.0	0.7	01.1	C3.4	-01.0	14.5	20	-05.4	22	C1	00.2	*	*	C7	01.3	07	01.4	08	01.7	01	00.2	C2	C0.4	02	C0.4	65				
II	742.4	02.4	04.5	04.9	08.9	01.3	15.8	12	-03.1	11	02	C3.3	06	C1.7	*	*	C8	01.2	09	02.8	05	02.1	05	00.9	03	00.5	46					
III	745.8	02.9	11.2	06.6	06.8	12.1	01.5	23.2	22.21	-04.8	01	02	00.3	07	01.8	C3	00.5	06	01.0	05	00.9	10	03.7	03	00.4	02	00.3	55				
IV	742.5	03.4	14.2	08.6	09.2	15.0	01.2	21.0	10	-03.6	04	09	C2.6	19	05.7	C5	01.2	05	01.0	07	01.6	03	00.9	02	00.6	03	00.3	37				
V	747.1	11.3	18.2	12.4	13.6	19.2	07.3	25.4	20	01.7	27	10	02.4	C7	06.4	C4	00.7	03	00.6	07	01.9	10	02.7	*	*	06	C1.2	51				
VI	742.5	13.4	20.9	14.4	15.9	21.8	05.8	24.6	12	06	C6.9	04	00.4	04	00.6	C8	01.5	05	00.6	05	00.6	14	04.3	11	01.4	17	04.6	21				
VII	744.9	16.1	23.7	17.8	18.9	25.0	12.1	30.4	31	07.0	20	16	03.0	C8	01.0	C4	00.6	12	01.8	08	01.6	18	04.1	02	00.4	06	00.8	19				
VIII	745.7	16.8	25.6	15.0	20.1	26.2	13.5	32.4	16	04.0	13	03.0	C3	00.4	C8	01.8	02	00.5	06	00.8	02	00.3	06	01.3	43							
IX	744.9	11.7	19.1	13.2	14.4	20.1	09.2	26.8	C4.3	C6.7	28	04	C1.2	10	07.0	C2	00.5	07	01.4	08	02.6	04	00.9	02	00.3	05	C1.0	48				
X	741.2	03.3	10.1	05.5	06.1	10.7	01.9	14.9	25	-04.7	31	08	C1.6	07	01.2	02	01.2	12	03.3	14	04.2	*	*	04	C0.7	42						
XI	745.7	03.2	09.3	05.0	05.6	09.9	01.8	17.1	16	-05.4	09	08	C1.3	09	01.5	C4	00.8	06	01.2	21	08.3	12	03.5	*	*	04	C0.5	41				
XII	747.9	-00.5	C6.3	01.5	02.2	06.9	-01.9	16.4	29	-07.7	15	08	C2.1	C5	00.7	C9	01.3	05	00.7	04	01.2	07	01.0	03	00.4	09	C1.7	43				
GOD.	744.7	07.4	14.1	09.1	09.9	15.0	04.8	32.4	KvM	-07.7	15 XII	04	01.9	53	02.5	45	00.9	81	01.4	96	03.4	104	03.2	32	00.8	67	C1.9	496				
$\varphi = 46^{\circ}28' N \lambda = 16^{\circ}12' E$ Gr. $\Delta G = + 1h 05 min.$																																
I	-	-00.4	C2.5	C0.8	00.9	03.2	-01.3	14.5	20	-04.0	15.13	.	.	38	05.2	C7	01.5	12	02.6	*	*	33	05.1	02	00.4	C1	C0.2	*				
II	-	03.2	C7.5	04.7	05.0	05.0	C8.2	01.7	15.0	12	-02.8	28	.	.	40	09.0	C2	00.3	07	01.3	*	*	33	08.3	02	00.7	*	*	*			
III	-	04.4	10.4	07.7	07.5	11.2	03.3	22.5	21	-04.0	01	.	.	59	12.7	C1	00.2	03	00.6	*	*	29	06.2	*	*	01	00.1	*				
IV	-	07.0	13.2	09.1	09.6	14.2	04.4	20.0	10	-02.0	17	.	.	57	14.8	*	*	*	*	*	*	29	05.6	*	*	04	00.7	*				
V	-	12.1	17.3	12.7	13.7	18.1	08.7	24.1	20	01.5	19	08.7	08	02.3	13	02.7	C1	00.2	07	01.8	*	*	42	09.3	03	00.6	07	C1.7	*			
VI	-	14.6	20.4	14.7	16.1	21.3	11.3	26.0	24.0	05.0	12	08	02.4	12	03.7	C1	00.2	01	00.2	02	01.2	01	00.3	02	00.3	05	03.8	01	00.1	07	01.7	51
VII	-	16.7	22.7	18.1	18.9	24.0	14.0	30.0	17	10.0	20	.	.	17	04.7	C1	00.3	11	02.3	*	*	59	12.4	*	*	04	C1.0	01				
VIII	-	17.6	24.4	20.2	20.6	25.1	15.9	32.0	16	11.5	12	.	.	35	08.6	C1	00.2	10	02.4	*	*	42	07.7	*	*	05	C1.2	*				
IX	-	13.1	18.5	14.6	15.2	19.4	11.3	26.5	03	04.5	27	.	.	41	08.9	*	*	16	03.0	*	*	23	05.4	*	*	06	C1.3	04				
X	-	04.7	09.3	05.7	06.4	10.4	03.8	14.5	25	04.0	31.30	.	.	36	07.9	*	*	14	03.1	*	*	35	08.9	*	*	08	01.0	05				
XI	-	04.4	09.0	05.5	05.6	09.1	01.7	16.1	18	-05.0	09	22	02.2	03.2	04.0	03	00.5	06	01.0	10	03.2	28	06.4	07	00.8	05	01.					

Mjesec	Oblačnost Rm (0-10)				Insolacij broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na s: H = 251 m H <sub>b</sub> = m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m																			
	e <sub>m</sub>			U		m	t		Tn			In	Ix	Tz	Tn			F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	□			
	7	14	21	Sred. (0-10)		mm	7	14	21	Stv.	Min	Max	Dat.	30.00	0.0	0.25	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	○	▲	■	□
<b>PHAGERSKO</b>																															
<b>BR. ST.21</b>																															
I 8.3	5.6	7.2	7.4	-	04.7	95	62	94	90	52	031	006.2	02	.	.	25	.	.	.	.	03	19	08	08	•	06	04	.	.		
II 7.8	7.0	6.6	7.1	-	05.6	88	68	88	81	48	037	C27.0	07	.	.	09	.	.	.	01	.	04	13	05	03	04	02	.	03		
III 6.7	6.5	5.9	6.4	-	06.1	92	67	85	81	45	076	C41.3	05	.	.	11	.	.	.	.	06	14	09	05	03	05	08	03	.		
IV 5.2	6.0	5.8	5.9	-	06.2	83	56	75	71	34	020	004.4	26	.	.	09	.	.	.	.	08	14	04	04	•	04	.	.	.		
V 5.8	7.2	6.5	6.5	-	09.5	90	64	89	81	44	128	C33.6	05	.	.	01	.	.	.	.	03	12	12	11	05	12	.	.	01		
VI 6.1	6.7	7.0	6.6	-	11.3	91	66	88	82	47	127	C32.6	30	.	.	04	.	.	.	.	02	14	13	13	05	13	.	.	02		
VII 4.7	4.7	5.1	4.8	-	13.0	93	63	85	80	48	062	C25.2	25	.	.	17	05	.	.	.	08	08	08	01	06	.	.	01	.		
VIII 4.4	3.8	4.5	4.2	-	15.7	97	77	93	69	54	194	C26.4	11	.	.	15	04	.	.	.	12	07	11	11	07	11	.	.	04		
IX 6.4	5.1	4.6	5.3	-	11.4	96	77	94	89	58	137	026.3	23	.	.	04	.	.	.	.	08	10	10	10	06	10	.	.	01		
X 7.2	6.9	5.7	6.6	-	06.6	96	82	94	91	64	185	C49.4	21	.	.	05	.	.	.	01	.	04	13	13	05	14	.	.	01		
XI 6.1	6.2	6.2	6.2	-	05.9	86	72	86	82	52	054	C15.3	24	.	.	09	.	.	.	01	.	04	11	10	08	01	10	.	02		
XII 6.0	5.6	5.8	5.8	-	04.5	84	67	82	78	44	010	004.6	17	.	01	20	.	.	.	.	08	11	02	02	•	02	.	.	04		
GOD.	6.2	6.1	5.9	6.1	-	08.4	90	70	87	82	34	1021	044.4	21X	.	01	80	41	14	.	02	.	70	144	106	102	34	95	14	C3	.
<b>MURSKA SRPSKA</b>																															
<b>BR. ST.22</b>																															
I 5.2	5.1	7.8	8.4	038.5	04.5	53	63	92	89	47	041	C12.2	02	.	.	19	.	.	.	.	02	24	11	07	02	08	05	01	.		
II 8.4	7.9	5.2	7.2	057.2	052.4	91	67	83	60	34	039	C20.4	07	.	.	09	.	.	.	02	13	11	06	01	10	02	.	05			
III 7.7	7.2	6.4	7.1	097.7	05.8	91	59	82	70	36	051	C17.0	08	.	.	08	.	.	.	03	17	10	05	02	06	06	01	.			
IV 5.9	7.1	4.6	6.0	171.9	05.9	63	45	72	68	26	018	009.1	26	.	.	11	.	.	.	04	11	08	04	•	06	.	.	C1			
V 5.9	7.1	6.1	6.4	181.9	00.8	85	56	84	75	29	083	C24.8	02	.	.	02	.	.	.	01	03	08	17	11	02	17	.	04			
VI 6.2	6.0	6.2	6.2	196.5	10.0	83	53	83	73	35	111	C32.5	30	.	.	05	.	.	.	01	02	17	18	11	03	15	.	04			
VII 5.6	5.2	5.3	5.4	239.6	11.6	83	51	80	71	31	070	C24.6	07	.	.	16	04	.	.	05	04	13	12	04	13	.	02				
VIII 5.5	4.3	5.6	5.0	253.4	13.8	91	56	87	78	42	141	C34.0	28	.	.	15	06	.	.	07	07	14	12	05	14	.	05				
IX 8.1	5.8	4.5	6.1	145.0	10.3	94	64	90	83	32	112	C36.1	02	.	.	03	.	.	.	03	08	13	09	04	13	.	03				
X 8.4	7.7	7.3	7.8	084.4	06.0	95	69	90	85	37	182	C47.4	21	.	.	09	.	.	.	02	19	18	14	06	18	01	01	.			
XI 7.7	6.6	6.2	6.8	105.9	05.7	90	69	88	82	35	069	C13.9	29	.	.	11	.	.	.	05	10	10	06	02	10	.	07				
XII 7.6	6.9	5.2	6.6	074.8	04.7	94	73	91	86	50	014	006.4	07	.	01	23	.	.	.	01	03	13	05	03	05	01	01	.			
GOD.	7.2	6.6	5.9	6.6	1646.8	07.7	89	62	85	79	26	912	C47.4	21X	.	01	90	41	12	.	14	.	37	141	148	100	30	135	15	03	01
<b>JERUZALEM</b>																															
<b>BR. ST.23</b>																															
I 8.6	7.1	6.1	7.2	053.1	04.5	93	90	93	92	55	051	C20.0	02	.	05	26	.	.	.	04	18	10	10	01	07	04	.	.			
II 8.4	7.4	5.4	7.0	057.4	05.5	86	77	84	63	43	043	C23.2	07	.	.	07	.	.	.	02	14	10	05	01	09	02	.	06			
III 6.1	6.5	5.2	6.0	103.9	05.9	84	69	74	75	45	067	C24.5	06	.	.	08	.	.	.	05	10	16	09	05	05	07	03	.			
IV 5.6	7.1	5.0	6.9	154.2	05.8	73	53	67	64	26	022	016.0	26	.	.	01	.	.	.	06	11	08	05	01	08	02	01	.			
V 5.0	7.3	7.3	6.5	145.8	08.8	81	64	76	74	42	106	C28.0	02	.	.	02	.	.	.	03	13	18	10	05	18	.	01				
VI 5.5	6.5	5.5	6.8	169.4	10.7	83	76	78	78	50	117	C04.14	30	.	.	05	.	.	.	01	02	17	15	11	03	15	.	07			
VII 4.7	5.7	4.0	4.8	243.8	12.5	84	66	75	75	40	069	C30.5	07	.	.	13	01	.	.	09	07	10	07	01	10	01	02	.			
VIII 5.1	4.2	4.5	4.6	254.8	14.6	85	70	80	80	47	206	C47.2	26	.	.	15	04	04	.	11	10	13	12	06	13	.	05				
IX 5.8	5.3	4.5	5.2	156.2	10.8	85	73	82	82	48	082	C32.2	25	.	.	07	.	.	.	02	08	09	13	05	13	.	02				
X 7.4	7.0	6.5	7.0	089.4	08.2	92	76	85	85	50	195	C46.7	21	.	.	08	.	.	.	02	14	21	15	06	21	.	01				
XI 5.0	5.2	5.3	5.3	105.2	05.7	85	71	81	80	41	057	C18.2	25																		

Mesec	Vrednost Pratiljk Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																		
		Tm			Sred. (tjess)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.									
$\varphi = 45^{\circ}51'$ N $\lambda = 13^{\circ}40'$ E Gr. $\Delta G = + 55$ min.																														
I	-	64.0	68.1	64.9	65.5	68.6	62.5	14.5	21	-02.6	26	03	01.0	.	.	20	07.8	01	00.2	01	00.3	.	.	02	00.6	.	.	66		
II	-	65.5	68.7	66.1	64.6	69.5	64.0	13.0	20.15	-06.3	07	01	00.4	.	.	35	15.2	04	01.5	06	02.7	.	.	*	*	.	.	36		
III	-	66.9	71.5	67.7	68.5	72.2	65.0	22.6	22	-06.6	01	03	01.0	01	00.3	45	18.4	05	01.8	01	00.2	.	.	03	00.8	.	.	35		
IV	-	69.3	73.0	69.8	70.6	74.4	66.8	17.6	09	03.4	19	.	.	02	00.8	43	16.7	05	02.3	08	02.6	.	.	05	01.8	.	.	27		
V	-	72.9	77.1	71.7	73.9	78.2	71.4	24.0	21	07.0	05	01	00.3	.	.	15	14.9	01	00.4	11	03.3	.	.	06	02.9	.	.	59		
VI	-	75.4	79.6	75.7	76.6	80.5	72.6	26.5	05	04.6	12	.	.	.	.	21	07.5	02	00.5	06	01.7	01	00.3	11	02.0	.	.	54		
VII	-	79.2	84.0	79.4	80.5	84.8	76.0	30.0	30.29	11.7	25	.	.	.	.	22	08.0	.	06	02.2	.	.	13	03.8	.	.	52			
VIII	-	81.1	86.4	81.7	82.7	87.2	78.3	32.2	16	10.4	11	.	.	.	.	40	13.9	05	01.7	10	03.0	.	.	03	00.9	.	.	35		
IX	-	85.9	91.2	86.5	87.5	91.7	83.9	28.0	15	07.8	25	.	.	.	.	38	13.8	01	00.2	11	03.8	.	.	03	01.0	.	.	37		
X	-	87.1	90.8	87.5	88.1	91.6	85.5	14.7	07	02.0	17	02	CC.8	.	.	31	12.2	01	00.3	11	03.8	.	.	07	02.2	.	.	41		
XI	-	86.9	90.7	87.3	87.8	90.4	85.4	13.7	17	01.0	30	.	.	01	00.3	23	06.7	.	06	01.7	.	.	02	00.5	.	.	56			
XII	-	84.4	87.9	85.7	85.7	88.4	82.8	14.8	03	-01.0	15.14	.	.	01	00.4	09	02.6	01	00.2	03	00.8	.	.	.	.	.	.	79		
GOD.	-	10.7	14.9	11.2	12.0	15.6	8.6	32.2	KvM	-02.6	26.1	10	00.8	05	00.5	24	12.6	26	01.4	82	02.8	01	00.3	50	02.2	.	.	579		
$\varphi = 45^{\circ}32'$ N $\lambda = 13^{\circ}43'$ E Gr. $\Delta G = + 55$ min.																														
KOPER-SEMELDA																														
I	763.5	75.8	68.3	66.3	66.7	69.2	64.5	13.7	20	01.8	18	.	.	02	00.7	C5	01.5	14	02.8	.	04	00.7	10	02.3	08	01.8	50			
II	756.2	75.5	61.0	68.0	68.6	72.1	64.4	14.8	15	02.0	08	.	.	13	04.8	17	05.2	23	04.8	04	01.1	05	01.2	03	00.8	03	01.7	16		
III	755.0	77.9	12.8	09.0	09.7	13.9	06.9	22.2	26	01.1	01	.	.	14	04.6	25	07.7	11	02.2	01	00.4	03	01.0	06	01.7	07	C2.0	26		
IV	755.6	10.5	15.1	11.7	12.4	16.5	05.1	19.9	06	05.1	16	.	.	11	03.8	16	05.4	25	05.1	03	00.6	03	01.2	06	02.1	06	C2.0	20		
V	-	15.1	18.8	14.8	15.9	19.7	12.0	26.5	21	05.4	09	.	.	02	00.6	C7	02.0	28	04.5	06	02.3	04	01.4	07	01.8	18	C4.7	21		
VI	-	17.9	21.1	17.8	16.7	22.6	14.6	27.1	05	09.1	12	.	.	01	00.3	C5	01.5	17	03.4	03	00.7	01	00.3	05	01.4	19	C5.5	39		
VII	-	21.5	25.8	22.3	26.9	18.1	31.1	17	13.4	26	01	00.2	.	01	00.4	05	01.6	22	03.2	03	00.6	04	00.8	06	01.3	18	C3.9	33		
VIII	-	24.0	27.3	22.1	23.4	28.4	15.0	32.2	20	13.5	11	.	.	06	01.8	12	02.7	09	01.5	.	.	01	00.2	06	01.2	13	C3.4	46		
IX	-	17.5	22.7	18.1	19.1	23.6	15.8	25.7	14	05.2	26	.	.	07	02.1	C9	02.3	10	02.5	.	04	01.0	10	02.3	08	C1.7	42			
X	-	05.1	13.0	09.8	10.4	14.4	07.6	17.5	06	04.5	31	.	.	11	04.0	16	05.3	17	03.4	07	01.6	07	02.0	04	01.0	07	C2.1	24		
XI	-	05.3	12.0	09.1	09.9	12.9	07.8	18.5	17	02.0	30	.	.	09	03.2	12	04.1	19	03.8	C4	00.9	05	01.0	07	01.5	08	02.0	24		
XII	-	05.8	09.2	06.7	07.1	10.0	04.5	13.0	20.01	01.0	15	.	.	04	01.4	10	03.1	17	02.6	03	00.5	05	00.9	06	01.2	09	C2.1	39		
GOD.	-	12.5	16.4	12.9	13.7	17.5	10.5	32.2	KvM	-02.0	26.1	01.0	00.2	81	03.4	129	04.5	212	03.9	34	01.2	46	01.1	76	01.7	124	C3.3	382		
$\varphi = 45^{\circ}31'$ N $\lambda = 13^{\circ}52'$ E Gr. $\Delta G = + 55$ min.																														
KUBED																														
I	-	22.3	68.6	63.0	64.5	69.7	60.9	07.8	15.3	21	-02.0	24.18	05	01.0	04	00.7	C7	01.6	13	02.0	28	06.0	17	01.8	69	01.4	.	.	67	
II	-	05.3	09.9	05.9	06.8	11.1	03.8	15.4	15	-03.0	08	01	00.2	.	.	24	08.1	08	01.5	38	07.2	10	01.5	02	00.4	01	C0.1	.	.	41
III	-	02.0	12.3	07.0	07.8	13.4	03.8	21.5	22	-02.8	13	03	00.7	.	.	25	09.3	09	01.3	30	05.2	08	01.1	07	01.0	01	00.1	.	.	41
IV	-	08.2	14.2	08.9	10.1	15.5	05.3	19.0	08.07	-01.0	20	14	03.0	07	02.2	16	05.0	10	01.8	30	05.9	04	00.7	08	01.3	01	00.3	.	.	41
V	-	13.4	18.0	11.9	13.8	19.7	10.5	25.6	21	04.0	10	07	01.7	04	00.8	08	02.3	10	02.3	38	06.8	08	01.7	16	02.6	02	00.6	.	.	41
VI	-	14.1	20.9	14.8	16.7	22.3	12.0	28.5	05	04.5	12	04	00.6	.	.	08	01.9	13	02.8	40	07.7	09	01.5	15	04.6	01	C0.3	.	.	41
VII	-	18.9	25.5	17.8	20.0	26.4	14.2	30.5	31	08.0	19	13	03.1	02	00.6	14	04.5	07	01.6	16	02.2	17	02.1	21	04.0	03	00.7	.	.	41
VIII	-	19.0	26.4	18.8	20.8	28.3	15.5	33.5	16	11.0	11	16	03.3	C1	00.2	17	04.7	06	02.0	18	02.5	13	01.7	17	02.6	03	C0.3	.	.	41
IX	-	13.8	22.5	14.9	16.5	23.3	11.9	29.5	14	04.0	27	11	02.7	01	00.2	08	02.4	11	02.1	31	05.4	12	01.7	14	02.1	02	00.4	.	.	41
X	-	06.4	11.5	07.0	07.9	13.1	05.0	17.0	07	-02.6	17	01	0C.3	25	11.7	C5	02.2	08	01.7	01	00.3	05	00.9	08	02.0	.	.	41		



1974

Mesec	Vardušni pritisak Pr. mbar.	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s (0-12)																				
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C			
		7	14	21							8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.		
$\varphi = 45^{\circ}34'$ , N, $\lambda = 14^{\circ}15'$ , E Gr., $\Delta G = + 57$ min.																														
I	-	-66.3	66.9	61.5	02.6	07.6	-01.4	17.4	20	-04.4	22	12	C6.0	C6	00.4	C2	00.3	C1	00.4	14	03.1	C1	00.4	03	00.5	C6	C1.5	52		
II	-	63.0	67.7	65.0	05.4	09.5	01.6	12.4	16	-05.5	28	16	C6.1	C6	00.4	C4.2	04	C1.0	19	05.4	02	00.3	02	00.7	02	00.8	C2	23		
III	-	61.8	61.5	60.4	06.3	12.5	00.4	24.5	22	-06.1	C1	14	C7.8	C1	00.4	C4	01.3	C4	01.4	13	04.9	0.	01	01.3	06	01.5	C4	40		
IV	-	64.3	64.7	66.1	08.4	14.1	02.4	15.0	09	-04.5	20	21	11.7	11	00.5	C2	00.5	0.	01	14	03.9	03	00.6	07	02.1	0.	33			
V	-	65.0	66.7	61.6	12.0	16.1	06.4	24.3	20	02.0	10.05	18	C6.2	C1	00.2	C2	00.7	C3	01	01.2	21	06.1	03	01.1	02	00.4	C3	40		
VI	-	62.1	69.0	14.2	14.9	26.7	07.0	27.1	04	06.5	12	20	C6.7	C6	00.7	C2	00.7	C3	01	01.2	23	06.2	0.	02	00.5	01	01.3	C4	42	
VII	-	63.6	24.0	17.3	18.1	24.4	04.1	30.4	30	04.9	27	24	C6.1	C2	00.5	C7	01.9	C6	01.7	16	04.4	0.	04	01.5	01	02.2	C4	40		
VIII	-	63.7	26.1	14.3	19.1	27.0	11.8	32.0	17	06.1	12	14	C4.4	C7	00.6	C3	00.7	C1	00.3	18	04.7	01	00.3	03	00.6	02	00.4	C4	49	
IX	-	66.3	21.0	13.6	14.6	21.7	04.0	28.0	15	06.9	27	11	C1.2	0.	0.	C1	02.9	01	00.4	17	04.1	0.	0.	02	00.5	02	00.7	C4	46	
X	-	64.4	05.8	06.3	11.2	12.2	14.8	07	-03.3	30	20	C7.0	C1	00.3	C5	1.5	C4	01.6	C2	03	07.0	01	00.3	01	00.2	02	00.3	C4	38	
XI	-	64.1	65.6	65.3	06.1	10.3	02.5	14.9	10	-06.0	62	12	C4.2	C1	00.2	C6	01.2	C7	01.6	20	05.6	05	01.7	01	00.1	02	00.5	C4	36	
XII	-	60.2	67.5	62.4	03.1	Cd.6	-01.1	15.0	04	-06.9	17	17	C5.4	0.	0.	C8	02.3	07	C2.5	09	02.4	C1	00.3	02	00.6	01	00.1	C4	48	
GOD.	-	66.3	14.5	69.0	09.7	15.5	04.3	32.0	N/VW	-08.1	08	214	C6.6	10	00.4	66	02.3	38	01.6	207	05.1	17	06.9	29	01.0	27	C1.0	487		
$\varphi = 45^{\circ}38'$ , N, $\lambda = 14^{\circ}22'$ , E Gr., $\Delta G = + 57$ min.																														
I	-	-61.8	63.0	-01.1	-06.2	03.5	-03.4	13.3	20	-07.5	15	+	27	C3.7	0.	0.	C1	00.1	19	02.4	C2	00.2	26	C2.8	18					
II	-	60.1	02.4	60.1	60.1	61.5	07.4	16	-07.9	08	+	38	06.6	0.	0.	C1	00.2	0.	30	05.1	0.	0.	C2	00.2	13					
III	-	-00.4	05.2	00.5	01.4	C6.0	-01.7	16.0	22	-07.4	13	+	57	09.4	0.	0.	0.	0.	0.	07	01.0	0.	0.	15	C1.7	14				
IV	-	62.0	06.4	02.8	03.6	03.6	01.1	14.2	09	-05.2	20	+	56	10.2	0.	0.	0.	0.	0.	03	00.5	0.	0.	11	01.1	20				
V	-	60.4	12.1	06.3	06.3	13.4	03.5	15.5	30	00.0	26	+	19	07.3	0.	0.	C1	00.1	06	00.6	21	02.6	0.	0.	20	C2.0	26			
VI	-	61.0	14.1	06.5	16.7	16.0	06.7	22.0	04	-01.0	12	01	C0.2	15	02.3	0.	C5	09.9	02	03.2	0.	0.	08	00.8	24					
VII	-	64.1	18.9	14.5	14.5	14.9	05.9	25.4	30	04.5	05	+	28	05.0	0.	0.	C8	01.1	02	00.5	07	C1.1	0.	0.	28	C3.2	20			
VIII	-	64.4	20.0	13.6	15.6	21.1	16.3	26.0	15	03.7	12	01	C0.1	31	03.9	C3	00.3	C5	00.6	C2	03.0	10	01.2	0.	07	00.7	34			
IX	-	65.0	15.1	09.7	11.1	16.5	06.6	21.5	06	-01.5	27	+	25	03.9	0.	0.	C10	01.5	C8	00.9	18	02.2	0.	0.	05	C0.7	24			
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	61.2	04.7	01.8	02.4	05.9	-06.4	12.1	10	-07.6	02	05	C6.7	19	06.1	C2	00.3	C1	00.3	0.	30	06.2	02	00.5	10	C2.0	21			
XII	-	-61.3	04.2	-00.9	00.3	05.1	-03.7	13.4	29	-06.9	17	+	12	01.9	C4	0.6	C1	00.1	01	00.1	10	03.0	08	02.2	02	09.7	05			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 45^{\circ}53'$ , N, $\lambda = 14^{\circ}26'$ , E Gr., $\Delta G = + 58$ min.																														
I	-	-61.1	62.2	60.0	00.5	C4.2	-03.1	14.8	20	-10.3	22	22	C3.6	C9	01.9	C8	C1.6	09	01.6	10	01.6	06	C1.1	11	01.8	16	C3.9	02		
II	-	60.9	04.1	01.8	02.2	01.1	-06.5	06.5	01	-10.6	08	21	C5.5	04	C1.1	C9	C2.3	16	05.5	11	01.5	08	C2.1	05	C1.0	09	C2.6	0.		
III	-	60.8	07.0	02.9	03.4	C7.8	-05.5	20.6	22	-11.5	14	16	C3.3	13	01.0	C7	C1.8	17	04.0	17	04.8	08	C1.9	0.	0.	09	02.5	06	C1.5	0.
IV	-	62.0	09.2	03.6	05.1	10.4	-03.6	14.3	09	-05.6	20	09	C1.6	15	04.5	19	05.6	14	03.7	08	01.2	08	01.6	10	01.4	07	01.3	0.		
V	-	69.5	13.8	08.5	10.3	15.1	04.7	26.8	30	-01.2	26	15	C2.5	13	03.5	C4	C0.4	05	01.6	19	03.4	06	C2.0	09	01.4	17	C4.0	21		
VI	-	12.0	15.8	11.3	12.6	17.5	07.2	24.6	04	-01.4	12	11	C2.1	17	02.5	C5	05.9	12	03.1	06	01.0	06	01.3	12	02.0	24	C5.6	02		
VII	-	14.6	26.3	14.4	16.0	21.7	07.1	27.0	30	02.9	17	10	C1.6	14	02.9	C16	03.9	11	02.7	14	02.8	07	02.0	07	01.2	13	C2.8	03		
VIII	-	14.4	21.5	15.0	16.5	22.7	05.9	28.6	16	04.6	21	15	C2.4	07	04.9	C6	01.0	22	03.2	04	00.6	14	01.7	07	01.4	04	C4	04		
IX	-	10.1	16.3	11.3	12.2	17.5	07.3	27.4	14	-01.2	27	19	C2.0	05	01.2	C11	C2.3	07	01.6	15	02.7	08	01.5	16	C2.4	10				
X	-	02.3	05.9	02.4	03.4	07.7	-06.7	16.8	20	-04.7	30	10	C2.2	09	01.5	C13	C2.5	03	00.7	12	02.3	14	02.9	01	03.1	11	C3.2	04		
XI	-	02.4	05.8	02.7	03.5	03.6	06.9	00.2	12.3	17	-05.2	30	10	C3.1																

Mesec	Oblačnost Nm (0-10)				Inzolacijska broj sati	Vlažnost vazduha				Padavine R mm				Broj dana na sat																							
						Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	▲	▲	□	□														
	7	14	21	Sted. (dias.)		mm	7	14	21	Sted. M	Σ	Max	Dati.	10.00.0	0.0250.0	0.020.0	0.6	8	2.0	8.0	0.1	1.00.0	0	+													
<b>BR. ST.31</b>																																					
I	8.7	6.1	5.7	6.8	-	05.0	97	75	93	88	34	076	C34.4	01	.	20	*	*	*	*	C1	13	13	C8	02	12	*	*	*	*	12						
II	7.2	6.6	6.5	6.8	-	05.4	90	66	82	86	27	089	043.2	07	.	08	*	*	*	*	04	*	03	13	12	16	03	12	01	*	*	C1	05	01			
III	5.9	5.6	4.5	5.4	-	05.2	89	55	78	74	20	079	066.5	05	.	11	*	*	*	*	02	*	07	C7	04	04	01	C4	C2	C2	C1	04	01				
IV	4.9	6.6	5.6	5.6	-	05.5	83	52	70	68	25	136	045.4	29	.	09	*	*	*	*	03	*	07	C5	09	09	04	05	*	*	*	*	*	*			
V	7.0	6.5	5.9	6.6	-	08.1	92	58	85	78	33	155	C45.7	05	.	*	*	*	*	*	C2	*	01	11	18	13	06	16	*	*	*	*	01	C7	05		
VI	6.9	7.1	5.8	6.6	-	10.1	91	65	65	60	23	256	045.8	10	.	01	*	*	*	*	01	*	01	12	17	13	07	17	*	*	*	*	01	10	05		
VII	4.8	4.5	3.6	4.3	-	11.3	90	51	79	74	36	090	063.7	26	.	*	*	*	*	01	*	08	C4	09	06	04	05	*	*	*	*	*	C1	11	*		
VIII	6.5	5.6	5.1	4.2	-	12.3	96	56	83	76	29	092	077.0	11	.	*	*	*	*	01	*	07	04	10	08	C2	10	*	*	*	*	04	16	*			
IX	7.5	5.6	3.7	5.4	-	10.2	95	60	90	62	39	150	C31.7	23	.	*	*	*	*	05	C7	16	11	06	16	*	*	*	*	*	*	06	17	*			
X	4.5	7.5	6.7	7.7	-	06.2	94	70	51	65	40	264	C75.0	05	.	*	*	*	*	07	*	*	15	22	14	08	22	*	*	*	*	*	03	11	*		
XI	7.0	7.4	7.1	7.4	-	06.2	89	75	51	85	41	090	024.8	46	.	*	*	*	*	01	*	07	18	12	04	03	12	*	*	*	*	*	03	10	*		
XII	6.6	5.0	5.3	6.6	-	04.9	91	71	68	63	41	079	C16.3	12	.	*	*	*	*	06	C5	10	04	01	09	02	*	*	*	*	*	*	*	*			
GOD.	6.5	6.6	5.2	6.0	-	07.5	91	62	84	79	20	149	C75.0	05X	.	*	*	*	*	05	*	*	*	*	*	*	*	*	*	*	*	02	46	105			
<b>BR. ST.32</b>																																					
<b>RAŠUN</b>																																					
BR. ST.32																																					
H <sub>s</sub> = 1017	H <sub>b</sub> =	m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,5 m																																			
I	6.4	5.5	5.5	6.1	-	-	-	-	-	-	-	070	C34.4	01	*	04	20	*	*	*	*	04	13	08	07	02	06	C5	01	*	*	U'	14				
II	5.6	7.1	6.5	7.6	-	-	-	-	-	-	-	170	C74.8	07	*	05	20	*	*	*	*	02	16	16	13	04	12	C7	C2	*	*	91	C6				
III	4.5	7.1	5.4	6.5	-	-	-	-	-	-	-	070	C34.0	05	*	06	22	*	*	*	*	03	12	10	07	01	02	05	*	*	*	*	04	15			
IV	4.6	6.3	5.4	5.5	-	-	-	-	-	-	-	138	052.5	29	*	*	14	*	*	*	*	06	17	13	10	04	13	02	01	*	*	91	01				
V	4.7	6.4	5.5	5.6	-	-	-	-	-	-	-	181	C43.7	05	*	*	*	*	*	*	*	05	C7	17	15	05	17	*	*	*	*	02	03	C4	02		
VI	5.3	7.0	4.6	5.7	-	-	-	-	-	-	-	281	C52.2	07	*	*	01	*	*	*	*	04	10	21	12	05	21	*	*	*	*	02	01	C1	*		
VII	2.7	7.4	3.4	3.4	-	-	-	-	-	-	-	132	C74.0	26	*	*	02	*	*	*	*	12	C3	11	11	04	11	*	*	*	*	01	02	C1	*		
VIII	3.1	4.0	2.8	3.3	-	-	-	-	-	-	-	165	036.0	29	*	*	06	*	*	*	*	16	C6	11	10	04	11	*	*	*	*	04	04	*			
IX	4.3	5.0	3.2	4.2	-	-	-	-	-	-	-	217	C64.4	25	*	*	01	*	*	*	*	11	C7	15	12	06	15	*	*	*	*	01	02	*			
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
XI	6.2	6.2	6.4	6.3	-	-	-	-	-	-	-	133	C45.7	26	*	*	17	*	*	*	*	01	*	04	11	10	09	04	C6	04	*	*	03	04			
XII	5.1	5.5	4.0	4.6	-	-	-	-	-	-	-	067	C64.3	12	*	03	27	*	*	*	*	07	C5	10	09	01	C8	05	02	01	*	*	05				
GOD.	6.2	6.7	5.3	6.0	-	-	-	-	-	-	-	176	C59.1	05X	*	06	13	134	16	*	*	01	*	53	125	104	115	59	142	37	05	*	*	04	01	7	75
<b>RAKITNA</b>																																					
BR. ST.33																																					
H <sub>s</sub> = 787 m H <sub>b</sub> =	m h <sub>t</sub> = 1,8 m h <sub>r</sub> = 1,5 m																																				
I	7.4	7.3	5.5	6.8	-	-	-	-	-	-	-	045	C75.7	01	*	01	05	23	*	*	*	*	C3	14	C3	C5	01	05	01	01	*	*	20	C6			
II	8.2	6.6	7.6	8.2	-	-	-	-	-	-	-	094	C40.0	07	*	01	02	16	*	*	*	*	01	18	16	10	02	12	05	*	*	*	*	05	05		
III	7.2	7.4	5.6	6.7	-	-	-	-	-	-	-	025	C21.1	05	*	01	05	20	*	*	*	*	04	16	11	08	01	03	05	*	*	*	*	01	05		
IV	5.1	7.2	5.2	5.9	-	-	-	-	-	-	-	076	C19.4	29	*	*	16	*	*	*	*	07	10	12	09	01	11	02	*	*	*	*	01	03			
V	5.1	6.5	6.1	6.0	-	-	-	-	-	-	-	150	C74.4	25	*	*	03	*	*	*	*	02	C5	17	13	C7	17	*	*	*	*	01	01	C1			
VI	6.4	7.1	5.2	6.4	-	-	-	-	-	-	-	260	C54.5	07	*	*	01	*	*	*	*	02	08	17	14	08	17	*	*	*	*	01	02	01			
VII	3.6	4.0	4.0	4.2	-	-	-	-	-	-	-	040	C45.3	26	*	*	05	*	*	*	*	08	C3	10	07	02	10	*	*	*	*	02	02	02			
VIII	4.4	5.1	2.6	4.0	-	-	-	-	-	-	-	164	C73.0	29	*	*	12	*	*	*	*	12	C3	10	09	05	10	*	*	*	*	01	01	C1	12		
IX	6.0	6.0	4.6	5.5	-	-	-	-	-	-	-	210	C53.7	07	*	*	01	*	*	*	*	07	C7	11	14	11	06	14	*	*	*	*	02	11	*		
X	7.7	7.6	6.4	7.3	-	-	-	-	-	-	-	398	C29.1	05	*	*	19	*	*	*	*	01	16	23	20	11	20	08	04	*	*	01	01	C6			
XI	7.5	7.1	6.4	7.0	-	-	-	-	-	-	-	131	C46.5	26	*	*	14	*	*	*	*	02	14	18	09	05	16	06	04	*	*	01	05	C7			
XII	5.1	5.4	3.7	4.7	-	-	-	-	-	-	-	052	C32.5	12	*	03	01	27	*	*	*	*	05	C4	09	04	C1	07	02	*	*	*	01	04			
GOD.	6.4	6.6	5.3	6.1	-	-	-	-	-	-	-	176	C59.1	05X	*	06	13	134	16	*	*	01	*	53	125	104	115	59	142	37	05	*	*	02	01		
<b>BABNE PCLJE</b>																																					
BR. ST.35																																					
H <sub>s</sub> = 756 m H <sub>b</sub> =	m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m																																				
I	7.6	7.7	5.2	6.9	-	-	-	-	-	-	-	046	C54	01	*	03	03	31	*	*	*	*	03	13	06	06	01	C6	04	*	*	*	*	04	12		
II																																					

Mesec	Vrijednost Prstenskog Prašnog	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																		
		Im				Dat.				Dat.				N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (mies.)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\phi = 45^{\circ} 18'$ N $\lambda = 14^{\circ} 32'$ E Gr. $\Delta G = + 59$ min.														KLCJEVJE												BR. ST. 36				
I	-	-01.3	03.1	00.0	00.4	03.8	-01.5	15.4	20 -03.3	26 01	00.4	20	04.4	17	03.4	02	00.2	*	*	*	*	*	*	*	*	23	04.1	20		
II	-	03.1	07.3	04.2	04.7	07.5	00.0	13.4	10 -02.8	08 07	03.9	12	04.3	13	06.9	04	01.5	*	*	*	*	*	*	*	*	23	05.5	06		
III	-	01.5	09.9	04.7	05.0	10.5	01.0	24.4	21 -04.3	14 16	03.1	04	01.3	10	02.9	12	03.4	*	*	*	01	00.4	*	*	*	31	05.0	13		
IV	-	03.7	12.1	07.2	07.7	13.0	01.7	15.6	09 -03.7	09 06	11.7	15	05.5	17	04.6	07	01.6	01	00.4	02	00.3	*	*	*	*	20	04.4	12		
V	-	04.7	16.7	11.7	12.3	17.7	06.6	25.0	20 00.1	10 02	00.4	26	05.3	15	01.7	10	03.4	*	*	*	04	00.6	*	*	*	20	04.0	17		
VI	-	12.0	16.0	13.9	16.7	20.5	05.1	26.0	04 01.9	13 12	02	00.8	17	03.9	13	05.3	03	00.6	*	*	*	*	*	*	*	*	36	06.9	17	
VII	-	14.7	17.5	17.0	18.0	14.8	11.2	30.0	30 05.6	09	*	*	39	07.5	18	05.7	11	03.0	*	*	*	*	*	*	*	*	14	03.2	12	
VIII	-	14.5	19.4	17.8	18.6	20.4	1.6	32.0	14 00.0	12	*	*	14	03.7	15	01.4	13	03.7	*	*	*	*	*	*	*	*	31	06.2	25	
IX	-	11.2	19.5	12.6	14.5	20.4	05.8	25.4	14 00.3	01.3	27	01	00.1	24	04.7	12	02.5	03	01.1	*	*	*	*	*	*	*	14	02.2	21	
X	-	03.7	08.2	04.2	04.8	04.3	01.5	15.5	25 -03.7	31 09	02.0	27	04.5	20	05.0	03	01.2	*	*	*	*	*	*	*	*	15	03.3	19		
XI	-	02.9	03.3	04.4	05.0	04.2	01.5	14.5	18 -00.1	04 02.0	36	02.7	13	01.9	03	01.0	*	*	01	00.3	*	*	*	*	*	20	04.3	09		
XII	-	01.7	04.9	00.2	00.8	06.1	-03.0	05.9	08 -09.3	15 02	00.4	18	03.4	13	05.5	04	00.9	*	*	*	*	*	*	*	*	41	07.4	17		
GDU.	-	06.0	13.1	06.3	06.9	14.0	04.3	32.0	05VM -09.3	15XII 54	02.0	291	04.9	187	04.6	77	02.5	01	00.4	08	00.4	*	*	*	*	*	268	05.2	187	
$\phi = 45^{\circ} 18'$ N $\lambda = 10^{\circ} 11'$ E Gr. $\Delta G = + 1h 01$ min.														NEVC MESTO-GOTNA VAS												BR. ST. 37				
I	74.6 -00.5	03.7	00.6	03.8	03.8 -00.9	16.1	20 -03.9	18	*	08	01.7	09	01.2	06	00.8	07	01.0	19	02.9	12	01.8	05	00.7	27						
II	74.6 03.0	05.4	05.4	05.6	05.4 02.3	14.0	11 -02.1	28 01	02.2	10	02.0	16	04.3	05	00.6	09	01.4	18	03.1	14	03.0	04	01.0	07						
III	74.4 -1.1	04.0	10.8	06.6	11.6	06.2	24.4	21 -03.7	14 03	00.4	12	02.4	15	03.0	12	01.4	15	02.9	14	04.7	14	01.9	06	01.0	02					
IV	74.6 04.0	13.0	05.5	04.9	14.3	03.0	20.9	16 -01.6	05 02	00.4	21	06.3	13	03.8	04	01.6	07	00.9	21	02.5	14	01.5	06	01.0	02					
V	74.6 16.6	16.6	12.8	13.5	14.4	06.1	25.9	22 03.0	10 06	01.4	13	02.8	04	00.9	01	00.1	10	01.7	27	05.0	21	04.0	08	01.9	03					
VI	74.1 13.2	16.5	16.1	21.1	16.6	26.6	26	04.1	12	02	00.5	07	01.4	11	02.0	03	00.4	14	01.9	15	02.4	26	04.2	11	02.0	01				
VII	74.2 15.1	16.9	16.9	15.3	25.6	12.1	31.4	17 06.6	09	02.0	09	02.6	10	02.6	08	01.3	12	02.1	25	04.6	17	02.5	06	01.1	02					
VIII	74.6 16.1	17.7	19.7	20.1	17.5	14.7	33.9	04 08.7	13 12	04	06.8	16	03.3	11	02.6	06	01.2	13	01.4	15	02.1	13	01.4	07	00.7	06				
IX	75.1 11.7	16.4	14.2	14.5	20.6	10.7	27.6	03 01.4	27	08	01.3	15	02.5	08	01.5	01	00.1	13	01.4	13	01.5	14	02.1	02	00.3	16				
X	73.5 05.7	05.2	05.2	10.3	02.6	15.7	25 -02.4	30 02	02.2	05	02.5	07	01.3	05	00.6	10	01.3	16	02.3	21	02.0	10	01.4	07						
XI	74.7 03.4	04.0	05.0	05.6	05.8	02.3	17.4	17 -04.0	29 01	00.2	14	02.3	09	01.6	03	00.4	08	01.0	28	05.1	17	03.1	03	00.3	07					
XII	74.6 -00.5	05.9	01.6	02.1	06.7	-01.5	12.2	03 -07.5	15 02	00.3	04	00.8	06	00.9	01	00.7	19	02.7	32	04.3	21	02.8	03	00.5	06					
GDU.	74.2 07.0	11.7	09.6	10.0	14.9	05.6	32.9	04VM -07.5	15XII 35	00.9	01.9	143	02.6	119	02.5	57	01.0	127	01.7	251	03.7	204	02.8	71	03.2	86				
$\phi = 15^{\circ} 04'$ N $\lambda = 15^{\circ} 12'$ E Gr. $\Delta G = + 1h 01$ min.														CRNCMELJ												BR. ST. 38				
I	-	-00.5	03.0	00.6	01.0	03.8 -01.3	15.4	20 -05.6	22 05	00.6	10	01.5	10	01.2	*	*	08	01.1	02	00.3	06	01.0	*	*	*	52				
II	-	03.7	08.8	06.4	06.2	09.1	02.7	14.5	12 -10.3	09 15	02.8	11	02.4	09	01.8	*	*	02	00.4	15	05.2	10	01.2	*	*	22				
III	-	01.8	11.5	07.6	07.6	11.5	02.9	22.3	21 -04.6	14 17	03.6	03	00.7	07	01.6	02	00.3	05	01.0	15	03.9	15	03.1	*	*	24				
IV	-	05.7	14.0	09.7	09.7	15.1	03.7	22.1	10 -00.8	04 19	05.7	09	02.7	09	03.0	07	01.2	08	01.5	13	03.2	03	00.6	01	00.2	27				
V	-	11.4	18.8	13.4	14.3	19.9	06.6	25.4	20 01.9	10 05	01.1	05	00.9	07	01.4	*	*	05	01.2	14	04.4	07	01.4	01	00.4	44				
VI	-	13.9	26.8	16.1	16.7	22.6	11.1	27.3	26 03.8	13 02	04.4	08	01.6	08	01.6	06	02.5	07	01.3	16	04.6	07	01.4	02	00.4	42				
VII	-	15.4	24.9	19.1	19.7	26.3	13.3	31.6	17 06.1	09 02	05.5	11	02.2	03	01.3	05	02.0	04	00.8	13	03.5	09	01.7	01	00.2	36				
VIII	-	16.0	16.2	19.8	20.4	14.4	14.0	33.8	04 07.4	12 15	02.8	06.0	10	01.4	05	00.9	04	00.7	05	00.9	*	*	*	*	*	42				
IX	-	11.1	18.4	15.2	15.5	21.5	10.7	25.1	03 02.7	27 02	00.8	05	01.0	08	01.0	06	00.8	01	00.1	08	02.0	02	00.3	01	00.1	56				
X	-	03.7	04.4	04.5	04.5	11.1	02.2	17.0	25 -03.8	30 07	01	01.9	06	01.0	02	00.3	04	01.0	13	03.0	04	00.6	*	*	48					
XI	-	04.0	09.6	04.5	05.4	10.2</																								

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm			Broj dana na sat																								
	7	14	21	Stred. (Dnev.)	Insolacija broj sati	mm	7	14	21	Sred. Min	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
<b>KCCEVJE</b>																																		
BR. ST.36																																		
I 5.5 7.3 6.6 6.6	-	04.4	55	87	95	52	58	043	C26.3	01	.	01	27	.	.	.	.	.	.	23	07	06	01	05	05	.	.	.	.	.	18	C6		
II 7.6 1.6 6.6 7.3	-	05.4	90	71	91	84	24	C78	C26.3	07	.	.	09	.	.	.	02	15	15	07	04	12	05	01	.	.	.	.	.	01	03	02		
III 8.3 7.0 5.6 7.0	-	05.4	93	65	85	81	36	C91	C30.1	05	.	.	16	.	.	.	01	12	15	11	08	04	02	10	.	.	.	.	.	01	04	15		
IV 5.9 7.1 5.2 6.1	-	05.9	90	57	84	76	30	092	C32.1	25	.	.	13	.	.	.	05	11	13	07	04	12	01	.	.	.	.	.	.	.	01	.	.	
V 5.5 7.0 5.7 6.1	-	08.2	94	58	83	76	29	151	C32.4	01	.	.	01	.	.	.	01	09	21	14	06	21	.	.	.	.	.	04	03	.				
VI 6.2 7.3 5.5 7.4	-	10.1	91	64	86	80	35	196	C34.2	30	.	.	01	.	.	.	02	09	20	14	07	20	.	.	.	.	.	01	05	04				
VII 4.8 4.3 3.0 4.0	-	11.3	88	56	77	73	37	112	C59.6	26	.	.	17	01	.	.	08	02	11	10	03	11	.	.	.	.	.	01	07	03				
VIII 7.9 4.8 3.6 5.5	-	12.9	96	62	84	81	35	293	110.2	29	.	.	15	07	.	.	05	09	11	08	06	11	.	.	.	.	.	10	12	.				
IX 9.2 5.6 4.6 6.5	-	10.5	96	67	89	84	28	208	C52.1	25	.	.	06	.	.	.	09	15	15	07	15	03	03	.	.	.	.	.	02	15	.			
X 9.1 6.0 6.0 7.7	-	05.8	96	76	95	89	38	334	C55.7	21	.	.	10	.	.	.	01	15	25	21	09	25	03	03	.	.	.	.	.	03	07	.		
XI 7.4 7.4 6.7 7.2	-	05.7	92	74	90	85	38	118	C37.1	29	.	.	13	.	.	.	02	15	16	09	05	16	02	01	.	.	.	.	.	01	02	04		
XII 6.6 5.6 3.7 5.3	-	04.4	93	79	93	88	49	032	C16.8	12	.	.	25	.	.	.	01	05	07	07	04	01	06	02	.	.	.	.	.	10	08	.		
GOD. 7.3 6.6 5.4 6.5	-	07.5	92	68	87	82	24	1748	110.2	29VM	.	01	113	40	06	.	07	.	32	139	172	123	57	157	28	05	.	.	04	01	38	E7	36	
<b>NOVO PESTO-GOTVA VAS</b>																																		
BR. ST.37																																		
I 9.6 8.8 8.0 9.8	019.3	04.6	97	89	97	94	48	032	C09.5	18	.	01	24	.	.	.	.	24	11	05	08	04	C1	.	.	.	.	.	21	C1	.			
II 8.1 7.8 7.5 8.0	072.1	05.5	90	68	83	80	29	033	C11.7	15	.	.	05	.	.	.	03	.	18	10	05	02	06	02	01	.	.	.	.	.	01	05	.	
III 7.6 7.3 6.8 7.3	115.6	05.7	93	61	79	78	33	078	C26.2	06	.	.	08	.	.	.	02	01	15	12	08	04	10	05	01	.	.	.	.	.	01	03	09	
IV 6.4 7.4 6.7 6.8	155.0	05.7	87	51	68	69	26	050	C15.2	26	.	.	05	.	.	.	03	02	12	11	09	02	11	.	.	.	.	.	01	01	C1			
V 6.2 7.1 7.1 6.8	200.6	08.5	89	55	80	75	25	145	C25.8	01	.	.	02	.	.	.	03	02	11	17	15	06	17	.	.	.	.	.	06	C5	.			
VI 6.7 7.1 6.2 6.7	182.3	10.4	89	56	84	77	28	163	C30.3	30	.	.	02	.	.	.	02	10	17	14	07	17	.	.	.	.	.	01	04	.				
VII 5.1 4.9 4.5 4.6	286.9	11.9	86	52	77	72	34	062	C33.4	26	.	.	19	04	.	.	01	07	05	11	07	01	11	.	.	.	.	.	07	03	.			
VIII 6.4 5.3 5.3 5.2	247.1	14.3	95	62	88	82	40	147	C05.6	26	.	.	16	04	.	.	04	14	10	10	06	10	.	.	.	.	.	05	14	.				
IX 7.9 6.1 5.2 6.4	160.4	11.2	57	69	96	87	41	160	C43.5	25	.	.	03	.	.	.	03	12	16	11	07	14	.	.	.	.	.	03	16	.				
X 8.5 7.9 6.5 7.6	074.5	06.3	97	76	95	90	39	275	C05.0	21	.	.	06	.	.	.	01	15	23	17	09	21	01	01	.	.	.	.	.	04	17	.		
XI 6.0 7.2 6.9 7.8	085.6	05.8	93	70	90	84	30	082	C23.3	29	.	01	10	.	.	03	01	11	12	07	04	12	01	01	.	.	.	.	.	02	07	02		
XII 6.9 6.5 5.5 6.3	092.9	04.7	96	74	91	87	25	029	C15.9	12	.	01	22	.	.	01	03	11	08	04	01	08	02	01	.	.	.	.	.	16	04	.		
GOD. 7.2 7.0 6.3 6.8	1692.3	07.9	92	65	85	81	26	1752	C55.0	21X	.	03	83	80	42	08	.	15	.	26	151	158	112	49	146	15	09	02	.	02	01	44	119	7
<b>ČRACPELJ</b>																																		
BR. ST.38																																		
I 5.7 8.7 8.5 9.0	-	04.6	96	88	96	94	36	048	C18.0	01	.	01	18	.	.	.	.	24	21	06	02	18	04	02	.	.	.	.	.	18	06	.		
II 6.0 6.1 7.9 6.0	-	05.6	89	72	82	81	32	041	C12.6	15	.	.	03	.	.	.	03	.	16	17	C5	01	15	02	.	.	.	.	.	04	.			
III 5.3 6.9 7.3 7.1	-	05.9	91	63	73	78	29	092	C22.5	05	.	.	04	01	.	.	02	14	12	08	04	09	11	04	03	.	.	.	.	.	01	06	04	
IV 5.9 6.6 6.9 6.3	-	06.0	84	52	68	68	22	061	C24.1	26	.	.	02	.	.	.	01	06	12	12	05	01	12	01	01	.	.	.	.	.	02	.		
V 5.6 7.1 7.5 6.7	-	08.7	87	54	77	73	29	162	C33.3	01	.	.	04	.	.	.	C1	01	11	17	13	07	17	.	.	.	.	.	07	01	.			
VI 7.7 7.2 6.8 6.6	-	10.8	85	60	81	75	41	168	C34.5	30	.	.	06	.	.	.	01	02	18	20	13	02	20	.	.	.	.	.	07	01	.			
VII 4.1 4.4 4.2 4.2	-	12.1	86	54	75	71	34	085	C35.4	26	.	.	21	05	.	.	01	10	04	09	08	03	09	.	.	.	.	.	05	04	.			
VIII 4.2 4.7 4.1 4.3	-	14.2	93	59	86	79	30	278	C07.1	26	.	.	19	10	.	.	11	06	10	10	05	10	.	.	.	.	.	10	11	.				
IX 6.6 5.6 6.3 6.2	-	11.3	56	88	90	85	46	186	C04.0	21	.	.	08	.	.	.	C1	04	12	14	12	07	14	.	.	.	.	.	05	16	.			
X 7.9 7.0 6.5 7.4	-	06.4	96	76	93	88	45	324	C04.0	21	.	.	08	.	.	.	C1	02	16	24	21	12	24	01	.	.	.	.	.	01	16	C7		
XI 6.4 7.3 7.2 7.6	-	06.2	92	74	87	94	34	105	C36.2	29	.	.	10	.	.	.	C1	01	16	13	08	04	13	01	01	.	.	.	.	.	01	10	C7	
XII 6.1 5.4 5.6 5.7	-	05.6	90	73																														

Mesec	Vardubljan pritisak mm Pm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm			Max	Min	Max.	Dat.	Min.	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dnev.)						8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.			
$\varphi = 41^{\circ}18'$ N $\lambda = 16^{\circ}23'$ E Gr. $\Delta G = + 1h 05$ min.																													
I	752.9	-00.1	03.4	01.0	01.3	03.9	-00.6	13.0	20	-04.3	22	11	01.8	01	02.0	14	01.8	10	01.8	28	02.7	07	01.6	12	01.7	04	01.5	06	
II	745.5	03.0	08.7	05.0	05.4	09.5	02.0	15.8	12	-02.5	28	10	02.5	11	02.4	14	01.7	04	01.5	15	02.8	14	03.4	11	02.7	02	01.0	03	
III	748.6	03.4	11.5	06.7	07.1	12.1	02.3	22.8	21	-03.2	01	14	02.2	16	02.3	21	02.0	01	01.0	10	02.1	13	02.5	10	02.4	02	02.0	06	
IV	745.4	06.2	14.3	09.4	15.1	03.1	03.1	10	10	-02.0	16	04	18	C3.0	12	02.9	11	02.4	*	*	18	02.6	07	02.1	14	01.9	07	01.9	03
V	745.2	12.3	18.0	12.6	13.9	19.0	08.6	25.4	20	02.3	10	11	02.2	07	02.1	08	02.1	03	02.0	17	02.6	09	02.8	26	01.8	09	01.9	03	
VI	745.8	15.0	11.2	15.4	16.8	22.2	11.1	27.0	26	04.0	12	10	02.7	C7	02.0	03	01.3	01	01.0	15	02.1	21	02.5	16	01.9	15	01.9	02	
VII	747.9	17.2	23.7	18.0	19.2	25.0	13.3	30.6	31	09.8	26	11	02.2	07	01.5	10	01.6	05	01.2	17	01.9	20	02.4	13	01.3	08	01.9	01	
VIII	748.4	17.4	25.6	19.3	20.4	26.5	14.4	32.4	16	07.1	13	15	02.0	08	01.4	10	01.9	03	02.0	12	02.2	09	01.7	16	02.7	05	01.6	15	
IX	747.7	12.9	19.7	13.9	15.1	20.6	10.6	27.2	14	02.8	27	12	02.0	04	02.5	17	01.5	08	01.6	10	02.3	08	02.9	16	01.6	04	01.5	06	
X	744.3	04.3	10.0	06.1	06.6	10.8	02.9	14.8	20	-01.8	30	11	02.3	08	01.9	05	02.0	03	01.3	09	02.9	26	02.4	17	01.6	08	01.5	06	
XI	748.7	03.7	09.9	05.5	06.2	10.4	02.6	17.7	16	-03.8	10	16	02.3	05	01.6	10	01.5	*	*	23	02.8	21	03.0	07	02.0	04	01.2	04	
XII	750.7	01.0	07.1	02.7	03.4	07.9	-00.3	16.4	03	-06.0	15	06	02.5	03	02.3	07	01.3	05	01.4	16	01.9	24	02.0	18	01.6	05	01.2	04	
GOD.	747.6	08.0	14.4	09.6	10.4	15.2	05.8	32.4	KvM	-06.0	15.0	11.5	02.3	84	02.2	130	01.8	43	01.6	190	02.4	179	02.5	176	01.8	75	01.6	73	
$\varphi = 46^{\circ}02'$ N $\lambda = 16^{\circ}33'$ E Gr. $\Delta G = + 1h 07$ min.																										KRIJEVCI		BR. ST.41	
I	754.6	-00.1	02.4	00.9	01.0	02.9	-00.8	14.0	20	-04.6	15	04	02.2	17	02.5	09	02.3	13	02.3	12	02.4	28	02.2	04	02.0	06	C2.3	*	
II	746.7	03.1	08.9	05.5	05.8	09.6	02.0	15.5	12	-02.5	09	10	03.7	28	02.9	04	03.5	01	03.0	10	02.6	20	03.3	03	05.0	07	C2.4	*	
III	749.8	04.0	11.6	07.8	07.8	12.5	03.0	22.9	22	-03.0	14	10	03.4	42	03.1	12	03.8	04	02.0	03	02.3	15	03.1	03	02.0	04	02.0	*	
IV	746.4	06.3	14.5	08.8	09.6	15.3	03.6	21.4	28	-00.5	24	24	03.4	24	03.8	08	04.0	02	04.0	10	02.2	06	02.3	03	02.7	13	02.7	*	
V	746.2	11.6	17.9	12.5	13.6	18.9	08.4	24.8	20	03.7	09	16	02.9	17	02.6	C3	02.3	06	02.3	10	02.4	20	02.9	07	02.4	14	02.3	*	
VI	746.9	15.0	20.5	15.7	16.7	22.0	11.2	26.7	26	06.0	12	09	12	04.1	12	03.3	05	02.4	11	02.5	22	02.9	06	02.7	20	02.5	*		
VII	749.0	16.9	23.8	18.2	19.3	25.0	13.0	31.5	17	06.2	21	18	03.2	12	03.1	07	02.4	09	02.7	20	02.8	04	02.5	16	02.8	*			
VIII	749.4	17.7	25.6	19.7	20.7	26.5	14.9	32.2	16	07.3	13	20	02.9	26	03.0	06	02.7	12	02.4	07	02.6	*	*	17	02.0	*			
IX	748.8	12.6	20.2	14.2	15.3	21.0	10.8	28.2	03	03.0	28	20	02.6	22	03.1	03	02.3	05	02.2	17	03.0	*	*	17	02.1	*			
X	741.6	04.3	09.9	06.3	06.7	10.5	02.8	14.5	20	-0.2	31	20	03.0	15	02.7	02	03.0	04	02.0	13	02.6	23	02.7	03	02.0	13	02.0	*	
XI	750.3	03.1	09.3	04.0	05.6	06.9	09.8	01.7	18.2	16	-0.4	10	13	03.5	11	03.4	04	02.0	04	02.0	14	02.8	33	02.8	03	02.9	09	C2.8	*
XII	752.3	00.6	05.3	02.3	02.6	06.2	-00.6	13.5	04	-05.5	17	16	01.7	03.9	14	02.5	02	02.5	03	02.0	19	02.2	30	02.2	06	02.2	12	02.2	*
GOD.	748.8	07.9	14.2	09.7	10.4	15.0	05.8	32.2	KvM	-05.5	17.0	11.7	02.4	240	03.0	65	02.9	57	02.3	129	02.4	241	02.7	42	02.5	147	C2.1	*	
$\varphi = 46^{\circ}11'$ N $\lambda = 16^{\circ}49'$ E Gr. $\Delta G = + 1h 07$ min.																										KOPRIVNICA		BR. ST.43	
I	-	00.4	03.0	01.1	01.4	03.7	-00.2	12.0	20	-04.5	15	04	01.2	09	01.0	10	01.7	16	01.4	21	01.4	23	01.6	01	01.0	09	01.6	*	
II	-	03.4	09.1	05.3	05.8	09.8	02.4	15.6	12	-02.4	28	12	01.8	18	01.9	04	03.5	04	01.0	10	01.9	27	02.3	02	02.0	07	01.4	*	
III	-	04.3	12.3	07.0	07.7	12.9	03.1	24.0	23	-23.2	01	10	01.5	36	01.8	08	01.6	07	01.4	17	01.8	06	02.5	04	01.8	*			
IV	-	07.0	15.3	08.9	10.1	16.0	04.4	22.5	28	-06.7	04	09	02.0	25	02.3	04	02.0	05	01.2	22	02.0	20	02.0	15	01.6	*			
V	-	12.5	18.8	12.9	14.3	19.6	09.7	26.2	30	04.5	10	04	01.2	13	01.8	C3	02.0	08	01.4	33	02.2	02	02.0	22	01.7	*			
VI	-	15.2	21.6	15.5	17.0	22.8	12.1	28.3	04	05.5	08	04	01.2	14	02.1	C1	01.0	05	01.0	36	01.9	03	01.7	20	01.4	*			
VII	-	17.5	24.7	17.9	19.5	25.6	14.1	32.0	17	10.0	27	04	02.0	22	01.3	C1	01.0	23	01.4	20	01.6	20	01.4	06	01.3	13	01.6	*	
VIII	-	17.6	26.6	19.5	20.8	27.6	15.2	33.0	17	16.6	07	13.0	02.2	22	01.4	04	01.0	10	01.2	23	01.4	02	01.0	15	01.4	*			
IX	-	13.4	20.7	14.1	15.6	21.6	11.3	28.2	03	04.5	27	10	01.7	20	01.6	02	01.5	11	01.2	13	01.9								



Meseč Vremenski Splitsak PM MM	Temperatura vazduha °C	Čestina pravaca i srednja jačina vетра m/s (0-12)																																					
		Tm						Dm						Dat.						N		NE		E		SE		S		SW		W		NW		C			
		7	14	21	Sred. (Dm)	Mx	Mn	Mx	Dat.	Mn	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.										
$\varphi = 45^{\circ}14'$ N $\lambda = 13^{\circ}56'$ E Gr. $\Delta G = + 56$ min.																				PAZIN		BR. ST. 46																	
I	735.6	01.8	09.4	03.8	04.7	10.5	06.4	16.4	21	-04.5	22	05	01.2	03	01.3	07	01.4	08	01.5	04	01.2	04	01.2	05	01.0	02	01.0	05	01.0	02	01.0	05							
II	732.5	03.7	10.3	05.5	06.3	11.1	02.0	14.5	20	-05.2	28	.	.	07	02.0	11	02.2	15	02.3	13	01.8	03	02.3	04	02.0	.	.	02	01.0	03	01.0	05	01.0	03					
III	735.3	02.8	13.1	06.6	07.3	14.0	01.7	24.3	22	-07.0	01	03	02.0	05	01.8	13	02.4	15	02.2	05	02.4	04	02.5	01	02.0	01	02.0	04	02.0	01	02.0	04	02.0	01	02.0	04			
IV	732.2	05.7	14.4	08.6	09.4	15.5	03.6	19.3	09	-01.6	20	03	02.0	09	02.0	12	02.2	18	01.8	08	02.5	06	02.8	03	02.7	01	03.0	03	02.7	01	03.0	03							
V	732.3	11.0	18.9	12.7	13.8	20.0	07.9	27.0	21	03.0	10	04	01.8	*	*	06	02.8	20	02.2	07	02.7	08	02.4	06	02.6	01	02.0	01	02.0	04	02.0	01	02.0	04					
VI	734.2	13.8	21.5	15.8	16.7	23.0	10.8	30.4	04	04.2	12	07	02.5	03	01.7	08	01.6	07	02.3	10	02.6	11	02.6	05	02.6	04	02.0	04	02.0	04	02.0	04							
VII	736.1	15.1	26.8	19.5	20.2	27.6	13.0	39.7	30.29	08.6	24	02	01.0	05	01.6	07	02.4	07	02.6	08	02.5	36	02.5	06	02.3	06	02.0	04	02.0	06	02.0	04							
VIII	736.1	15.3	26.7	20.2	21.1	30.0	13.5	35.0	04	08.5	12	03	02.3	04	01.5	07	02.3	07	02.3	04	02.5	02	03.0	04	02.0	04	02.0	04	02.0	04	02.0	04							
GOD.	735.2	07.7	16.6	10.3	11.2	17.6	05.7	35.0	04/VIII	-07.0	04/III	32	01.9	51	01.7	103	02.0	120	02.1	97	02.3	75	02.3	52	02.0	29	01.8	53	02.0	29	01.8	53	02.0	29					
$\varphi = 45^{\circ}20'$ N $\lambda = 14^{\circ}27'$ E Gr. $\Delta G = + 58$ min.																				RIJEKA		BR. ST. 47																	
I	756.7	05.6	10.4	07.0	07.5	11.3	04.5	20.0	20	01.4	15	03	01.0	38	01.7	05	02.0	01	01.0	03	01.0	09	01.0	.	.	01	01.0	03	01.0	09	01.0	03	01.0	09	01.0	03			
II	749.6	07.7	16.9	08.5	08.9	11.7	06.7	16.0	16	01.7	28	03	01.7	31	03.7	07	03.6	06	02.5	09	01.8	06	01.3	.	.	03	02.0	01	02.0	04	02.0	01	02.0	04					
III	752.4	07.6	12.7	09.7	09.9	13.9	06.7	21.7	22	-00.3	01	05	03.0	35	02.8	07	03.7	02	02.0	05	01.4	10	01.6	02	02.0	.	.	02	01.0	03	01.0	02	01.0	03					
IV	745.0	10.1	14.9	12.0	12.3	16.0	08.5	20.3	08	04.5	16	06	02.7	36	03.1	04	03.5	02	02.5	05	01.6	05	02.6	02	01.0	05	02.6	02	01.0	05	02.6	02	01.0	05					
V	745.9	14.1	18.4	14.7	15.5	19.8	11.6	26.3	21	08.0	09	02	02.0	14	01.9	04	02.2	04	01.5	05	01.4	17	01.4	05	01.6	02	03.0	04	01.6	05	01.6	02	03.0	04					
VI	750.3	17.2	21.1	17.5	18.3	22.6	14.6	27.9	04	08.6	12	04	02.0	17	02.6	02	01.5	06	02.5	06	01.5	11	01.4	02	02.5	01	01.0	04	02.5	01	01.0	04							
VII	752.1	20.4	26.0	21.3	22.2	27.2	17.7	32.7	30	14.2	25	01	01.2	26	02.6	04	02.2	02	03.5	05	01.0	21	01.5	02	01.0	.	.	02	01.0	03	01.0	02	01.0	03					
VIII	751.9	11.6	26.3	22.9	23.9	29.2	19.6	34.8	16	13.3	12	02	02.5	29	02.3	02	02.5	02	02.5	03	01.3	14	01.4	01	02.0	01	01.0	03	01.0	01	01.0	03							
IX	751.4	16.7	23.2	18.2	19.1	24.1	15.4	29.4	15	08.8	27	01	01.0	30	02.0	05	01.8	02	02.0	06	02.3	12	02.0	01	02.0	.	.	02	01.0	03	01.0	02	01.0	03					
X	748.4	08.9	12.3	09.6	10.1	14.0	07.2	17.2	07	03.3	17	.	.	45	02.2	07	02.1	03	02.3	06	02.8	09	02.0	01	02.0	.	.	02	01.0	03	01.0	02	01.0	03					
XI	753.4	09.0	12.5	09.6	10.2	13.3	07.7	16.0	14	02.4	02	05	02.0	26	01.7	05	01.8	02	02.0	06	02.0	07	01.4	.	.	02	01.0	03	01.0	02	01.0	03							
XII	755.8	05.7	10.5	07.1	07.6	11.4	04.7	16.2	03	01.3	13	04	02.2	31	01.7	03	01.3	02	01.0	05	01.4	02	01.0	.	.	02	01.0	04	01.0	02	01.0	04							
GOD.	751.8	12.0	16.8	13.2	13.8	17.9	10.4	34.8	16/VIII	-00.3	04/III	36	02.1	358	02.4	56	02.5	30	02.2	71	01.7	123	01.5	19	02.0	10	01.7	393	01.0	02.0	01.0	02.0	01.0	02.0					
$\varphi = 45^{\circ}36'$ N $\lambda = 14^{\circ}38'$ E Gr. $\Delta G = + 59$ min.																				PAG		BR. ST. 48																	
I	691.0	-00.4	02.7	00.3	00.7	03.9	-02.3	13.2	20	-06.9	15	02	01.0	06	01.3	03	01.0	50	01.2	25	01.3	05	01.6	.	.	02	01.0	01	01.0	05	01.6	02	01.0	05	01.6	02	01.0		
II	684.9	01.8	03.9	02.2	02.5	05.0	00.0	08.9	20	-06.0	08	.	.	01	01.0	01	04.0	24	01.4	20	02.5	32	02.7	01	02.0	04	02.2	01	02.0	04	02.2	01	02.0	04					
III	688.4	02.2	07.2	03.6	04.1	08.5	00.5	19.8	21	-04.9	14	01	01.0	04	01.5	02	01.5	53	01.5	20	01.3	10	02.6	.	.	03	01.0	03	01.0	05	01.0	03	01.0	05	01.0	03			
IV	685.1	04.4	09.0	05.5	06.1	10.7	16.6	03.0	03	-01.4	18	01	01.0	15	02.6	04	03.0	37	01.7	18	01.6	10	02.4	.	.	02	01.0	03	01.0	05	01.0	03	01.0	05	01.0	03			
V	686.5	08.8	12.7	09.0	09.9	14.7	05.3	21.2	20	01.6	09	02	01.0	08	01.8	05	01.8	41	01.7	14	01.4	18	02.4	.	.	03	01.0	02	01.0	04	02.4	01	02.0	04	02.4	01	02.0		

Meseč	Oblačnost Nm (0-10)	Inzocijacija broj sati (Dles)	Vlažnost vazduha			Padavine R mm	Broj dana na sa:												•	*	*	Δ	Δ	▲	▲	R	T	III	■								
			a <sub>m</sub>	U m t			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	III	■												
				7	14	21	Sred. (Dles)	Σ	Max	Dati.	≤	<	<	≥	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV											
PAZIN																																					
BR. ST.46																																					
I	7.7	7.1	6.2	7.0	-	05.3	93	66	91	83	30	070	040-1	01	.	.	16	.	.	.	.	02	15	14	07	01	13	.	.	.	.	.	16				
II	7.3	7.4	6.5	7.1	-	05.4	86	58	81	75	22	080	018-1	07	.	.	09	.	.	.	.	04	09	15	12	03	14	.	.	.	.	.	02	04			
III	6.7	6.6	5.6	6.1	-	05.5	89	48	78	72	12	171	160-4	05	.	.	10	.	.	.	.	04	09	05	03	01	05	01	.	.	.	.	.	01	04		
IV	5.6	7.0	5.0	5.9	-	05.7	81	44	69	65	18	104	046-8	29	.	.	05	.	.	.	.	05	09	09	08	04	09	.	.	.	.	.	02	.			
V	4.7	7.2	5.9	6.3	-	06.5	86	52	80	73	27	068	022-9	05	.	.	03	.	.	.	.	02	12	16	11	01	16	.	.	.	.	.	04	01			
VI	4.3	7.2	4.5	6.0	-	10.4	88	54	78	73	26	135	036-0	30	.	.	06	01	.	.	.	02	17	14	13	06	14	.	.	.	.	.	12	02			
VII	3.3	4.4	3.6	3.7	-	11.2	88	40	69	65	17	017	014-7	07	.	.	27	07	.	.	.	10	02	05	03	01	05	.	.	.	.	.	05	.			
VIII	3.0	4.9	3.5	3.6	-	12.4	93	40	77	70	17	080	039-8	11	.	.	26	16	.	02	01	13	02	09	06	02	09	.	.	.	.	.	01	16			
IX	4.8	5.4	3.1	4.5	-	10.7	93	49	87	74	26	162	043-8	25	.	.	15	.	.	.	.	08	06	11	10	05	11	.	.	.	.	.	01	11	04		
X	7.7	7.8	5.2	6.9	-	06.4	93	63	90	82	24	238	040-6	05	.	.	08	.	.	.	.	11	21	19	08	21	.	.	.	.	.	08	11				
XI	6.1	7.6	6.4	7.4	-	06.5	91	65	90	82	22	092	022-0	26	.	.	09	.	.	.	.	01	15	11	09	05	11	.	.	.	.	.	01	09			
XII	6.6	6.2	5.0	5.9	-	04.9	92	63	85	80	22	032	014-9	12	.	.	20	.	.	.	.	06	12	15	06	01	09	.	.	.	.	.	02	17			
GND.	6.1	6.6	4.6	4.9	5.9	-	07.7	89	53	81	74	12	1252	160-4	058	.	.	77	79	24	.	02	01	53	109	145	107	38	137	01	.	.	.	.	02	59	68
RIJEKA																																					
BR. ST.47																																					
I	6.7	7.0	5.3	6.3	084.7	05.6	75	65	74	71	37	058	022-2	01	.	.	01	.	01	03	12	13	09	02	12	.	.	.	.	.	02	.					
II	7.8	7.6	5.6	7.0	096.2	06.1	73	64	72	70	24	129	040-3	07	.	.	01	.	06	02	03	12	12	09	05	12	.	.	.	.	.	01	.				
III	6.4	6.8	5.4	6.2	143.8	05.9	70	54	65	63	22	096	079-2	05	.	.	01	.	04	05	11	05	04	02	05	.	.	.	.	.	01	.					
IV	6.5	7.4	6.2	6.7	166.4	06.2	63	52	59	58	24	167	048-4	29	.	.	01	.	01	05	15	09	07	04	05	.	.	.	.	.	03	.					
V	5.8	7.4	6.1	6.5	203.6	09.2	74	60	74	70	34	170	037-1	05	.	.	02	.	01	03	13	17	14	08	17	.	.	.	.	.	01	06					
VI	6.2	6.5	5.7	7.2	187.2	11.2	71	63	77	70	32	176	051-1	30	.	.	07	.	02	02	12	17	15	07	17	.	.	.	.	.	01	12					
VII	3.0	4.1	3.4	3.7	330.3	12.6	67	51	67	62	31	088	042-5	26	.	.	24	05	05	01	11	02	07	04	03	07	.	.	.	.	.	05	.				
VIII	3.4	4.0	2.4	3.2	302.5	13.0	64	45	64	58	29	067	025-1	11	.	.	28	14	16	02	01	16	C2	03	07	02	08	.	.	.	.	.	09	.			
IX	5.6	4.9	3.4	4.6	207.5	10.8	73	51	69	64	27	215	077-5	25	.	.	17	.	01	03	01	09	06	14	12	05	14	.	.	.	.	.	07	.			
X	7.6	8.3	5.9	7.2	101.3	06.4	74	60	72	69	32	257	049-6	21	.	.	07	.	02	02	12	17	17	08	21	.	.	.	.	.	01	05					
XI	6.1	7.3	6.7	7.3	080.0	06.7	74	63	72	70	26	118	038-4	26	.	.	01	.	01	02	16	16	11	03	16	.	.	.	.	.	02	.					
XII	5.4	6.1	5.0	5.5	094.2	05.5	73	63	70	69	29	033	016-2	12	.	.	01	.	01	06	10	10	05	01	10	.	.	.	.	.	01	01					
GND.	6.1	6.5	5.1	5.9	1999.7	08.3	70	57	69	66	22	1572	079-2	058	.	.	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01		
PARG																																					
BR. ST.48																																					
I	7.7	7.8	6.0	7.2	061.5	04.2	90	81	89	87	32	033	C10-0	01	.	.	07	28	.	.	.	04	15	14	05	01	08	07	.	.	.	.	.	11	18		
II	8.7	8.6	7.9	8.4	043.3	04.6	85	79	84	83	18	158	059-2	07	.	.	01	11	.	.	.	01	22	16	11	05	11	06	.	.	.	.	.	05	07		
III	7.6	7.5	7.5	7.5	100.3	05.1	89	70	86	82	35	085	033-1	05	.	.	01	16	.	.	.	03	20	11	10	04	04	10	.	.	.	.	.	01	19		
IV	5.9	7.3	7.8	7.0	133.7	05.1	76	72	74	71	34	120	039-7	29	.	.	06	.	01	01	05	15	09	04	12	06	.	.	.	.	.	03	08				
V	5.2	7.9	7.2	6.8	162.3	06.8	81	65	78	74	41	180	049-8	01	.	.	06	08	.	.	.	10	17	13	06	17	.	.	.	.	.	01	08	05			
VI	6.2	7.0	7.8	7.0	149.2	06.2	78	68	79	75	41	232	036-5	07	.	.	07	01	.	.	.	01	13	18	16	09	18	.	.	.	.	.	14	03			
VII	3.9	3.3	3.4	4.2	275.1	10.0	81	61	76	73	47	147	069-1	26	.	.	04	04	.	.	.	06	01	11	09	04	11	.	.	.	.	.	08	06			
VIII	4.9	5.4	4.2	4.8	236.8	11.9	66	87	84	79	42	206	065-6	29	.	.	13	.	.	.	.	09	08	12	11	05	12	.	.	.	.	.	11	03			
IX	5.9	6.6	5.5	6.2	162.6	09.3	88	74	88	83	48	227	087-9	25	.	.	12	01	.	.	.	06	12	15	15	06	1										

Mjesec M	Vrijeme prijevoda M Hr	Temperatura vazduha °C										Gestina pravaca i srednja jačina vjetra m/s, fm (0-12)																										
		Tm				RH				P		RH		Dm		N		NE		E		SE		S		SW		W		NW		C						
		7	14	21	Sred. (Dm)	IN	IN	IN	IN	P1.	P2.	P3.	P4.	Dm1	Dm2	Dm3	Dm4	E1.	E2.	E3.	E4.	S1.	S2.	S3.	S4.	W1.	W2.	W3.	W4.	NW1.	NW2.	C1.	C2.					
$\varphi = 45^{\circ}25'$ N $\lambda = 14^{\circ}33'$ E Gr. AG - + 1h 00 min.																														SRM&C		BR. ST. 51						
I	-	00.3	03.5	01.1	01.3	04.3	-01.4	19.2	20	-04.0	15	.	.	37	02.0	09	02.2	01	02.0	.	.	35	02.3	10	02.0	03	02.0	.	.	.	.	.						
II	-	02.4	05.3	03.6	03.0	06.1	01.3	09.8	20	.	.	35	02.4	06	02.2	02	02.5	.	.	27	03.2	11	02.3	03	02.0	.	.	.	.	.								
III	-	03.0	07.6	04.7	05.0	08.7	01.5	21.7	21	-04.4	01	.	.	38	02.3	14	02.4	03	02.0	.	.	29	02.5	07	02.8	04	02.0	.	.	.	.							
IV	-	05.4	10.3	06.8	07.4	11.3	02.5	16.3	10	-02.0	14	.	.	45	02.9	06	02.0	03	02.7	.	.	19	02.5	17	02.1	.	.	.	.	.	.							
V	-	10.6	15.4	10.7	11.9	16.6	06.9	23.0	20	02.8	10	.	.	26	02.4	12	02.5	04	03.0	.	.	42	02.5	13	02.5	06	02.2	.	.	.	.							
VI	-	13.4	18.0	13.5	14.6	19.4	09.7	25.0	04	03.5	13	.	.	27	02.4	09	02.6	01	01.0	.	.	46	02.4	07	02.4	04	02.5	.	.	.	.							
VII	-	16.0	22.0	16.8	17.9	23.2	11.7	26.0	17.16	05.3	13	.	.	26	02.5	19	02.4	01	03.0	.	.	40	02.4	15	02.2	02	02.0	.	.	.	.							
VIII	-	16.4	21.8	18.4	19.0	24.0	13.8	26.9	04	08.2	12.11	01	02.0	44	02.3	09	02.6	03	02.2	.	.	18	02.2	13	02.0	03	02.3	.	.	.	.							
IX	-	12.1	17.2	13.9	14.5	18.1	09.6	23.5	02	01.9	27	.	.	38	02.4	16	02.3	02	02.5	.	.	37	02.7	08	01.9	04	02.2	.	.	.	.							
X	-	03.4	06.6	04.0	04.5	07.7	01.0	13.8	04	-04.4	30	.	.	32	02.2	11	02.0	01	03.0	.	.	31	02.8	17	02.4	01	02.0	.	.	.	.							
XI	-	04.1	07.1	04.5	05.1	08.2	00.7	18.0	16	-08.5	28	07	02.9	18	02.2	05	02.4	01	01.0	79	02.9	12	02.0	15	03.0	03	.	.	.	.								
XII	-	02.5	05.2	03.3	03.6	06.9	-01.1	14.7	29	-04.8	15	01	01.0	11	02.8	03	03.7	15	02.3	.	.	05	01.4	22	02.8	34	03.0	02	.	.	.							
GOD.	-	07.5	11.8	08.4	09.0	12.0	04.7	29.9	04W	-09.8	15XII	04	02.0	377	02.4	25	02.3	43	02.4	01	01.0	351	02.6	152	02.3	77	02.7	05	.	.	.							
$\varphi = 45^{\circ}18'$ N $\lambda = 15^{\circ}14'$ E Gr. AG - + 1h 01 min.																														COULIN		BR. ST. 52						
I	739.0	-00.6	04.1	00.8	01.3	05.1	-01.4	18.9	20	-05.6	26	06	01.9	11	01.7	11	01.4	10	01.5	07	01.7	06	01.8	10	01.7	13	01.5	14	.	.	.							
II	730.7	04.4	07.7	05.8	08.5	03.4	03.4	13.7	02	-01.6	08	07	02.1	18	02.0	01	01.7	08	03.2	14	03.2	16	02.6	10	02.3	11	02.7	05	04	.	.	.						
III	733.7	03.7	10.2	06.4	06.7	10.8	02.9	24.0	21	-04.6	14	14	02.1	14	02.1	15	01.6	05	01.8	07	04.0	06	03.7	18	02.3	16	02.7	08	.	.	.							
IV	730.4	05.1	12.3	08.6	07.7	13.4	03.9	19.6	29	00.3	04	14	02.6	18	02.7	10	02.2	03	02.0	02	02.0	05	04.0	15	02.4	16	02.7	07	.	.	.							
V	730.4	10.8	17.2	12.5	13.2	18.5	08.6	24.1	27	03.2	10	06	02.3	07	02.1	10	02.0	05	02.4	14	03.7	12	02.2	19	01.4	19	.	.	.	.								
VI	731.7	13.3	19.6	15.2	16.1	21.3	11.0	25.7	04	03.8	12	04	02.2	02	02.5	08	01.9	06	02.2	13	03.5	16	02.4	17	01.4	19	.	.	.	.								
VII	733.8	16.1	23.6	18.4	19.1	25.0	12.9	30.0	17	08.0	27	04	02.7	13	02.0	10	02.0	04	01.8	06	02.5	11	04.0	16	02.4	17	01.4	19	.	.	.							
VIII	734.2	16.1	24.5	18.5	19.4	25.5	14.3	32.0	18	06.1	12	06	01.6	15	01.7	11	01.7	04	01.8	03	02.5	03	03.0	20	01.7	29	01.6	01	01.7	01	01.7	01	01.7	01	01.7			
IX	733.3	12.1	19.3	14.3	15.0	20.5	10.5	26.4	03	01.7	27	07	01.0	12	01.9	12	02.0	06	01.3	04	02.2	10	03.3	18	01.7	22	01.5	04	.	.	.	.						
X	729.7	04.2	08.8	05.4	06.0	10.4	02.4	16.0	25	-04.7	30	06	02.0	08	02.1	04	01.8	08	03.0	14	02.7	25	01.7	15	01.9	04	.	.	.	.								
XI	734.3	04.9	09.2	05.8	06.4	10.3	03.4	17.0	19	-02.5	10	09	01.4	08	01.9	09	01.2	07	01.9	07	01.1	20	02.2	16	02.5	14	01.9	.	.	.	.							
XII	734.2	01.9	08.9	04.0	04.7	10.7	-00.0	17.1	03	-09.8	19	04	02.5	11	01.9	02	01.5	03	02.0	05	02.4	14	04.2	26	03.0	20	02.3	04	01.9	04	01.9	04	01.9					
GOD.	733.1	07.8	13.8	09.6	10.2	15.0	06.0	32.0	04W	-09.8	15XII	04	02.0	137	02.1	93	01.8	71	01.8	66	02.4	130	03.4	212	02.2	157	01.9	100	.	.	.	.						
$\varphi = 45^{\circ}30'$ N $\lambda = 15^{\circ}33'$ E Gr. AG - + 1h 02 min.																															KARLOVAC		BR. ST. 53					
I	737.3	30.0	02.8	01.3	01.3	03.5	-00.3	18.5	20	-03.8	22	02	01.0	30	01.1	02	01.9	.	.	05	01.2	01	01.0	01	01.3	50	.	.	.	.	.	.	.	.	.	.		
II	749.5	05.6	06.6	06.7	10.1	03.4	01.3	13.7	11	-01.1	20	08	06	01.2	24	01.6	04	03.0	.	.	23	02.3	.	.	07	02.5	28	.	.	.	.	.	.	.	.	.		
III	752.5	04.1	12.0	06.8	08.1	12.9	01.6	25.7	21	-02.6	14	04	01.2	37	01.6	06	01.5	.	.	09	02.4	.	.	01	02.0	41	.	.	.	.	.	.	.	.	.			
IV	749.0	05.5	14.6	10.2	15.6	04.6	2.2	21	10	01.0	20	04	04	01.5	37	02.1	02	01.5	.	.	03	02.7	.	.	03	02.0	41	.	.	.	.	.	.	.	.	.		
V	745.0	10.4	19.3	14.2	14.7	20.3	09.6	26.4	20	03.9	10	02	01.5	24	01.7	03	01.3	01	02.0	.	.	17	02.1	01	01.0	01	01.0	44	.	.	.	.	.	.	.	.	.	.
VI	749.7	14.1	22.0	17.7	17.7	23.3	12.3	28.2	24	04.5	13	03	01.7	14	01.7	01</td																						

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine mm	Broj dana na sat																															
							Tn				Tx				Tz				F(0-12)		Nm(0-10)		R mm		•	*	•	Δ	•	▲	▲	R	T	≡	■			
	7	14	21	Sred. (Dnev.)			7	14	21	Stred.	Min	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV						
<b>SKRAD</b>																																						
<b>BR. ST.51</b>																																						
I	7.3	7.7	5.4	6.8	-	04.3	88	81	85	84	36	046	015.7	01	•	04	25	•	•	•	04	14	15	07	02	11	07	03	•	•	•	•	15	19				
II	6.5	8.2	5.2	8.3	-	05.1	85	81	82	83	44	118	046.4	07	•	•	10	•	•	•	01	01	20	17	10	04	14	04	•	•	•	•	01	11	05			
III	7.5	7.4	7.4	7.4	-	05.0	82	71	74	76	27	111	030.2	05	•	02	15	•	•	•	01	17	15	12	04	04	11	•	•	•	•	01	06	19				
IV	5.6	7.3	7.2	6.7	-	05.1	75	56	68	66	19	144	044.5	26	•	•	05	•	•	•	04	13	15	09	05	13	04	02	•	•	•	•	03	07	03			
V	5.5	7.1	7.6	6.7	-	07.7	79	62	77	73	37	214	069.9	01	•	•	•	•	•	•	01	13	22	17	07	22	•	•	•	•	05	05	•					
VI	5.5	6.8	6.2	6.2	-	09.0	74	61	77	71	30	237	046.7	30	•	•	01	•	•	•	03	10	19	13	08	19	•	•	•	•	04	03	•					
VII	4.5	5.3	3.7	3.5	3.9	-	10.6	73	60	69	67	29	111	062.6	26	•	•	11	•	•	•	09	02	09	07	02	05	•	•	•	•	05	05	•				
VIII	5.3	4.9	3.8	4.7	-	12.6	63	66	78	76	39	234	069.2	29	•	•	14	•	•	•	09	07	10	09	05	13	•	•	•	•	05	08	•					
IX	6.7	5.3	6.0	6.0	-	09.6	88	72	83	80	43	220	068.4	21	•	•	•	•	•	•	05	13	13	11	08	13	•	•	•	•	04	07	•					
X	8.1	7.6	6.9	7.5	-	05.7	93	80	92	89	46	439	067.5	21	•	•	15	•	•	•	01	15	24	21	17	24	10	08	01	•	•	•	C3	13	08			
XI	8.3	8.1	7.6	8.0	-	06.0	92	87	88	89	54	146	037.9	26	•	•	14	•	•	•	01	17	18	12	05	17	08	05	•	•	•	•	03	10	07			
XII	4.8	5.3	4.2	4.8	-	05.7	90	92	91	91	33	059	033.1	12	•	01	17	•	•	04	09	07	09	06	01	05	03	•	•	•	•	01	06	06				
GOD.	6.5	6.6	6.2	6.4	-	07.2	83	72	80	78	19	2081	069.2	27	Wm	•	07	101	26	•	06	•	47	148	186	134	70	165	47	18	01	•	•	•	41	96	67	
<b>BR. ST.52</b>																																						
<b>CGULIN</b>																																						
<b>BR. ST.52</b>																																						
I	7.9	7.7	6.8	7.5	-	050.0	04.5	95	81	93	90	32	062	020.2	01	•	01	25	•	•	02	02	17	14	07	02	14	08	06	•	•	01	•	14	09			
II	9.8	6.6	6.0	8.5	-	056.4	05.5	82	72	82	80	27	100	025.8	25	•	•	05	•	•	08	02	•	21	16	10	04	12	05	01	•	•	01	02	03			
III	7.5	7.1	7.0	7.2	-	114.5	05.6	88	62	80	77	30	115	029.8	05	•	•	07	•	•	04	02	01	12	13	11	04	02	10	03	•	•	02	01	14			
IV	6.3	7.6	6.5	6.8	-	154.6	05.6	84	52	68	66	29	080	016.2	14	•	•	•	•	•	06	04	16	14	11	02	14	04	07	•	•	01	•	01				
V	5.5	7.5	7.1	6.7	-	199.1	08.3	86	57	79	74	38	176	053.3	01	•	•	•	•	06	10	01	02	13	21	17	06	21	•	•	•	•	03	01	•			
VI	5.5	7.4	5.4	6.1	-	205.6	10.1	81	59	79	73	39	185	039.3	25	•	•	02	•	•	06	01	04	08	19	14	06	19	•	•	06	01	•					
VII	4.0	4.2	3.5	3.9	-	309.6	11.6	83	55	73	71	40	101	026.5	19	•	•	15	01	•	04	01	12	04	09	08	04	09	•	•	05	01	•					
VIII	5.0	5.4	3.6	4.7	-	227.6	13.8	92	63	89	81	32	270	069.4	26	•	•	16	04	•	•	09	08	11	11	08	11	•	•	•	•	08	01	•				
IX	5.7	6.2	5.5	5.8	-	167.0	10.9	94	49	91	85	40	267	067.4	21	•	•	05	•	•	06	09	15	12	06	15	•	•	•	•	05	05	•					
X	7.5	8.1	6.1	7.2	-	082.1	06.1	92	75	86	84	46	458	063.2	29	•	•	05	•	•	03	01	03	15	26	22	14	26	04	04	•	•	02	07	05			
XI	8.2	7.6	7.0	7.6	-	065.9	06.6	93	73	86	82	31	181	047.6	26	•	•	05	•	•	06	03	02	19	15	11	08	15	05	04	01	01	02	03	07			
XII	5.4	5.6	5.0	5.3	-	108.8	04.9	84	64	79	76	29	082	036.8	12	•	04	14	•	•	13	04	07	09	08	02	07	03	02	01	01	04	07					
GOD.	7.0	6.4	6.0	6.4	-	1741.2	07.7	87	65	82	78	27	2021	069.4	26	Wm	•	01	61	38	05	•	62	15	52	152	181	142	67	171	35	22	02	•	04	41	38	42
<b>KARLOVAC</b>																																						
<b>BR. ST.53</b>																																						
I	5.5	5.2	8.1	8.9	-	021.0	04.7	97	90	94	94	44	052	C11.0	02	•	01	17	•	•	•	01	23	16	08	02	16	03	C1	•	•	•	12	04				
II	8.2	8.6	6.2	7.5	-	061.3	03.0	90	70	84	81	28	045	010.8	25	•	•	03	•	•	01	15	12	09	01	12	03	03	•	•	01	02	01					
III	8.3	8.3	6.8	7.2	-	116.0	06.4	93	64	81	79	31	081	C21.0	06	•	02	02	•	•	03																	

Meseč vazdušni pratilac M E	Temperatura vazduha °C Tm 7 14 21 Sred. Sred. (Dana)	Čestina pravaca i srednja jačina veta m/s, fm (0-12)																																															
		N			NE			E			SE			S			SW			W			NW																										
		E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.																								
$\varphi = 45^{\circ}36'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$																																																	
I	- 01.1 02.8 01.6 01.8 04.5 -00.1 11.4 20 -05.2 15.14 06 01.2 12 01.7 C7 00.7 21 02.5 08 01.5 18 02.3 03 02.3 13 02.5 05	STUBIČKA GORA																							BR. ST.56																								
II	- 03.0 05.4 03.4 03.8 06.4 02.1 11.6 12 -04.4 20 . . 24 02.3 07 02.9 18 03.0 05 03.0 14 03.9 07 02.9 09 02.1 .																																																
III	- 04.5 06.1 05.3 05.9 08.4 03.6 21.6 22 -03.6 03.01 . . 25 02.3 14 01.7 28 02.1 01 02.0 14 03.3 03 02.0 05 02.6 03																																																
IV	06.7 10.6 07.1 07.9 11.4 04.5 17.8 10 -01.8 17 01 01.0 44 02.8 05 02.2 16 . . . 10 02.5 02 01.0 00 02.5 02																																																
V	- 11.2 14.8 10.9 12.0 15.6 08.0 21.4 20 04.8 15 03 01.0 21 02.1 04 02.2 12 02.7 03 03.0 08 03.2 07 02.1 31 02.4 04																																																
VI	- 13.6 17.8 13.5 14.6 18.8 10.5 23.8 26 05.2 11.10 05 C2.0 12 02.6 06 01.5 14 . . . 08 03.0 11 01.8 31 02.8 03																																																
VII	- 16.6 21.8 17.2 18.1 22.7 - 28.6 15 . . 07 01.3 16 02.4 06 01.8 14 02.9 04 02.5 12 03.2 14 02.3 19 02.4 01																																																
VIII	- 18.4 22.5 18.9 19.7 23.5 16.0 29.8 17 08.8 11 07 01.1 24 02.3 12 02.0 22 02.7 01 04.0 05 02.0 03 02.7 16 02.2 03																																																
GOD.	- 08.5 11.7 08.7 09.4 12.6 - 29.8 07.VM - 52 01.3 257 02.4 79 01.7 213 02.7 34 02.1 169 03.0 68 02.2 185 02.6 38																																																
$\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$																									ZAGREB-GRIC																								
																								BR. ST.57																									
I	753.2 01.1 03.2 02.3 02.2 03.8 00.6 14.8 20 -02.1 22 05 01.4 18 01.2 08 01.6 15 01.3 16 01.2 16 01.2 12 01.5 03 01.3 .																																																
II	745.3 05.4 09.1 07.2 07.4 09.6 04.8 14.9 11 00.0 28 06 02.5 25 02.0 10 01.9 02 01.0 10 01.3 11 02.6 17 02.2 03 02.0 .																																																
III	748.3 06.2 11.9 09.6 09.4 12.6 05.8 23.1 22 00.4 14 13 01.9 35 01.9 18 01.6 04 02.5 04 02.0 06 01.7 11 02.7 02 02.5 .																																																
IV	744.9 08.3 14.5 11.2 11.3 15.2 07.3 20.8 10 03.1 14 18 01.9 29 02.4 07 01.9 05 01.6 06 02.2 09 01.8 11 02.0 04 01.5 01 .																																																
V	745.0 12.7 18.6 14.3 15.0 19.4 11.1 25.6 22 07.3 10 14 01.6 16 01.7 C8 01.6 07 02.0 09 01.8 19 01.7 10 01.6 10 01.8 .																																																
VI	745.7 17.7 21.7 17.4 22.8 13.3 27.5 26 08.3 12 11 01.6 09 01.7 09 01.7 05 02.0 12 01.7 18 02.2 15 01.9 11 01.9 .																																																
VII	747.9 18.0 24.7 20.6 21.0 26.1 16.1 32.6 17 12.4 08 14 01.7 18 01.8 07 02.1 09 02.0 08 01.9 09 02.2 10 01.9 14 01.7 04 .																																																
VIII	748.2 18.9 25.9 21.8 22.1 26.8 17.3 33.2 11 04 11.3 13 15 C1.6 21 01.7 16 01.6 13 01.5 08 01.9 04 01.2 03 01.3 08 01.5 .																																																
IX	747.5 14.2 20.1 16.4 16.8 20.9 13.2 27.3 03 06.3 27 11 01.5 23 01.6 07 01.7 06 01.8 11 01.5 10 01.8 13 01.5 06 01.2 03 .																																																
X	744.2 06.0 09.8 07.4 07.3 10.6 05.1 15.1 20 01.0 30 11 01.5 18 01.7 09 01.3 03 01.7 09 01.8 19 01.6 18 01.4 06 01.3 .																																																
XI	748.8 05.4 09.5 07.2 07.3 10.0 04.8 18.9 16 -00.5 30 06 01.3 19 01.4 09 01.4 04 01.8 10 01.6 17 01.9 18 01.6 07 01.6 .																																																
XII	750.9 03.0 06.2 04.6 04.6 07.5 01.8 13.6 29 -03.8 15 09 01.8 13 01.5 11 01.3 07 01.1 08 01.2 11 01.8 23 01.7 11 02.0 .																																																
GOD.	- 07.9 15.3 09.2 10.4 16.2 04.6 34.4 04.VM -08.6 45.M 84 01.5 103 02.0 97 01.6 147 02.1 47 01.8 187 01.9 97 01.5 167 01.7 206																																																
$\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$																									ZAGREB-NAKSIMIR																								
																									BR. ST.59																								
I	756.4 00.2 02.8 01.3 01.4 03.5 -00.5 16.2 20 -04.9 22 09 01.4 13 01.3 14 01.4 15 01.1 18 01.2 04 01.0 08 01.4 03 01.0 .																																																
II	748.4 0																																																

Mjesec	Oblakost Nm (0-10)			Inzolacijs- noj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																									
	7	14	21		U m s			R mm			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■											
					mm	7	14	21	U	S	E	mm	Max	Dat.	≤	<	<	≥	≥	≥	≤	>	≥	≤	≥	Δ										
BR. ST.56	STUBIČKA GOMA																																			
I	8-3	7.7	5-7	7-2	-	04.3	86	63	80	83	52	054	021.4	02	•	07	17	•	•	•	03	17	07	06	01	06	01									
II	7.9	6.6	6-6	7-5	-	05.1	87	68	86	84	45	067	033.4	07	•	08	•	•	03	01	03	14	08	06	01	06	05	02								
III	6.7	6.6	5-9	6-5	-	05.3	79	69	75	74	34	049	016.3	06	•	04	12	•	02	01	04	13	07	07	02	03	06	01								
IV	5.8	7.2	5-4	6-1	-	05.2	68	57	66	64	30	045	013.5	26	•	02	•	•	05	11	10	08	02	09	02	•	•	01	01							
V	6.0	6.0	6-4	6-8	-	07.6	75	65	77	72	37	221	046.2	01	•	•	•	•	01	•	02	13	16	15	07	16	•	•	02	04						
VI	6.4	6.6	6-1	6-4	-	05.2	76	66	75	72	47	162	064.9	30	•	•	•	•	03	10	14	12	05	14	•	•	01	03	01							
VII	4.7	4.3	3-7	4-2	-	10.4	72	59	66	63	23	063	029.6	07	-	-	11	•	01	•	08	05	08	06	02	08	•	•	02	02						
VIII	3.8	5.2	3-4	4-1	-	13.0	78	78	76	75	49	171	045.1	28	•	•	14	•	06	12	06	10	10	05	10	•	•	04	09	•						
IX	5.6	6.1	4-2	5-3	-	10.4	84	77	84	82	49	169	039.8	21	•	•	•	02	•	08	09	12	10	06	12	•	•	01	11	•						
X	7.0	7.8	6-2	7-0	-	-	-	-	-	-	-	288	055.8	31	•	•	02	•	01	03	14	18	18	09	16	03	01	•	01	03						
XI	6.6	6.5	6-2	6-4	-	05.6	83	78	82	81	38	065	033.4	29	•	•	08	•	03	01	02	10	10	09	01	07	08	03	•	01	04	04				
XII	5.4	5.4	5-6	5-5	-	04.8	77	74	78	76	50	037	023.5	12	•	02	10	•	03	06	07	04	03	01	03	01	•	01	02	14						
GOD.	6-2	6-6	5-4	6-1	-	-	-	-	-	-	-	1392	064.9	30VI	-	13	-	25	•	-	16	03	59	129	124	110	42	110	26	09	•	•	01	13	73	62
BR. ST.57	ZAGREB-GRIC																									$H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$										
I	9.5	8.6	8-7	8-9	023.7	04-8	92	86	90	89	60	046	015.6	02	•	•	12	•	•	•	24	14	07	01	14	02	07	•	•	20	01					
II	7.8	7.0	7.0	7.5	066.5	05-5	79	64	73	72	31	034	014.0	07	•	•	•	•	04	•	02	15	10	08	01	10	03	02	•	•	01	02	08			
III	7.4	7.2	6-7	7-1	110.8	05-6	74	56	64	65	31	032	011.7	06	•	•	•	•	01	•	02	14	08	04	01	08	06	04	•	•	01	03				
IV	6.3	7.6	6-9	6-9	154.3	05-5	67	44	56	56	21	036	012.9	26	•	•	•	02	03	15	11	07	01	11	02	01	•	•	02	02						
V	5.9	7.7	7.2	6-9	181.0	08-5	77	54	73	68	33	189	041.5	01	•	•	02	•	02	•	03	12	18	13	06	18	•	•	•	07	•					
VI	6.4	6.6	6-1	6-3	179.6	10-4	77	54	69	67	34	127	050.5	30	•	•	08	•	01	•	02	09	18	10	04	16	•	•	04	•	04					
VII	4.5	4.8	4-6	4-6	274.8	11-7	73	51	64	63	36	052	018.4	07	•	•	19	05	01	01	09	08	06	03	08	•	•	01	07	04						
VIII	3.8	4.4	3-5	3-9	266.5	13-9	83	57	72	71	35	118	047.3	22	•	•	18	11	08	02	14	06	09	09	03	04	•	•	02	06						
IX	5.8	5.4	4-7	5-3	159.7	11-0	88	65	78	77	39	142	022.7	07	•	•	03	•	01	•	07	09	13	10	06	13	•	•	•	01	03	04				
X	7.7	7.6	6-5	7-3	074.9	06-5	90	74	83	83	37	224	034.5	21	•	•	•	•	03	15	22	16	07	22	•	•	•	02	07	07						
XI	8-1	7-0	7-6	7-5	081.4	05-9	84	68	79	77	28	062	029.0	29	•	•	02	•	02	•	14	11	07	01	11	01	01	•	•	01	13	02				
XII	7-2	7-2	6-2	6-9	076.6	04-9	84	72	78	78	39	022	010.3	12	•	01	10	•	04	•	03	13	10	04	01	09	04	•	01	•	14					
GOD.	6-7	6-8	6-3	6-6	1649.8	07-8	80	62	73	72	21	1084	050.5	30VI	-	01	24	50	16	08	19	01	48	152	152	101	35	151	18	10	01	02	03	32	69	04
BR. ST.58	TOPUSKO																									$H_s = 129 \text{ m } H_b = 2.0 \text{ m } h_t = 1.0 \text{ m}$										
I	9-1	6-0	6-7	8-9	-	05.0	97	97	97	97	82	053	016.7	02	•	01	25	•	•	01	26	10	08	02	09	01	•	•	•	20	01					
II	7-7	7-7	7-2	7-5	-	06.5	97	94	96	96	73	035	007.3	25	•	10	•	•	01	01	16	10	09	•	10	02	•	•	11	•						
III	8-1	7-7	7-2	7-9	-	07-9	97	91	95	95	61	067	018.5	06	•	10	01	•	01	19	11	10	03	09	C5	02	•	•	02	18	C3					
IV	7-4	7-9	6-9	7-4	-	08-6	97	91	94	94	74	047	012.4	26	•	10	•	•	01	02	17	14	12	01	14	01	•	•	02	10	•					
V	6-4	7-6	6-2	6-7	-	11.7	98	86	96	93	35	124	025.2	23	•	•	06	•	•	03	13	16	15	05	16	•	•	•	05	02						
VI	6-9	7-4	6-3	6-9	-	14.5	96	89	96	93	34	137	040.3	30	•	•	12	•	•	01	11	15	12	04	15	•	•	•	04	04						
VII	4-5	5-2	3-9	4-6	-	16.9	98	88	95	94	75	076	021.0	07	•	•	22	06	•	01	06	05	08	03	06	•	•	04	06	06						
VIII	H-2	6-5	4-4	6-4	-	18-6	97	92	96	95	57	157	037.4	24	•	•	20	11	•	•	02	10	12	10	06	12	•	•	05	20	•					
IX	8-1	6-7	6-2	7-0	-	13.5	99	92	97	96	79	125	055.0	30	•	•	09	01	•	01	11	11	10	05	11	•	•	02	18	01						
X	8-4	8-1	8-3	8-3	-	07-5	97	91	94	93	73	272	047.2	03	•	07	•	•	01	01	21	20	18	08	20	•	•	02	07	07						
XI	7-2	6-6	6-4	7-1	-	07-2	96	93	96	95	79	079	028.4	29	•	12	07	•	01	16	13	12	13	21	03	01	•	01	13	C7						
XII	8-5	6-7	7-6	7-6	-	06-0	97	94	96	96	83	040	013.8	12	•	03	17	•	•	01	16	06	06	01	05	02	•	•	01	12	01					
GOD.	6-9	7-0	5-9	6-6	1663-8	08-0	86	63	63	77	22	1091	052.9	30VI	-	03	54	51	17	•	04	-	45	144	145	102	41	144	12	08	•	03	04	42	55	05
BR. ST.59	ZAGREB-PAKSIMIR																									$H_s = 123 \text{ m } H_b = 127.6 \text{ m } h_t = 2.0 \text{ m } h_r = 2.0 \text{ m}$										
I	9-2	8-5	8-5	8-9	020.0	04-7	95	88	93	92	52	042	011.8	02	•	•	16	•	•	•	24	11	08	02	07	03	02	•	•	•	7C	02				
II	7-9	8-1	7-1	7-7	067.7	05-6	87	65	80	77	31	039	014.1	07	•	•	04	•	•	03	15	07	02	07	03	02	•	•	01	02	01					
III	7-6	7-9	6-4	7-1	125.0	05-7	83	57	74	71	27	029	010.7	06	•	•	04	•	•	03	14	07	04	01	06	04	03	•	•	03	01	01				
IV	6-1	7-2	6-5	6-6	163.5	05-7	75	45	67	62	22	035	012.8	26	•	•	04	•	•	03	12	07	01	12	07	02	•	•	•	01	01					
V	6-2	7-6	6-0	6-6	185.7																															

Mjesec	Vrstdinski pritisak Pm hPa	Temperatura vazduha °C										Cestine pravaca i srednja jačina vjetra ND, Pm (0-12)																	
		Tm			Sred. (Dnev.)	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.				
$\varphi = 45^{\circ}30'$ N $\lambda = 16^{\circ}22'$ E Gr. $\Delta G = +1h\ 06\ min.$																													
I	757.4	00.3	02.9	01.5	01.6	03.5	-00.7	13.3	20	-03.7	22	04	01.8	03	01.0	13	01.1	07	01.6	02	01.0	.	02	01.5	.	62			
II	749.6	04.1	09.9	06.5	06.7	10.7	02.3	16.7	12	-04.4	28	11	01.8	07	02.0	10	01.6	04	01.5	04	01.5	10	02.2	04	02.5	03	01.2	31	
III	752.6	04.0	12.3	08.1	08.1	13.0	02.7	23.4	21	-03.4	14	11	01.9	17	01.8	04	01.0	04	01.3	.	05	01.8	02	01.5	01	01.0	47		
IV	745.2	06.4	14.6	09.8	10.2	15.7	03.5	21.7	10	-01.1	20	10	02.8	12	02.7	11	01.3	03	01.5	01	02.0	03	02.0	02	02.0	43			
V	749.4	12.7	19.1	14.3	15.1	20.4	09.1	26.1	27	22	05.4	09	07	02.4	08	02.6	09	02.2	07	02.3	03	02.7	08	02.2	14	01.6	08	01.8	29
VI	749.9	16.0	21.9	17.0	17.9	23.3	11.3	26.6	26	05.4	12	09	02.3	11	03.0	04	01.5	03	02.0	02	03.0	10	02.5	17	01.9	03	03.7	31	
VII	752.0	18.0	25.3	19.9	20.8	26.5	13.5	33.7	17	08.4	28	04	02.5	08	02.4	07	02.1	09	01.9	03	02.3	05	02.8	10	01.8	04	01.8	43	
VIII	752.3	17.8	26.3	20.8	21.4	27.4	15.1	34.1	04	08.8	13	13	02.1	11	02.4	06	02.0	05	01.8	01	03.0	01	03.0	09	01.7	06	01.5	41	
IX	751.7	13.1	21.0	15.7	16.4	22.0	10.9	29.2	03	02.3	27	12	02.4	07	02.7	06	01.8	03	02.0	03	01.7	02	03.0	07	01.6	03	02.0	47	
X	748.5	06.4	10.8	08.0	08.3	11.7	04.6	17.9	20	-02.6	31	13	02.0	07	03.3	05	02.2	03	01.7	05	01.8	06	02.5	06	01.9	04	01.8	42	
XI	753.1	04.0	09.9	06.3	06.8	10.4	02.9	19.4	16	-04.8	29	06	02.8	05	02.6	10	01.2	09	01.3	01	02.0	05	02.4	03	02.3	03	01.7	48	
XII	755.4	01.4	06.3	02.9	03.3	07.3	-00.5	16.3	29	-04.6	24	04	01.8	03	02.3	11	01.2	03	01.3	01	01.0	04	01.0	06	01.5	.	61		
GOD.	751.8	08.8	15.0	10.9	11.4	16.0	06.2	34.1	04.VII	-04.8	29.VII	104	C2.2	99	02.4	96	01.5	61	01.7	26	02.0	62	02.2	85	01.8	37	01.9	525	
$\varphi = 45^{\circ}45'$ N $\lambda = 16^{\circ}38'$ E Gr. $\Delta G = +1h\ 06\ min.$																									CAZMA		BR. ST.61		
I	*	00.7	03.3	01.5	01.5	03.9	-00.5	12.4	20	-04.8	14	13	01.2	12	01.2	11	01.5	09	01.4	25	01.7	17	01.6	05	01.4	01	C1.0	*	
II	-	04.4	09.6	06.2	06.6	10.2	02.6	15.3	12	-03.4	28	14	01.6	22	02.2	08	02.4	02	01.0	03	01.7	04	01.2	*	*	*	*		
III	-	04.3	12.4	08.1	08.4	13.1	02.4	24.3	22	-03.0	14.01	15	01.8	38	02.0	12	01.8	02	02.0	04	01.8	09	02.4	04	01.8	*	*		
IV	-	07.0	15.0	09.3	10.2	15.9	03.2	21.4	29	-01.4	16	27	02.3	16	02.4	14	02.2	02	02.5	08	01.8	12	02.4	04	02.2	07	02.3	*	
V	-	11.7	18.7	13.6	14.4	19.8	08.2	26.8	20	03.5	10	20	02.1	09	02.2	08	02.6	05	02.2	18	02.7	20	02.4	07	02.1	06	02.0	*	
VI	-	15.5	22.4	16.6	17.8	23.2	11.2	29.7	28	04.8	13	19	01.9	09	02.4	06	02.0	03	02.0	05	02.4	26	02.8	10	02.2	12	02.0	*	
VII	-	17.6	25.3	18.6	20.0	26.2	13.0	33.6	17	08.8	27	21	02.1	10	01.1	08	02.1	03	02.0	16	01.8	19	07.4	10	01.6	06	02.2	*	
VIII	-	17.9	27.2	21.8	22.1	28.2	13.7	34.6	17	08.6	13	30	02.0	13	01.6	02	02.0	01	02.0	18	02.1	13	01.9	*	*	*	*		
IX	-	13.7	21.6	17.1	17.4	23.2	10.5	28.9	01	04.5	27	19	01.8	10	01.9	07	01.9	05	01.8	14	01.9	12	02.0	11	01.6	12	01.9	*	
X	-	05.8	10.9	08.8	08.6	11.9	02.8	16.6	25	-01.7	31	28	02.0	14	02.0	06	01.8	05	02.2	08	03.0	16	02.2	05	02.0	11	C1.0	*	
XI	-	05.0	10.1	07.6	07.6	11.6	02.7	19.1	16	-03.7	10	22	02.1	04	01.5	04	02.0	02	01.8	22	02.3	25	02.3	01	02.0	04	02.0	*	
XII	-	01.5	06.4	04.1	04.0	07.6	-00.9	14.8	29	-06.2	23	09	02.1	06	02.0	06	01.5	09	01.7	14	01.9	40	01.7	09	01.4	01	02.0	*	
GOD.	-	08.8	15.3	11.1	11.6	16.2	05.7	34.6	17.VIII	-06.2	23.XII	236	02.0	163	02.0	103	C1.9	55	01.8	155	02.1	222	02.2	80	01.9	81	01.4	*	
$\varphi = 45^{\circ}54'$ N $\lambda = 16^{\circ}51'$ E Gr. $\Delta G = +1h\ 07\ min.$																									BJELOVAR		BR. ST.62		
I	754.6	00.2	03.0	01.2	01.4	03.3	-01.2	13.0	20	-05.4	15	11	01.0	21	01.1	10	01.1	11	01.0	09	01.0	16	01.0	10	01.0	05	C1.0	*	
II	746.9	0.9	0.9	0.6	0.6	10.5	0.2	17.0	10	-02.5	28	10	02.1	21	01.5	18	01.1	03	01.0	03	01.0	25	02.1	02	01.0	02	02.0	*	
III	749.9	0.9	12.6	07.9	08.1	13.5	02.4	24.5	22.21	-04.5	01	07	02.6	33	01.3	22	01.3	13	01.3	03	01.0	12	01.2	03	02.0	*			
IV	746.6	06.7	15.1	08.9	09.9	15.7	03.0	22.5	28	-02.0	22.20	22	02.3	20	01.5	17	01.1	04	01.0	07	01.0	09	01.2	06	01.3	05	01.4	*	
V	746.6	11.9	18.7	13.0	14.2	19.6	08.2	25.6	20	02.0	10	06	01.2	10	01.6	11	01.3	03	01.0	09	01.0	23	01.3	13	01.2	18	C1.2	*	
VI	747.2	15.4	21.8	16.6	17.3	22.9	11.9	26.5	27	05.2	12	14	01.8	03	01.0	05	01.0	02	01.0	03	01.6	15	02.4	10	01.8	01	01.0	*	
VII	749.4	17.7	24.8	18.8	20.0	26.0	13.1	33.5	17	05.2	27	21	01.8	09	01.4	08	01.0	16	01.0	21	01.2	13	01.0	05	01.6	*			
VIII	749.7	16.3	26.8	20.1	21.4	27.8	14.7	33.5	17	07.4	13	10	01.3	33	01.2	10	01.0	14	01.1	01	01.0	08	01.0	04	01.0	13	01.2	*	
IX	749.2	13.0	21.2	14.7	15.9	21.8	10.4	26.0	03	03.3	28	03	01.3	24	01.5	12	01.0	07	01.0	05	01.2	14	01.4	11	01.1	13	01.0	01	

Meseč o.	Oblačnost Nm (0-10)			Insolacija broj sati mm	Vlažnost vazduha			Padavine R mm	Broj dana na sa:																						
	7	14	21		7	14	21		Sred. Min	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	▲	■	■		
					mm	mm	mm		mm	mm	mm	mm	≤	<	≤	>	≤	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV				
SISAK																															
<b>BR. ST.61</b>																															
I 5.5 6.8 7.4 8.6	-	016.0	04.8	95 89 94 93 65	050	016.1	07	-	-	17	-	-	-	-	-	-	20	17	10	02	13	07	01	-	04	-	14	01			
II 7.8 7.7 6.5 7.3	-	076.2	05.8	87 67 80 78 36	037	012.2	05	-	-	-	-	-	-	-	-	-	02	13	14	07	01	13	01	-	-	01	01	03	-		
III 7.9 7.6 6.5 7.3	-	146.0	06.1	91 60 78 76 28	044	015.7	07	-	-	06	-	-	-	-	-	-	03	17	10	05	02	09	06	02	-	01	03	-	01	02	
IV 6.2 6.0 5.6 6.6	-	157.8	06.3	84 50 70 78 27	034	012.1	26	-	-	05	-	-	-	-	-	-	03	12	12	10	01	11	01	-	-	-	02	03	-		
V 6.4 7.2 5.9 6.5	-	206.8	09.3	84 56 78 73 35	126	022.2	01	-	-	-	07	-	-	01	02	03	11	19	16	08	15	-	-	-	-	01	08	01	-		
VI 6.3 6.7 6.5 6.5	-	111.5	83 59 79 74 41	108	034.9	30	-	-	-	-	10	-	-	01	01	01	12	09	05	17	-	-	-	-	05	02	-	-			
VII 4.0 4.5 4.0 4.4	-	300.1	13.0	81 54 78 71 40	047	C19.7	07	-	-	-	-	21	09	-	-	-	11	06	11	06	01	10	-	-	-	-	03	01	-		
VIII 5.3 4.4 3.1 4.3	-	252.1	15.3	92 62 87 80 41	065	029.0	24	-	-	-	20	10	-	-	-	11	06	12	09	01	12	-	-	-	-	12	14	-			
GOD. 7.0 6.9 5.7 6.6	-	1770.5	08.5	88 65 83 79 27	948	048.1	20IX	-	-	02	58	68	3	-	07	04	47	153	174	116	35	159	17	03	-	01	07	02	46	65	06
ČAZMA																															
<b>BR. ST.62</b>																															
I 5.7 6.5 6.5 8.9	-	05.0	95 95 94 95 69	056	013.5	07	-	-	01	14	-	-	-	-	-	-	24	11	09	02	10	02	02	-	-	-	-	16	-		
II 7.5 7.9 6.6 7.3	-	06.9	93 90 91 91 61	041	016.8	07	-	-	03	-	-	-	-	-	-	-	03	17	09	07	01	09	01	01	-	-	01	04	-		
III 7.5 6.8 6.5 6.9	-	08.2	92 91 91 91 69	024	007.8	07	-	-	05	-	-	-	-	-	-	-	04	18	06	04	-	04	05	03	-	-	01	03	-		
IV 6.6 6.9 5.5 6.5	-	05.2	93 92 93 93 78	021	013.1	26	-	-	05	-	-	-	01	-	04	10	07	06	01	07	-	-	-	-	-	-	01	-			
V 6.4 6.7 6.5 6.7	-	12.1	93 92 93 93 73	149	036.8	01	-	-	02	-	-	-	-	-	-	-	04	12	17	13	05	17	-	-	-	01	06	-			
VI 7.0 7.3 7.1 7.1	-	15.2	94 94 94 94 85	114	045.2	30	-	-	11	-	-	-	-	-	-	-	02	12	14	11	03	14	-	-	-	01	01	-			
VII 3.8 4.3 5.3 4.4	-	17.4	92 92 93 93 77	068	023.8	07	-	-	21	08	-	-	-	-	-	-	10	04	08	07	03	08	-	-	-	02	02	-			
VIII 5.4 5.3 5.3 5.0	-	16.9	93 94 95 94 87	068	014.3	12	-	-	24	13	-	-	-	-	-	-	09	09	10	08	03	10	-	-	-	01	05	-			
IX 7.2 6.1 6.4 6.6	-	14.5	94 91 94 93 66	119	026.3	30	-	-	02	-	-	-	-	-	-	-	02	12	12	10	05	12	-	-	-	01	01	-			
X 8.0 8.3 7.7 8.0	-	07.9	93 92 94 93 76	222	C29.3	21	-	-	02	-	-	-	-	-	-	-	03	21	20	20	09	20	-	-	-	05	-	-			
XI 8.1 7.1 6.0 7.8	-	07.5	92 91 91 92 72	059	021.0	29	-	-	03	-	-	-	-	-	-	-	16	14	09	02	10	01	-	-	-	06	02	-			
XII 8.3 7.1 7.6 7.7	-	05.7	91 91 92 92 72	030	010.8	18	-	-	01	17	-	-	-	-	-	-	02	19	08	04	01	06	02	02	-	-	08	01	-		
GOD. 7.1 6.8 6.8 6.9	-	10.8	92 92 93 92 61	971	045.2	30VI	-	-	02	49	72	21	-	01	-	-	43	174	136	108	35	131	11	09	-	02	-	14	58	03	
BJELOVAR																															
<b>BR. ST.63</b>																															
I 8.8 8.8 8.4 8.7	-	04.8	55 65 56 53	056	015.8	07	-	-	01	19	-	-	-	-	-	-	01	24	12	09	02	12	03	02	-	-	01	14	-		
II 7.0 7.0 7.2 7.2	-	05.7	90 67 82 79	439	C12.2	07	-	-	03	-	-	-	-	-	-	-	01	02	14	09	09	01	05	02	02	-	-	01	03	01	
III 5.5 5.7 4.6 5.3	-	06.0	89 61 75 75	23	020	010.5	06	-	-	09	-	-	-	-	-	-	09	13	06	05	01	05	04	02	-	-	01	02	-		
IV 6.0 6.7 5.4 6.0	-	06.2	83 49 70 67	27	022	010.8	26	-	-	03	-	-	-	-	-	-	05	11	08	03	01	08	01	01	-	-	01	01	-		
V 6.6 7.3 5.7 6.5	-	05.3	86 59 84 77 37	183	052.0	01	-	-	03	-	-	-	-	-	-	-	03	11	17	13	06	17	-	-	01	06	01	-	-		
VI 6.2 6.3 5.4 6.0	-	11.2	83 60 80 74 44	142	056.0	30	-	-	09	-	-	-	-	-	-	-	01	07	13	09	05	13	-	-	05	02	-	-			
VII 4.0 4.2 3.7 4.0	-	12.6	78 56 77 71	41	074	029.4	07	-	-	18	06	-	-	-	-	-	12	07	10	07	03	10	-	-	02	02	-	-	04	01	
VIII 5.0 3.9 3.6 4.2	-	14.9	87 58 86 77 42	077	020.7	12	-	-	24	12	-	-	-	-	-	-	14	06	08	07	05	08	-	-	-	04	01	-			
IX 6.6 5.2 3.9 5.2	-	11.2	92 64 88 81 42	097	C26.6	21	-	-	09	-	-	-	-	-	-	-	07	07	10	09	04	16	-	-	-	02	06	-			
X 7.8 7.7 6.3 7.2	-	06.5	94 75 91 87 48	176	027.5	21	-	-	05	-	-	-	-	-	-	-	01	17	20	17	08	20	-	-	-	06	02	-			
XI 7.3 6.0 5.7 6.3	-	05.9	92 70 88 83 41	051	023.0	29	-	-	09	-	-	-	-	-	-	-	05	17	20	19	08	20	-	-	-	07	01	-			
XII 7.7 6.5 5.4 6.5	-	05.0	93 78 92 87 48	040	010.8	18	-	-	02	20	-	-	-																		

Mesec	Vrstdusni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																	
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21								c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.				
$\varphi = 45^{\circ}36'$ N $\lambda = 17^{\circ}14'$ E Gr. AG = + 1h 09 min.																									DARUVAR				
I	752.5	00.4	03.3	01.6	01.6	04.2	-06.3	13.0	31	-05.7	15	13	01.5	05	01.4	C7	01.1	03	02.0	08	C1.4	C3	01.0	06	01.3	20	C1.0	28	
II	745.7	04.1	05.9	06.1	06.5	10.9	02.9	16.0	12	-04.5	28	20	02.0	08	01.9	C6	01.2	06	01.5	17	C2.4	C8	02.2	04	02.2	02	C1.5	13	
III	748.6	03.6	12.5	07.6	07.8	13.5	02.7	25.0	22	-21	-05.4	01	18	02.1	16	01.8	C5	02.2	06	01.8	03	01.0	01	01.0	05	02.0	05	C1.2	34
IV	745.1	06.2	15.0	08.8	09.7	16.1	03.7	24.0	29	-01.4	20	18	01.9	13	01.8	C2	01.0	06	01.0	06	01.3	04	01.5	06	01.3	30			
V	745.3	12.2	16.7	12.6	14.1	19.9	09.1	26.6	30	03.5	09	12	01.6	10	01.6	C7	01.0	13	01.0	10	01.4	07	01.3	02	02.0	11	C1.4	21	
VI	745.8	15.4	22.0	16.1	17.4	23.2	11.8	25.0	27	05.0	12	19	02.1	05	01.4	C5	01.4	05	01.0	08	01.4	10	01.7	C7	01.4	09	C1.3	17	
VII	746.0	18.2	25.3	19.0	20.4	26.7	13.8	35.4	27	09.2	16	C1.6	07	01.4	08	01.0	14	01.1	11	01.3	05	01.4	07	01.1	09	C1.4	16		
VIII	746.2	18.0	27.1	19.6	21.1	28.0	15.0	34.5	04	08.7	13	13	01.3	19	01.5	C4	01.2	07	01.3	06	01.0	04	01.2	02	01.5	05	C1.2	33	
IX	747.7	13.0	21.0	14.8	16.1	23.0	11.0	30.6	03	06.6	27	20	01.6	08	01.5	C3	01.0	06	01.0	06	01.2	05	C1.4	03	01.0	08	C1.2	31	
X	744.6	05.3	10.7	07.0	07.5	11.9	04.1	17.6	04	-01.6	31	15	C1.5	C9	01.1	C2	01.0	06	01.2	18	C1.6	07	01.3	04	01.2	07	C1.3	25	
XI	745.4	04.4	10.2	05.5	06.4	11.1	03.1	15.6	10	14	01.6	04	01.2	C3	01.0	13	01.0	16	01.4	07	01.4	08	01.1	04	C1.5	21			
XII	751.4	03.8	07.2	03.9	04.5	06.2	01.3	16.6	29	-04.4	24	16	01.5	C4	01.0	18	01.1	12	01.2	09	01.1	04	01.0	06	C1.0	20			
GOD.	747.8	08.6	15.3	10.2	11.1	16.4	06.5	35.2	47V	-05.7	15.1	194	C1.7	108	01.5	56	01.2	106	01.5	72	01.4	56	01.4	92	C1.2	289			
$\varphi = 45^{\circ}44'$ N $\lambda = 17^{\circ}38'$ E Gr. AG = + 1h 11 min.																									DONJI MELJANI				
																										BR. ST.67			
I	-	CG.5	C3.3	01.6	01.6	04.7	-06.9	11.3	21	-07.0	29	07	01.6	07	01.1	25	C1.4	18	01.3	09	01.0	05	01.6	10	01.5	12	C1.8	.	
II	-	04.7	06.6	06.7	11.1	02.1	16.8	12.11	-02.8	28	10	C1.7	C3	01.3	14	01.6	C5	01.4	05	01.2	05	01.4	24	01.4	12	01.8	11	C1.5	.
III	-	03.9	12.0	08.3	08.1	13.5	02.4	24.2	21	-04.4	01	10	02.3	05	01.8	23	02.0	24	C1.5	08	01.0	13	01.0	12	01.2	04	C1.2	01	
IV	-	06.5	14.9	10.2	10.4	16.5	04.0	24.8	26	-02.2	04	07	C2.1	C6	02.2	C5	01.0	12	C1.2	07	01.1	23	01.2	14	01.2	16	C1.6	.	
V	-	13.1	16.7	14.2	15.0	20.4	05.5	27.4	21	05.0	09	10	01.9	04	01.8	C4	01.2	07	01.3	06	01.2	21	C1.4	23	01.5	18	C1.7	.	
VI	-	21.9	17.1	16.1	23.9	11.7	3.2	27	07.4	08	C9	C1.8	03	01.3	06	C1.0	06	01.0	03	01.3	16	01.4	19	C1.7	27	04.0	01		
VII	-	19.2	25.4	20.2	21.2	27.2	13.5	34.5	14	08.2	27	08	01.9	06	01.7	11	01.1	09	01.7	02	01.0	32	01.1	11	01.5	21	C1.7	.	
VIII	-	26.6	20.8	22.1	29.0	14.9	35.8	04	09.0	08	16	01.6	04	01.0	14	C1.3	C6	01.2	06	01.0	20	01.0	14	01.4	13	C1.5	.		
IX	-	14.6	21.5	16.3	17.2	23.5	10.5	31.2	03	01.2	14	C9	01.7	10	01.2	14	01.1	09	01.3	07	01.3	15	01.0	11	01.1	15	C1.7	.	
X	-	06.1	11.1	07.3	08.0	12.9	03.6	17.5	19	-06.5	31	06	C1.7	C5	01.0	05	C1.2	05	01.4	12	01.2	23	01.4	18	01.4	15	C1.3	.	
XI	-	05.9	10.2	07.0	07.0	12.3	02.8	22.4	16	-02.0	28	07	06	02.0	04	01.5	C5	01.2	22	01.4	06	01.0	33	01.3	07	01.4	07	C1.6	.
XII	-	03.4	07.0	04.2	04.7	09.1	01.1	19.3	29	-04.2	25	C6	C1.8	05	01.0	07	C1.4	09	01.3	02	01.0	37	01.5	14	01.4	13	C1.9	.	
GOD.	-	09.3	15.2	11.2	11.7	17.0	06.3	35.8	04V	-07.0	29.1	97	01.8	64	01.4	133	01.4	136	01.3	74	01.1	252	01.3	165	01.4	172	C1.7	02	
$\varphi = 45^{\circ}20'$ N $\lambda = 17^{\circ}41'$ E Gr. AG = + 1h 11 min.																									SLAVONSKA PEŽEGA				
																										BR. ST.68			
I	-	06.2	04.0	C2.5	02.3	04.7	-00.6	11.1	20	-04.5	15	21	C1.2	14	01.1	21	01.2	C7	01.0	01	01.0	06	01.0	08	01.2	15	C1.1	.	
II	-	02.0	10.1	06.3	06.2	11.1	00.5	17.0	12	-04.3	29	12	C1.3	11	01.8	C7	01.3	C6	01.3	05	01.2	09	C1.4	17	01.7	17	C1.1	.	
III	-	02.9	12.0	07.9	07.9	13.6	01.7	24.5	22	-04.5	01	10	01.2	12	01.7	18	C1.4	C3	01.7	06	01.5	08	02.0	23	01.2	17	C1.2	.	
IV	-	06.2	09.7	10.2	10.2	16.0	03.2	23.5	29	-01.9	04	22	01.6	09	01.4	10	01.5	04	01.7	07	01.3	16	01.3	13	01.2	10	C1.5	.	
V	-	11.7	19.4	14.3	14.9	20.2	08.4	26.5	31	02.8	10	13	C1.4	11	01.6	C6	01.2	03	01.3	12	01.1	14	01.2	25	C1.3	10	C1.3	.	
VI	-	15.4	21.1	16.8	17.8	23.1	11.0	25.6	27	05.9	13	25	C1.5	C9	01.0	05	C1.0	03	01.3	17	01.4	22	01.1	10	C1.3	.			
VII	-	17.3	25.3	19.6	20.4	26.3	12.3	34.0	17	06.1	27	11	C1.5	10	01.2	10	01.3	05	01.0	06	01.5	15	01.5	24	01.2	12	C1.2	.	
VIII	-	17.9	27.3	21.1	21.6	28.1	14.1	34.1	04	09.0	10	17	C1.2	C8	02.1	C3	01.7	17	01.8	09	01.4	18	01.1	10	C1.7	11	C1.7	.	
IX	-	12.7																											

Meseč	Oblačnost Nm (0-10)				Vlažnost vazduha				Padavine mm				Broj dana na sa:																						
													Tn	Tx	In	Tx	In	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	□	■	☒				
	7	14	21	Sred. (Dnes)	Insolacije broj sati	mm	7	14	21	Sred. Min	Σ	Max	Dat.	V	<	<	V	V	V	V	V	<	>	N	N	N	•	Δ	*	Δ	○	▲	▲	□	■
<b>CARUVAR</b>																																			
BR. ST.66																												$H_s = 161 \text{ m } H_b = 162.1 \text{ m } h_t = 2.0 \text{ m } h_r = 2.0 \text{ m }$							
I 6.5 8.7 6.5 7.9	034.1	04.8	96	86	94	92	51	076	014.7	07	.	01	17	.	.	.	.	01	17	11	09	03	11	.	.	.	01	.	.	13	.				
II 6.7 7.6 6.3 6.8	091.4	05.6	88	62	81	77	32	020	004.7	07	.	04	.	.	.	01	.	02	11	09	07	05	02	01	.	.	.	01	.	.	02	.			
III 5.7 6.5 5.3 5.6	127.8	05.8	92	57	78	75	26	020	006.4	05	.	07	02	.	.	.	.	05	13	07	05	06	04	01	.	.	.	01	.	.	01	.			
IV 5.7 6.4 5.2 5.8	143.5	06.0	67	42	73	68	23	019	004.7	26	.	03	.	.	.	.	06	11	12	05	12	.	.	.	.	.	.	.	.	.	.				
V 6.6 6.8 5.2 6.2	169.9	09.1	55	86	75	73	31	116	014.0	23	.	.	05	.	.	.	01	01	03	12	22	17	04	22	.	.	.	.	.	.	.	05	01		
VI 5.7 6.8 6.4 6.3	192.9	10.8	82	53	82	72	34	144	053.0	30	.	.	10	.	.	.	03	09	16	05	18	.	.	.	.	.	.	.	.	08	.				
VII 4.2 4.5 3.8 4.2	278.4	12.5	78	50	80	69	32	059	017.6	07	.	.	21	04	01	.	13	07	11	09	03	11	.	.	.	.	.	.	.	05	.				
VIII 3.9 4.2 2.8 3.6	233.4	14.4	89	54	88	77	35	060	019.9	12	.	.	27	13	.	01	13	04	11	08	02	11	.	.	.	.	.	.	.	06	.				
IX 5.1 5.7 4.7 5.2	171.5	10.8	91	57	88	79	32	097	024.2	30	.	.	12	01	.	.	07	07	10	09	05	10	.	.	.	.	.	.	.	01	01				
X 7.5 7.8 7.2 7.5	079.3	06.4	91	69	87	82	40	230	050.5	06	.	02	.	.	.	02	16	23	19	08	25	.	.	.	.	.	.	.	01	01					
XI 7.0 6.8 5.4 6.6	075.5	05.7	88	65	86	80	35	061	023.7	29	.	06	.	.	.	03	11	14	08	02	14	01	01	.	.	.	.	.	.	07	.				
XII 7.6 6.2 5.7 6.5	077.2	04.9	86	68	82	78	33	052	011.1	12	.	11	.	.	.	04	10	14	10	02	12	03	01	.	.	.	.	.	.	05	.				
GOD. 6.6 6.5 5.4 6.0	1705.9	08.1	87	59	83	77	23	949	053.0	3061	.	01	50	73	23	01	04	01	62	128	162	115	34	159	10	04	.	.	01	.	25	30			
<b>CGNJI MELJANI</b>																											$H_s = 120 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m }$								
BR. ST.67																																			
I 9.2 8.3 7.8 8.4	-	04.8	89	93	86	89	47	059	014.2	07	.	02	.	.	.	.	02	22	12	10	03	14	01	.	.	.	.	.	.	21	.				
II 7.6 7.6 6.8 7.3	-	06.7	91	86	89	89	66	020	008.5	07	.	02	.	.	.	.	01	14	09	06	01	01	.	.	.	.	.	.	07	.					
III 4.8 4.8 5.1 4.9	-	07.9	62	88	91	96	53	023	008.8	08	.	08	.	.	.	.	10	08	05	05	04	03	.	.	.	.	.	.	07	.					
IV 6.4 6.6 6.2 6.3 6.3	-	08.3	89	80	86	85	40	013	004.7	26	.	03	.	.	.	.	05	13	06	05	06	.	.	.	.	.	.	.	.	.					
V 6.8 7.5 5.3 6.5	-	10.3	83	73	80	79	40	122	040.2	01	.	.	05	.	.	.	02	12	15	14	04	15	.	.	.	.	.	.	.	.	.				
VI 5.8 6.4 4.8 5.7	-	11.8	83	60	82	75	31	173	070.5	30	.	.	13	01	.	.	05	07	12	10	05	12	.	.	.	.	.	.	.	03	.				
VII 4.4 4.4 3.6 4.0	-	13.6	78	61	73	70	20	075	042.0	07	.	.	19	01	.	.	11	06	09	09	01	05	.	.	.	.	.	.	.	04	.				
VIII 4.5 3.8 3.2 3.8	-	15.2	83	64	73	74	40	144	040.5	27	.	.	26	13	.	.	15	05	11	11	04	11	.	.	.	.	.	.	.	02	02				
IX 6.5 8.5 4.7 5.7	-	11.7	89	65	75	78	21	075	016.4	27	.	.	13	01	.	.	04	11	08	08	04	08	.	.	.	.	.	.	.	01	02				
X 6.3 8.1 6.5 7.6	-	06.8	90	79	80	83	26	218	038.5	05	.	01	.	.	.	02	16	21	15	09	21	.	.	.	.	.	.	.	04	.					
XI 7.7 5.7 5.0 5.8	-	05.5	86	74	75	78	42	061	021.4	26	.	05	.	.	.	.	6.4	10	08	07	02	06	01	.	.	.	.	.	.	13	01				
XII 8.5 7.3 5.6 7.2	-	05.5	86	81	94	84	44	077	027.4	18	.	12	.	.	.	.	01	15	12	11	02	11	05	04	02	.	.	.	07	01					
GOD. 6.6 6.6 5.4 5.6	-	09.0	86	74	81	81	20	107C	070.5	3031	.	01	49	76	25	.	01	.	61	134	128	113	34	126	12	08	02	.	.	.	04	62	02		
<b>SLAVASKA POZEGA</b>																											$H_s = 152 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m }$								
BR. ST.68																																			
I 8.4 7.8 6.5 7.6	-	05.0	93	87	93	91	60	064	017.6	07	.	17	.	.	.	.	01	17	12	09	03	11	02	.	.	.	.	.	.	17	01				
II 6.0 6.4 3.5 5.3	-	05.9	93	69	88	84	40	C24	005.€	14	.	11	.	.	.	.	04	05	09	07	05	01	01	.	.	.	.	.	.	04	.				
III 6.6 6.5 4.1 5.6	-	06.5	90	65	86	81	31	027	009.8	06	.	09	.	.	.	.	05	08	07	06	05	04	01	.	.	.	.	.	.	01	.				
IV 6.0 7.0 6.0 4.8	-	07.2	89	56	87	77	33	018	006.4	26	.	04	.	.	.	.	05	09	11	06	01	01	01	.	.	.	.	.	.	01	.				
V 6.3 6.8 4.5 5.9	-	10.1	89	63	85	79	45	069	010.2	12	.	08	.	08	.	.	01	06	20	12	01	20	.	.	.	.	.	.	11	01					
VI 5.4 6.0 5.1 5.5	-	12.2	86	65	85	79	48	136	038.6	11	.	10	.	08	.	.	01	03	03	18	11	05	18	.	.	.	.	.	.	07	.				
VII 3.4 4.4 3.1 3.6	-	13.9	87	60	85	77	44	053	013.3	19	.	21	09	.	.	.	14	06	10	07	03	16	.	.	.	.	.	.	02	.					
VIII 3.3 4.0 2.7 3.3	-	15.3	86	61	86	78	40	094	027.0	28	.	24	13	.	.	.	13	03	11	11	04	11	.	.	.	.	.	.	09	01					
IX 5.7 5.9 4.2 5.3	-	12.3	52	65	88	83	46	097	019.1	27	.	10	.	.	.	.	04	06	09	07	05	09	.	.	.	.	.	.	02	03					
X 7.3 7.5 5.6 6.8	-	06.9	76	71	87	84	44	208	034.1	06	.	05	.	.	.	.	04	11	19	15	08	19	.	.	.	.	.	.	01	06					
XI 7.1 6.3 5.1 6.7	-	06.1	92	73	89	85	45	047	018.6	26	.	13	.	.	.	.	03	11	12	09	01	12	.	.	.	.	.	.	12	.					
XII 6.6 6.9 6.0 6.6	-	05.4	92	80	90	87	49	032	007.0	12	.	13	.	.	.	.	02	08	13	10	•	13	01	01	.	.	.	.	.	07					
GOD. 6.6 6.6 4.6 5.6	-	08.9	90	68	87	82	31	865	038.6	41	.	72	65	22	.	04	.	59	93	151	110	30	148	09	03	.	.	.	.	32	52	01			
<b>SLAVSKI BROD</b>																											$H_s = 89.0 \text{ m } H_b = 2.1 \text{ m } h_t = 1.2 \text{ m }$								
BR. ST.69																																			
I 9.6 8.6 7.6 8.6	-	033.9	04.5	98	50	97	95	61	061	018.5	20	.	01	19	.	.	.	02	01	01	22	15	10	03	15	02	01	.	.	26	.				
II 7.2 7.4 5.8 6.8	-	097.4																																	

Mjesec	Vrijednost Prstensk Broj	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra nD, fm (0-12)																												
		Tm			Max.			Min.			Dat.			N			NE			E			SE			S			SW			W			NW			C		
		7	14	21	Sred. Dnev.	Max.	Min.	Max.	Min.	Max.	Dat.	Min.	Dat.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.			
$\varphi = 45^{\circ}17'$ N $\lambda = 18^{\circ}25'$ E Gr. $\Delta G = + 1h\ 14\ min.$																															LJAKOVO		BR. ST. 71							
I	-	00.0	03.0	01.4	01.4	03.6	-01.0	05.6	22	-06.6	15	14	01.5	6	01.3	C6	01.3	C6	01.1	6	01.0	16	01.3	C7	01.4	35	C1.5	.	.	.	.	.	.	.						
II	-	02.2	05.8	05.8	05.8	10.7	01.3	16.8	12	-02.5	28	01	18	01.7	6	01.7	C8	02.1	6	01.6	09	01.3	10	01.3	C5	01.8	17	C1.3	.	.	.	.	.	.	.					
III	-	05.8	13.0	07.6	08.0	13.4	02.3	15.0	22	-21	-02.6	02	37	01.6	6	01.8	C4	02.6	6	02.2	.	11	01.4	02	01.0	16	C1.4	.	.	.	.	.	.	.						
IV	-	11.7	15.1	09.5	10.4	15.9	03.8	25.0	20	-01.0	04	32	C1.8	6	02.4	C4	03.0	07	01.3	08	02.1	08	02.0	23	C1.9	.	.	.	.	.	.	.								
V	-	17.7	18.8	13.2	14.5	19.7	08.9	26.4	31	03.6	10	17	01.6	6	07.8	C1	02.0	6	01.2	09	01.3	16	01.8	15	02.3	27	C2.0	.	.	.	.	.	.	.						
VI	-	16.4	21.3	16.6	17.7	24.9	12.4	30.6	27	07.2	13	08	01.8	6	01.0	C3	01.7	6	01.5	04	01.8	14	01.7	17	02.3	37	C2.2	.	.	.	.	.	.	.						
VII	-	14.2	24.8	18.7	20.1	26.2	13.4	34.4	14	05.5	27	08	02.2	6	01.7	C1	01.0	18	01.4	04	01.8	12	01.8	11	02.4	33	C2.0	.	.	.	.	.	.	.						
VIII	-	18.9	27.2	19.9	21.4	28.0	15.5	33.5	04	10.5	10	09	01.9	6	01.6	09	02.0	14	01.9	06	01.5	03	01.3	09	01.4	34	C1.6	.	.	.	.	.	.	.						
IX	-	13.9	27.1	15.3	16.6	22.8	11.6	30.8	03	02.8	28	16	01.4	6	01.6	.	09	01.6	12	01.2	06	01.3	C5	02.0	31	C1.7	.	.	.	.	.	.	.							
X	-	05.4	11.0	07.2	07.4	12.0	03.7	18.0	04	-01.0	31	11	01.5	6	02.5	C2	01.3	11	02.0	04	02.0	08	02.0	09	02.2	45	C1.7	.	.	.	.	.	.	.						
XI	-	02.5	09.7	04.5	05.3	10.2	01.3	19.6	16	-02.8	10	07	02.3	11	01.8	C1	02.0	22	01.4	10	01.5	03	02.0	05	02.0	31	C1.6	.	.	.	.	.	.	.						
XII	-	01.8	06.0	02.8	03.4	07.0	06.2	16.4	29	-04.6	23	04	C2.5	6	02.3	02	02.0	20	01.4	04	02.0	30	01.6	07	01.9	23	C2.1	.	.	.	.	.	.	.						
GOD.	-	08.6	19.2	10.2	11.0	16.0	06.1	34.4	Fm	-06.6	15	181	01.7	6	01.8	45	02.1	141	01.6	6	01.4	137	C1.6	100	02.0	347	C1.8	03	.	.	.	.	.	.						
$\varphi = 45^{\circ}42'$ N $\lambda = 18^{\circ}44'$ E Gr. $\Delta G = + 1h\ 16\ min.$																																BREŠTOVAC-BELJE		BR. ST. 72						
I	760.0	00.0	03.5	01.4	01.6	04.1	-01.1	05.8	20	-06.6	15	03	03.7	6	01.6	23	C1.8	12	01.8	08	01.5	02	01.5	14	01.4	12	C2.1	.	.	.	.	.	.	.						
II	750.7	01.6	10.1	04.7	05.3	10.6	03.7	17.0	12	-03.0	28	22	06	C1.5	12	01.7	16	01.6	05	01.6	17	01.5	16	01.6	07	01.4	05	C1.4	.	.	.	.	.	.	.					
III	754.6	01.4	13.3	07.5	07.9	11	02.1	25.5	21	-04.0	03	02	04	C1.5	12	01.4	24	02.0	25	02.4	01	01.0	07	01.9	04	02.8	06	C1.3	.	.	.	.	.	.	.					
IV	752.1	07.1	15.2	09.9	10.5	15.5	04.1	24.5	28	-01.1	04	12	03.0	21	02.1	13	02.2	11	02.5	05	01.8	04	02.0	12	C1.7	11	C2.1	.	.	.	.	.	.	.						
V	751.4	12.5	19.9	13.4	14.6	20.0	09.2	28.0	31	04.0	10	10	C2.6	6	02.0	05	01.8	05	02.4	09	01.6	08	01.9	23	C1.7	30	C2.6	.	.	.	.	.	.	.						
VI	752.3	16.0	21.4	16.4	17.6	22.6	12.4	30.0	27	06.9	08	14	C2.9	6	01.8	C5	01.6	05	02.4	05	01.8	10	01.5	16	01.6	30	C2.4	.	.	.	.	.	.	.						
VII	754.4	17.9	24.8	18.7	20.0	25.5	13.7	33.9	14	05.6	09	16	C2.8	6	01.2	05	C1.4	10	01.8	09	02.0	03	02.3	16	01.6	30	C2.0	.	.	.	.	.	.	.						
VIII	754.8	18.8	27.0	20.1	21.5	27.0	15.0	34.0	03	10.1	07	08	01.8	23	01.7	18	01.9	05	02.0	07	01.9	08	01.2	10	01.1	14	C2.7	.	.	.	.	.	.	.						
IX	754.4	13.4	21.0	15.3	16.4	22.5	11.3	29.8	03	02.4	28	14	02.5	20	01.8	08	01.6	08	02.1	09	01.6	03	01.0	14	C1.9	14	C2.0	.	.	.	.	.	.	.						
X	751.6	05.7	11.0	06.7	07.4	11.6	03.8	17.5	12	-01.5	31	16	C2.3	7	02.0	08	01.8	12	01.6	12	01.9	11	C1.9	11	C2.0	.	.	.	.	.	.	.								
XI	752.1	05.5	09.7	04.5	05.4	10.1	01.5	17.6	16	-02.9	10	09	02.7	11	01.9	10	01.4	10	01.3	19	01.8	12	01.8	11	02.2	.	.	.	.	.	.	.								
XII	752.6	01.6	15.5	02.4	03.0	06.2	00.6	13.5	04	-04.3	23	09	C2.8	6	05.0	02.0	09	01.7	05	01.6	15	01.5	10	01.6	27	C1.4	3	.	.	.	.	.	.							
GOD.	754.5	06.3	18.4	10.1	10.9	16.0	06.1	34.0	Fm	-06.6	15	121	C2.6	132	01.8	164	01.8	109	02.0	116	C1.7	95	C1.7	173	C1.7	185	C2.7	.	.	.	.	.	.	.						
$\varphi = 45^{\circ}42'$ N $\lambda = 18^{\circ}44'$ E Gr. $\Delta G = + 1h\ 15\ min.$																																LJOK		BR. ST. 71						
I	-	00.7	04.1	02.6	02.5	05.8	-00.7	11.8	04	-08.0	15	01	01.0	02	02.5	C6	01.5	29	01.7	04	01.8	.	.	.	22	02.0	04	C1.8	25	.	.	.	.	.	.	.				
II	-	04.1	10.1	04.1	06.6	11.0	02.9	16.1	18	-03.5	28	.	6	01.8	C3	02.3	27	01.9	12	01.8	07	01.7	14	01.8	02	01.5	14	.	.	.	.	.	.	.						
III	-	05.5	13.1	07.4	08.4	13.7	04.0	26.6	19	-02.0	14	.	6	01.6	04	02.7	04	02.0	06	02.0	12	01.8	02	01.5	11	.	.	.	.	.	.	.								
IV	-	07.5	14.7	09.0	10.1	15.7	05.3	23.9	28	00.0	06	01	01.0	6	01.6	02	02.0	07	02.6	03	02.2	05	01.8	15</td																

Mjesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																							
	e <sub>m</sub>	7	14	21		7	14	21	Stred. Sred. (Ukupno)			Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
	7	14	21	Sred. (Ukupno)	mm	7	14	21	Stred. Sred. Min	Σ	Max	Dat.	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<				
<b>BR. ST.71</b>																																			
<b>DJAKOVAC</b>																																			
I	8.7	8.1	7.5	8.1	-	04.5	87	86	90	89	70	061	C12.0	20	.	.	19	.	.	.	.	.	16	13	09	02	12	03	.	.	.	19	.		
II	7.6	6.2	5.5	6.4	-	06.1	84	80	88	84	47	025	006.6	05	.	.	09	.	.	.	.	.	01	06	10	07	.	09	01	.	.	06	.		
III	5.7	6.0	5.7	5.8	-	06.4	84	64	85	78	17	020	005.5	07	.	.	07	02	.	.	.	.	09	08	05	.	04	06	.	.	03	.			
IV	5.6	6.4	6.4	6.4	-	07.0	75	56	91	71	27	020	010.6	18	.	.	02	01	.	.	.	01	01	08	01	10	02	01	01	.	01	.			
V	6.0	6.5	5.5	6.0	-	09.5	82	61	83	75	40	082	C16.0	01	.	.	03	.	.	01	.	.	04	17	13	03	17	.	.	.	08	.			
VI	5.6	6.7	6.7	5.3	-	11.6	79	62	84	75	45	114	044.8	11	.	.	04	01	.	.	.	.	09	14	11	04	14	.	.	.	05	.			
VII	5.6	5.2	5.6	5.0	-	13.3	79	59	85	74	42	054	C09.6	20	.	.	21	08	.	.	.	.	04	06	12	09	.	12	.	.	02	.			
VIII	5.9	4.6	4.6	4.4	-	15.0	86	59	95	76	43	084	C28.0	26	.	.	24	12	.	.	.	02	02	04	07	04	05	.	.	07	01				
IX	6.7	5.7	4.8	5.7	-	11.9	84	69	88	81	46	060	C24.6	05	.	.	10	01	.	.	.	.	08	08	05	02	08	.	.	.	C1	05			
X	6.1	7.4	7.2	7.6	-	06.8	85	79	86	84	49	155	029.8	29	.	.	02	.	.	.	.	.	15	19	14	05	15	.	.	.	10	.			
XI	7.2	6.6	5.6	6.5	-	05.7	84	77	86	82	53	056	C18.0	29	.	.	07	.	.	.	.	10	13	11	02	13	01	.	.	.	10	.			
XII	7.2	7.2	7.0	7.1	-	04.9	83	76	85	82	26	050	006.9	12	.	01	16	.	.	.	.	11	16	11	.	14	02	.	.	.	07	G2			
God.	6.4	6.4	6.0	6.3	-	06.6	82	49	85	79	17	789	C44.8	44VI	.	01	62	70	22	.	05	.	08	104	149	11C	23	143	15	01	01	.	24	61	02
<b>BRESTOVAC-BELJE</b>																																			
BR. ST.72													H <sub>a</sub> = 91 m H <sub>b</sub> = 92.3 m h <sub>i</sub> = 2.0 m h <sub>r</sub> = 1.0 m																						
I	9.1	8.0	7.5	8.2	041.0	04.6	93	83	91	89	62	034	C14.3	20	.	.	22	.	.	.	.	01	21	11	05	01	1C	03	01	01	.	19	01		
II	6.7	6.6	4.1	5.8	079.4	06.2	92	60	93	90	52	018	C06.0	24	.	.	13	.	.	.	.	06	07	09	04	.	06	01	.	.	.	07	.		
III	5.5	5.9	4.9	5.3	151.3	05.8	88	63	77	76	21	029	C09.0	06	.	.	09	01	.	.	.	09	11	06	07	.	05	05	.	.	08	01			
IV	6.1	7.0	6.0	6.3	155.0	06.0	77	47	67	64	27	025	005.7	18	.	.	02	.	.	.	.	06	14	12	06	.	12	.	.	.	01	C2	01		
V	6.5	7.5	6.6	6.8	169.5	09.4	84	55	82	75	37	072	C17.5	23	.	.	04	.	.	.	.	01	13	21	12	02	21	.	.	.	06	02	.		
VI	5.5	7.6	7.6	7.6	180.1	11.7	94	63	76	74	44	197	C07.3	30	.	.	10	01	.	.	.	01	10	15	13	05	15	.	.	.	1C	01	.		
VII	4.4	4.7	6.0	5.1	245.8	12.8	81	53	82	72	37	055	C19.0	22	.	.	17	05	.	.	.	07	07	08	06	02	06	.	.	.	02	C1	.		
VIII	4.6	4.5	4.4	4.2	247.5	14.8	88	55	85	76	38	076	C22.0	27	.	.	24	12	.	.	.	11	06	12	08	03	12	.	.	.	08	04	.		
IX	5.5	5.5	4.3	5.1	161.7	11.3	92	61	88	80	42	019	C07.6	27	.	.	05	.	.	.	.	06	05	08	05	.	08	.	.	.	01	11	.		
X	7.8	6.2	7.3	7.8	070.5	06.9	94	76	91	87	54	156	C03.7	29	.	.	02	.	.	.	.	02	18	21	17	05	21	.	.	.	01	10	.		
XI	5.6	6.3	6.2	6.7	065.3	05.8	94	71	90	85	47	050	C15.6	26	.	.	04	.	.	.	.	07	12	13	09	03	13	01	.	.	.	12	.		
XII	9.3	8.2	7.4	8.3	047.2	05.0	90	80	89	87	54	050	C01.4	19	.	02	15	.	.	.	.	01	22	18	11	01	17	05	03	01	.	11	.		
God.	6.6	6.7	5.9	6.4	1616.3	08.4	88	65	84	79	21	781	C07.3	30VI	.	02	67	65	18	.	.	53	151	156	105	22	150	15	05	02	.	33	90	01	
<b>CSIJEK</b>																																			
BR. ST.73													H <sub>a</sub> = 89 m H <sub>b</sub> = 91.8 m h <sub>i</sub> = 2.0 m h <sub>r</sub> = 1.5 m																						
I	7.9	6.0	6.5	7.5	046.3	04.9	96	87	96	93	63	032	C12.3	20	.	.	22	.	.	.	.	02	18	10	05	01	69	03	01	.	01	C1	.		
II	6.4	6.4	4.6	5.8	087.4	05.9	97	72	89	86	47	020	C06.6	24	.	.	11	.	.	.	.	04	06	12	05	.	10	01	.	.	02	.			
III	5.5	6.4	4.4	5.3	160.9	06.2	95	61	79	78	23	021	C06.4	08	.	.	06	03	.	.	.	01	07	11	08	05	06	04	01	.	01	0!			
IV	6.0	6.9	5.3	6.1	161.5	07.1	90	50	56	60	73	26	045	C14.0	16	.	.	01	01	.	.	.	06	12	14	08	.	14	.	.	01	.			
V	6.5	6.5	4.4	5.8	173.4	10.2	92	62	89	81	43	074	C12.0	23	.	.	05	.	.	.	.	01	05	09	22	13	02	22	.	.	C1	05	01		
VI	5.1	7.0	5.6	5.6	194.4	12.5	90	65	86	80	48	157	C04.6	11	.	.	12	01	.	.	.	03	10	18	14	04	18	.	.	06	.				
VII	3.6	4.2	3.5	3.8	251.0	14.0	89	58	75	77	42	062	C02.2	20	.	.	19	09	.	.	.	12	04	11	09	02	11	.	.	04	.				
VIII	3.0	2.7	3.1	3.2	257.1	15.9	94	60	89	81	45	050	C18.6	27																					

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Pm (0-12)																					
		Tm			Max.				Min.			Dat.				N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Max.	Min.	Max.	Dat.	Min.	Dat.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.						
$\psi = 14^{\circ}58'$ N $\lambda = 14^{\circ}24'$ E Gr. $\Delta G = + 58$ min.																									GRES		BR. ST.76						
I	-	05.1	11.1	05.2	06.6	12.6	03.0	14.0	22	-04.5	18	22	C1.2	19	C1.6	+	+	03	03.7	13	01.4	01	01.0	14	01.0	15	C1.2	06					
II	-	07.9	12.4	08.0	09.1	13.3	06.5	16.0	18	01.8	09.8	12	C1.5	22	02.8	+	+	09	03.2	27	03.1	05	01.6	02	01.0	04	C1.0	03					
III	-	07.4	14.2	07.4	09.1	14.8	06.5	19.8	31	02.8	01	39	C1.3	09	04.3	+	+	03	05.0	20	02.2	03	01.0	10	01.0	09	C1.3	.					
IV	-	11.9	15.8	11.6	12.7	16.6	08.1	21.0	09	03.8	08	38	C1.2	01	02.0	16	02.2	12	02.6	06	01.7	01	01.0	10	01.7	02							
V	-	12.9	20.1	13.7	15.1	21.7	16.3	27.0	21	05.2	11	14	C1.1	08	01.8	+	+	11	02.2	01	01.0	13	01.4	33	01.2	.							
VI	-	16.4	23.0	16.6	18.2	24.1	13.7	28.8	12	24	01.6	06	02.0	01	01.0	15	02.4	06	C2.0	08	03.4	10	01.4	20	C1.4	.							
VII	-	20.9	28.2	21.6	23.1	28.5	17.1	37.4	29	13.6	10	08	01.4	13	02.4	C2	03.0	08	02.5	05	01.6	04	01.0	18	01.4	01							
VIII	-	23.7	30.2	23.9	25.4	31.3	19.3	-	-	-	04	C1.2	25	02.0	02.5	03	03.0	+	+	06	01.3	35	01.4	11	C1.1	07							
IX	-	18.5	25.1	18.6	20.2	26.3	16.4	32.0	16	11.0	30	23	C1.2	12	01.7	+	+	20	02.3	06	02.7	01	02.0	12	01.4	16	01.2	.					
X	-	08.5	14.1	08.7	10.0	15.3	06.1	18.8	05	02.7	17	07	01.8	35	02.3	C4	C1.2	15	02.6	06	01.5	08	01.5	05	01.6	06	C1.3	02					
XI	-	08.3	13.4	08.7	09.8	14.1	06.6	17.5	17	03.0	29	01	C1.0	25	01.7	35	02.3	05	01.8	14	01.4	+	+	04	01.0	06	.						
XII	-	04.7	10.5	04.9	06.2	11.4	02.9	13.5	03	-00.5	16	01	02.0	18	01.2	+	+	03	02.0	+	10	01.3	25	01.4	36	01.5	.						
GOD.	-	12.2	18.2	12.4	13.8	19.2	09.7	-	-	-	160	C1.4	230	02.3	10	02.3	145	02.5	101	02.3	79	01.7	161	01.4	182	01.3	27						
$\psi = 44^{\circ}32'$ N $\lambda = 14^{\circ}28'$ E Gr. $\Delta G = + 58$ min.																									MALI LOSINJ		BR. ST.77						
I	761.6	08.5	10.4	08.7	09.1	11.3	07.4	15.4	20	05.7	26	14	C2.6	16	02.5	C4	C1.5	18	02.7	04	02.8	+	+	10	01.9	12	C2.0	15					
II	754.2	09.2	12.0	08.8	10.2	12.7	08.4	15.9	16	05.2	07	06	03.0	17	03.0	C5	C2.2	27	03.4	08	03.1	05	C2.2	04	02.8	04							
III	757.0	09.0	12.5	10.1	10.4	13.6	08.3	16.6	21	04.8	16	09	03.2	27	02.6	C7	C2.1	11	04.3	11	03.6	06	02.2	03	03.7	14	02.4	06					
IV	753.5	11.4	14.8	12.1	12.7	15.9	10.5	19.0	07.00	06.9	17	09	03.1	29	03.0	C5	02.6	18	04.0	10	03.2	04	02.2	09	02.8	03	01.7	03					
V	754.6	15.0	18.3	15.4	16.0	19.4	13.0	25.7	21	05.9	01	05	02.4	16	02.8	C4	C1.8	02	03.0	25	03.2	12	02.8	16	02.4	06	C2.4	03					
VI	755.1	18.9	21.9	18.7	19.6	23.0	16.6	26.0	05	11.5	11	13	C2.5	28	02.4	C7	C1.9	05	02.0	21	03.3	10	02.8	08	02.5	06	C2.2	02					
VII	756.7	22.3	26.6	22.7	23.6	27.7	20.1	32.5	16	17.5	26	08	02.6	21	03.1	C7	C2.1	05	02.4	20	03.2	09	01.9	09	03.2	03	C2.0	11					
VIII	756.4	23.4	28.1	24.2	24.9	29.2	21.3	34.6	05	15.1	11	11	C2.6	30	02.2	C9	01.9	04	02.2	05	02.8	11	02.3	10	02.4	04	C2.5	08					
IX	756.1	19.2	23.5	20.0	20.7	24.3	18.0	28.5	16	15.15	25	15	02.7	71	C2.1	C5	02.2	11	02.5	11	C2.1	12	03.0	06	02.7	03	C2.3	06					
X	753.0	12.0	14.3	12.4	12.8	15.6	10.8	20.0	04	06.5	72	14	C3.1	20	03.6	C3	C1.7	10	02.4	20	03.0	16	03.3	05	03.4	03	C2.0	02					
XI	758.2	11.6	13.5	12.0	12.3	14.3	10.5	18.0	16	07.6	01	05	02.8	14	01.9	C6	C2.5	33	02.8	12	03.1	C9	02.8	04	02.8	03	01.3	01					
XII	761.0	09.1	11.0	09.4	09.7	11.8	07.7	14.4	06.0	-05.3	03.0	11	C3.2	15	04.3	C3	02.0	06	02.7	02	01.5	19	02.5	10	01.7	12	C1.9	15					
GOD.	756.5	14.4	17.2	14.6	15.2	18.2	12.6	34.6	05.00	-05.3	05.0	113	C2.9	254	03.0	65	02.1	150	03.0	150	03.1	116	02.7	97	02.5	74	C1.2	76					
$\psi = 44^{\circ}45'$ N $\lambda = 14^{\circ}46'$ E Gr. $\Delta G = + 59$ min.																									RAB		PR. ST.78						
I	764.2	07.3	11.1	08.1	08.7	12.2	05.9	20.3	20	02.6	15	17	C1.8	08	01.0	C2	C1.0	18	03.2	03	01.0	07	01.4	28	.	.	.	.					
II	755.5	05.2	12.5	05.7	10.3	13.3	07.7	16.2	20	03.7	28	08	01.4	13	02.8	C7	02.3	34	05.0	06	C2.3	05	01.6	01	01.0	02	C3.5	08					
III	755.6	08.7	13.6	10.2	10.7	14.4	07.4	20.6	21	02.4	01	09	01.6	15	02.3	C5	C1.8	16	04.2	03	0.0	11	01.2	04	01.5	26							
IV	754.7	11.7	14.2	12.4	13.0	16.7	10.7	21.1	06.3	06	17	15	04.4	08	02.4	C8	03.7	05	03.0	07	02.7	02	C3.0	17									
V	757.4	15.0	19.4	15.8	16.4	20.1	12.6	27.8	21	05.0	01	13	C2.7	04	01.5	C4	C1.5	18	02.2	09	02.2	07	01.3	01	01.0	11	01.5	23					
VI	757.1	16.7	20.5	17.9	19.7	23.7	15.8	27.6	30	10.2	11	06	C2.8	04	03.0	C7	01.7	21	02.9	08	02.1	02	C2.0	05	C1.6	26							
VII	759.1	21.3	26.0	22.4	23.2	27.7	19.9	31.7	30	15.4	26	03	C1.5	14	01.6	C7	C2.9	12	03.0	11	02.5	11	01.0	02	03.5	25							
VIII	758.9	22.4	28.0	24.0	24.8	29.7	20.1	35.6	20	13.2	11	14	C1.4	05	02.2	C3	02.3	04	02.2	02	01.1	06	C1.3	38									
IX	758.7	18.3	23.9	19.5	20.3	24.5	18.8	29.6	16	10.8	26	10	01.5	07	02.0	C2	03.5	23	04.0	02	03.0	11	01.3	04	01.2	25							
X	755.7	10.7	15.9	11.1																													

Měsíc	Oblačnost Nm (0-10)				Intenzita hoří sítí (Index)	Vlhkost vzduchu				Padavina mm				Broj dana na rok:																																		
														Tr		Tx		Tn		Tx		Tn		F(0-12)		Nm(0-10)		R mm		●		*		■		▲		▲		R		T		≡		■		
	7	14	21	Sed.		mm	7	14	21	Σ	Min	Max	Max	Min	Σ	10.00.0	0.05.0	0.020.0	0.6	8	2.0.8.0	0.1.1.0	1.0.10.0	6	8	2.0.8.0	0.1.1.0	1.0.10.0	6	8	2.0.8.0	0.1.1.0	1.0.10.0	6	8	2.0.8.0	0.1.1.0	1.0.10.0	6	8	2.0.8.0	0.1.1.0	1.0.10.0					
<b>BR. ST.76</b>																																																
<b>CHES</b>																																																
I	5.7	6.0	6.0	5.9	-	05.6	77	65	79	74	35	082	C36.5	01	.	.	02	.	.	.	.	10	14	C8	07	02	06	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.						
II	6.8	6.3	6.4	6.5	-	06.6	77	65	77	73	37	066	C23.0	06	.	.	.	.	.	.	.	01	.	06	14	06	03	06	.	.	.	.	.	.	.	.	.	.	.	.	.							
III	5.5	5.7	5.6	5.6	-	05.2	57	55	56	56	19	051	C30.2	05	.	.	.	.	.	.	.	09	12	03	02	02	03	.	.	.	.	.	.	.	.	.	.	.	.	.								
IV	5.6	5.6	5.5	5.6	-	04.9	63	57	63	61	30	102	C37.1	13	.	.	.	.	.	.	02	01	08	11	07	06	05	07	.	.	.	.	.	.	.	.	.	.	.	01	.							
V	4.6	4.6	5.1	4.8	-	08.2	63	60	63	62	29	115	C39.5	01	.	.	04	.	.	.	.	09	09	09	09	05	05	C5	.	.	.	.	.	.	.	.	.	.	.	.								
VI	5.6	5.8	5.6	5.7	-	09.3	62	53	60	58	21	093	C23.4	11	.	.	12	.	.	.	.	C5	C9	06	07	05	08	.	.	.	.	.	.	.	.	.	.	02	.									
VII	2.5	2.1	2.2	2.3	-	11.5	57	44	59	53	15	132	C14.3	26	.	.	29	09	05	.	.	21	C2	03	03	02	03	.	.	.	.	.	.	.	.	.	02	.										
VIII	1.7	2.3	2.0	2.3	-	13.3	57	49	54	54	-	031	C12.4	09	.	.	.	.	.	.	17	01	04	03	02	04	.	.	.	.	.	.	.	.	.	05	.											
IX	3.5	3.6	4.1	3.7	-	11.5	68	55	69	64	34	155	C34.6	30	.	.	22	04	.	.	.	12	C6	09	09	06	05	.	.	.	.	.	.	.	.	01	02	.										
X	7.6	7.7	8.1	7.8	-	07.0	79	67	77	74	23	262	C0.0	09	.	.	.	.	.	.	01	.	04	20	19	19	13	19	.	.	.	.	.	.	.	.	07	.										
XI	6.6	6.9	6.5	6.7	-	06.9	74	71	76	73	42	670	C26.4	26	.	.	.	.	.	.	04	14	15	05	03	05	.	.	.	.	.	.	.	.	.	02	.											
XII	4.8	5.5	5.5	5.3	-	05.3	74	67	74	71	47	028	C14.2	12	.	.	03	.	.	.	.	09	13	03	03	02	03	.	.	.	.	.	.	.	.	.	05	.										
GOD.	5.0	5.2	5.3	5.2	-	08.1	67	58	67	64	-	1107	C27.1	45W	.	.	.	.	.	.	04	01	114	123	84	79	50	84	.	.	.	.	.	.	.	.	01	20	.									
<b>BR. ST.77</b>																																																
<b>MALI LOSINJ</b>																																																
I	6.5	7.0	4.6	6.0	-	104.1	07.0	82	15	84	86	072	C20.6	67	.	.	.	.	.	01	.	04	C8	11	10	03	11	.	.	.	.	.	.	.	.	.	04	.										
II	6.9	6.4	4.0	5.9	-	120.1	07.0	78	65	77	35	071	C14.9	05	.	.	.	.	.	04	04	05	12	02	11	.	.	.	.	.	.	.	.	03	.													
III	5.5	6.1	4.5	5.5	-	167.5	07.5	80	65	80	25	064	C23.5	05	.	.	.	.	.	04	06	10	06	04	03	05	.	.	.	.	.	.	.	.	03	.												
IV	6.3	6.5	5.2	5.8	-	187.9	07.5	73	57	69	24	080	C47.7	26	.	.	.	.	.	06	05	09	06	04	05	05	.	.	.	.	.	.	.	.	01	02												
V	5.6	5.2	5.0	5.3	-	276.0	09.8	77	62	75	71	34	127	C34.2	25	.	.	01	.	01	.	04	C8	14	11	04	14	.	.	.	.	.	.	.	.	07	.											
VI	5.6	5.3	4.5	5.1	-	275.5	12.4	74	63	77	29	094	C20.7	11	.	.	04	01	01	.	06	C4	12	09	04	12	.	.	.	.	.	.	.	.	06	.												
VII	2.5	2.3	2.5	2.4	-	167.0	03.1	68	47	64	01	31	024	C08.6	06	.	.	27	06	14	02	16	C1	05	05	05	05	.	.	.	.	.	.	.	03	.												
VIII	2.0	3.0	1.8	2.5	-	336.7	15.3	74	52	68	45	24	054	C14.3	12	.	.	29	12	23	01	16	01	07	07	02	07	.	.	.	07	.																
IX	4.8	4.9	3.5	4.1	-	242.9	13.4	80	60	77	72	40	209	C66.6	21	.	.	15	.	06	02	12	C6	15	15	07	15	.	.	.	.	.	.	.	01	05	.											
X	7.3	7.7	5.7	6.9	-	117.0	03.7	74	65	70	37	227	C33.5	02	.	.	03	.	03	.	04	C8	12	18	14	08	18	.	.	.	.	.	.	.	01	01	10											
XI	8.0	7.4	5.6	7.0	-	094.5	05.1	79	65	76	75	39	124	C21.4	07	.	.	03	01	11	14	13	06	14	.	.	.	.	.	.	.	03	.															
XII	5.1	6.0	4.6	5.0	-	108.2	06.7	78	68	75	40	021	C01.1	31	.	.	02	.	04	.	04	01	07	08	07	01	07	.	.	.	01	.																
GOD.	5.6	5.6	4.4	5.1	-	240.8	07.7	85	76	82	70	24	1322	C78.5	20X	.	.	88	22	31	74	33	79	96	141	109	45	140	.	.	.	01	02	03	66	02												
<b>BR. ST.78</b>																																																
<b>RAD</b>																																																
I	6.6	7.4	4.2	6.1	-	111.7	06.7	63	71	81	78	46	071	C17.8	07	.	.	01	.	04	16	11	05	02	11	.	.	.	.	.</td																		

1974

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																	
		Tm			Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dnev.)	Max	Min	Max	Dat.	Min	Dat.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.				
$\varphi = 44^{\circ}27'$ N $\lambda = 15^{\circ}04'$ E Gr. $\Delta G = + 1h\ 00\ min.$																													
I	-	06.7	11.0	08.1	06.5	11.6	05.3	15.4	28	06.6	15	12	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0				
II	-	09.3	12.2	09.7	10.2	12.7	07.4	16.3	16.17	03.4	09	15	C0.2	C14	C0.4	C2	C1.0	C20	C2.8	C22	C2.6	*	02	01.5	09	C1.4			
III	-	08.7	13.7	10.9	11.0	14.3	07.6	20.8	26	04.8	01	18	C2.7	C1	C1.1	C6	C1.2	C17	C2.2	C11	C3.1	C4	C1.5	C3	C1.0	C1.4			
IV	-	12.4	15.2	12.8	13.3	16.5	09.8	20.8	30	05.7	21	19	C3.4	C15	C3.6	C6	C1.2	C17	C2.4	C13	C2.8	C2	C1.0	C5	C2.0	C1.5			
V	-	16.0	19.8	16.7	17.3	20.7	13.4	24.5	21	05.8	10	19	C1.7	C6	C0.2	C5	C1.0	C16	C1.9	C14	C2.1	C3	C0.9	C19	C1.6	*			
VI	-	19.6	23.5	19.9	20.7	24.4	15.9	28.1	05	11.7	11	14	C2.4	C6	C0.2	C1	C1.0	C19	C1.9	C14	C1.8	C8	C0.4	C19	C1.8	*			
VII	-	22.7	27.5	23.4	24.3	28.5	19.4	34.6	16	15.5	27	19	C2.3	C10	C0.3	C8	C1.4	C17	C1.8	C13	C1.9	C7	C1.9	C8	C1.6	C1.4			
VIII	-	23.9	29.0	24.8	25.5	30.2	20.5	36.4	20	13.5	11	20	C0.1	C9	C0.6	C12	C1.0	C11	C1.5	C8	C0.8	C4	C1.2	C6	C0.3	C25	C1.7		
IX	-	18.7	24.3	20.4	20.9	25.1	16.9	26.7	16	10.5	27	14	C1.9	C6	C0.7	C3	C1.2	C15	C1.6	C12	C2.2	C2	C1.5	C8	C1.6	C1.5	*		
X	-	10.9	14.1	11.4	11.9	15.0	08.8	19.0	04	03.8	31	19	C0.5	C13	C0.8	C5	C1.0	C19	C2.1	C17	C2.1	C3	C1.3	C10	C1.4	C9	C1.3		
XI	-	10.1	13.5	10.5	11.2	14.5	05.1	18.0	07	01.7	02	10	C0.1	C6	C0.4	C1	C1.0	C20	C1.8	C10	C1.9	C1	C1.0	C6	C0.8	C1.8	*		
XII	-	06.4	11.0	07.6	08.2	12.7	04.3	18.7	06	06.5	22	10	C0.1	C8	C0.5	C3	C1.0	C17	C1.5	C13	C1.5	C2	C1.0	C4	C1.0	C1.8	C1.4		
GOD.	-	13.7	17.9	14.7	15.2	18.9	11.5	36.4	00	00	29	00	196	C2.5	C111	C0.3	C8	C1.1	C17	C2.0	C178	C0.2	C1	C35	C1.5	C68	C1.5	C207	C1.5
$\varphi = 44^{\circ}08'$ N $\lambda = 15^{\circ}13'$ E Gr. $\Delta G = + 1h\ 01\ min.$																													
ZADAR													ZADAR																
BR. ST.R2																													
I	765.5	07.1	11.1	08.1	08.6	11.5	06.6	15.9	21	01.0	15	07	C3.0	C4	C1.7	C11	C1.7	C24	C1.8	C6	C1.3	*	03	C2.3	C17	C2.5	29		
II	756.5	08.2	12.7	09.4	09.9	13.5	06.5	16.6	18	02.1	28	02	C1.5	C10	C2.3	C17	C2.0	C30	C2.7	C6	C3.0	*	02	C2.5	C7	C2.3	10		
III	760.9	07.9	13.3	10.0	10.3	14.0	06.9	18.1	26	02.0	12.01	03	C2.3	C6	C0.5	C13	C1.9	C10	C3.5	C9	C2.8	*	01	C0.6	C19	C2.7	34		
IV	757.5	11.2	15.1	12.2	12.7	16.7	04.1	20.9	06	06.2	20.19	02	C0.1	C8	C0.7	C17	C2.7	C25	C0.5	C3	C0.2	C0	14	C2.4	C15	*			
V	758.7	15.3	18.8	15.8	16.4	19.8	14.4	24.5	21	05.5	10	01	C1.0	C5	C0.7	C0	C1.6	C11	C1.9	C16	C2.2	*	01	C0.2	C29	C2.6	25		
VI	759.1	19.5	23.0	19.6	20.4	24.0	16.0	27.4	20	10.4	13	06	C0.2	*	*	C3	C0.0	C21	C1.5	C1.7	*	06	C0.2	C17	C2.9	22			
VII	760.5	22.1	26.5	23.4	27.4	28.6	18.6	32.3	17	14.7	21	01	*	*	C3	C0.0	C2	C1.5	C13	C1.8	C7	*	06	C0.0	C22	C2.4	40		
VIII	760.1	22.3	27.7	23.3	24.2	28.9	18.5	32.7	17	14.0	12	05	C2.6	C2	C0.5	C15	C1.9	C9	C0.9	*	03	C0.3	C19	C2.2	38				
IX	760.0	18.0	23.8	19.8	20.3	24.5	16.5	28.1	15.04	11.0	26	02	C2.3	C5	C0.2	C21	C11	C1.6	C15	C1.5	C9	*	03	C1.1	C18	C2.6	26		
X	757.4	10.6	15.1	11.6	12.2	16.2	08.9	20.3	04	04.1	31	19	C0.7	C1.6	C0	C1.5	C2	C1.4	C9	C0.8	*	07	C0.4	C17	C2.7	16			
XI	762.2	09.6	14.0	10.8	11.3	15.1	08.2	17.6	11	02.3	02	05	C1.4	C7	C1.9	C29	C1.5	C24	C2.2	C4	C2.2	02	C0.0	C12	C3.5	12			
XII	764.8	07.5	11.8	08.4	09.0	12.5	05.8	15.3	02	02.0	15.13	06	C3.7	C6	C0.3	C27	C1.7	C21	C1.5	C8	C0.8	01	C1.0	C4	C2.6	31			
GOD.	760.0	14.3	17.7	14.3	14.9	18.7	11.2	32.7	07	07.0	20	02.2	C129	C1.7	C0.7	C2.5	C100	C0.2	C3	C1.7	C44	C0.1	C180	C2.5	C298	*			
$\varphi = 41^{\circ}48'$ N $\lambda = 15^{\circ}19'$ E Gr. $\Delta G = + 1h\ 01\ min.$																													
LICKE LESTCE													LICKE LESTCE																
BR. ST.R3																													
I	-00.7	03.3	00.2	00.7	03.6	-01.9	15.5	20	-05.8	22	15	C1.1	C1	C1.0	C4	C1.0	C7	C1.7	C11	C1.1	C6	C1.0	C3	C1.3	C1				
II	-03.7	07.7	04.3	05.0	06.7	01.5	14.3	12	-05.2	08	15	C2.2	C6	C1.8	C1	C1.0	C6	C2.8	C16	C2.9	C8	C2.2	C1	C1.7	C11				
III	-02.6	10.7	05.5	06.1	11.5	01.1	23.4	22	-04.8	14	21	C1.8	C6	C1.8	C2	C1.0	C9	C1.2	C7	C1.6	C4	C2.0	C2	C1.5	C18				
IV	-05.4	11.7	07.6	07.6	07.6	01.8	18.6	29	-03.1	20	18	C0.0	C11	C0.1	C7	C1.4	C9	C0.8	C2.0	C0.9	C16	*	16	C1.5	C17				
V	-	10.0	17.4	10.2	11.9	18.4	05.9	24.4	30	-01.4	10	19	C1.6	C6	C1.7	C7	*	*	C0.4	C1.4	C0.6	C2.0	C2	C1.5	C1.5	C29			
VI	-	13.4	20.3	12.9	14.9	21.3	06.1	27.2	04	03.0	13	11	C0.5	C5	C0.7	C1	C1.0	C12	C2.2	C10	C2.7	C3	C1.3	C18	C1.4	28			
VII	-	15.4	24.8	15.4	17.7	25.6	10.3	31.0	30	05.1	27	12	C1.6	C6	C1.8	C2	C1.0	C9	C1.2	C7	C1.9	C4	C2.2	C26					
VIII	-	15.0	25.7	15.7	18.0	26.6	11.6	33.0	16	04.4	12	11	C2.0	C6	C1.5	C1	C1.0	C20	C0.3	C1.3	C1	C1.4	C49	*					
IX	-	12.0	20.4	12.9	14.6	21.4	05.2	26.8	03	01.1	28	09	C1.7	C6	C1.8	*	*	*	C0.4	C1.8	C6	C2.0							

Mjesec	Oblačnost Nm (0-10)			Insolacija broj sati Sred. (Dnev.)	Vlažnost vazduha			Padavine mm			Broj dana na se												•	*	*	Δ	Δ	▲	▲	T	III	II		
					em			Um R			Tn Tx Tn Tx Tn Tx F(0-12)			Nm(0-10)			R mm			•	*	*	Δ	Δ	▲	▲	T	III	II					
	7	14	21					7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min			
<b>PAG</b>																													$H_s = 3 \text{ m } H_p = - \text{ m } h_i = 2.0 \text{ m } h_t = 1.0 \text{ m}$					
I	6.6	6.5	4.4	5.9	086.6	06.3	80	68	78	75	36	095	C28.1	07	•	•	•	•	•	•	06	13	12	05	04	12	•	•	•	•	03	•		
II	7.8	6.2	4.6	6.2	087.3	06.5	71	63	71	68	39	095	C19.7	05	•	•	•	•	•	03	10	10	10	05	10	•	•	•	•	02	•			
III	5.7	5.4	5.1	5.4	162.0	06.7	74	56	69	66	29	055	C24.3	05	•	•	•	•	•	01	09	09	08	04	02	07	•	•	•	•	02	•		
IV	6.3	5.9	4.9	5.7	166.5	06.6	58	54	61	58	23	096	C27.7	26	•	•	•	•	•	05	08	12	09	08	04	05	•	•	•	•	04	•		
V	5.7	5.1	4.4	5.7	245.3	05.8	69	58	70	66	35	109	C46.6	01	•	•	•	01	•	•	06	08	11	05	04	11	•	•	•	•	06	•		
VI	4.7	4.8	5.1	5.9	258.6	11.9	69	56	64	56	36	084	C33.5	11	•	•	•	14	•	01	07	08	14	09	02	14	•	•	•	•	06	•		
VII	2.5	2.4	2.1	2.3	315.1	13.1	62	47	51	57	34	022	C00.6	16	•	•	•	27	10	12	01	17	01	04	04	•	•	•	•	05	•			
VIII	2.4	2.5	2.0	2.3	320.8	15.3	71	51	55	52	34	098	C26.6	10	•	•	•	29	15	17	•	18	02	08	07	05	08	•	•	•	•	06	01	
IX	5.7	5.3	3.7	3.9	226.3	13.1	75	64	74	70	34	154	C68.0	30	•	•	•	18	•	02	•	14	05	12	10	08	14	•	•	•	•	09	•	
X	7.6	7.4	6.3	7.1	108.5	07.6	76	62	71	71	27	071	C42.0	21	•	•	•	•	•	02	02	13	15	11	22	•	•	•	•	02	•			
XI	6.0	6.9	5.3	6.7	064.9	07.5	76	67	76	73	41	132	C30.6	27	•	•	•	•	•	02	03	12	11	10	05	11	•	•	•	•	04	•		
XII	6.4	5.2	5.0	5.5	081.5	06.3	82	66	79	76	38	030	C11.0	19	•	•	•	02	•	01	07	11	08	05	01	06	•	•	•	•	01	03		
GOD.	5.7	5.2	4.5	5.1	2165.8	05.2	72	58	70	67	23	1408	C42.0	218	•	•	02	05	25	32	12	01	09	104	127	103	52	127	•	•	•	•	03	54
<b>ZADAR</b>																													$H_s = 5 \text{ m } H_p = 7.3 \text{ m } h_i = 2.0 \text{ m } h_t = 1.0 \text{ m}$					
BR. ST. 82																									$H_s = 5 \text{ m } H_p = 7.3 \text{ m } h_i = 2.0 \text{ m } h_t = 1.0 \text{ m}$									
I	6.9	6.9	4.2	6.0	108.1	06.6	82	74	83	79	37	117	C33.1	07	•	•	•	•	•	05	10	09	04	05	•	•	•	•	•	•	03	•		
II	6.9	6.6	4.1	5.9	136.1	06.7	78	63	75	72	39	063	C16.6	05	•	•	•	09	•	02	07	11	00	02	11	•	•	•	•	03	•			
III	5.3	5.5	3.5	4.9	179.9	07.2	72	69	70	75	27	071	C28.7	05	•	•	•	•	01	06	06	05	02	07	•	•	•	•	01	06				
IV	6.4	6.2	5.5	5.4	175.1	07.5	65	63	70	67	37	075	C15.0	26	•	•	•	03	•	06	05	11	07	02	11	•	•	•	•	01	02			
V	5.7	5.2	4.5	5.0	276.7	10.7	79	66	79	75	41	124	C49.6	20	•	•	•	05	•	07	10	06	04	10	•	•	•	•	05	•				
VI	4.1	4.1	4.0	5.3	277.6	12.9	75	62	76	71	23	084	C14.7	11	•	•	05	01	•	04	05	07	06	03	07	•	•	•	•	06	•			
VII	5.4	5.5	4.7	5.7	316.1	14.3	68	56	72	65	34	034	C16.4	20	•	•	24	04	02	01	15	01	05	04	01	05	•	•	•	•	04	•		
VIII	5.7	5.0	4.7	5.2	315.7	16.6	77	61	76	72	35	041	C13.4	29	•	•	30	11	18	•	18	04	09	09	02	05	•	•	•	•	09	02		
IX	5.3	4.4	3.1	3.8	238.4	13.5	82	63	79	75	40	113	C26.4	16	•	•	18	02	01	17	05	12	10	04	12	•	•	•	•	05	•			
X	7.2	6.7	5.2	6.4	128.6	08.1	81	64	78	74	35	340	C10.4	06	•	•	01	•	03	10	26	17	09	20	•	•	•	•	01	10	•			
XI	7.5	7.2	4.4	6.4	110.7	07.6	80	65	78	76	42	086	C30.0	26	•	•	•	•	•	02	05	15	11	12	15	•	•	•	•	03	•			
XII	5.1	5.1	3.4	4.6	113.9	06.7	80	67	79	76	37	039	C21.7	28	•	•	•	01	•	04	07	05	01	07	•	•	•	•	01	01				
GOD.	5.4	5.4	3.7	4.9	2422.6	09.9	77	64	77	73	22	1186	C10.2	063	•	•	86	15	28	11	•	91	75	123	99	39	123	•	•	•	•	02	44	
<b>LICKE LESC</b>																													$H_s = 463 \text{ m } H_p = - \text{ m } h_i = 2.0 \text{ m } h_t = 2.0 \text{ m}$					
BR. ST. 83																									$H_s = 463 \text{ m } H_p = - \text{ m } h_i = 2.0 \text{ m } h_t = 2.0 \text{ m}$									
I	8.6	7.7	7.0	7.8	-	04.2	87	79	87	F4	44	050	C24.4	01	•	02	27	•	•	•	02	18	12	07	01	11	06	01	01	01	01	11	06	
II	8.1	7.8	7.5	7.8	-	05.0	80	73	75	75	26	098	C29.4	07	•	•	09	•	02	01	16	17	06	14	06	01	01	01	01	01	01	02		
III	7.9	6.6	6.7	7.1	-	05.1	83	57	78	73	23	051	C17.5	05	•	•	14	•	•	•	12	07	06	01	04	06	•	•	•	•	02	05		
IV	5.8	7.0	5.6	6.4	-	05.3	77	54	72	68	28	124	C45.2	26	•	•	11	•	•	05	11	17	11	04	16	04	03	01	01	01	01			
V	6.4	6.5	5.8	6.3	-	07.7	81	54	72	78	18	138	C11.7	1	•	•	01	•	•	01	11	15	10	05	15	•	•	•	•	03	05			
VI	6.2	6.2	4.6	5.7	-	09.4	80	55	83	73	26	118	C31.1	10	•	•	03	•	02	02	04	14	13	10	06	04								

Mesec	Vadutski Pritisak Fm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																					
		Tm				Sred. (Dnes)				N		NE		E		SE		S		SW		W		NW							
		7	14	21		Max	Min	Max	Dat.	Min	Dat.	Min	Dat.	Max	Min	Max	Dat.	Min	Dat.	Max	Min	Max	Dat.	Min	Dat.						
$\psi = 44^{\circ}02'$ , N $\lambda = 16^{\circ}12'$ , E Gr., $\Delta G = +1h\ 05\ min.$																							BR. ST-86								
I	744.4	06.1	09.9	06.4	05.4	11.1	01.1	16.5	20	-03.6	15	31	C1.0	C2.0	C3.0	C4.0	C5.0	C6.0	C1.2	C6	C1.7	C6	01.7	03	02.0	02	01.0	03	01.7	34	
II	737.5	06.1	11.1	06.8	07.7	12.0	04.4	16.6	20	-03.3	09	33	C1.0	C2.0	C3.0	C4.0	C5.0	C6.0	C1.2	C6	C2.4	C7	02.6	16	C2.4	*	02	01.0	03	C2.0	16
III	735.7	05.6	15.2	08.9	09.6	16.0	04.6	21.6	22	-02.3	01	34	C1.8	C2.5	C3.1	C4.0	C5.0	C6.0	C1.0	C6	C2.4	C7	02.3	06	C1.5	05	C2.2	21			
IV	736.4	06.2	14.9	10.3	11.1	16.4	06.5	21.6	09	06.3	21	42	C3.0	C3.7	C4	C2.5	C3.0	C3.0	C2	C2.0	C0	C2.3	C1.7	C6	01.7	02	C1.5	13			
V	737.8	12.7	20.3	14.3	15.4	21.4	05.4	21.6	20	04.3	11	24	C2.1	C5	C7.4	C7	C1.6	C4	C1.8	C10	C2.2	C8	C1.9	04	C1.5	03	C1.7	28			
VI	738.4	16.5	23.1	17.9	19.0	24.0	12.4	31.0	04	06.9	13	23	C2.5	C6	C1.8	C3.0	C1.0	C1.8	C3	C0.0	C1	C2.4	C2	C1.5	03	C3.2	25				
VII	740.3	18.6	26.2	20.5	22.1	25.2	14.6	31.7	31	08.6	04	30	C6.7	C1	C1.0	C2	C1.0	C1.2	C0	C2.0	C10	C1.8	C3	03	C2.0	29					
VIII	740.0	19.3	29.2	21.5	23.1	31.5	16.1	36.7	16.0	03	12	31	C1.8	C2	C1.0	C2	C1.0	C0	C1.0	C5	C1.6	C2	C1.5	09	C2.1	03	C1.0	35			
IX	736.7	14.8	24.4	17.0	19.3	25.5	12.4	31.1	15	05.8	26	45	C5.1	C2	C1.0	C5	C2.0	C3	C1.7	C6	C1.8	C7	C1.9	05	C1.6	04	C1.8	29			
X	736.5	08.8	12.5	07.4	08.6	14.2	04.7	18.5	04	-06.4	31	50	C1.3	C7	C0.1	C3	C1.3	C4	C0.0	C11	C2.4	C1	C2.0	05	C2.0	24					
XI	741.5	05.7	13.1	07.3	08.4	13.0	04.4	20.1	17	-02.5	02	21	C6.7	C9	C0.3	C8	C2.1	C*	C1.7	C1	C1.0	C2	C0.2	01	C2.0	31					
XII	745.5	01.6	10.9	04.0	04.4	10.2	04.1	18.4	04	-06.2	23	53	C3.4	C1	C1.1	C6	C1.5	C4	C1.0	C11	C1.3	C2	C2.0	01	C1.0	37					
GDH.	735.6	09.6	17.4	11.8	12.8	16.8	07.7	36.7	16.0	00.2	25	52	C1.6	C2	C0.1	C7	C1.7	C8	C2.1	C13	C2.0	C3	C1.6	40	C1.9	320					
$\psi = 43^{\circ}44'$ , N $\lambda = 15^{\circ}55'$ , E Gr., $\Delta G = +1h\ 04\ min.$																							SIBENIK								
I	759.2	06.6	11.5	06.4	05.7	12.7	04.4	15.4	20	06.6	15	37	C3.2	C1	C2.2	C17	C1.9	C8	C2.5	*	*	*	*	C1.7	03	C2.0	37				
II	756.1	08.6	12.7	09.3	10.0	15.8	06.9	17.6	18	C1.7	09	49	C0.4	C1	C1.2	C2.6	C1.7	C5	C4.6	C1	C2.0	C0	C1.0	02	C2.0	17					
III	756.5	08.7	14.3	10.4	10.5	15.5	07.4	21.7	26	02.4	13.0	51	C2.7	C1	C1.7	C3.0	C1.7	C17	C1.9	C4.6	C2	C3.5	06	C1.8	07	C1.4	23				
IV	756.9	11.7	15.7	11.7	12.9	17.2	09.3	31.0	06	07.7	21	54	C1.7	C1	C1.0	C6.0	C1.7	C10	C3.1	C5.0	*	*	*	*	C0.8	04	C3.2	07			
V	751.4	15.6	20.1	16.0	17.0	21.4	14.5	17.7	21	05.9	15	45	C4.2	C10	C1.6	C3	C2.3	C6	C1.3	C6	C4.0	C7	C2.6	12	C2.6	25					
VI	752.8	19.7	24.0	20.0	20.6	25.4	16.3	25.7	26	10.8	11	48	C3.4	C6	C2.0	C2	C2.0	C10	C2.3	C6	C2.8	10	C2.0	07	C2.4	36					
VII	754.4	22.5	27.2	23.2	24.1	29.4	19.4	30.0	16	14.1	19	55	C1.7	C12	C1.0	C1.7	C2.0	C3	C1.7	C7	C2.5	06	C3.3	16	C1.6	35					
VIII	757.4	23.4	28.8	24.4	25.2	30.5	20.4	35.6	0	12.8	15	54	C1.6	C1	C1.0	C7	C1.0	C2.0	C1.7	C10	C2.0	C14	14	C3.0	39						
IX	752.6	16.8	24.0	20.0	20.7	25.4	16.8	25.0	16.0	03.0	10	44	C4.2	C7	C0.1	C10	C1.4	C11	C2.5	C8	C3.1	06	C2.7	09	C1.0	34					
X	751.0	16.3	14.3	11.1	11.7	16.0	08.4	21.0	15	04.0	28	51	C1.4	C10	C1.2	C11	C1.5	C17	C3.4	C1	C1.0	02	C1.0	04	C1.0	33					
XI	754.6	05.6	14.2	10.7	11.4	15.7	07.1	18.6	17	03.1	02	12	C4.1	C5	C2.7	C17	C2.6	C27	C3.6	C10	C2.6	04	C1.2	07	C1.0	34					
XII	756.4	06.5	11.2	07.8	08.7	12.0	04.4	17.7	03	01.8	24.1	53	C4.5	C19	C13	C14	C1.5	C4	C2.7	*	*	01	C1.0	*	*	C1	01	C3.0	34		
GDH.	755.1	13.4	18.7	16.0	15.4	19.4	11.4	19.4	11	02.6	51	51	C1.4	C10	C1.2	C10	C1.5	C17	C3.5	C1	C1.0	02	C1.0	04	C1.0	34					
$\psi = 43^{\circ}03'$ , N $\lambda = 16^{\circ}05'$ , E Gr., $\Delta G = +1h\ 04\ min.$																							KOMPITA								
I	-	04.8	12.0	05.7	05.7	13.7	06.7	16.0	20	02.4	16	51	C1.9	C1	C2.2	C20	C2.4	C14	C1.4	C1	C1.8	C6	01.0	14	C2.4	05					
II	-	10.4	19.7	10.4	11.0	14.2	08.7	18.7	19	05.3	15	57	C1.7	C11	C3.0	C25	C1.7	C10	C2.8	05	C3.4	05	C3.0	04	C2.5	03					
III	-	11.0	14.5	11.1	11.6	15.3	07.5	14.9	21	01.6	08	54	C1.1	C1.7	C1.5	C3.5	C3.0	C3.4	04	C2.5	*	C8	C1.9	02	C2.4	14					
IV	-	13.0	16.7	11.6	13.6	16.7	09.2	16.7	04	03.6	19	51	C1.6	C1	C1.4	C10	C1.4	C10	C3.5	C1	04.2	*	*	*	*	16	C2.0	09			
V	-	12.8	19.0	12.0	15.6	17.1	12.0	19.6	22	01.0	10	51	C1.7	C10	C1.2	C1.7	C2.0	C2	C1.0	C1.8	03	C2.0	04	C1.8	26	C2.3	07				
VI	-	20.4	24.1	19.5	20.6	24.4	15.4	24.0	24	11.6	12	51	C1.7	C1	C1.2	C1.7	C1.2	C28	C1.1	04	C1.2	02	C1.0	04	C1.7	05					
VII	-	24.4	27.4	21.0	24.6	28.4	15.6	32.4	17	15.2	24	51	C1.6	C1	C1.0	C2.0	C1.0	C20	C1.7	02.8	C1.0	04	C1.5	03	C1.0	21	C1.7	16			
VIII	-	24.6	29.1	21.5	25.4	26.7	15.7	34.7	06	15.2	30.12	51	C1.6	C1	C1.0	C1.7	C1.0	C10	C1.6	04	C1.0	02	C1.0	04	C1.4	19	C1.5	21			
IX	-	11.4	15.4	11.3	12.3	15.3	06.4	17.0	26	12.2	51	51	C1.7	C1	C1.2	C1.7	C1.2	C22	C1.1	04	C1.2	02	C1.0	04	C1.4	13					
X	-	13.2	17.2	13.7	14.6	17.8	10.4	22.0	20	14.0	50	51	C1.6	C1	C1.2	C1.7	C1.2	C24	C1.1	04	C1.2	02	C1.0	04	C1.4	24					
XI	-	11.7	15.5	11.4	12.8	16.1	05.0	17.4	15	04.6	36	51	C1.7	C1.5	C1.0	C1.7	C1.0	C20	C1.1	04	C1.2	02	C1.0	04	C1.4	09					
XII	-	06.4	12.6	08.6	09.4	12.1	04.3	16.8	04	03.3	13	51	C1.6	C1	C1.2	C1.7	C1.2														

Mjesec Z.	Oblačnost Nm (0-10)			Isolacijski Ljetni sati (dnev.)	Vlažnost vazduha			Padavine R mm		Br. n. j. d. a. n. s. a:																			
	e mm	m mm	t mm		Tn	Tx	Tn			F(0-12)	Nm(0-10)	R mm	●	★	●	★	●	▲	▲	R	T	III	II						
	7	14	21	Secđ. Sred. (dnev.)	7	14	21	Secđ. Sred. (dnev.)	Hm	Mx	Dat.	10.00.0	0.0250	0.020.0	6	8	2.0	8.0	0.1	1.0	10.0	●	★	●	▲	▲	R	T	III
<b>KRKA</b>																													
<b>BR. ST. 86</b>																													
I 5.9 6.7 4.2 5.6	122.7	04.5	89 56 77 74 29	086 C23.0	02	•	•	11	•	•	•	•	•	•	•	C7	11	12	05	04	12	•	•	•	•	•	01	01	
II 7.0 7.5 4.8 6.7	113.6	05.5	74 56 75 69 23	092 C30.1	07	•	•	02	•	•	•	02	•	•	•	01	10	11	04	04	11	•	•	•	•	•	02	•	
III 5.7 6.5 4.1 5.4	103.9	05.5	76 43 70 63 14	062 C23.0	06	•	•	03	02	•	•	01	•	•	•	C5	07	06	02	07	07	•	•	•	•	•	03	•	
IV 6.2 7.6 5.4 6.4	102.6	05.9	65 48 66 59 19	072 C22.1	13	•	•	•	•	•	•	03	•	•	•	03	12	13	04	03	13	•	•	•	•	•	04	•	
V 6.7 6.5 4.2 5.8	227.9	08.2	77 45 71 64 23	098 024.9	01	•	•	07	•	•	•	•	•	•	•	C3	05	37	13	05	17	•	•	•	•	•	07	•	
VI 5.4 6.9 5.1 5.9	236.7	10.3	74 46 68 63 28	171 041.6	11	•	•	15	01	01	•	•	•	•	•	C8	10	15	13	05	15	•	•	•	•	•	01	01	
VII 5.0 4.3 2.6 3.5	343.8	11.0	70 38 61 56 20	023 020.3	20	•	•	24	16	•	•	•	•	•	•	C10	C3	03	02	01	03	•	•	•	•	•	02	02	
VIII 3.2 5.3 2.3 3.6	318.9	12.5	75 43 66 61 18	052 012.7	28	•	•	30	18	01	•	•	•	•	•	C12	C3	09	08	02	05	•	•	•	•	•	11	•	
IX 4.5 5.5 2.5 4.4	223.9	11.1	86 50 79 72 21	264 058.1	25	•	•	17	06	•	•	•	•	•	•	C3	08	17	10	06	11	•	•	•	•	•	07	02	
X 7.2 7.7 6.1 7.0	121.4	06.7	86 64 86 78 26	316 C78.0	06	•	•	01	•	•	•	02	•	•	•	C2	14	21	19	09	21	•	•	•	•	•	05	03	
XI 6.9 7.2 5.1 6.4	126.2	06.2	83 57 80 74 30	072 C22.6	26	•	•	04	•	•	•	01	•	•	•	C1	11	11	08	03	11	•	•	•	•	•	02	01	
XII 5.6 5.8 5.2 5.9	127.7	04.7	89 60 77 73 30	052 C24.6	13	•	•	13	•	•	•	04	01	04	09	C9	09	05	02	02	12	•	•	•	•	•	02	12	
<b>GOD. 5.5 6.5 4.3 5.5</b>																													
<b>SIBENIK</b>																													
<b>BR. ST. 87</b>																													
I 6.0 6.8 3.8 5.6	122.0	05.6	70 59 69 66 29	099 C25.2	02	•	•	•	•	•	•	04	•	•	•	C5	09	12	08	05	12	•	•	•	•	•	02	•	
II 7.1 7.0 5.6 6.6	123.3	06.0	66 56 67 64 22	070 C20.0	04	•	•	•	•	•	•	14	02	•	•	C1	10	12	02	13	13	•	•	•	•	•	01	03	
III 5.6 6.9 4.7 5.7	103.5	06.2	67 52 68 62 19	110 051.0	05	•	•	•	•	•	•	13	01	•	•	C4	07	07	04	07	07	•	•	•	•	•	02	06	
IV 5.6 6.8 5.3 6.1	178.3	06.1	57 49 58 54 17	034 C13.4	27	•	•	•	•	•	•	16	02	•	•	C5	11	13	05	01	13	•	•	•	•	•	01	01	
V 6.1 6.3 5.2 5.6	272.2	08.6	65 50 63 59 22	052 013.6	01	•	•	04	•	•	•	07	02	•	•	C6	13	06	02	13	13	•	•	•	•	•	06	•	
VI 6.0 6.0 5.0 5.7	277.5	10.8	62 48 63 58 26	046 C20.0	30	•	•	18	•	•	•	02	10	02	•	C5	04	12	06	01	12	•	•	•	•	•	02	02	
VII 3.2 2.5 2.0 2.7	358.4	11.2	54 42 53 50 21	046 045.5	20	•	•	27	10	12	•	08	01	•	•	C3	01	01	01	01	01	•	•	•	•	•	01	01	
VIII 3.3 3.7 2.3 3.1	319.5	12.9	57 46 57 53 24	064 013.7	24	•	•	31	16	19	•	06	01	•	•	C1	09	05	05	06	06	•	•	•	•	•	16	•	
IX 4.6 4.1 3.1 4.0	251.5	11.9	70 55 68 64 25	215 056.2	21	•	•	18	•	03	10	•	12	05	11	09	05	11	11	•	•	•	•	•	06	02			
X 7.0 7.5 6.3 6.9	124.9	07.2	73 60 71 68 25	247 G50.1	06	•	•	15	•	03	03	12	05	24	15	24	17	07	24	17	•	•	•	•	•	04	12		
XI 6.6 6.6 5.2 6.4	127.4	06.9	72 58 70 67 26	054 012.0	26	•	•	•	•	•	•	05	01	04	05	C4	14	08	02	14	14	•	•	•	•	•	01	10	
XII 5.3 4.9 4.0 5.1	135.0	05.6	73 57 72 67 25	021 C08.7	13	•	•	•	•	•	•	06	04	07	08	C7	08	06	04	06	04	•	•	•	•	•	01	06	
<b>GOD. 5.7 5.7 4.4 5.6</b>																													
<b>KONIZA</b>																													
<b>BR. ST. 88</b>																													
I 3.7 4.1 3.2 3.6	-	07.1	77 68 76 73 45	138 C45.3	02	•	•	•	•	•	•	14	06	07	07	04	07	•	•	•	•	•	•	•	•	•	01	•	
II 4.6 4.0 4.5 4.3	-	07.3	72 63 74 70 28	101 050.7	23	•	•	•	•	•	•	15	02	07	07	03	07	•	•	•	•	•	•	•	•	•	02	•	
III 2.6 4.3 3.1 3.5	-	07.6	74 66 72 71 49	164 C60.7	05	•	•	•	•	•	•	02	01	12	05	C5	06	05	06	06	06	•	•	•	•	•	02	•	
IV 5.0 4.6 4.2 4.6	-	07.9	68 61 70 66 34	112 055.6	18	•	•	•	•	•	•	04	•	14	09	07	07	04	07	•	•	•	•	•	•	•	•	•	
V 2.5 2.1 2.5 2.4	-	09.0	63 52 66 60 36	056 C19.4	69	•	•	02	•	•	•	13	02	05	05	05	C3	C4	•	•	•	•	•	•	•	•	02	•	
VI 3.0 1.5 2.5 2.5	-	11.9	64 55 68 62 40	054 019.2	11	•	•	15	•	02	02	14	•	04	04	02	04	02	04	•	•	•	•	•	01	•	•	01	•
VII 1.0 1.0 0.5 0.9	-	12.3	53 47 55 52 32	056 006.2	20	•	•	26	11	10	•	05	01	01	01														

M	Vremenski pristupak 2m	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s (0-12)																				
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (dies)							8.	9.	10.	11.	8.	9.	10.	11.	8.	9.	10.	11.	8.	9.	10.	11.			
<i>13°13' N, λ = 16°40' E Grd. AG = + 1h 07 min.</i>																														
I	-	02.4	05.9	04.9	05.5	10.6	01.0	15.6	20	-05.4	15	11	02.2	07	02.7	03	01.0	09	01.7	06	01.5	06	01.5	*	*	04	01.2	47		
II	-	04.9	10.6	06.8	07.3	11.4	03.4	15.4	20	-03.8	09	10	03.4	14	02.9	01	07.0	15	02.5	16	02.4	02	01.5	01	03.0	05	01.2	20		
III	-	05.4	14.5	09.4	09.4	15.4	03.8	25.1	22	-02.5	01	14	02.4	06	03.5	03	01.0	10	02.4	16	02.1	07	02.6	*	*	04	01.2	33		
IV	-	08.7	14.0	09.8	10.6	15.2	06.3	19.4	06	-00.8	21	16	03.0	17	01.3	03	01.0	09	02.9	15	02.3	05	02.8	02	01.5	04	01.5	15		
V	-	12.3	19.1	13.5	14.6	20.0	08.8	26.1	20	04.8	11	11	07.8	09	05.1	01	01.0	08	02.1	07	02.1	14	02.7	01	02.0	06	01.7	36		
VI	-	16.3	22.8	16.9	16.2	24.1	12.9	25.2	04	06.2	13	15	02.5	09	03.2	02	01.5	06	04.0	06	03.7	16	02.1	02	02.0	07	01.9	27		
VII	-	19.4	27.3	20.2	21.5	28.2	14.4	34.8	16	08.8	09	15	02.1	17	02.5	*	*	*	*	*	*	01	03.0	18	01.9	03	03.0	05	01.4	41
VIII	-	19.6	28.9	21.9	22.8	30.1	15.3	35.4	02	05.8	12	08	02.0	07	07.1	*	*	06	01.3	02	01.5	18	01.6	02	01.5	06	02.8	44		
IX	-	14.6	24.2	17.5	18.4	25.3	11.9	30.4	15	02.1	28	10	02.1	09	01.8	*	*	11	02.1	13	01.8	10	01.8	*	*	05	01.8	32		
X	-	04.9	12.7	08.4	09.1	13.9	04.6	17.4	04	-02.3	31	20	01.8	01	07.0	12	02.4	15	01.7	07	02.0	02	01.5	11	01.5	23				
XI	-	06.3	12.0	07.1	07.6	13.1	02.5	19.2	17	-02.1	02	07	04.0	07	04.0	*	*	14	01.6	18	01.4	01	01.0	01	02.0	06	01.5	36		
XII	-	06.3	07.4	02.9	03.4	08.4	-01.8	17.3	04	-10.2	24	19	02.8	19	04.2	02	01.0	04	01.0	09	01.1	*	*	01	01.0	01	01.0	49		
GOD.	-	05.4	17.0	11.6	12.4	18.0	06.9	35.4	02.0	-10.2	24	16	02.5	10.7	03.0	17	01.2	104	02.2	12.3	02.6	104	02.0	13	01.8	64	01.6	403		
<i>43°18' N, λ = 17°01' E Grd. AG = + 1h 08 min.</i>																														
<b>MAKARSKA</b>																														
BR. ST. 92																														
I	-	07.0	11.8	08.0	08.7	12.7	04.8	17.5	20	00.5	15	02	04.5	15	01.3	29	01.3	32	01.1	01	01.0	04	01.2	03	02.7	07	03.6	*		
II	-	09.5	12.9	10.4	10.8	13.8	06.1	17.5	18	02.0	11	09	01	01.0	14	02.0	31	01.4	16	01.1	04	01.2	02	C2.0	*	*	14	03.6	*	
III	-	06.8	14.7	10.9	11.5	15.4	07.4	21.5	26	03.0	11	06	05.0	07	01.3	35	01.2	22	01.4	15	01.2	*	*	01	02.0	03	03.3	04		
IV	-	13.0	15.9	11.5	14.0	17.1	09.4	23.5	30	06.0	25	17	05.2	14	02.6	23	01.2	19	01.4	09	03.1	01	02.0	*	*	01	03.6	08		
V	-	16.8	19.8	17.6	17.6	21.0	12.7	26.0	22	05.5	11	07	03.7	08	02.6	11	01.1	10	02.0	54	01.7	*	*	*	*	02	03.0	05	*	
VI	-	0.8	23.5	20.8	21.5	24.5	16.2	28.5	27	16.0	16	04	01	11	01.7	03	02.0	*	*	52	01.2	*	*	02	03.5	03	05.0	10		
VII	-	1.4	27.4	23.1	24.2	28.2	18.2	34.5	21	11.6	21	09	02.2	17	01.5	37	01.0	11	02.0	09	01.9	16	01.6	03	02.7	11	03.5	15		
VIII	-	1.4	28.7	19.8	25.0	30.0	19.8	35.5	20	16.5	14	01	04.0	16	01.6	27	01.4	19	01.4	16	01.6	07	01.7	12	02.0	20	02.0	08		
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	12.7	19.1	15.1	15.5	20.2	-	36.8	02.0	-	15	04.0	07	03.3	125	03.1	503	03.0	19	03.6	120	03.2	162	03.2	24	02.9	*			
<b>PALAGRUZ</b>																														
BR. ST. 94																														
I	757.0	10.6	11.9	10.7	11.0	12.5	10.0	14.5	01	07.8	28	27	17	02.6	47	02.7	02	02.0	*	*	*	02	02.6	05	01.0	01	01.5	27	02.6	05
II	749.5	10.2	1.1	11.1	11.1	13.4	05.6	15.5	16	06.6	08	05	02.4	10	02.6	05	03.6	42	02.8	*	*	*	01.6	03	01.3	12	02.1	03		
III	751.4	10.4	12.9	11.0	11.3	13.3	05.6	16.6	09	02.6	10	06	02.0	07	01.3	08	01.4	33	02.0	05	01.4	06	01.4	01	01.4	01	01.4	01		
IV	746.7	12.4	14.3	12.7	12.9	15.4	11.2	18.0	26	07.2	18	08	02.5	07	01.4	06	03.7	15	04.2	14	03.7	02	03.0	08	02.8	24	02.4	02		
V	-	150.6	15.6	18.2	19.4	16.1	15.3	23.6	25	10.6	09	06	02.4	03	02.0	04	03.2	13	03.1	13	02.8	08	02.5	12	02.3	06	02.9	06		
VI	-	19.8	22.5	19.8	20.5	23.9	18.1	26.2	28	12.6	13	04	03.0	04	02.5	05	02.5	29	03.4	01	02.0	07	03.4	01	01.0	01	01.0	01		
VII	-	752.6	23.2	26.3	22.6	23.7	27.1	30.7	16	15.0	21	17	02.9	03	01.0	03	01.0	16	02.6	07	03.6	06	02.8	23	03.2	11	03.0	05		
VIII	-	752.2	23.7	27.0	23.9	24.6	27.9	22.0	32.1	05	16.5																			



Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																	
		Tm			Sred. (Dies)		Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21									8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 42^{\circ}40'$ , N $\lambda = 10^{\circ}54'$ , E Gr., AG = + 1h 08 min.																													
I	- 748.9	09.0	10.5	09.4	05.5	11.3	07.5	15.4	20	05.2	15	04	C1.5	14	01.9	12	02.1	23	02.8	*	C2	01.0	*	*	22	C1.8	16		
II	- 742.2	09.5	11.1	09.8	10.0	12.2	08.1	15.8	16	05.4	07	01	C1.0	16	03.4	16	04.5	34	03.7	04	02.8	*	C1	06.0	08	C1.5	12		
III	- 744.5	09.8	12.6	10.7	11.0	13.5	08.5	15.6	21	04.3	03	01	C1.2	12	01.9	10	01.5	28	05.5	01	05.0	01	01.0	01	01.0	28	C2.2	11	
IV	- 741.0	11.8	13.8	11.6	12.2	15.1	09.7	18.9	29	05.0	17	03	C1.3	10	03.1	08	03.0	34	03.4	03	02.7	*	*	01	01.0	24	C1.6	07	
V	- 742.7	15.2	18.0	15.1	15.6	19.3	12.9	24.4	22	05.2	09	01	C1.0	05	02.4	02	03.0	32	02.1	01	01.0	07	02.0	*	*	37	C1.9	08	
VI	- 743.3	19.2	22.5	18.9	19.8	23.7	17.0	27.6	26	11.2	13	02	C0.9	06	01.8	06	02.0	25	02.7	04	01.5	03	03.3	C2	02.0	33	C2.3	05	
VII	- 744.8	23.4	26.5	22.7	23.8	27.9	20.3	33.8	15	15.7	10	05	C2.4	05	02.0	C7	01.9	20	01.7	01	04.0	02	02.5	*	*	35	C2.1	18	
VIII	- 744.4	24.2	27.3	24.2	25.0	29.1	21.7	34.0	05	14.5	29	02	C2.5	01	02.0	08	01.4	16	01.9	C1	03.0	02	01.0	*	*	45	C2.0	18	
GOD.	- 744.3	14.7	17.0	14.8	15.3	18.3	12.9	24.0	05 VM	04.0	15	11	28	C2.0	57	02.6	76	C2.1	330	C2.6	30	02.9	41	01.9	C9	C2.2	355	C2.6	129
$\varphi = 42^{\circ}58'$ , N $\lambda = 17^{\circ}09'$ , E Gr., AG = + 1h 12 min.																									KUKČULA				
I	-	08.7	12.0	09.3	09.6	12.8	06.4	16.9	20	03.1	15	02	C5.5	01	C1.0	23	C4.9	14	01.9	C9	01.1	19	01.3	19	C1.8	05	C3.0	01	
II	-	16.0	12.6	10.6	10.9	13.4	07.8	16.3	20	02.9	09	03	C2.5	04	C5.5	40	C3.1	15	02.1	C7	C1.1	05	C2.0	03	C1.3	*			
III	-	10.6	14.3	11.3	11.9	14.9	05.0	0	18.8	30.5	03.3	05	*	*	C1	05.0	27	03.1	13	01.8	11	01.1	16	01.7	13	C1.8	02	C2.5	*
IV	-	13.4	15.7	12.7	13.6	16.6	09.5	18.9	06	05.4	17	02	C1.0	05	C3.8	38	C2.3	16	02.1	C1	05	09	01.2	15	02.1	05	C2.2	*	
V	-	17.2	19.4	15.6	17.1	20.0	12.5	25.3	21	05.4	26	*	*	C3	03.3	36	C2.4	12	02.1	C3	01.0	06	01.3	17	02.0	06	C1.5	*	
VI	-	21.0	23.4	19.9	21.6	-	16.6	-	-	12.2	15	04	C3.0	01	01.0	39	C2.6	11	02.1	C2	01.5	02	01.5	24	C1.9	06	C2.3	01	
VII	-	24.4	26.5	23.2	24.3	27.4	19.3	32.7	16	16.5	23	05	C1.2	05	C7.4	29	02.1	C9	C6.4	03	01.0	06	01.3	35	C1.8	11	C2.4	*	
VIII	-	25.0	28.1	24.5	25.5	29.5	20.9	34.5	06.0	16.6	12	05	0.0	01.0	26	C2.2	05	C2.0	05	C1.2	13	01.5	25	C1.9	06	C1.5	02		
IX	-	22.0	24.7	21.1	22.2	25.4	18.1	29.7	16	13.0	28	04	C1.8	*	*	*	C3.0	17	02.1	06	01.8	06	01.2	20	C1.8	07	C2.4	*	
X	-	13.5	16.2	13.6	14.1	17.1	10.5	19.7	01	05.4	31	04	02.0	03	02.0	17	02.5	18	01.7	08	01.1	13	01.0	19	C1.7	11	C2.5	*	
XI	-	12.2	14.2	12.2	12.7	15.1	05.4	17.7	07	04.2	02	*	*	C4	03.8	35	02.6	17	01.9	09	01.1	14	01.2	07	01.7	C3	C2.7	01	
XII	-	09.1	12.0	09.7	10.1	12.8	05.5	16.1	04	02.8	17	*	*	C7	02.9	16	02.3	16	01.5	10	01.1	25	01.3	17	01.5	08	C1.8	*	
GOD.	-	15.6	18.3	15.3	16.1	-	12.1	-	-	02.8	07 VM	11	C1.4	39	C3.5	364	C1.7	151	02.0	75	01.2	139	01.2	270	01.4	73	C2.2	05	
$\varphi = 42^{\circ}58'$ , N $\lambda = 17^{\circ}10'$ , E Gr., AG = + 1h 09 min.																									GREBIC				
I	-	07.8	12.6	08.0	09.1	13.1	05.6	17.9	20	00.5	15	27	C1.3	18	07.5	C9	C2.7	12	02.7	*	04	02.0	04	02.5	13	C2.4	06		
II	-	05.5	13.0	05.6	10.3	10.9	07.4	17.5	16	01.0	05	15	C1.5	26	07.7	C5	C2.2	24	02.8	04	02.2	*	C1	03.0	04	C2.0	05		
III	-	05.7	14.6	10.0	11.1	15.1	07.2	15.6	25	03.0	11	01	22	C1.5	13	02.8	C2.7	25	02.8	01	02.0	07	02.6	08	C1.4	09			
IV	-	13.5	15.5	11.7	13.1	16.9	09.5	21.1	06	05.8	17	09	C1.1	24	04.8	C9	C3.1	26	02.8	01	02.5	05	02.4	05	C1.6	05			
V	-	16.7	19.2	15.2	16.5	20.0	12.2	25.9	26	07.5	11	14	C1.6	12	02.4	C5	C2.0	26	02.4	02	C2.0	07	C3.1	11	02.8	07	C1.7	09	
VI	-	20.6	23.2	19.1	20.5	24.1	16.2	27.0	25.20	11.9	14	11	C1.9	19	C2.5	C3	C2.7	28	02.3	01	02.0	04	03.6	11	C3.0	08	C2.1	05	
VII	-	23.9	26.5	21.4	23.3	27.8	18.3	32.0	16	12.2	09	22	C1.4	14	02.6	C2	C3.0	27	02.2	04	01.2	09	02.2	04	C3.1	02	C1.5	09	
VIII	-	24.4	28.7	23.2	24.8	29.5	20.9	35.5	16	15.7	21	06.0	15	07.0	06	C1.8	26	02.2	C3	01.7	07	C5.4	13	02.5	*	*	02		
IX	-	21.3	25.1	20.1	21.7	26.2	17.8	31.4	11	16.6	26	14	C1.3	17	02.9	C4	C2.5	28	02.9	04	02.8	10	02.2	02	C1.8	07			
X	-	12.6	17.0	12.5	15.9	17.6	10.1	20.7	01	05.0	31	26	01.5	08	02.5	*	*	24	03.1	06	C2.3	04	03.0	13	02.5	07	C2.3	*	
XI	-	12.0	14.8	11.4	12.4	15.7	05.1	16.0	17.06	03.8	02	28	C1.3	23	01.7	C7	C3.4	19	03.2	04	01.8	03	C2.3	02	C3.0	02	C1.9	02	
XII	-	08.4	13.0	08.7	07.3	12.3	03.3	17.5	04	-02.0	24.27	41	02.5	05	02.8	C1	03.0	08	02.7	01	01.0	01	01.0	07	01.3	06	01.7	19	
GOD.	-	13.4	18.4	13.4	14.6	19.7	05.4	37.5	05 VM	-03.0	03	263	C2.1	41	02.1	43	02.9	216	C3.2	53	C2.1	30	02.0	80	01.4	78	02.1	291	
$\varphi = 42^{\circ}50'$ , N $\lambda = 17^{\circ}42'$ , E Gr., AG = + 1h 11 min.																									STAKA				
I	-	05.6	11.9	06.4	07.6	12.6	04.8	17.4	21	-02.0	15	42	C1.6	C4	C1.0	C2	C2.5	11	C3.2	04	C1.5	*	*	09	C1.0	01	C1.0	20	
II	-	08.0	12.9																										

Mesec	Udajalost Rm (0-10)				Trsodaj sati	Vlažnost vazduha	Padavine R mm		Broj dana nasa:																					
	7	14	21	Sred. Dnes				Um t	Σ	Max	Min.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡
<b>LASTEVE</b>																										$H_s = 186 \text{ m } H_b = 186.7 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$				
BR. ST-96																														
I 5.6 6.1 7.9 4.7	118.0	06.6	76	71	76	74	39	106	040.1	03	.	.	.	.	.	.	02	.	10	05	10	08	03	10	.	.	.	01	.	
II 6.6 7.6 8.2 5.0	107.7	06.9	76	75	74	39	129	055.4	23	.	.	.	.	.	.	.	08	.	01	07	11	10	04	11	.	.	.	02	04	
III 5.2 5.7 4.4 5.5	160.4	07.3	78	69	72	73	24	086	031.2	05	.	.	.	.	.	.	05	02	09	09	07	04	09	.	.	.	02	01		
IV 5.7 5.7 4.5 5.4	161.9	08.0	76	69	79	75	36	087	036.4	18	.	.	.	.	.	.	05	02	12	16	12	02	16	.	.	.	03	.		
V 4.5 4.4 3.7 2.4	263.6	09.9	77	66	76	73	39	046	018.8	09	.	.	.	.	.	.	03	02	10	07	01	05	.	.	.	05	01			
VI 4.7 3.9 2.5 1.5	294.4	12.6	75	64	76	71	36	225	011.6	19	.	.	.	.	.	.	11	01	08	04	01	06	.	.	.	01	07			
VII 1.9 1.5 1.1 1.5	387.0	12.5	58	49	60	56	29	001	000.5	21	.	.	.	26	01	16	.	23	01	01	.	01	.	.	.	02	.			
VIII 2.5 2.4 1.9 1.3	320.8	14.3	64	55	65	61	19	051	017.1	25	.	.	.	28	13	22	03	18	09	07	03	09	.	.	.	11	.			
IX 3.4 3.2 2.7 2.2	256.8	14.4	80	67	78	75	36	047	030.1	21	.	.	.	14	01	15	05	15	04	08	04	01	08	.	.	.	01	08		
X 6.7 6.1 5.1 6.0	145.9	08.8	76	69	75	73	36	170	044.4	01	.	.	.	.	.	.	07	04	08	21	07	21	.	.	.	01	11			
XI 6.0 5.7 4.0 5.2	107.6	08.2	78	75	76	74	45	052	013.0	01	.	.	.	.	.	.	06	04	05	11	06	01	11	.	.	.	06	.		
XII 5.6 5.1 4.5 5.5	127.9	06.7	74	67	73	71	31	004	003.5	13	.	.	.	.	.	.	02	01	10	02	04	03	04	.	.	.	01	.		
GOD. 4.7 4.6 3.4 4.3	2456.8	09.7	74	65	73	71	19	012	065.8	038	.	.	.	76	21	53	45	03	122	56	118	85	28	116	.	.	.	07	03	
<b>KORČULA</b>																										$H_s = 15 \text{ m } H_b = 15 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$				
BR. ST-97																														
I 5.6 5.2 3.4 4.8	-	06.5	74	63	72	70	37	111	035.0	03	.	.	.	.	.	.	01	.	10	05	12	04	12	.	.	.	02	.		
II 7.8 6.4 5.9 6.7	-	07.1	75	66	74	72	33	222	059.1	04	.	.	.	.	.	.	02	.	01	14	13	11	05	13	.	.	.	04	.	
III 5.6 5.4 4.5 5.2	-	07.6	76	67	74	72	31	086	044.3	03	.	.	.	.	.	.	03	02	07	09	06	03	08	.	.	.	03	01		
IV 5.7 5.8 5.1 5.5	-	04.0	69	61	73	68	34	123	032.7	18	.	.	.	.	.	.	02	01	06	11	17	13	04	17	.	.	.	06	.	
V 5.7 4.7 3.9 4.7	-	10.3	72	62	75	70	41	126	043.6	09	.	.	.	01	.	.	02	.	08	06	11	05	03	11	.	.	.	03	02	
VI 4.9 4.2 3.5 4.1	-	13.5	72	65	75	71	36	063	012.5	30	.	.	.	03	.	.	10	01	10	08	01	10	.	.	.	06	.			
VII 1.9 1.7 1.5 1.7	-	13.1	57	53	58	56	31	006	006.3	20	.	.	.	27	03	11	01	22	01	01	01	.	01	.	.	.	01	.		
VIII 2.6 2.4 2.2 2.4	-	14.6	65	54	61	60	25	034	017.2	25	.	.	.	29	15	20	.	19	04	03	02	02	03	.	.	.	07	.		
IX 4.7 3.9 2.8 3.8	-	14.1	71	60	76	69	33	093	057.6	21	.	.	.	20	.	05	.	14	07	05	02	05	.	.	.	08	.			
X 6.9 7.1 5.5 7.5	-	09.2	78	68	76	74	34	280	045.6	06	.	.	.	07	.	04	13	21	18	12	21	.	.	.	01	01				
XI 6.2 4.1 5.0 5.8	-	08.4	76	71	71	75	38	068	021.3	26	.	.	.	02	.	04	09	12	09	03	12	.	.	.	05	.				
XII 5.3 5.9 3.0 4.7	-	06.4	72	61	70	68	21	016	013.8	13	.	.	.	03	01	06	04	02	01	04	.	.	.	01	.					
GOD. 5.2 4.9 3.9 4.7	-	05.9	71	62	71	68	21	1220	059.1	038	.	.	.	35	15	01	111	85	121	93	40	121	.	.	.	04	01			
<b>CREBIC</b>																										$H_s = 6 \text{ m } H_b = 6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$				
BR. ST-98																														
I 5.7 5.5 3.9 5.0	-	06.1	74	55	74	69	23	13P	038.8	03	.	.	.	.	.	.	10	10	12	10	05	12	.	.	.	02	.			
II 6.1 6.6 6.2 7.0	-	06.8	72	62	76	70	31	229	072.5	04	.	.	.	.	.	.	02	13	12	06	12	12	.	.	.	03	.			
III 4.9 5.4 4.5 4.9	-	07.1	79	61	74	72	31	136	072.9	03	.	.	.	.	.	.	03	09	06	04	05	.	.	.	04	.				
IV 6.5 5.6 5.2 5.4	-	07.9	65	65	75	68	33	116	052.4	18	.	.	.	.	.	.	05	06	16	12	03	16	.	.	.	02	.			
V 5.4 4.6 4.4 4.8	-	10.1	72	63	75	70	23	145	042.3	05	.	.	.	02	.	01	.	06	05	10	09	04	10	.	.	.	04	.		
VI 5.0 4.4 3.8 4.4	-	12.4	65	61	73	66	37	045	014.6	30	.	.	.	14	.	02	.	07	03	01	01	10	.	.	.	02	.			
VII 1.9 2.2 1.6 1.9	-	12.7	57	53	60	57	33	002	002.5	20	.	.	.	28	07	06	.	21	01	01	01	.	.	.	02	.				
VIII 2.5 2.5 2.7 2.6	-	14.0	62	51	63	58	31	038	032.6	24	.	.	.	29	16	15	.	18	06	04	02	06	.	.	.	06	.			
IX 4.8 4.3 3.6 4.2	-	13.6	71	60	75	68	28	103	053.4	21	.	.	.	21	03	05	01	14	07	08	04	02	06	.	.	.	06	.		
X 6.7 6.6 5.8 6.4	-	09.2	79	65	80	74	26	280	039.7	01	.	.	.	04	.	04	13	21	00	11	21	.	.	.	05	.				
XI 6.2 5.5 5.9 5.9	-	08.1	75	67	73	73	41	074	020.6	26	.	.	.	02	.	04	05	12	11	02	12	.	.	.	04	.				
XII 4.8 5.5 3.9 4.8	-	04.1	71	56	71	66	22	019	014.1	13	.	.	.	08	.	04	02	08	03	02	01	02	.	.	.	01	01			
GOD. 5.2 4.9 4.3 4.8	-	04.5	70	62	72	72	28	1335	072.9	038	.	.	.	94	26	28	04	106	81	120	95	42	120	.	.	.	01	35		
<b>DUBROVNIK</b>																										$H_s = 49 \text{ m } H_b = 49 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$				
BR. ST-100																														
I 5.6 5.5 4.5 5.2	-	05.7	60	58	65	61	26	094	037.4																					

Mesec	Vardušni Prilisek mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21								8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	
SR BOSNA I HERZEGOVINA φ = 45°03' N λ = 16°23' E Gr. ΔG = + 1h 06 min.																												
I	-	00.5	04.6	01.4	01.7	05.4	-00.5	15.0	20 -04.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	02.0	04.9	05.6	05.8	11.0	01.2	14.0	12 -05.0	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	07.0	12.9	06.7	07.5	13.9	01.2	26.0	22.21 -03.0	14.02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	04.4	15.0	08.1	08.9	16.1	02.5	24.0	10 -01.0	20.09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.4	19.4	11.6	13.3	20.4	07.9	27.0	27.22 02.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	13.3	21.6	14.5	16.0	22.6	10.4	25.0	26 05.0	13.12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	14.9	25.7	16.9	18.6	27.3	12.4	35.0	13.12 08.0	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	16.5	26.6	18.7	20.1	27.8	14.7	34.0	16.04 06.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	14.5	21.4	14.6	15.8	22.9	10.8	31.0	03 03.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	07.1	11.2	06.0	07.2	12.0	02.9	21.0	20 -03.0	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	02.9	10.3	04.3	05.4	11.3	01.2	21.0	18 -04.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	00.1	06.0	01.1	02.2	07.4	-01.5	14.0	29.27 -05.2	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	07.5	15.4	09.2	10.2	16.6	05.3	35.0	44.0 W -09.2	65.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BOSANSKI NOVI																												
BOSANSKA GUBICA																												
BR. ST.102																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	06.1	14.2	08.7	09.6	15.9	-	21.4	29	-	-	06	02.5	17	02.1	06	02.2	10	01.4	08	01.9	09	01.7	06	02.0	05	02.6	2n
V	-	11.6	19.6	13.0	14.1	20.0	-	26.4	22	-	-	15	01.7	01	01.0	10	02.5	04	01.8	11	01.2	21	01.6	09	01.4	15	01.7	07
VI	-	15.0	22.1	16.0	17.4	23.7	10.4	29.0	26 06.0	12	12	01.0	03	03.0	04	01.8	10	01.6	05	01.5	17	01.9	23	02.0	19	01.2	04	
VII	-	17.0	25.6	18.5	19.9	26.3	12.1	34.0	14 08.0	27	07	02.1	02	01.0	19	01.9	12	01.8	06	01.7	16	01.4	16	01.6	11	01.8	04	
VIII	-	17.9	26.7	19.1	21.0	27.1	14.1	33.0	04 08.2	12	10	02.1	03	01.7	08	02.4	06	02.3	13	01.9	27	01.5	13	01.7	09	02.0	04	
IX	-	12.4	21.3	14.6	15.6	21.9	09.3	30.0	03 02.2	28	07	02.7	02	02.0	13	02.1	07	02.1	05	01.8	06	02.4	04	02.0	13	02.4	36	
X	-	05.3	10.8	06.7	07.4	11.7	07.7	20.5	04 -03.6	31	08	02.6	03	07.0	05	02.4	06	02.3	05	02.4	19	02.1	06	02.0	07	02.4	34	
XI	-	02.9	10.7	04.0	05.3	10.5	06.9	20.5	16 -04.4	02	11	02.4	05	01.7	13	02.7	09	02.1	08	02.0	16	02.1	10	02.5	03	03.3	20	
XII	-	00.6	05.6	01.4	02.3	06.0	-01.0	12.0	29.03 -05.8	23.17	08	02.0	01	04.0	20	02.0	04	02.0	07	02.1	13	01.9	06	02.2	02	04.0	31	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
DERVENTA																												
BR. ST.103																												
I	-	00.3	03.6	01.4	01.7	04.0 -00.1	10.8	20 -05.6	15	+	0	0.2	01.0	*	*	*	*	*	*	*	*	*	*	02	01.0	01	03.0	84
II	-	02.0	10.6	05.7	05.7	11.5	01.0	19.4	12 -04.6	28	+	0	0.4	01.8	06	01.3	*	07	01.0	*	*	*	*	02	04.5	*	*	70
III	-	03.0	11.5	07.0	07.6	14.1	01.2	24.2	19 -04.4	02	+	0	0.4	01.0	10	01.6	01	0.1	01.0	*	01	01.7	*	01.7	04	02.6	74	
IV	-	06.0	15.6	08.9	10.0	16.2	04.7	24.8	29 -02.0	04	01	01.0	*	+	0	0.4	01.5	01	0.1	01.0	*	01	02.0	02	02.0	69		
V	-	12.3	19.8	13.2	14.5	20.5	09.0	27.4	31 04.8	10	01	0.1	01	01.0	C1	01.7	*	*	*	*	*	*	*	*	*	*	*	84
VI	-	16.0	25.5	16.8	17.8	23.5	12.6	30.4	27 07.0	13.12	+	0	0.2	01.0	C3	01.0	01	0.1	01.0	*	*	*	*	*	*	*	*	73
VII	-	17.8	25.0	19.0	20.2	25.7	13.9	34.6	14 08.4	27	07	02.1	02	01.0	C3	01.2	*	*	02	01.0	*	*	02	01.0	*	02	01.0	82
VIII	-	18.0	27.1	19.1	20.8	26.0	12.9	33.2	17 07.0	09	05	01.4	06	02.0	C7	02.4	14	01.8	14	01.6	10	02.1	11	01.5	06	01.3	76	
IX	-	13.3	20.9	15.1	16.1	23.4	11.0	30.0	04 01.6	27	02	0.4	02.0	C2	01.0	05	01.8	11	01.5	09	01.7	08	01.6	07	01.6	36		
X	-	07.4	10.3	06.5	07.1	11.7	02.9	15.4	04 -02.4	31	05	01.2	03	02.7	C1	01.0	21	01.9	12	02.1	17	01.4	10	01.4	05	01.4	19	
XI	-	01.3	10.3	03.6	07.2	11.7	03.1	15.4	17 -03.2	02	04	01.5	07	01.0	C5	03												

Mjesec	Oblačnost Nm (0-10)				Insolacijja Broj sati (Dnev.)	Vlažnost vazduha				Padavine R mm		Broj dana na mjesec																								
						U m s						Tn	Tx	Tn	Tx	Tn	Tx	Tp	F(0-12)	Nm(0-10)	R mm	●	★	▲	▲	▲										
	7	14	21	Sred. Sred. (Dnev.)		mm	7	14	21	Sred. Min.	Max	Dat.	1/1	1/2	1/3	1/4	1/5	1/6	1/7	1/8	1/9	1/10	1/11	1/12	1/13	1/14	1/15									
SRBIJSKA HERCEGOVINA																																				
BR. ST.101		HLSANSKI NOVI												H <sub>b</sub> = 119 m H <sub>b</sub> = ~ m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m																						
I 9.5	7.9	7.6	6.3	-	-	-	-	-	-	059	013.4	01	-	-	14	-	-	-	-	-	19	13	10	01	12	02	C2	-	-	-						
II 6.2	7.1	7.1	-	-	-	054.6	81	72	81	55	034	004.5	02	-	-	06	-	-	-	-	01	11	12	10	01	12	02	-	-	-	26					
III 7.4	6.2	6.5	5.6	-	-	054.6	75	65	72	29	046	014.6	06	-	-	06	02	-	-	-	04	05	07	06	02	07	03	03	-	-	27					
IV 7.8	7.9	7.1	7.3	-	-	064.0	81	56	74	26	057	020.1	14	-	-	04	-	-	-	-	11	14	09	01	14	-	-	-	-	-	28					
V 8.5	6.8	7.0	7.6	-	-	054.7	86	57	82	36	125	036.0	29	-	-	08	-	-	-	-	13	21	16	04	11	-	-	-	-	-	28					
VI 6.7	6.6	6.4	7.3	-	-	094.8	42	56	71	30	019	040.6	07	-	-	12	-	-	-	-	01	15	14	09	03	14	-	-	-	-	-					
VII 7.7	3.8	3.4	4.5	-	-	104.9	73	52	66	42	079	014.4	07	-	-	22	10	-	-	-	04	04	10	07	05	10	-	-	-	-	-	02				
VIII 6.9	4.4	4.1	5.5	-	-	134.0	80	64	76	35	094	024.6	74	-	-	24	15	-	-	-	02	07	10	10	03	10	-	-	-	-	-	25				
IX 9.0	6.1	5.6	6.9	-	-	114.3	88	70	86	50	151	059.8	39	-	-	13	01	-	-	-	07	14	11	06	14	-	-	-	-	-	-					
X 9.3	7.4	6.7	7.8	-	-	064.5	85	77	84	62	272	045.6	06	-	-	02	-	-	-	-	17	20	16	20	01	01	-	-	-	-	-	21				
XI 6.8	6.4	5.9	7.0	-	-	054.6	85	72	82	53	066	017.4	25	-	-	07	-	-	-	-	01	14	12	11	02	14	01	01	-	-	25					
XII 7.5	5.5	5.0	6.3	-	-	044.6	87	76	86	83	47	051	015.0	12	-	-	19	-	-	-	-	01	01	07	02	07	02	-	-	-	-	-	29			
GOD.	8.5	6.3	6.0	6.9	-	-	-	-	-	1122	059.8	390	-	-	60	81	26	-	-	14	134	154	124	37	153	09	04	-	-	-	-	-	-			
HOSANSKA DUBICA		H <sub>b</sub> = 98 m H <sub>b</sub> = ~ m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m												H <sub>b</sub> = 98 m H <sub>b</sub> = ~ m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m																						
BR. ST.102	H <sub>b</sub> = 98 m H <sub>b</sub> = ~ m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m												H <sub>b</sub> = 98 m H <sub>b</sub> = ~ m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m												C1											
I -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
II -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
III -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV 5.7	7.3	5.9	6.6	-	-	064.5	86	55	82	74	28	037	006.5	13	-	-	03	-	-	-	04	13	10	10	-	10	-	-	-	-	-	C1				
V 6.6	6.9	5.0	5.2	-	-	054.8	89	63	98	40	101	016.0	23	-	-	07	-	-	-	04	10	18	16	03	16	-	-	-	-	-	-					
VI 5.1	6.0	6.2	6.5	-	-	114.8	35	62	86	73	40	150	040.6	11	-	-	14	-	-	-	01	07	14	12	05	14	-	-	-	-	-	-				
VII 4.2	4.1	3.5	4.0	-	-	134.6	85	58	67	77	23	006	019.4	20	-	-	07	-	-	-	12	05	08	06	03	08	-	-	-	-	-	-				
VIII 3.9	3.6	3.0	3.7	3.7	-	154.4	91	63	90	81	49	101	024.0	10	-	-	19	12	-	-	16	08	10	10	04	10	-	-	-	-	-	-				
IX 7.4	5.6	4.7	5.9	-	-	115.4	94	67	92	64	44	137	010.6	36	-	-	10	01	-	-	02	02	03	10	12	10	06	12	-	-	01	-	21			
X 6.0	7.7	7.6	7.9	-	-	066.9	71	79	74	88	40	200	034.5	6	-	-	02	-	-	-	01	17	19	17	10	18	-	-	-	-	-	31				
XI 5.7	7.2	5.6	6.7	-	-	064.1	95	77	85	99	37	061	016.7	19	-	-	09	-	-	-	01	16	06	13	01	13	-	-	-	-	-	05				
XII 5.4	7.2	7.2	7.4	-	-	054.3	95	50	97	94	61	144	010.6	1	-	-	01	19	-	-	02	21	11	05	01	11	03	03	-	-	-	-	-	21		
GOD.	6.2	6.4	5.8	6.0	-	084.7	92	65	91	83	17	996	046.0	8	-	01	67	64	22	-	02	01	71	143	147	170	34	145	15	11	-	01	01	12	54	07
BIRAC		BIHAC												H <sub>b</sub> = 246 m H <sub>b</sub> = 250,4 m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m												C7										
I 6.5	7.4	6.4	7.4	-	-	044.8	04.6	94	60	91	88	46	063	026.0	01	-	-	25	-	-	-	03	23	11	09	02	11	01	01	-	-	-	14			
II 5.9	6.4	5.5	6.0	-	-	054.7	85	64	89	83	41	030	049.0	04	-	-	11	-	-	-	06	10	11	07	01	10	01	-	-	-	66					
III 5.1	5.7	6.0	5.6	-	-	054.9	90	58	87	77	20	071	021.6	07	-	-	09	02	-	-	08	12	06	04	05	06	04	-	-	-	-	-	01			
IV 6.5	6.9	6.2	6.2	-	-	064.7	87	50	80	65	28	058	016.6	16	-	-	03	-	-	-	06	11	12	10	02	12	02	-	-	-	-	-	-			
V 5.9	6.0	5.7	6.4	-	-	187.4	68	70	74	68	30	115	078.6	23	-	-	06	-	-	-	01	04	12	19	15	03	15	-	-	-	-	-	07			
VI 5.9	7.7	5.8	6.5	-	-	185.3	09.5	76	55	72	35	115	023.6	11	-	-	07	-	-	-	03	23	19	07	01	23	05	01	-	-	-	61				
VII 4.5	4.6	3.2	4.1	-	-	277.6	11.4	30	50	69	36	091	035.2	20	-	-	23	06	02	05	-	11	05	13	09	03	13	-	-	-	-	-	02			
VIII 5.7	5.8	2.9	4.8	-	-	210.2	13.5	91	62	87	32	148	066.0	23	-	-	18	12	-	04	08	07	11	09	04	11	-	-	-	-						

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Sred. (Cles)			Max	Min	Dat.	Min	Dat.	N		NL		E		SE		S		SW		W		NW			
		7	14	21									E.	J.	E.	J.	S.	J.	E.	J.	S.	J.	E.	J.	S.	J.				
$\Delta t = +1h\ 00\ min$																														
I	44°23'	N	1	16°24'	E	Gra.	ΔG =	+1h 00 min																						
I	723.7	-01.3	05.1	00.7	01.3	05.8	-02.2	13.6	20	-06.0	26	*	*	C1	04.0	*	*	03	02.0	04	02.5	01	02.0	02	02.5	01				
II	716.9	02.6	04.3	04.5	04.9	09.2	00.9	14.2	12	-04.0	09	13	04.2	05	04.3	*	05	03.4	16	03.2	04	03.5	01	03.0	02	02.5	37			
III	715.1	02.3	12.1	06.4	06.8	13.2	01.1	25.0	22	-04.6	14	03	04.6	06	04.9	C1	02.0	02	04.5	06	03.5	07	02.3	01	04.0	16	03.2	45		
IV	716.1	05.1	12.0	07.9	08.3	13.3	03.0	18.0	29	-02.8	20	17	04.5	14	04.7	*	*	05	03.2	09	04.6	05	03.6	02	03.5	40				
V	717.1	04.5	17.8	11.6	12.7	19.0	06.0	24.4	30	06.4	10	07	04.0	05	04.2	02	C1.0	07	03.1	07	03.4	02	04.0	02	03.0	54				
VI	716.0	12.6	19.0	14.7	15.4	21.7	09.7	28.2	05	02.0	13	12	03.4	07	03.7	*	*	05	03.0	02	05.5	09	03.6	02	02.0	51				
VII	720.3	14.0	24.6	17.1	18.2	25.6	10.6	32.8	16	04.1	09	11	03.4	05	04.5	*	*	02	03.5	04	03.4	06	03.0	01	04.0	10	03.2	55		
VIII	720.3	14.2	26.5	17.0	19.0	27.6	11.6	34.4	17	03.8	31	05	04.0	07	04.6	*	*	03	04.3	04	03.8	07	02.7	*	*	02	02.7	63		
IX	715.4	10.0	11.1	13.0	14.6	22.5	08.8	28.2	06.0	06.6	28	05	04.8	02	04.0	*	*	04	03.8	09	04.1	07	03.3	01	04.0	02	03.4	54		
X	715.6	03.5	09.8	04.7	05.6	11.2	01.6	17.8	04	-05.6	31	04	01.2	*	*	02	0.0	02	04.6	05	03.9	02	03.0	06	03.3	63				
XI	720.4	01.6	09.1	03.7	04.6	10.2	00.0	18.4	17	-05.2	02	03	01.8	*	*	*	*	*	04	04.8	11	03.4	*	*	01	03.0	66			
XII	711.6	-01.8	05.2	00.5	01.1	07.0	-03.4	12.6	10	-05.5	29	06	03.3	04	06.0	*	*	*	*	*	*	*	*	*	01	05.0	82			
GOD.	719.1	06.1	14.3	08.6	09.4	15.6	04.0	34.4	07.0	-09.5	94.0	43	14.0	11	04.0	C1	01.0	0	36	03.4	70	03.9	73	03.4	13	03.2	63	03.2	691	
$\Delta t = +1h\ 00\ min$																														
$\Delta t = +1h\ 00\ min$																														
I	-	44°01'	N	1	16°28'	E	Gra.	ΔG =	+1h 00 min																					
I	-	01.4	04.0	-00.8	-01.2	04.1	-03.5	05.5	20	-09.0	15	05	01.0	02	01.5	C1	01.5	*	*	13	02.1	C1	02.0	*	*	07	01.6	52		
II	-	01.9	05.6	02.0	03.1	05.5	-00.2	12.5	17	-05.0	08	03	02.0	12	03.0	12	02.0	*	*	49	03.2	*	*	*	*	*	*	08		
III	-	00.7	05.4	03.5	04.5	09.5	00.2	21.5	22.1	-06.0	14	03	02.5	04	04.0	*	*	*	*	17	02.8	*	*	02	02.0	06	01.8	35		
IV	-	05.4	05.4	05.3	06.1	10.8	01.2	16.5	29.10	-01.5	20	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
V	-	09.5	14.4	09.5	10.8	15.9	05.1	22.0	27	-04.5	10	02	03.0	14	01.1	*	*	*	*	46	02.3	*	*	*	*	*	*	31		
VI	-	13.6	17.6	12.9	14.2	19.3	08.4	24.0	05	01.0	13.12	15	04.5	06	01.7	*	*	*	*	36	02.5	01	04.0	05	02.8	*	*	27		
VII	-	14.9	27.1	15.2	16.0	22.9	09.7	30.0	16	03.5	09	15	01.0	05	01.0	*	*	*	*	22	02.3	*	*	*	*	*	*	46		
VIII	-	15.0	23.6	16.4	17.0	24.3	10.9	36.5	05	02.4	17	14	02.4	05	02.4	*	*	*	*	14	02.0	*	*	*	*	*	*	66		
IX	-	12.1	18.2	12.6	13.9	20.1	08.1	26.0	11	-06.5	27	16	07.0	*	*	*	*	*	*	21	02.3	*	*	02	01.5	*	*	57		
X	-	03.4	06.8	03.2	04.1	09.1	00.1	15.0	04	-06.5	31	01	02.0	*	*	*	*	*	*	01	02.0	15	03.2	*	*	03	02.3	01	02.0	72
XI	-	03.0	07.4	03.6	04.4	08.5	-00.3	-	-	-	20	03	01.0	*	*	*	*	*	*	25	02.4	*	*	*	*	*	*	67		
XII	-	-	-	-	-	-	-	-	-	-	2	03	01.3	*	*	*	*	*	*	22	02.5	*	*	*	*	*	*	59		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\Delta t = +1h\ 00\ min$																														
$\Delta t = +1h\ 00\ min$																														
I	-	44°46'	N	1	16°12'	E	Gra.	ΔG =	+1h 00 min																					
I	-	00.1	05.1	01.4	02.1	05.8	-06.4	14.0	20	-04.0	22	06	01.7	C4	01.5	02	01.0	01	02.0	02	02.0	05	01.4	06	01.7	08	01.9	59		
II	-	02.4	09.9	05.7	05.9	11.1	01.3	15.0	12	-04.0	09	10	01.3	01	02.0	05	04.5	05	02.4	C3	02.3	03	02.3	10	02.1	36				
III	-	03.5	12.6	07.0	07.5	13.4	02.1	24.8	22	-04.4	02	04	02.2	06	02.0	C1	02.0	03	02.3	06	02.7	05	03.0	10	01.4	09	02.3	44		
IV	-	05.0	14.1	08.0	08.8	19.5	04.6	23.0	29	-01.6	20.0	09	02.6	08	02.4	02	02.0	01	02.0	04	02.5	03	02.2	05	02.2	50				
V	-	11.7	19.2	11.9	13.5	20.8	07.7	26.7	31	06.8	10	03	01.0	07	01.1	C3	02.3	08	07.1	08	03.2	02	01.5	12	02.2	46				
VI	-	14.8	27.1	15.9	17.2	24.3	10.8	30.4	27	01.6	12	05	02.6	02	02.0	C1	01.3	*	*	05	02.4	16	02.5	07	01.9	16	02.5	42		
VII	-	15.8	25.7	17.4	19.1	26.1	11.9	35.2	17	06.7	09	03	02.0	04	02.5	03	02.3	04	01.2	02	02.5	07	01.7	10	01.8	55				
VIII	-	16.2	26.6	18.4	19.5	27.7	12.7	33.0	04	03.6	12	14	01.6	04	02.8	C5	02.0	07	02.3	04	01.8	02	03.0	08	01.6	06	01.8	58		
IX	-	13.3	22.0	15.3	16.5	23.0	14.0	36.8	03	04.7	27	08	03.5	C1	01.0	01	03.0	04	02.2	04	01.2	04	02.5	09	02.1	06	01.5	50		

Meseč	Oblačnost Nm (0-10)				Insolacija broj sati em mm	Vlažnost vazduha				Padavine mm				Broj dana na sat															
	7	14	21	Sred. (Dnev.)		7	14	21	Sum. Min	Σ	Mx	Dat.	Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	▲	▲
						mm	mm	mm	mm	mm	mm	mm	≤	<	≤	>	≤	>	≤	>	•	Δ	*	Δ	▲	▲	▲	▲	
DRVAR																													
BR. ST.106																													
I 8.0 6.8 6.0 6.9	-	04.5 96 75 93 88 49	068 023.8	01	•	01	25	•	•	•	•	•	01	15	11	09	02	11	03	02	•	•	•	•	•	14	05		
II 8.5 7.8 6.0 7.4	-	05.2 90 65 83 79 48	067 028.4	07	•	•	08	•	•	•	10	03	02	14	11	09	02	11	02	01	•	•	•	•	•	01	01		
III 6.7 7.0 4.5 6.1	-	05.3 88 57 75 73 20	036 011.4	06	•	•	11	01	•	•	07	03	02	11	07	06	01	07	02	•	•	•	•	•	01	02			
IV 5.8 8.0 6.1 6.7	-	05.6 82 55 70 69 35	050 009.8	14	•	•	08	•	•	•	10	02	03	13	12	10	•	12	02	01	•	•	•	•	•	01	02		
V 6.4 7.9 4.0 6.1	-	08.1 89 55 79 74 36	161 044.7	25	•	•	01	•	•	•	03	03	03	10	18	13	07	18	•	•	•	•	•	01	04	02			
VI 6.5 7.6 5.1 6.4	-	10.0 88 60 81 76 36	176 051.5	11	•	•	06	•	•	•	05	05	02	11	15	13	05	15	•	•	•	•	•	03	04	•			
VII 4.7 4.6 2.7 4.0	-	11.2 86 52 78 72 35	043 024.4	20	•	•	22	07	•	•	04	04	11	66	05	05	03	05	•	•	•	•	•	03	04	•			
VIII 4.5 5.1 2.0 3.8	-	12.8 96 52 88 79 27	074 022.8	24	•	•	20	15	•	•	02	01	10	04	11	10	03	11	•	•	•	•	•	13	08	•			
IX 7.6 5.7 3.5 5.6	-	10.6 97 63 93 84 41	180 039.8	30	•	•	15	•	•	•	01	01	05	08	12	10	06	12	•	•	•	•	•	07	14	•			
X 8.2 7.9 6.2 7.4	-	06.1 95 74 94 88 43	299 058.6	06	•	•	06	•	•	•	05	02	03	16	22	19	10	22	03	02	•	•	•	07	06	01			
XI 8.5 8.0 5.1 7.2	-	05.7 96 73 93 87 53	070 017.8	26	•	•	13	•	•	•	03	03	01	12	09	08	03	09	02	01	•	•	•	•	•	08	04		
XII 7.4 5.4 4.0 5.6	-	04.4 93 74 91 86 55	042 015.2	13	•	•	28	•	•	•	05	03	03	09	07	06	02	06	03	02	•	•	•	•	•	11	06		
GOD. 6.9 6.8 4.6 6.1	-	07.5 91 62 84 79 20	1306 058.6	06x	•	01	99	65	22	•	55	30	44	129	140	118	44	139	17	09	•	•	01	01	45	77	18		
DRINIĆ																													
BR. ST.107																													
I 5.4 6.7 4.6 5.6	-	04.2 91 86 91 89 63	065 025.0	20	•	04	30	•	•	•	•	•	06	09	08	03	06	07	01	•	01	•	•	•	06	31	•		
II 7.7 7.9 7.3 7.6	-	05.1 89 82 87 86 58	059 016.0	04	•	01	15	•	•	•	03	•	01	15	12	11	02	08	06	•	•	•	•	•	05	09	•		
III 6.3 7.9 6.1 6.8	-	05.1 86 66 87 80 27	043 019.3	06	•	01	15	•	•	•	01	•	02	15	07	07	01	03	05	•	•	•	•	•	04	10	•		
IV 6.5 8.3 6.5 7.1	-	06.5 84 87 88 86 62	071 029.0	14	•	•	14	•	•	•	03	13	11	11	02	08	05	01	•	•	•	•	•	01	04	•			
V 7.0 7.6 6.6 7.1	-	08.9 87 87 89 87 52	142 040.0	25	•	•	01	•	•	•	01	•	•	16	15	13	03	16	16	01	•	01	•	•	05	•	•		
VI 5.8 8.3 6.4 6.8	-	11.6 87 89 88 88 69	156 072.6	11	•	•	01	•	•	•	01	13	13	10	05	13	•	•	•	•	•	•	•	07	•	•			
VII 4.1 5.2 3.1 4.1	-	13.9 87 89 88 88 67	084 044.0	20	•	•	13	01	•	•	10	06	07	05	04	07	•	•	•	•	•	•	•	02	•	•			
VIII 3.0 5.0 3.7 3.9	-	- - - - -	132 031.1	24	•	•	16	03	•	•	14	05	12	11	05	12	•	•	•	•	•	•	•	01	08	•			
IX 5.2 5.8 5.5 5.5	-	11.5 91 90 91 91 79	169 044.9	30	•	•	01	04	•	•	07	05	10	10	06	10	•	•	•	•	•	•	•	03	03	•			
X 6.8 7.6 6.0 6.8	-	05.9 89 89 91 90 62	363 079.0	06	•	•	16	•	•	•	01	05	15	19	18	18	17	07	01	•	•	•	•	02	02	09			
XI 7.5 6.9 4.8 6.4	-	05.7 87 87 85 87 -	083 029.4	26	-	-	-	-	-	-	01	06	12	09	08	05	05	07	•	•	•	•	•	04	13	•			
XII 5.4 5.5 5.8 5.6	-	- - - - -	052 018.2	13	-	-	-	-	-	-	08	10	07	02	03	07	01	•	•	•	•	•	•	•	•	24			
GOD. 5.9 6.9 5.5 6.1	-	- - - - -	1421 079.0	06x	-	-	-	-	-	-	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
SANSKI MOST																													
BR. ST.108																													
I 9.3 8.1 6.9 8.1	043.5 04.9 96 81 95 91 56	C63 015.0	20	•	•	18	•	•	•	01	•	21	16	10	02	16	01	01	•	•	•	•	•	14	•	•			
II 6.8 7.9 6.2 7.0	085.9 05.5 93 64 84 81 34	041 006.7	04	•	•	10	•	•	•	02	01	02	13	17	12	•	17	02	01	•	•	•	•	06	•	•			
III 7.9 7.7 6.1 7.2	102.5 05.8 91 59 82 77 23	040 014.2	06	•	•	06	•	•	•	02	01	05	10	07	01	09	04	02	•	•	•	•	•	02	03	01			
IV 6.4 7.7 6.4 6.8	134.1 06.1 06.2 92 50 82 75 22	060 020.6	14	•	•	08	•	•	•	03	15	13	12	03	13	01	01	02	01	•	•	•	•	•	02	01			
V 6.5 6.6 5.1 6.1	192.1 09.0 87 55 89 77 31	108 030.3	23	•	•	06	•	•	•	04	01	03	09	17	14	03	17	•	•	•	•	•	04	•	•				
VI 5.9 7.2 5.7 6.3	191.1 11.1 85 57 84 75 38	125 050.1	11	•	•	11	02	•	•	02	01	02	08	13	10	03	13	•	•	•	•	•	04	02	•				
VII 5.4 4.5 3.2 4.3	273.4 12.7 84 54 87 76 28	088 029.5	20	•	•	22	09	•	•	02	09	06	11	06	03	11	01	03	09	•	•	•	•	03	12	•			
VIII 7.4 4.8 3.3 5.2	225.1 14.5 95 59 92 82 42	118 026.7	23	•	•	23	13	•	•	02	05	07	10	09	04	10	•	•	•	•	•	•	•	08	12	•			
IX 8.6 5.6 4.7 6.3	147.9 11.4 97 63 92 84 39	116 034.2	30	•	•	10	02	•	•	02	01	02	09	16	11	05	14	•	•	•	•	•	02	15	•				
X 8.5 7.8 6.2 7.5	081.3 06.3 92 69 91 84 36	293 061.5	04	•	•	06	•	•	•	01	01	•	16	21	18	18	20	04	03	•	•	•	03	07	02				
XI 8.0 7.0 5.4 6.8	079.1 05.8 93 69 90 84 35	077 021.0	29	•	•	10	•	•	•	02	02	03	12	14	10	02	14	02	01	•	•	•	•	09	13	•			
XII 7.5 6.6 5.6 6.6	078.6 04.9 93 74 91 86 53	066 021.5	13	•	•	23	•	•	•	01	01	02	12	12	08	02	10	05	02	•	•	•	•	09	08	•			
GOD. 7.4 6.8 5.4 6.5 6.5	-	08.2 92 61 87 80 21	1084 054.0	06x	•	•	59	72	22	•	86	17	36	133	130	118	36	128	11	07	•	•	•	07	119	07			
MLINISTE																													
BR. ST.110																													
I 7.6 7.6 8.1 7.8	-	03.5 74 74 75 74 56	069 016.4	19	•	07	28	•	•	•	•	•	18	07	07	03	03	04	01	•	•	•	•	•	11	31	•		
II 8.2 8.1 8.0 8.1	-	03.6 75 69 77 53 20	073 015.8	05	•	07	22	•	•	•	02	•	17	09	08	03	05	06	02	•	•	•	•	•	09	26	•		
III 7.2 7.9 8.0 7.7	-	04.0 68 61 71 66 2*	032 009.5	06	•	09	15	•	•	•	01	•	01	18	07	06	04	03	•	•	•	•	•	15	19	•			
IV 7.3 7.9 8.1 7.8	-	04.2 73 61 75 70 1	04 018.6	18	•	03	13	•	•	02	01	19	13	13	05	10	05	•	•	•	•	•	01	11	09	•			
V 7.6 7.7 7.7 7.8	-	06.1 72 6																											

Mjesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova ND, fm (0-12)																	
		Tm			Sred. (Dnev.)	Max.	Min.	Max.	Min.	Dat.	Min.	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21									E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\varphi = 44^{\circ}03' \quad N \quad \lambda = 16^{\circ}52' \quad E \quad Gr. \Delta t = +1h 07 min.$														GLAMCO												BR. ST. 111			
I	-	-01.3	04.1	-00.5	00.4	05.6	-04.4	05.2	30.12	-11.0	11	52	C1.0	.	.	.	.	01	07.0	03	05.7	03	02.3	19	03.2	15			
II	-	01.0	04.6	01.0	01.9	06.3	-01.7	11.2	17	-08.0	25	46	C1.5	06	01.3	.	.	03	07.0	01	07.0	.	.	28	01.9	.			
III	-	04.4	16.1	05.0	06.1	11.5	00.8	22.6	22	-06.2	08	50	C1.3	12	01.5	.	.	.	.	03	07.0	.	.	26	C2.2	.			
IV	-	09.4	09.6	04.4	05.7	10.9	01.5	17.2	30	-04.2	17	59	C1.6	.	.	.	.	.	.	.	.	09	03.0	22	03.0	.			
V	-	05.9	14.8	04.6	10.5	16.6	05.0	24.6	30	06.8	15	49	C1.3	09	01.4	.	.	.	.	.	.	.	.	25	02.0	.			
VI	-	15.3	17.1	14.2	14.4	19.9	07.	25.4	05	03.6	12	52	C1.1	03	02.7	.	.	.	.	.	.	.	02	07.0	33	07.3	.		
VII	-	11.5	17.1	16.1	17.8	23.4	16.1	31.2	16	03.6	22	40	C1.7	.	.	.	.	.	.	.	.	01	01.0	12	C2.7	.			
VIII	-	17.0	19.1	17.1	19.0	25.2	10.1	31.8	04	03.8	11	64	C1.4	04	01.5	.	.	.	.	.	.	.	.	25	C2.5	.			
IX	-	12.0	19.8	13.7	14.2	21.1	06.0	26.8	03	06.4	26	46	C1.3	.	.	.	.	.	.	.	.	01	07.0	43	03.6	.			
X	-	03.4	07.7	03.6	04.5	06.6	00.2	13.2	06	-07.4	31	30	C1.6	.	.	.	.	.	.	.	.	01	01.0	52	C2.2	.			
XI	-	05.4	10.1	06.7	01.7	05.5	-02.5	16.4	17	-14.6	29	14	C1.4	01	02.5	.	.	.	.	.	.	.	03	01.0	39	03.2	32		
XII	-	08.5	10.1	-05.4	-04.1	C1.4	-05.7	04.0	04	-18.0	23	55	C1.7	.	.	.	.	01	01.0	01	01.0	.	.	36	C3.3	.			
GOD.	-	10.2	11.7	05.6	07.7	13.1	02.0	31.8	04	VM -16.0	23	61	C1.4	36	02.4	.	.	03	07.0	03	05.0	07	05.6	20	03.0	362	02.7	47	
$\varphi = 44^{\circ}11' \quad N \quad \lambda = 17^{\circ}14' \quad E \quad Gr. \Delta t = +1h 09 min.$														BANJA LUKA												BR. ST. 112			
I	17.6	00.1	04.1	01.1	01.8	04.8	-00.8	11.0	20	-04.9	13	28	C1.3	24	01.3	C1	C2.0	02	C1.0	02	01.5	04	C1.8	04	C1.0	30			
II	19.6	0.1	15.1	06.1	06.4	11.3	01.6	15.1	17	-04.0	09	13	C1.6	17	01.9	C1	C2.2	02	C2.0	10	03.7	05	C2.0	07	C2.0	22			
III	17.9	0.0	0.1	17.2	17.4	07.4	07.5	13.5	01.1	24.4	19	03.9	02	01.9	26	02.0	C1.3	.	04	03.2	01	01.0	06	02.2	05	C3.0	24		
IV	17.4	0.7	14.1	15.1	08.7	09.4	15.7	05.3	22.7	29	-06.9	04	19	C2.2	18	07.6	04	C1.0	05	01.0	01	02.0	01	01.0	11	C1.1	21		
V	17.0	11.9	19.9	15.1	14.4	10.5	08.3	27.4	31	03.2	10	16	C1.7	C1	C1.0	14	C1.9	03	01.7	10	01.6	06	03.5	14	C2.3	03	C2.7	25	
VI	17.0	15.1	15.7	17.4	17.6	18.1	23.8	11.8	31.2	27	04.9	12	18	C1.1	10	01.9	C2.4	08	01.4	09	01.3	05	03.0	11	C1.8	10	C1.8	14	
VII	17.0	17.4	15.5	18.0	20.1	26.4	13.0	34.2	17	06.0	27	11	C1.1	15	01.9	C1.9	C1.9	13	01.8	06	01.3	03	01.7	08	02.1	02	C2.5	26	
VIII	17.0	19.9	17.1	19.3	20.7	27.4	14.1	33.4	04	07.7	12	07	C1.1	13	01.2	C2.5	07	01.1	05	01.8	.	.	04	02.0	04	C2.0	40		
IX	17.8	21.0	14.9	16.1	22.6	11.0	30.8	03	03.2	28	69	C1.4	14	01.1	C7	C2.0	02	01.6	07	01.9	01	01.0	06	02.6	07	C1.6	37		
X	17.5	19.8	11.3	06.5	07.3	12.8	02.8	22.0	04	-07.6	31	10	C1.3	10	01.7	C5	C2.2	02	01.5	15	02.5	15	02.0	02	C2.0	35			
XI	17.0	20.9	10.6	04.7	11.3	01.1	21.8	16	-04.1	29	18	C1.5	17	01.2	C5	C1.0	01	01.0	08	01.6	06	C2.8	05	01.6	04	C1.5	32		
XII	17.0	21.1	01.0	07.7	02.9	03.8	00.8	-06.9	15.4	29	-06.1	24	11	C1.5	14	01.4	C4	C1.5	05	01.2	10	01.2	08	02.1	02	01.5	04	C1.2	35
GOD.	17.0	18.4	08.1	15.6	10.1	11.0	16.6	05.6	36.2	17	VM -06.1	24	69	C1.9	C17	C1.8	C2.0	50	01.4	78	01.7	51	02.7	93	02.4	63	341		
$\varphi = 44^{\circ}21' \quad N \quad \lambda = 17^{\circ}16' \quad E \quad Gr. \Delta t = +1h 09 min.$														JAJCE												BR. ST. 113			
I	-	-06.2	-97.7	05.0	-65.7	04.6	-01.4	11.4	31	-05.2	27	*	*	*	*	C1	C1	02.0	.	*	03	02.7	C5	01.2	01	C2.0	82		
II	-	01.6	09.1	05.0	05.2	10.1	00.5	17.0	18	-04.6	10	06	C5.2	C5	01.0	13	C2.7	C2	01.0	02	07.0	02	02.0	02	03.0	47			
III	-	03.1	12.5	07.4	07.7	13.5	07.1	24.8	22	21	-03.2	02	02	C3.5	C2	01.6	17	C2.8	02	02.0	01	03.0	04	C1.0	64				
IV	-	05.1	17.9	09.0	08.6	14.1	03.1	27.8	29	-01.4	21	02	C4.0	C0	03.0	C6	C3.3	*	*	03	03.0	07	C4.4	06	C2.8	01	03.0	63	
V	-	10.2	19.3	13.0	13.1	19.5	07.3	26.4	31	02.6	10	04	C5.0	C1	01.0	C6	C3.0	01	02.7	03	02.0	10	01.9	01	03.0	64			
VI	-	13.6	21.0	15.5	16.7	22.6	11.0	28.0	28	05	05.2	13	02	C3.0	C8	C4.2	07	C2.7	02	02.0	09	C2.1	*	*	55				
VII	-	15.5	24.9	18.0	19.1	25.5	12.1	34.8	16	07.8	09	*	*	*	*	C6	C2.6	03	03.0	03	01.7	14	C2.1	*	*	59			
VIII	-	15.0	23.6	18.0	19.7	27.1	13.4	33.0	03	07.8	12	04	C2.7	C7	02.1	01	01.6	05	02.0	04	01.5	03	C1.0	61					
IX	-	12.0	11.7	07.4	16.0	22.1	11.2	30.2	04	C1.6	28	07	C2.4	C4	01.8	10	C2.9	C3	02.0	02	02.0	04	01.5	03	C1.0	61			
X	-	04.7	10.6	04.6	04.6	11.8	03.0	14.6	04	-03.0	31	01	C5.0	C4	01.7	10	C3.4	04	02.5	C1	04.0	03	02.0	02	C2.0	65			
XI	-	07.2	19.1	04.2	05.0	04.1	01.1	19.0	16	-02.2	30	01	C1.5	C3	01.5	05	C2.2	*	*	01	02.0	04	02.8	02	03.5	*	73		
XII	-	-0.1	0.1	0.1	-0.1	0.1	0.1	0.1	0.1	-0.1	24	*	*	*	*	C5	C3.2	01	04.0	04	04.0	12	C1.9	01	01.0	*	*	70	
GOD.	-	07.0	17.1	09.1	-79.1	15.5	05.1	34.8	46	VM -09.4	24</td																		

Meseč	Oblačnost Nm (0-10)	Temperatura Ljeto sati Srednje vrijednosti	Precipitacija Ljeto sati Srednje vrijednosti	Vlažnost vazduha		Podzemne vode mm	Projekti podzemnih voda																							
				m	mm		7	14	21	24	Min	Max	7	14	21	24	Min	Max	7	14	21	24	Min	Max	7	14	21	24	Min	Max
				7	14	21	24	Min	Max	7	14	21	24	Min	Max	7	14	21	24	Min	Max	7	14	21	24	Min	Max			
<b>BR. 51-111</b>																														
<b>GRAD C</b>																														
I 4.2 4.3 4.2 4.3	-	04.0 17 22 27 28 55	145 027.6	20	61	27	*	*	*	03	*	13	09	09	06	06	04	01	*	*	*	*	*	*	*	*	*	*	*	02
II 4.2 4.3 4.2 4.3	-	04.0 13 20 21 29	134 029.4	20	*	04	16	*	*	04	*	12	10	10	06	16	04	01	*	*	*	*	*	*	*	*	*	*	10	
III 3.1 3.2 3.3 3.2	-	05.5 15 25 23 35	137 023.8	05	*	10	*	*	*	04	*	16	06	06	01	05	02	*	*	*	*	*	*	*	*	*	*	*	01	02
IV 4.2 4.2 4.2 4.3	-	05.1 17 26 25 35	041 016.0	19	*	07	*	*	*	03	*	12	09	15	11	01	12	03	*	*	*	*	*	*	*	*	*	*	*	02
V 4.0 4.0 4.3 4.2	-	05.0 17 26 28 33	125 016.0	21	*	*	*	*	*	*	*	12	04	19	16	05	19	*	*	*	*	*	*	*	*	*	*	*	*	*
VI 5.0 5.0 4.5 4.3	-	07.4 20 55 58 58	203 015.6	11	*	*	01	*	*	01	*	11	05	14	10	02	14	*	*	*	*	*	*	*	*	*	*	*	*	
VII 3.1 3.2 3.8 2.2	-	09.4 15 55 61 58	027 033.7	06	*	*	15	01	*	*	02	04	06	06	01	08	*	*	*	*	*	*	*	*	*	*	*	*	*	
VIII 3.3 3.3 4.1 3.4	-	06.9 20 54 55 54	051 004.6	19	*	*	14	07	*	*	03	16	09	11	10	11	01	*	*	*	*	*	*	*	*	*	*	*	*	
IX 4.0 4.0 4.0 4.0	-	09.1 70 69 69 70	197 036.4	27	*	*	07	*	*	06	*	12	11	12	11	06	15	*	*	*	*	*	*	*	*	*	*	*	*	
X 7.2 7.2 7.2 7.2	-	05.4 22 20 20 20	302 076.0	01	*	01	16	*	*	03	*	05	10	20	19	06	18	01	02	*	*	*	*	*	*	*	*	*	*	
XI 5.7 5.7 5.5 5.5	-	04.3 7.2 25 20 22	036 019.8	06	03	04	10	*	*	04	*	07	12	19	09	06	07	04	*	*	*	*	*	*	*	*	*	*	01	
XII 5.7 5.7 5.7 5.7	-	02.5 60 71 63 63	061 017.0	15	16	31	*	*	04	*	06	13	07	07	02	03	04	*	*	*	*	*	*	*	*	*	*	*	*	
GDH 4.0 4.0 4.0 4.0	-	06.1 69 69 69 69	- 14.5 100.0	050	15	21	03	35	07	*	152	167	143	122	44	126	07	06	*	*	*	*	*	*	*	*	*	*	01	
<b>BR. 51-112</b>																														
<b>HAKJA LUKA</b>																														
I 8.7 7.0 6.0 6.3	026.5	04.7 9.2 8.9 6.6	078 021.6	20	*	*	09	*	*	01	*	01	21	14	10	03	16	*	*	*	*	*	*	*	*	*	*	07		
II 7.9 7.9 6.9 6.8	078.0	05.5 8.9 6.6 7.8	030 040.4	04	*	*	06	*	*	02	02	03	13	15	10	*	16	02	*	*	*	*	*	*	*	*	*	*	02	
III 7.6 7.6 6.7 7.0	162.5	05.9 9.9 6.1 7.6	030 013.6	01	*	*	09	*	*	01	*	02	13	09	05	02	04	*	*	*	*	*	*	*	*	*	*	*	01	
IV 7.6 7.6 6.6 6.7	127.7	06.1 8.1 50 73	030 074.6	18	*	*	07	*	*	01	*	03	12	15	10	02	15	*	*	*	*	*	*	*	*	*	*	*	06	
V 6.3 7.0 6.0 6.4	177.2	08.6 8.5 52 40	113 031.6	25	*	*	06	*	*	06	*	01	01	11	21	12	04	21	*	*	*	*	*	*	*	*	*	*	05	
VI 5.6 5.6 5.6 5.6	106.7	10.5 8.0 53 77	104 042.6	11	*	*	13	07	*	07	*	05	10	13	09	05	15	*	*	*	*	*	*	*	*	*	*	*	03	
VII 5.7 5.7 5.7 5.7	175.0	12.5 7.8 70 70	115 046.1	20	*	*	21	05	*	05	*	11	07	11	08	01	14	*	*	*	*	*	*	*	*	*	*	04		
VIII 5.7 5.7 5.7 5.7	125.4	14.4 50 50 56	101 015.4	23	*	*	20	13	*	07	*	13	05	11	10	05	11	*	*	*	*	*	*	*	*	*	*	03		
IX 5.6 5.6 5.7 5.7	162.0	11.5 9.5 62 62	136 027.0	30	*	*	06	01	*	01	*	08	18	13	10	06	14	*	*	*	*	*	*	*	*	*	*	11		
X 5.6 5.6 5.6 5.6	105.7	06.5 5.5 68 61	026 056.2	06	*	*	03	*	*	05	01	03	16	21	17	01	02	05	*	*	*	*	*	*	*	*	*	10		
XI 5.6 5.6 5.6 5.6	105.2	05.8 9.6 60 91	026 022.5	29	*	*	10	*	*	01	*	01	04	13	13	04	12	02	*	*	*	*	*	*	*	*	*	09		
XII 5.6 5.6 5.6 5.6	035.7	05.0 65 61 88 82	026 015.1	19	*	*	19	*	*	02	*	03	14	10	09	02	08	*	*	*	*	*	*	*	*	*	*	12		
GDH 6.3 6.3 6.3 6.4	146.6	07.3 6.3 61 61	071 013.2	06	*	*	74	01	*	02	*	22	03	57	143	166	121	41	06	07	*	*	*	*	*	*	*	*	23	
<b>BR. 51-113</b>																														
<b>JAJUJ</b>																														
I 7.2 7.2 7.2 7.2	04.7	04.7 9.2 7.2 7.2	04.7 021.6	20	*	*	21	*	*	*	*	14	16	09	02	06	01	*	*	*	*	*	*	*	*	*	*	*	02	
II 7.2 7.2 7.2 7.2	04.5 4	04.5 9.2 7.2 7.2	05.7 019.3	04	*	*	12	*	*	01	*	01	13	05	03	03	02	*	*	*	*	*	*	*	*	*	*	*	01	
III 7.2 7.2 7.2 7.2	105.9	05.7 9.2 7.2 7.2	015 005.0	06	*	*	11	*	*	01	*	02	15	08	06	04	01	*	*	*	*	*	*	*	*	*	*	01		
IV 7.2 7.2 7.2 7.2	125.1	05.7 7.2 7.2 7.2	030 066.5	18	*	*	03	*	*	01	*	02	14	08	*	14	02	02	*	*	*	*	*	*	*	*	*	06		
V 7.2 7.2 7.2 7.2	177.1	08.5 7.2 7.2 7.2	117 024.0	22	*	*	06	*	*	06	*	01	15	15	02	10	01	*	*	*	*	*	*	*	*	*	*	05		
VI 7.2 7.2 7.2 7.2	160.3	11.0 9.3 7.2 7.2	126 040.4	07	*	*	05	*	*	01	*	01	15	04	02	04	01	*	*	*	*	*	*	*	*	*	*	07		
VII 7.2 7.2 7.2 7.2	144.7	12.7 9.2 7.2 7.2	126 020.0	20	*	*	16	*	*	05	*	05	17	09	04	06	02	*	*	*	*	*	*	*	*	*	*	03		
VIII 7.2 7.2 7.2 7.2	144.7	12.7 9.2 7.2 7.2	126 020.0	20	*	*	16	*	*	05	*	05	17	09	04	06	02	*	*	*	*	*	*	*	*	*	*	03		
IX 7.2 7.2 7.2 7.2	177.1	11.5 9.2 7.2 7.2	117 019.4	28	*	*	15	*	*	05	*	05	17	09	04	06	02	*	*	*	*	*	*	*	*	*	*	03		
X 7.2 7.2 7.2 7.2	162.0	11.5 9.2 7.2 7.2	117 019.4	21	*	*	17	*	*	05	*	05	17	09	04	06	02	*	*	*	*	*	*	*	*	*	*	03		
XI 7.2 7.2 7.2 7.2	144.7	12.7 9.2 7.2 7.2	126 020.0	26	*	*	23	*	*	05	*	05																		





Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetroa mD, Pm (0-12)																
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. (Dies)							8.	15.	22.	Dat.	8.	15.	22.	Dat.	8.	15.	22.	Dat.	8.	15.	22.	Dat.	
$\varphi = 44^{\circ}44'$ N $\lambda = 18^{\circ}06'$ E Gr. $\Delta G = +1h\ 12\ min.$																												
I	-	00.3	05.0	01.6	02.1	05.4	-00.4	11.2	31.27	-04.8	27	.	.	02	01.0	C8	01.6	C7	01.7	03	C1.0	08	01.1	12	01.6	02	C1.5	51
II	-	02.8	10.9	05.4	06.1	11.8	01.6	19.2	12	-04.2	28	01	C2.0	03	02.0	06	01.7	C4	02.2	07	02.3	11	01.4	09	01.2	02	C1.5	41
III	-	03.5	13.9	07.7	08.2	14.4	02.0	26.8	19	-03.4	02	02	01.0	10	01.7	13	02.6	08	01.6	02	01.0	01	01.0	02	01.0	08	01.9	47
IV	-	06.3	14.8	08.6	09.7	16.1	03.9	24.8	28	-01.2	04	02	C1.0	10	01.2	C1	03.0	03	02.3	05	01.8	01	02.0	08	02.0	57		
V	-	11.0	19.1	12.7	14.0	20.0	08.8	28.0	31	01.7	10	.	.	06	01.8	C3	C1.3	05	01.6	04	02.5	11	02.1	12	01.8	03	03.0	49
VI	-	15.3	22.3	16.5	17.6	23.5	12.3	30.5	27	04.5	13	03	C2.7	C2	01.5	02	02.0	10	01.4	06	01.5	26	02.0	06	02.2	39		
VII	-	16.8	24.9	18.6	19.7	26.3	13.6	36.5	17	06.8	03	02	02.5	06	02.0	C3	01.7	06	01.5	07	02.0	08	01.5	09	01.6	04	02.0	48
VIII	-	16.8	27.0	19.2	20.6	27.8	14.7	34.5	04	08.0	12	01	02.0	06	02.0	04	01.8	09	02.0	03	01.7	06	01.3	08	01.2	01	C3.0	55
IX	-	14.9	22.2	15.2	16.6	22.9	12.3	30.2	04	03.6	28	.	.	08	01.9	C3	02.0	10	01.6	01	01.0	03	01.3	05	01.4	13	C1.5	47
X	-	05.6	11.7	07.0	07.8	13.1	04.0	22.8	04	-01.2	31	.	.	04	02.0	02	01.0	04	01.8	07	01.9	07	01.3	17	01.7	04	C1.8	48
XI	-	02.9	10.9	04.4	05.6	11.6	01.7	21.3	16	-02.6	30	.	.	02	01.0	C4	01.5	08	01.8	08	01.5	12	01.3	05	02.0	03	01.7	48
XII	-	01.0	06.0	02.6	03.0	06.8	-00.2	13.4	29	-06.6	24	03	C1.3	04	01.5	04	02.0	16	01.6	02	01.0	02	01.0	01	02.0	06	02.2	55
GOD.	-	08.1	15.7	10.9	10.6	16.6	06.4	36.5	Pm	-06.6	24.VII	14	01.8	C3	01.8	53	02.0	82	01.7	57	01.7	80	01.5	101	01.7	60	01.9	585
$\varphi = 44^{\circ}59'$ N $\lambda = 18^{\circ}18'$ E Gr. $\Delta G = +1h\ 13\ min.$																										MODRICA		
BR. ST.122																												
I	-	00.5	02.9	01.3	01.5	03.9	-01.3	05.6	21	-06.8	15	00	C2.5	04	C2.0	14	01.5	10	01.2	01	01.0	04	01.5	04	01.5	16	C1.0	27
II	-	02.8	10.2	05.4	06.0	11.1	C0.8	17.5	12	-04.0	28	13	02.2	12	C1.8	C7	02.1	11	01.5	03	02.3	06	01.7	05	01.4	19	C1.3	49
III	-	03.8	12.9	07.2	07.8	13.5	02.0	25.5	19	-04.0	02	06	C1.3	18	C1.3	10	02.0	19	02.3	01	02.0	06	01.2	06	01.5	10	C1.3	17
IV	-	07.3	14.6	08.2	09.6	15.4	03.9	23.4	28	-06.4	04	07	C1.1	07	C3.0	18	01.9	08	01.9	.	.	15	01.3	12	01.5	11	C2.3	12
V	-	13.1	19.0	13.2	14.6	19.7	08.5	27.4	31	03.7	02	06	01.5	C8	01.5	C3	02.0	05	01.4	.	.	09	01.4	11	01.6	37	C1.9	19
VI	-	16.8	21.9	16.9	17.1	22.6	12.1	30.3	27	06.7	10.0	09	C3.0	C4	01.4	C3	01.7	03	01.0	.	.	05	01.2	11	01.4	36	C2.2	21
VII	-	18.5	24.6	19.2	20.4	25.7	12.8	34.8	27.14	05.2	27	04	01.2	07	C1.1	C3	01.0	12	01.6	01	01.0	09	C4.0	03	01.8	26	C1.8	26
VIII	-	18.8	26.6	20.7	21.7	27.3	13.4	34.0	04	10.4	29	05	04.4	12	C3.2	C5	02.6	11	01.9	01	01.0	03	01.3	02	01.5	29	C1.4	26
IX	-	14.6	21.5	16.5	17.3	22.2	11.5	30.2	C3	03.7	28	04	01.8	07	01.3	12	01.6	05	01.6	01	01.0	05	01.2	02	01.5	25	C1.3	27
X	-	06.0	11.2	07.8	08.2	12.2	C3.4	21.2	04	-02.1	31	05	C1.6	04	01.2	07	01.9	10	01.3	.	.	09	01.4	10	01.5	24	C1.4	24
XI	-	02.8	09.8	05.4	05.8	10.5	01.4	20.5	16	-02.4	28	01	01.0	07	01.8	05	01.0	04	01.0	01	01.0	09	01.3	07	01.7	40		
XII	-	02.1	06.2	03.1	03.6	07.0	-00.2	15.5	29	-05.4	25	10	C1.7	.	.	01	02.0	04	01.2	01	01.0	06	01.0	19	C1.3	30	C1.6	21
GOD.	-	08.9	15.1	10.4	11.2	16.0	05.7	34.0	Pm	-07.4	15.I	71	C1.4	04	01.6	54	01.8	102	01.6	10	01.8	85	01.3	92	C1.5	276	C1.7	269
$\varphi = 44^{\circ}11'$ N $\lambda = 18^{\circ}20'$ E Gr. $\Delta G = +1h\ 14\ min.$																										PONIKVE		
BR. ST.123																												
I	-	-02.8	04.3	-01.5	-00.3	05.5	-03.5	09.0	24	-10.0	13	24	C1.0	01	01.0	.	.	C1	01.0	.	.	.	.	05	C1.0	.	.	62
II	-	-01.8	04.4	-01.1	00.1	05.6	-02.5	05.5	17	-05.4	09	20	C1.0	08	01.2	.	.	.	.	.	.	.	13	C1.5	.	.	43	
III	-	00.0	09.8	02.9	04.9	11.0	-00.6	23.0	22	-05.0	12.0	01	01.0	09	01.0	05	01.0	.	01	01.0	.	07	01.0	.	.	64		
IV	-	02.6	11.4	02.7	04.9	12.0	01.8	21.0	06	-01.2	19	17	C1.1	07	C1.0	01	01.0	05	01.2	02	01.0	.	07	01.0	.	.	46	
V	-	06.4	15.1	05.2	06.0	16.7	04.4	23.4	26	02.2	10	04	01.0	09	01.0	02	01.0	02	01.0	02	01.0	.	.	13	C1.0	01	01.0	62
VI	-	10.2	17.4	11.6	12.7	20.7	07.8	28.0	31	02.8	10	01	01.0	01	01.0	18	01.6	C5	02.8	.	.	.	01	01.0	23	C1.3	40	
VII	-	14.8	20.9	14.4	16.1	22.1	11.0	30.6	27	04.2	13	.	.	03	01.0	C1	01.0	01	01.0	02	01.0	.	.	02	01.0	20	C1.3	37
VIII	-	16.0	23.7	16.1	18.0	25.1	12.3	35.0	17	06.0	09	03	C1.0	01	01.0	19	01.6	01	02.0									

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha em	Padavine R mm				Broj dana na sat:																					
	Temperatura Iznosljivosti Broj sati					Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	—	■							
	7	14	21	Sred. (Dnev.)	mm	7	14	21	Stred. Min.	Σ	X	at.	-10.00.0	0.025.0	0.00.0.6	8	2.0	8.0	0.1	1.00.0.0	•	Δ	*	Δ	▲	▲	T	—	■		
<b>BR. ST.121</b>																															
DOBOJ																															
I	9.0	7.8	6.3	7.7	044.8	04.9	95	83	94	91	56	087	034.2	20	•	•	18	•	•	•	•	01	18	15	09	03	15	01	01	—	
II	7.0	7.6	6.9	7.1	089.1	05.6	92	63	85	80	40	030	035.4	04	•	•	08	•	•	•	•	02	13	13	06	01	13	•	•	03	
III	6.4	6.5	5.7	6.2	121.6	06.2	93	58	79	77	17	018	007.9	07	•	•	07	02	•	•	•	03	13	06	04	04	02	•	•	03	
IV	6.1	7.4	4.9	6.2	140.8	06.6	91	54	80	75	26	068	C13.4	14	•	•	05	•	•	•	•	01	63	C1	12	10	02	12	01	•	04
V	5.5	7.2	5.2	6.1	174.6	05.7	97	90	61	89	80	40	129	C26.0	23	•	•	•	06	•	•	•	01	03	09	20	16	05	20	•	•
VI	5.9	6.6	4.8	5.8	160.3	12.0	89	60	88	79	44	177	C42.0	11	•	•	12	01	•	•	•	02	10	13	13	08	13	•	•	04	
VII	3.9	4.4	3.0	3.8	249.3	13.1	87	57	85	76	37	121	049.4	20	•	•	19	09	•	•	•	13	04	12	09	03	12	•	•	01	
VIII	4.5	4.3	3.1	4.0	237.4	14.5	95	56	85	80	40	065	C28.0	12	•	•	22	12	•	•	•	10	03	12	06	02	12	•	•	09	
IX	7.5	6.0	4.1	5.9	141.1	12.3	97	66	92	85	43	106	C24.2	21	•	•	•	10	02	•	•	01	•	02	06	12	10	03	12	•	
X	8.6	7.0	6.6	7.4	091.1	07.0	95	73	92	87	44	159	C19.9	29	•	•	02	•	•	•	•	01	15	20	19	07	20	•	•	02	
XI	7.4	6.1	5.1	6.2	086.1	06.0	95	70	94	86	52	065	G13.1	29	•	•	09	•	•	•	•	01	01	04	11	11	03	12	03	01	
XII	8.8	6.1	6.5	7.2	062.5	05.2	96	80	92	90	59	058	C14.6	13	•	•	17	•	•	•	•	01	13	14	12	01	13	05	04	•	
GOD.	6.6	5.6	5.2	6.1	1598.7	06.6	92	65	88	82	17	1091	C49.4	20VI	•	•	66	71	24	•	04	02	45	124	161	125	38	158	14	11	•
<b>MODRIČA</b>																															
BR. ST.122																															
I	8.7	8.7	7.5	8.3	-	04.6	93	86	92	90	54	062	022.5	20	•	01	21	•	•	•	01	•	19	12	07	03	10	02	•	01	
II	6.7	6.0	5.1	5.9	-	05.6	91	64	85	80	36	029	008.5	04	•	•	10	•	•	•	•	02	09	10	07	•	10	01	01	02	
III	5.6	5.5	4.9	5.3	-	05.9	90	56	81	76	22	019	004.3	08	•	•	09	01	•	•	•	06	10	06	04	•	06	04	•	02	
IV	5.5	6.2	6.5	6.1	-	06.5	82	51	84	72	28	085	C36.7	14	•	•	01	•	•	•	•	04	08	11	10	03	11	01	•	02	
V	5.3	6.0	5.1	5.4	-	09.6	84	60	83	76	41	078	C22.5	25	•	•	•	04	•	•	•	04	01	04	05	18	15	02	18	•	
VI	5.3	5.2	5.4	5.5	-	11.6	62	58	80	73	40	122	045.0	11	•	•	11	01	•	•	•	03	07	15	14	03	15	•	•	06	
VII	4.1	4.2	4.7	4.3	-	13.2	63	57	80	73	25	086	032.0	20	•	•	17	07	•	•	•	12	06	11	08	02	11	•	•	04	
VIII	3.2	3.3	3.4	3.3	-	14.4	67	57	79	74	38	085	030.5	26	•	•	15	12	•	•	•	15	04	13	10	02	13	•	•	08	
IX	6.4	4.8	4.8	5.3	-	12.4	91	68	88	83	40	072	026.3	05	•	•	07	01	•	•	•	04	06	10	06	02	10	•	•	01	
X	8.2	7.1	6.6	7.3	-	07.1	92	77	91	87	49	156	C24.6	06	•	•	03	•	•	•	•	02	18	20	17	07	20	•	•	05	
XI	7.5	6.2	5.3	6.4	-	06.0	94	74	90	86	45	061	016.9	09	•	•	07	•	•	•	•	01	13	10	08	02	10	01	•	10	
XII	8.1	6.5	5.3	6.7	-	05.3	89	79	92	87	49	065	C19.8	19	•	•	17	•	•	•	•	02	11	13	10	07	11	03	•	02	
GOD.	6.2	5.9	5.4	5.8	-	08.5	88	65	85	79	22	920	C45.0	44VI	•	01	68	59	21	•	10	01	60	115	149	118	28	145	14	01	01
<b>PORNITVE</b>																															
BR. ST.123																															
I	6.5	6.4	6.2	6.4	-	-	-	-	-	-	-	148	035.0	16	01	•	27	•	•	•	•	03	12	12	11	04	07	08	•	•	
II	6.7	6.2	6.9	6.6	-	-	-	-	-	-	-	102	028.5	04	•	•	25	•	•	•	•	02	11	10	10	03	07	08	04	•	
III	4.9	5.2	5.2	5.1	-	-	-	-	-	-	-	048	010.2	08	•	•	15	•	•	•	•	08	09	08	08	01	02	06	•	07	
IV	6.0	6.6	6.7	6.6	-	05.0	91	50	93	78	24	101	C13.5	19	•	•	01	•	•	•	•	02	09	16	13	07	01	•	•	15	
V	5.6	6.0	6.5	6.0	-	05.9	86	41	93	73	23	194	C28.5	23	•	•	•	•	•	•	•	02	10	17	17	07	17	•	•	05	
VI	4.9	5.1	5.5	5.2	-	-	-	-	-	-	-	166	040.0	30	•	•	•	•	•	•	•	03	05	14	14	04	14	•	•	02	
VII	3.5	4.1	4.6	4.2	-	08.4	86	37	89	70	17	101	C20.0	22	•	•	16	07	•	•	•	11	05	10	10	05	10	•	•	01	
VIII	3.4	3.4	4.7	3.8	-	11.2	87	56	91	78	23	104	C17.5	26	•	•	15	07	•	•	•	01	06	13	13	06	13	•	•	04	
IX	5.9	5.6	6.8	6.1	-	08.5	90	48	92	77	23	097	C21.0	27	•	•	04	•	•	•	•	07	12	12	02	12	12	•	•	24	
X	7.5	7.5	7.7	7.6	-	-	-	-	-	-	-	186	024.3	24	•	•	•	•	•	•	•	14	18	18	18	06	14	05	•	26	
XI	5.5	5.6	6.9	6.6	-	-	-	-	-	-	-	084	023.0	29	•	•	03	•	•	•	•	08	09	09	02	02	08	06	•	17	
XII	7.1	7.3	7.2	7.2	-	-	-	-	-	-	-	136	C26.0	19	•	•	02	•	•	•	•	14	13	13	07	06	10	03	•	27	
GOD.	5.4	5.9	4.8	5.4	-	07.7	84	63	88	79	12	1330	058.6	02VI	•	01	56	57	22	•	05	02	90	108	170	129	51	159	36	17	•
<b>MAGAČA</b>																															
BR. ST.124																															
I	6.2	6.2	4.6	5.7	-	04.5	88	77	89	85	12	104	055.4	20	•	•	19	•	•	•	•	04	09	12	06	03	11	06	04	•	
II	5.9	6.4	4.8	5.9	-	04.5	88	58	86	76	29	080	C27.2	04	•	•	08	•	•	•	•	05	09	12	04	02	•	•	06	01	
III	5.6	5.5	4.6	5.2	-	05.5	80	53	82	72	13	017	005.6	08	•	•	07</td														

Mesec	Vardušni pritisak Pn mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Pm (0-12)																						
		Tm			Max				Dat.			Min			Dat.			N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.							
$\psi = 44^{\circ}57'$ N $\lambda = 18^{\circ}50'$ E Gr. $\Delta G = +1h\ 15\ min.$																																		
I	-	01.2	03.4	01.7	02.0	-	-01.0	-	-	-06.8	16	03	02.3	*	*	01	03.0	*	*	03	02.7	18	02.5	*	*	06	03.0	47						
II	-	04.3	10.6	05.2	06.3	-	06.9	-	-04.0	28	02	02.0	02	02.0	16	02.8	02	02.0	01	02.0	05	04.8	06	02.2	01	03.0	47							
III	-	05.3	13.5	07.6	08.5	14.4	02.0	27.0	19	-04.0	02	*	*	39	03.2	06	03.7	07	02.0	*	*	04	02.6	*	*	42								
IV	-	08.4	14.3	09.5	10.7	16.6	-	24.6	29	-	-06	02.2	02	02.0	24	02.6	03	03.7	03	02.3	08	02.2	17	07.8	15	02.7	12							
V	-	13.7	19.1	13.0	14.7	20.6	-	28.5	31	-	-07	02.4	*	*	09	02.4	03	03.0	02	02.0	03	04.3	36	02.4	06	03.7	27							
VI	-	19.1	22.6	16.9	18.8	24.5	-	31.5	27	-	-07	02.3	*	*	02	02.5	*	*	11	02.5	03	02.0	32	02.6	13	04.1	22							
VII	-	19.5	25.5	18.6	20.6	27.0	-	36.0	17	-	-	02	02.0	22	01.7	05	01.8	04	01.5	09	01.7	34	02.5	02	02.5	15								
VIII	-	20.0	27.7	20.0	21.9	28.6	14.6	36.0	04	10.0	31.0	08	03.0	02	04.5	35	01.6	06	02.2	05	01.0	*	*	19	03.0	03	02.0	21						
IX	-	15.9	22.4	15.9	17.5	23.6	11.3	30.0	04.0	03	05.0	30.28	15	01.4	04	01.8	12	01.8	04	02.2	02	03.5	*	*	30	02.6	05	03.2	18					
X	-	08.1	11.7	07.4	08.7	13.1	03.7	22.0	04	00.0	20.18	01	03.0	*	*	22	01.5	04	02.6	06	03.8	07	02.4	44	02.2	*	*	09						
XI	-	04.3	10.6	04.1	05.8	11.3	01.3	21.5	16	-03.0	28	05	03.0	*	*	24	01.7	04	01.8	03	02.7	09	01.7	16	02.1	*	*	19						
XII	-	01.9	06.1	02.4	03.2	07.4	-00.3	14.0	27	-05.5	25	01	02.0	*	*	17	01.2	03	01.3	03	01.0	09	01.3	36	01.9	*	*	24						
GOD.	-	10.1	15.7	10.2	11.6	-	-	-	-	-	49	02.1	12	02.4	22.3	02.1	46	02.4	42	02.3	56	02.3	294	02.4	45	03.0	34							
$\psi = 44^{\circ}12'$ N $\lambda = 18^{\circ}57'$ E Gr. $\Delta G = -1h\ 10\ min.$																																		
I	-	00.1	02.6	00.7	01.0	03.5	-01.8	09.2	31	-06.8	17	*	*	04	01.0	08	01.0	06	01.0	12	01.1	14	01.2	15	01.4	68	01.6	26						
II	-	02.9	08.1	04.5	05.0	05.8	01.3	15.6	17	-06.0	28	02	01.5	09	01.3	10	01.2	14	01.7	05	01.2	14	01.1	11	02.4	08								
III	-	05.3	11.3	06.3	07.3	11.8	02.6	23.6	21	-05.6	01	02	02.5	19	01.1	20	01.4	15	01.4	15	02.8	04	01.5	10	02.0	05								
IV	-	07.3	11.7	07.0	08.2	12.8	04.2	21.6	28	-06.6	17	03	01.7	07	01.4	09	01.7	12	02.1	13	01.2	10	01.1	13	01.4	66								
V	-	12.4	16.2	11.5	12.9	17.5	08.1	23.0	31	04.6	16.10	03	01.3	16	01.4	06	01.3	06	01.7	07	01.3	14	02.5	15	01.3	13	02.1	13						
VI	-	16.2	18.7	15.0	16.2	20.1	11.5	28.0	27	05.6	13	01	01.0	06	01.0	04	01.0	08	01.4	04	01.0	20	01.8	21	01.4	10	01.9	16						
VII	-	18.1	23.1	17.7	19.1	24.0	13.3	36.4	17	08.4	20.09	04	01.0	10	01.4	06	01.3	03	01.0	05	01.0	19	01.1	16	01.2	07	01.6	19						
VIII	-	18.6	24.6	18.0	19.9	-	14.6	-	-05.4	12	02	01.5	10	01.1	04	01.2	05	01.0	14	01.1	13	01.2	16	01.1	14	02.5	13							
IX	-	14.9	19.8	14.5	16.0	20.9	11.4	26.6	04	05.2	28	*	*	06	01.2	08	01.1	07	01.4	15	01.0	07	02.4	19	01.0	05	01.7	21						
X	-	05.6	09.8	05.5	06.9	11.3	03.3	19.6	04	-04.8	31	03	01.0	08	01.6	06	01.0	08	02.4	08	01.0	12	01.2	17	01.4	14								
XI	-	04.2	08.2	04.8	05.5	09.4	02.1	17.4	16	-03.8	28	01	02.0	04	01.2	06	01.5	14	01.5	07	01.3	13	01.5	17	01.2	13	01.4	15						
XII	-	01.8	04.1	02.3	02.7	05.0	-00.5	13.6	29	-05.8	18	04	01.2	07	01.6	04	01.0	07	01.4	12	01.4	16	01.2	23	01.3	07	01.7	15						
GOD.	-	09.0	13.2	09.0	10.1	-	05.8	-	-06.8	77	25	01.4	106	01.5	91	01.3	102	01.6	122	01.7	157	01.7	187	01.3	120	01.6	184							
$\psi = 44^{\circ}47'$ N $\lambda = 19^{\circ}16'$ E Gr. $\Delta G = +1h\ 17\ min.$																																		
I	-	00.1	04.4	01.6	01.9	05.2	-00.6	10.3	22	-06.6	15	01	02.0	02	01.5	27	01.4	06	01.2	01	01.0	01	01.0	07	01.1	07								
II	-	02.8	10.7	04.9	05.9	11.6	01.4	18.4	12	-05.2	14	*	*	06	01.7	05	02.2	09	01.2	19	01.6	13	01.0	07	01.1	21								
III	-	03.7	13.6	07.5	08.1	14.1	02.2	26.6	23.19	-03.3	13	*	*	05	01.0	25	01.8	15	02.2	08	01.4	*	01	01.0	*	17								
IV	-	07.3	15.0	08.9	16.0	16.3	04.3	23.7	29	-02.6	04	05	01.2	03	01.3	10	01.2	17	01.7	05	01.0	10	01.0	17	01.2	19								
V	-	12.8	19.1	12.5	14.4	20.5	09.3	25.4	31	03.4	10	07	01.0	05	01.4	02	01.0	02	01.0	07	01.1	19	01.1	19	01.1	21								
VI	-	16.2	22.4	16.3	17.8	23.9	13.1	30.7	27	06.9	13	01	01.0	*	*	01	01.0	18	01.2	04	01.0	16	01.2	23	01.6	22								
VII	-	18.0	25.8	18.6	20.2	27.4	14.0	36.7	17	05.8	28	07	01.0	04	01.2	02	01.5	01	01.0	15	01.0	04	01.0	10	01.2	27	01.5	21						
VIII	-	18.3	26.5	19.6	21.5	30.0	15.4	36.5	30	10.8	30	20	01.0	04	01.0	*	*	*	24	01.0	01	01.0	03	01.0	11	01.3	11							
IX	-	14.1	23.2	16.1	17.4	24.5	12.4	31.5	03	04.9	28	11	01.0	*	*	02	01.5	21	01.0	02	01.5	04	01.0	29	01.3	20								
X	-	06.1	12.1	07.4	08.2	13.3	04.7	22.3	04	-03.3	31	*	*	02	01.0	*	*	21	01.4	06	01.2	13	01.4	26	01.6	24								
XI	-	03.2	10.4	04.8	05.8	11.4	02.0	20.0	16	-01.2	30	04	01.2	01	01.0	05	01.0	01	01.0															



Mesec	Vrednost pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																
		Tm				Sred. (Dnes)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C
		7	14	21	E							J.	E	J.	E	J.	E	J.	E	J.	E	J.	E	J.				
$\varphi = 43^{\circ}34'$ N $\lambda = 17^{\circ}27'$ E Gr. $\Delta G = +1h\ 10\ min.$																												
I	-00.1	05.9	01.6	02.3	-	-	-	-	-	16	C2.2	01	01.0	.	.	.	.	04	02.0	.	.	07	01.6	.	.	65		
II	01.5	05.6	02.9	03.2	-	-	-	-	-	23	04.0	.	.	.	.	.	.	22	02.0	.	.	01	01.0	.	.	58		
III	-03.9	10.2	05.5	04.3	11.4	00.7	21.2	22	-05.2	13	17	03.8	03	03.7	04	03.0	.	.	17	03.1	.	.	02	01.0	02	03.5	48	
IV	-06.2	09.0	06.1	06.9	10.6	02.2	16.5	30	-01.6	24.17	36	C3.5	.	.	06	02.8	.	.	19	02.6	.	.	.	.	.	.	29	
V	-11.5	14.9	10.3	11.8	16.2	-	21.2	30.27	-	16	C3.3	.	.	C6	C4.0	.	.	08	02.5	.	.	02	03.0	.	.	61		
VI	-14.4	16.5	13.6	15.0	20.7	09.1	25.0	25	02.2	14	11	02.8	01	03.0	08	02.5	.	.	10	02.2	.	.	04	01.8	.	.	56	
VII	-16.9	23.1	16.3	18.2	25.1	12.7	32.0	16	06.2	08	26	02.6	.	.	C2	01.5	.	.	02	01.0	.	.	01	01.0	.	.	41	
VIII	-18.8	25.2	18.3	20.2	26.3	14.3	32.2	02	08.2	12	19	02.2	04	01.2	02	01.0	.	.	C1	C1.0	.	.	03	01.0	03	01.7	61	
IX	-14.7	19.4	14.3	15.7	20.7	10.8	27.4	06	03.6	28	21	02.4	.	.	C5	01.4	.	.	02	02.0	.	.	C2	01.0	05	01.0	55	
X	-04.7	08.7	05.3	06.0	10.1	01.9	14.0	11.06	-03.0	31	09	02.2	01	03.0	06	01.2	01	02.0	14	01.1	.	.	02	01.0	.	.	60	
XI	-C2.2	08.0	03.2	04.2	09.0	00.4	16.2	17	-05.0	29	17	C4.1	.	.	.	.	.	.	11	01.8	.	.	01	01.0	.	.	61	
XII	-00.6	04.7	00.4	01.2	06.1	-02.1	12.0	10	-07.0	22	19	04.3	.	.	C1	02.0	.	.	05	04.8	.	.	02	02.0	01	01.0	65	
GOD.	-	07.9	12.8	C8.2	09.2	-	-	-	-	230	C3.1	10	02.3	40	02.4	01	02.0	115	02.3	.	.	28	01.5	11	01.6	660		
$\varphi = 43^{\circ}23'$ N $\lambda = 17^{\circ}36'$ E Gr. $\Delta G = +1h\ 10\ min.$																												
I	01.6	09.6	03.9	04.8	10.6	-00.5	15.0	20	-06.0	15	04	C1.8	.	.	.	.	.	.	02	02.0	.	.	.	.	.	.	69	
II	04.7	10.7	06.4	07.0	11.7	02.3	16.8	16	-04.6	09	11	02.7	.	.	.	.	.	05	01.4	.	.	.	.	.	.	.	82	
III	-05.4	14.9	08.7	05.4	15.7	02.9	24.4	21	-02.4	13.12	06	C2.3	.	.	.	.	.	03	C2.3	.	.	.	.	.	.	.	70	
IV	-09.0	14.4	10.0	10.9	15.8	05.7	21.0	30	00.0	21.20	17	02.9	.	.	.	.	.	03	02.3	.	.	.	.	.	.	.	70	
V	-12.6	18.7	13.4	14.5	20.3	08.3	26.4	30.20	04.8	18.11	05	02.2	.	.	.	.	.	07	01.1	.	.	.	.	.	.	.	81	
VI	-16.2	23.6	17.3	18.6	24.8	12.1	29.4	26	05.4	12	11	01.7	.	.	.	.	.	02	01.5	.	.	.	.	.	.	.	77	
VII	-19.7	27.5	20.1	21.6	28.7	13.8	36.2	16	07.8	09	C9	C2.6	.	.	.	.	.	03	01.7	.	.	.	.	.	.	.	81	
VIII	-19.5	30.3	21.4	23.2	31.3	14.7	37.0	05	D9.0	13	07	01.7	.	.	.	.	.	03	01.7	.	.	.	.	.	.	.	83	
IX	-15.3	25.2	17.3	18.8	26.1	12.2	31.4	09	04.0	28	09	C1.9	.	.	.	.	.	04	02.0	.	.	.	.	.	.	.	77	
X	-07.5	13.4	08.6	09.5	14.4	04.7	19.2	06	-02.6	31	04	01.2	.	.	.	.	.	01	02.0	.	.	.	.	.	.	.	86	
XI	-04.7	12.4	06.6	07.6	13.2	02.0	19.0	17	-03.4	02	C7	C2.3	.	.	.	.	.	01	02.0	.	.	P1	.	.	.	.		
XII	-01.3	09.2	03.0	04.1	10.1	-00.4	16.6	04	-05.0	24	17	05.8	.	.	.	.	.	07	02.1	.	.	01	03.0	02	02.0	75		
GOD.	-	09.6	17.5	11.4	12.5	18.6	06.5	37.0	05VM-06.0	45.1	107	C2.8	.	.	.	.	.	01	02.0	32	01.6	.	.	.	.	.	955	
$\varphi = 43^{\circ}50'$ N $\lambda = 17^{\circ}38'$ E Gr. $\Delta G = +1h\ 10\ min.$																												
I	-01.5	05.6	00.1	01.1	06.7	-03.5	10.6	22	-05.4	15	06	C1.7	.	.	.	.	.	11	02.8	.	.	.	09	01.6	.	.	67	
II	00.3	06.7	02.2	02.9	07.8	-01.6	12.4	12	-06.6	09	08	02.0	.	.	.	.	.	12	02.4	.	.	.	11	01.8	.	.	53	
III	-01.4	11.8	04.9	05.8	13.2	-06.7	25.4	22	-05.6	02	16	C1.6	.	.	.	.	.	10	03.2	.	.	.	15	02.2	.	.	58	
IV	-05.0	10.9	05.9	06.9	12.4	01.8	19.4	30	-06.8	17	04	C1.5	.	.	.	.	.	13	03.1	.	.	.	17	01.9	.	.	56	
V	-09.4	15.7	10.1	11.3	17.2	05.5	24.6	30	02.6	23.05	07	C1.7	.	.	.	.	.	C3	02.3	.	.	.	09	02.1	.	.	74	
VI	-12.8	15.7	12.7	14.5	21.5	05.1	27.4	05	03.6	12	07	C1.9	.	.	.	.	.	02	02.5	.	.	.	14	02.4	.	.	67	
VII	-14.7	23.2	14.6	16.8	25.3	10.6	34.6	16	03.4	23.07	04	C1.3	.	.	.	.	.	01	03.0	.	.	.	15	01.9	.	.	71	
VIII	-15.5	25.8	19.3	18.0	27.6	10.9	34.4	04	04.8	12	06	C1.8	.	.	.	.	.	01	02.0	.	.	.	20	01.8	.	.	66	
IX	-10.7	20.6	12.4	14.1	22.7	07.0	29.4	10	-02.2	28	10	C1.7	.	.	.	.	.	07	02.6	.	.	.	19	01.9	.	.	54	
X	-02.7	09.6	03.8	05.0	11.3	00.3	18.6	19	-03.6	31	06	C1.7	.	.	.	.	.	17	02.4	.	.	.	08	02.1	.	.	42	
XI	-00.3	08.3	01.5	02.9	10.6	-01.6	17.8	19	-11.6	29	09	C1.8	01	03.0	.	.	.	07	02.3	01	02.0	.	07	01.9	.	.	48	
XII	-03.4	03.9	-01.4	-00.6	05.1	-05.7	14.2	05	-13.2	19	07	C1.1	01	02.0	.	.	.	07	02.1	.	01	03.0	02	02.0	01	03.0	74	
GOD.	-	05.7	13.5	06.8	06.2	15.1	02.6	34.6	KM -13.2	19.8	86	C1.7	C2	02.5	.	.	.	91	02.6	01	02.0	01	03.0	146	02.0	01	03.0	767
$\varphi = 43^{\circ}05'$ N $\lambda = 17^{\circ}43'$ E Gr. $\Delta G = +1h\ 11\ min.$																												
I	-02.4	11.0	04.4	05.5	12.0	06.9	15.0	31.11	-04.0	15	06	C2.6	06	02.2	C1	C1.0	C4	01.2	*	*	*	*	*	*	*	*	74	
II	-05.7	13.5	08.1	08.8	14.3	03.9	18.5	17	-02.0	09	04	C3.2	09	02.7	C4	C1.8	12	C3.7	C1	0								

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha em	Padavine R mm	Broj dana na sata:																											
	Insolacija broj sati					Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲												
	7	14	21	mm	7	14	21	%	Min	Σ	Max	Dat.	<	<	<	IV	IV	IV	IV	IV													
<b>RAKITNO</b>																																	
<b>BR. ST. 131</b>																																	
I 5.3 5.3 3.9 4.8	-	04.5	77	82	78	79	66	066	022.4	02	-	-	-	-	01	* 13	11	07	07	03	67	02	.	.	.	.	.	.	.	.	.	01	
II 7.4 6.5 5.7 6.5	-	04.9	82	82	82	70	70	221	062.4	04	-	-	-	-	04	02	04	13	11	11	04	10	05	.	.	.	.	.	.	.	.	.	05
III 4.6 5.7 3.7 4.7	-	06.3	84	81	82	85	115	079.4	05	-	13	.	.	.	05	03	09	07	04	04	02	03	01	.	.	.	.	.	.	.	.	.	01
IV 4.9 6.9 5.4 5.7	-	06.3	82	81	84	62	57	083	018.2	29	-	04	.	.	05	02	05	12	13	13	03	12	01	.	.	.	.	.	.	.	.	.	01
V 6.3 6.6 4.1 5.7	-	-	-	-	-	-	-	130	030.7	05	-	-	-	-	02	01	03	08	13	13	05	13	.	.	.	.	.	.	.	.	.	.	
VI 5.0 6.0 4.7 5.2	-	10.2	76	76	76	76	42	096	029.4	30	-	01	.	.	01	01	06	10	09	03	16	.	.	.	.	.	.	.	.	.	.		
VII 2.6 3.7 1.4 2.6	-	11.6	71	68	66	68	54	027	022.0	20	-	01	05	.	01	01	08	02	01	01	01	01	.	.	.	.	.	.	.	.	.		
VIII 2.5 4.5 2.1 3.0	-	12.3	70	59	69	66	39	066	020.4	30	-	01	01	07	03	01	12	07	07	03	07	.	.	.	.	.	.	.	.	.			
IX 3.9 4.5 3.3 3.9	-	10.2	71	72	74	72	53	155	025.6	25	-	01	07	.	01	01	15	06	11	11	07	11	.	.	.	.	.	.	.	.	.		
X 6.9 7.7 5.7 6.8	-	05.6	79	75	76	76	48	542	040.0	13	-	10	.	.	03	13	20	20	14	15	02	.	.	.	.	.	.	.	.	.	03		
XI 4.8 5.7 4.8 5.1	-	05.3	85	81	81	82	58	115	027.6	29	-	11	.	.	02	09	08	10	10	04	10	02	01	.	.	.	.	.	.	.	.	01	
XII 5.5 5.1 3.3 4.6	-	04.6	88	87	84	86	57	077	034.0	13	-	01	22	.	04	01	07	05	04	04	02	03	03	.	.	.	.	.	.	.	.	06	
GOD. 5.0 5.7 4.0 4.9	-	-	-	-	-	-	-	1686	050.6	12x	-	-	-	-	24	09	94	91	111	110	91	104	14	01	.	.	.	.	.	.	.	.	18
<b>LISTICA</b>																																	
<b>BR. ST. 132</b>																																	
I 4.8 5.1 3.7 4.5	-	05.2	79	73	79	77	42	105	061.8	02	-	19	.	.	01	13	06	10	10	04	10	.	.	.	.	.	.	.	.	.	.		
II 7.8 7.3 5.0 6.7	-	06.1	79	72	82	78	-	289	012.0	04	-	06	.	.	01	03	14	12	11	06	12	.	.	.	.	.	.	.	.	.	.		
III 4.6 5.0 3.5 4.4	-	06.6	73	63	79	72	26	150	084.2	05	-	04	.	.	01	09	05	05	05	02	05	.	.	.	.	.	.	.	.	.	01		
IV 5.5 7.1 6.1 6.2	-	07.5	75	71	76	74	45	085	018.0	13	-	01	.	.	01	05	11	14	13	04	14	.	.	.	.	.	.	.	.	.	01		
V 6.1 6.1 4.8 5.7	-	09.6	79	69	77	75	48	132	030.0	01	-	04	.	.	04	09	14	13	05	14	.	.	.	.	.	.	.	.	.	.			
VI 4.2 5.6 4.2 4.7	-	12.3	76	67	77	73	49	076	025.6	30	-	17	.	.	06	04	10	10	02	10	.	.	.	.	.	.	.	.	.	.			
VII 2.1 2.5 1.6 1.8	-	12.6	73	55	68	68	33	061	052.0	20	-	26	16	.	02	24	01	02	01	02	.	.	.	.	.	.	.	.	.	01			
VIII 1.8 3.0 0.9 1.9	-	14.0	72	52	70	65	25	060	029.6	12	-	29	19	.	02	20	06	06	01	06	.	.	.	.	.	.	.	.	.	03			
IX 4.0 3.9 2.7 3.5	-	12.7	82	64	80	75	39	166	054.2	25	-	19	05	.	01	16	05	10	10	06	16	.	.	.	.	.	.	.	.	.	.		
X 7.0 7.1 5.9 6.7	-	07.9	87	80	87	65	57	448	062.4	14	-	02	01	.	01	07	16	19	19	16	19	.	.	.	.	.	.	.	.	.	.		
XI 5.9 5.7 4.2 5.3	-	06.6	82	77	84	81	51	155	051.2	29	-	07	.	.	08	09	11	11	04	11	.	.	.	.	.	.	.	.	.	01			
XII 4.7 4.7 2.9 4.1	-	05.0	75	69	81	76	53	066	031.1	13	-	18	.	.	03	03	10	C5	03	02	03	.	.	.	.	.	.	.	.	.	01		
GOD. 4.9 5.3 3.7 4.6	-	08.6	78	67	78	74	-	1795	112.0	04.ii	-	56	95	40	.	07	03	125	85	116	113	53	11t	.	.	.	.	.	.	.	.	04	02
<b>PROZOR</b>																																	
<b>BR. ST. 133</b>																																	
I 5.2 5.5 4.9 5.2	-	04.1	78	75	84	79	44	091	023.8	20	-	22	.	.	.	10	11	11	10	04	08	06	02	.	.	.	.	.	.	.	05	04	
II 7.0 7.0 6.4 7.0	-	04.7	85	74	84	81	54	128	038.2	04	-	18	.	.	02	16	11	11	05	11	03	.	.	.	.	.	.	.	.	01	01		
III 4.6 4.5 4.6 4.6	-	05.1	83	59	79	74	09	044	016.4	06	-	19	01	.	02	12	08	07	06	02	06	02	01	.	.	.	.	.	.	.	.	02	
IV 6.3 7.1 7.2 6.9	-	05.8	77	71	78	76	37	061	008.4	18	-	02	.	.	04	14	16	15	0.	12	05	.	.	.	.	.	.	.	.	01			
V 6.6 6.2 7.4 6.7	-	08.3	76	76	79	77	57	128	021.6	16	-	07	.	.	04	14	16	16	04	16	.	.	.	.	.	.	.	.	.	02			
VI 5.5 6.7 7.3 6.5	-	10.7	81	79	82	81	52	107	029.6	30	-	07	.	.	04	14	13	12	02	13	.	.	.	.	.	.	.	.	.	02			
VII 2.5 3.9 3.6 3.3	-	12.4	79	76	79	78	29	058	030.9	20	-	19	09	.	06	06	06	06	01	04	.	.	.	.	.	.	.	.	.	01			
VIII 2.3 3.2 3.5 3.0	-	13.2	78	73	79	77	51	070	027.6	29	-	21	14	.	07	14	09	09	02	05	.	.	.	.	.	.	.	.	.	02			
IX 4.4 4.2 4.0 4.2	-	09.9	82	70	78	77	47	053	012.8	21	-	13	.	.	06	12	09	10	10	02	16	.	.	.	.	.	.	.	.	04			
X 6.6 7.1 7.1 7.0	-	05.5	83	77	82	81	58	239	074.4	14	-	12	.	.	06	19	22	21	12	20	05	.	.	.	.	.	.	.	.	04			
XI 5.9 5.8 5.0 5.6	-	04.9	85	73	85	81	47	074	023.8	29	01	16	.	.	06	11	11	10	02	09	04	02	.	.	.	.	.	.	.	.	05		
XII 6.6 6.1 5.3 6.0	-	03.8	78	80	80	79	46	052	030.4	13	06	03	28	.	06	11	07	01	05	04	02	.	.	.	.	.	.	.	.	03			
GOD. - - - - -	-	07.4	80	73	80	78	09	1105	038.2	04.ii	-	01	01	23	.	08	136	139	133	38	125	29	07	.	.	.	.	.	.	.	.	40	
<b>CAPLJINA-KLEPCI</b>																																	

Mesec	Vrstdišni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)															
		Tm			Sred. (dies)			Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C					
		7	14	21										N	NE	E	SE	S	SW	W	NW	C					
$\varphi = 43^{\circ}09'$ , N $\lambda = 17^{\circ}47'$ , E Gr., $\Delta G = +1h\,11\text{ min.}$														GLMANOVICI													
I	-	62.8	12.4	6.2	0.2	1.2	0.2	6.4	0.2	1.2	01-02-0	1.2	01-02-0	1.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2		
II	-	56.4	12.9	6.2	0.9	1.1	0.9	6.4	0.9	1.1	16-01-0	0.9	16-01-0	1.1	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2		
III	-	52.8	12.5	6.1	0.7	1.2	0.7	6.5	0.7	1.2	21-01-0	0.7	21-01-0	1.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2		
IV	-	50.1	12.6	6.2	0.5	1.3	0.5	6.5	0.5	1.3	22-01-0	0.5	22-01-0	1.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2		
V	-	44.7	20.5	14.2	15.9	20.7	0.4	24.5	20	05-0	16	16	02-9	16	02-9	16	02-9	16	02-9	16	02-9	16	02-9	16	02-9		
VI	-	39.4	20.4	16.8	20.6	25.5	13.6	29.4	05	07-0	12	20	02-8	12	02-8	12	02-8	12	02-8	12	02-8	12	02-8	12	02-8		
VII	-	32.3	20.4	20.7	23.1	29.1	15.3	34.6	16	05-0	09	12	02-5	12	02-5	12	02-5	12	02-5	12	02-5	12	02-5	12	02-5		
VIII	-	25.1	31.7	11.8	25.1	31.7	14.7	36.8	05	10-0	12	20	01-7	12	01-7	12	01-7	12	01-7	12	01-7	12	01-7	12	01-7		
IX	-	11.4	16.6	15.6	16.6	20.6	14.2	30.4	04	03-0	27	10	02-4	10	02-4	10	02-4	10	02-4	10	02-4	10	02-4	10	02-4		
X	-	10.0	15.9	10.2	11.4	16.0	21.5	21.5	01	06-0	31	07	01-1	07	01-1	07	01-1	07	01-1	07	01-1	07	01-1	07	01-1		
XI	-	6.3	14.2	6.1	0.9	2.2	0.4	14.3	04-0	16.8	16-15	-02-0	02	17	02-5	17	02-5	17	02-5	17	02-5	17	02-5	17	02-5		
XII	-	0.4	10.6	0.7	0.5	10.7	01-1	10.5	04	-02-2	20	23	01-4	20	01-4	20	01-4	20	01-4	20	01-4	20	01-4	20	01-4		
GOD.	-	12.1	16.1	12.7	14.1	19.3	0.2	26.8	05-0	06-0	0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0			
$\varphi = 43^{\circ}21'$ , N $\lambda = 17^{\circ}48'$ , E Gr., $\Delta G = +1h\,11\text{ min.}$														MESTAR													
I	757.0	64.6	10.2	6.5	0.6	11.9	0.6	14.6	31	-01-1	27	47	02-2	19	01-7	02	01-0	-	-	-	-	-	05	02-6	25		
II	756.5	65.9	12.0	0.6	0.2	14.0	0.5	18.6	16	00-1	09	29	04-7	13	04-8	-	03	02-3	07	01-4	-	-	04	01-5	02	02-5	
III	752.2	67.2	11.9	11.1	11.6	17.7	0.5	26.6	20-21	02-1	02	21	00-7	15	04-9	12	02-7	03	01-7	03	01-7	03	01-7	03	01-7		
IV	745.4	63.1	11.0	11.1	17.5	26.0	24-0	24	02-8	21	34	00-6	24	04-4	01	01-5	03	02-0	05	02-0	04	02-0	02	02-0	01	02-0	
V	750.1	13.7	20.4	19.3	16.2	21.7	10.4	24.4	30	07-0	11-06	03	01-2	16	01-2	02	01-7	03	02-0	07	02-7	02	01-5	11	01-6	02	01-6
VI	750.5	17.5	16.2	17.1	20.1	26.0	16.4	36.6	05-0	04-0	14	29	11	03-0	03	01-7	-	03	04-0	07	02-1	11	02-7	03	02-0	03	02-0
VII	751.0	21.0	17.5	17.9	19.9	30.7	13.3	37.9	16	12-0	09	26	01-0	17	01-3	02	01-5	01	05-0	03	02-7	09	02-0	03	04-0	03	04-0
VIII	751.5	21.7	11.7	13.7	19.1	31.3	16.1	36.0	05-0	34-0	12-1	12	43	01-1	02	04-0	-	02	03-0	03	02-0	04	02-0	04	02-0	04	02-0
IX	751.9	17.4	26.4	18.7	16.2	27.0	15.8	31-6	09	04-4	27	41	01-7	16	01-9	01	01-0	01	03-0	04	04-5	02	03-0	07	01-7	02	01-5
X	745.3	08.9	14.2	0.9	16.7	19.3	07-1	20.4	04	01-2	31	26	01-5	19	01-3	-	04	01-0	07	02-7	05	02-2	08	02-0	03	01-7	30
XI	754.4	15.6	12.6	0.9	0.9	13.6	04-5	18.6	17	00-0	02	01	01-0	16	01-6	01	01-0	01	01-0	02	03-5	01	01-0	06	01-7	48	
XII	746.0	01.7	0.9	0.8	0.4	0.7	0.7	17.8	04	-01-4	24-21	31	04-9	13-0	04-5	-	02	00-0	-	03	01-3	00	02-1	03	01-3	06	
GOD.	-	11.4	15-8	13-3	14-2	19-6	0-8	36-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	01-0	
$\varphi = 43^{\circ}24'$ , N $\lambda = 17^{\circ}51'$ , E Gr., $\Delta G = +1h\,12\text{ min.}$														PETOCCI-ŽELJUŠA													
I	-	64.9	10.2	0.5	0.6	10.5	0.2	14.6	02-6	20-0	1.2	01-1	-	-	03	01-7	-	06	01-7	-	-	-	44	02-5	04		
II	-	55.9	11.0	27.5	0.6	1	12.9	0.6	17-0	-01-1	09	47	01-2	19	01-9	-	04	01-5	02	01-0	10	02-4	-	37	02-5	-	
III	-	57.4	16.6	0.9	0.5	17.4	0.2	25.6	22-21	00-7	13	10	01-3	22	01-4	-	02	02-5	-	-	18	03-2	-	36	02-4	03	
IV	-	50.1	19.4	10.4	11.1	17.4	0.6	22.0	29-28	01-8	21	16	01-3	16	02-1	-	04	01-7	-	-	12	02-6	-	36	02-7	-	
V	-	14.7	20.4	14.5	15.6	21.6	10.4	27.7	26	06-7	11	23	01-1	11	01-8	-	06	01-7	-	-	13	01-9	02	01-0	38	02-0	
VI	-	17.2	23.6	16.1	19.4	24.4	13.4	24.8	05	06-0	14	29	11	03-0	03	01-7	-	04	01-0	01	01-0	16	02-6	04	01-0	34	02-2
VII	-	21.0	26.6	11.0	12.5	23.5	13.4	30.0	16-0	01-3	09	14	01-4	17	01-6	-	05	01-0	01	01-0	12	01-6	-	43	01-9	-	
VIII	-	17.0	31.7	12.1	14.4	31.0	17.7	34-1	09	12-8	12	13	01-0	11	01-5	-	10	01-3	-	-	11	01-8	-	45	01-8	-	
IX	-	17.5	26.0	16.4	20.1	27.0	14.5	31-5	01-5	06-0	27	05	01-4	23	01-3	-	05	02-0	-	-	18	01-5	-	35	01-5	-	
X	-	5.2	14.5	0.9	0.7	16.6	0-6	20-0	04	00-5	31	04	01-0	16	01-2	-	08	01-4	-	-	11	01-6	-	-	-	-	
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 43^{\circ}46'$ , N $\lambda = 18^{\circ}02'$ , E Gr., $\Delta G = +1h\,12\text{ min.}$														IVAN SEDLO													

Mjesec	Oblačnost Nm (0-10)				Indeks broj sati (0-100)	Vlažnost vazduha				Padavine mm				Broj i dana na sat:																	
	e <sub>m</sub>	7	14	21		mm	7	14	21	Sred. Min	Σ	Max	Min	Tn	Tx	T <sub>z</sub>	T <sub>14</sub>	T <sub>21</sub>	T <sub>10</sub>	P(0-10)	N <sub>mm</sub> (0-10)	N <sub>mm</sub>	•	+	Δ	Δ	▲	R	T	≡	■
	7	14	21	Sred. (Dnev.)		mm	7	14	21	Sred. Min	Σ	Max	Min	0.00.0	0.025.0	0.020.0	0.010.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	0.00.0	
<b>BR. ST.136</b>																															
<b>DECANOVICI</b>																															
I 4.5 4.8 3.7 4.1	-	05.3 84 55 81 73 23	056 616.1	19	-	-	06	-	-	-	01	-	10	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07		
II 6.0 5.9 5.3 5.9	=	06.2 87 78 72 37	142 556.3	21	-	-	02	-	-	-	02	-	12	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	
III 4.5 4.5 5.0 4.0	=	06.3 78 44 73 65 26	067 040.0	21	-	-	02	-	-	-	02	-	12	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	
IV 5.2 5.7 5.4 5.4	-	07.9 85 70 73 26	109 032.5	18	-	-	02	-	-	-	02	-	12	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	
V 4.5 4.8 4.5 4.6	-	10.2 82 57 80 73 38	067 025.5	61	-	-	04	-	-	-	04	-	10	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	
VI 3.6 3.4 3.8 3.6	-	12.0 73 49 71 69 33	003 020.0	07	-	-	01	-	-	-	01	-	07	01	08	00	01	02	03	04	05	06	07	08	09	01	02	03	04	05	
VII 1.9 2.0 1.1 1.7	-	12.9 69 39 74 61 22	022 014.0	20	-	-	04	-	-	-	04	-	12	04	05	06	07	08	09	01	02	03	04	05	06	07	08	09	01		
VIII 1.6 1.6 1.4 1.6	-	13.3 67 33 70 57 22	018 008.0	24	-	-	01	-	-	-	01	-	07	01	08	00	01	02	03	04	05	06	07	08	09	01	02	03	04	05	
IX 3.2 2.2 2.1 2.5	-	13.8 87 54 85 75 36	122 046.4	41	-	-	04	-	-	-	04	-	10	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	
X 6.5 6.1 6.2 6.4	-	09.5 90 81 92 87 62	411 056.5	14	-	-	01	-	-	-	01	-	07	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	
XI 4.3 3.9 4.1 4.1	-	06.8 84 61 84 76 38	008 050.0	06	-	-	01	-	-	-	01	-	07	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	09		
XII 4.1 4.5 3.5 4.0	-	05.0 78 54 75 65 39	038 026.0	15	-	-	01	-	-	-	01	-	07	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	
GOD.	4.2 4.0 3.7 4.0	-	09.1 79 53 78 71 27	1220 058.5	41	-	-	04	-	-	-	04	-	07	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08
<b>BR. ST.137</b>																															
<b>MOSTAR</b>																															
I 5.3 6.0 3.7 5.0	122.8	05.2 77 60 70 69 41	682 031.0	02	-	-	01	-	-	-	01	-	07	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	09	
II 8.5 6.8 5.7 7.0	095.9	05.8 75 58 70 69 43	230 052.9	04	-	-	01	-	-	-	01	-	14	03	02	12	12	11	07	01	02	03	04	05	06	07	08	09	01		
III 5.5 6.7 4.8 5.7	179.3	06.3 51 61 63 63 32	054 027.3	06	-	-	01	-	-	-	01	-	07	01	04	08	06	08	07	09	01	02	03	04	05	06	07	08	09		
IV 7.0 7.3 7.0 7.1	145.2	07.4 75 57 75 69 28	073 017.7	27	-	-	01	-	-	-	01	-	11	01	02	14	16	15	01	18	01	02	03	04	05	06	07	08	09		
V 6.5 6.6 5.1 6.0	190.4	09.9 82 61 73 72 32	153 030.4	01	-	-	04	-	-	-	04	-	07	01	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08	
VI 6.0 6.6 6.2 5.9	207.6	11.8 77 53 70 67 37	111 019.5	30	-	-	01	-	-	-	01	-	19	02	03	04	05	06	07	08	09	01	02	03	04	05	06	07	08		
VII 7.7 7.5 6.7 7.7	236.6	11.9 62 43 55 53 31	025 031.4	30	-	-	01	-	-	-	01	-	16	06	05	04	03	02	01	03	04	05	01	02	03	04	05	06	07	08	
VIII 2.6 2.6 2.4 2.6	111.1	12.9 62 41 55 53 27	076 032.6	12	-	-	01	-	-	-	01	-	30	21	12	11	01	15	01	10	04	03	10	01	02	03	04	05	06	07	
IX 4.0 4.4 4.0 4.4	212.4	11.8 75 50 67 64 37	159 041.0	22	-	-	04	-	-	-	04	-	19	10	02	12	01	12	06	13	09	05	13	01	02	03	04	05	06	07	
X 7.3 7.7 6.1 7.0	105.9	08.2 89 74 85 63 30	463 014.7	23	-	-	01	-	-	-	01	-	07	01	03	14	23	21	13	23	01	02	03	04	05	06	07	08	09		
XI 6.7 6.7 4.7 6.0	115.6	06.7 76 71 80 79 52	126 031.4	23	-	-	01	-	-	-	01	-	10	02	02	05	04	05	06	07	08	09	01	02	03	04	05	06	07	08	09
XII 5.6 6.3 4.1 5.4	102.9	05.1 65 67 71 73 38	077 052.9	13	-	-	01	-	-	-	01	-	04	04	04	07	09	04	07	09	01	02	03	04	05	06	07	08	09		
GOD.	5.7 6.1 4.4 5.4	2146.6	08.6 76 57 69 67 27	1639 056.7	7	-	-	08	-	-	-	08	-	08	106	52	19	111	17	73	56	154	120	57	111	120	57	111	120	57	111
<b>BR. ST.138</b>																															
<b>POTOCI - ŽELJUSA</b>																															
I 5.4 5.9 4.5 5.3	-	72 57 70 -	-	056 014.5	12	-	-	04	-	-	-	04	-	08	10	07	07	02	07	01	02	03	04	05	06	07	08	09	01		
II 7.9 7.1 6.2 7.1	-	05.5 74 56 69 67 28	200 045.8	04	-	-	01	-	-	-	01	-	02	15	12	10	07	11	01	02	03	04	05	06	07	08	09	01			
III 5.1 5.5 5.2 5.2	-	05.7 67 47 50 59 17	056 027.2	05	-	-	02	-	-	-	02	-	06	07	04	04	02	04	05	06	07	08	09	01	02	03	04	05	06	07	08
IV 6.6 7.6 6.6 7.0	-	06.4 72 54 69 65 22	061 014.7	21	-	-	01	-	-	-	01	-	01	14	14</td																

Mesec	Varduini Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																			
		Tm			Max			Min			Dat.			N			NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.				
$\varphi = 43^{\circ}43'$ N $\lambda = 18^{\circ}16'$ E Gr. $\Delta G = +1h\ 13\ min.$														BJELASNICA												BR. ST.141					
I	593.0	-05.3	-04.4	-05.3	-05.1	-03.3	-06.9	00.9	01	-12.0	14	44	06.2	02	04.5	01	03.0	.	.	08	05.1	23	05.6	.	.	03	02.7	12			
II	588.1	-05.2	-03.9	-04.4	-04.5	-02.9	-06.0	00.2	19.17	-12.2	09	23	04.9	06	03.5	01	04.0	.	.	14	07.0	29	07.4	08	04.6	02	06.0	01			
III	591.4	-02.0	-00.8	-01.6	-01.5	00.4	-03.2	07.4	21	-10.6	08	23	03.8	01	03.0	07	03.0	01	03.0	19	05.0	25	07.5	04	03.5	02	03.5	11			
IV	588.6	-03.5	-02.0	-03.1	-02.9	-01.3	-04.4	04.8	30	-08.6	19.18	42	05.1	04	03.0	02	02.0	.	.	11	05.3	25	07.0	.	.	.	.	06			
V	591.3	00.7	02.5	01.8	01.7	03.5	00.0	10.6	31	-04.0	10	30	04.9	04	03.2	.	.	.	.	06	06.5	35	02.6	05	02.2	08	04.1	05			
VI	593.9	04.9	07.0	05.4	05.7	07.8	03.6	12.8	27	-03.4	13	18	04.1	03	01.7	.	.	.	.	07	05.3	43	04.8	.	.	12	04.2	07			
VII	597.1	09.0	10.8	09.0	09.4	12.0	06.7	15.0	16	-01.0	20	15	03.5	01	02.0	.	.	.	.	09	05.4	28	04.6	01	02.0	22	05.5	17			
VIII	598.1	10.5	12.7	10.4	11.0	13.9	08.5	19.8	04	00.8	12	34	04.6	11	04.1	05	04.4	01	03.0	17	03.6	10	05.0	01	03.0	.	.	14			
IX	595.8	06.8	08.5	06.7	07.2	09.5	05.3	14.6	06.04	-03.0	27	16	03.1	01	02.0	02	03.0	.	.	13	05.4	41	06.2	01	04.0	08	05.8	08			
X	588.7	-01.1	-00.3	-00.1	-00.9	01.0	-02.6	05.4	13	-09.4	31.30	09	C4.1	.	.	.	.	.	.	15	06.9	61	06.9	02	03.0	05	03.4	01			
XI	592.2	-02.7	-01.7	-02.2	-02.2	-00.6	-03.8	07.7	18	-10.4	02	08	05.4	.	.	.	.	.	.	05	07.2	48	02.0	06	04.0	16	05.2	07			
XII	592.1	-04.7	-04.4	-04.9	-04.7	-02.7	-06.6	04.0	29	-14.0	31	44	07.5	.	.	.	.	.	.	01	06.0	16	06.6	04	05.5	24	05.6	04			
GOD.	592.6	00.6	02.0	01.0	01.1	03.1	-00.8	19.8	4VII	-14.0	31XII	306	05.2	33	03.4	18	03.3	02	03.0	125	05.6	384	05.9	32	03.8	102	05.0	93			
$\varphi = 43^{\circ}49'$ N $\lambda = 18^{\circ}20'$ E Gr. $\Delta G = +1h\ 13\ min.$														SARAJEVO-AERODROM												BR. ST.142					
I	722.2	-00.8	01.8	00.1	00.3	02.7	-01.8	06.6	22	-07.0	15	.	.	01	02.0	04	01.5	02	01.5	.	.	.	02	02.0	05	02.4	79				
II	715.2	00.4	08.9	03.7	04.2	10.0	-00.5	15.8	17.12	-05.7	09	02	02.5	04	01.5	03	02.0	08	03.8	05	03.6	03	03.3	07	01.9	05	02.0	47			
III	717.4	02.0	12.9	06.8	07.1	14.0	00.7	24.6	21	-04.4	02	.	.	04	03.8	01	03.0	09	02.6	02	03.0	01	02.0	11	02.0	09	C2.3	56			
IV	714.4	04.5	12.0	07.0	07.6	13.2	02.3	20.3	30	-02.4	21	01	C2.0	07	02.3	04	02.5	06	03.2	02	03.0	09	01.8	13	C2.5	45					
V	715.5	08.9	16.6	11.4	12.1	18.3	06.1	25.4	31	00.8	06	07	02.4	02	02.0	02	01.5	09	03.1	01	04.0	02	01.5	05	02.8	16	C2.0	49			
VI	716.3	12.9	20.8	15.1	16.0	22.4	05.9	26.0	27.23	03.2	14	03	01.7	01	02.0	05	02.2	17	02.2	03	02.3	.	.	02	02.0	22	02.4	37			
VII	718.7	13.8	23.9	16.8	17.8	25.2	10.5	33.8	15	-06.1	09	02	02.0	.	01	01.0	02	02.5	06	04.0	03	02.0	08	02.2	18	C2.2	57				
VIII	718.9	13.9	25.8	17.2	18.5	27.0	11.6	32.7	04	05.4	12	02	02.0	02	03.0	06	01.8	05	03.0	01	01.0	02	01.5	06	02.2	12	07.1	57			
IX	717.9	12.1	21.4	14.2	15.5	22.6	10.1	30.3	04	01.3	28	03	01.7	02	02.0	08	01.9	08	03.2	03	03.3	02	02.5	05	02.2	12	C2.1	47			
X	714.2	04.3	11.3	05.9	06.4	12.4	02.3	18.8	04	-03.2	31.28	01	01.0	01	02.0	05	02.8	09	03.4	02	02.0	01	03.0	06	02.3	10	02.2	58			
XI	719.2	00.1	08.1	02.8	03.4	09.1	-01.0	16.8	19	-08.0	29	01	02.0	.	.	.	.	03	03.3	01	02.0	.	.	03	02.0	04	03.0	78			
XII	721.2	-02.2	00.7	-01.4	-01.1	01.6	-04.0	05.4	12	-12.0	25	04	02.8	01	02.0	04	01.8	.	.	02	01.0	.	.	04	02.0	12	C2.2	64			
GOD.	717.6	05.8	13.7	08.3	09.0	14.9	03.8	33.8	4VII	-12.0	25.XII	26	02.2	25	02.4	43	02.0	78	02.9	24	02.9	17	02.3	70	02.1	138	C2.2	674			
$\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1h\ 14\ min.$															SARAJEVO												BR. ST.143				
I	710.9	-01.3	02.1	00.6	00.5	03.0	-01.7	08.7	22	-06.4	15	.	.	01	02.0	04	01.5	02	01.5	05	01.0	15	01.2	05	C1.6	44					
II	704.2	01.8	08.8	04.0	04.6	09.8	00.6	15.9	17	-05.6	09	01	01.0	03	03.3	22	02.2	18	02.4	03	04.3	13	01.9	11	01.5	01	01.0	12			
III	705.5	03.7	12.3	07.3	07.7	13.5	02.5	24.7	21	-04.1	01	02	02.0	01	04.0	25	02.6	31	02.4	04	02.8	05	02.2	10	01.9	05	01.6	10			
IV	703.6	05.0	11.4	07.0	07.6	13.0	03.0	20.3	30	-01.0	20	02	C2.0	04	01.8	16	02.0	18	02.1	06	02.0	07	02.0	10	01.8	04	C1.8	23			
V	704.8	09.2	15.9	11.7	12.2	17.8	06.8	26.0	31	03.6	10	02	03.0	03	01.7	11	01.8	11	01.4	09	02.3	08	01.5	13	01.6	05	C1.4	31			
VI	705.7	13.2	20.1	15.2	15.9	21.6	10.7	27.3	27	04.9	14	03	01.3	.	.	14	01.7	10	01.6	06	02.8	03	02.0	26	02.0	04	02.5	24			
VII	708.1	14.7	23.5	17.5	18.3	24.5	12.2	33.1	17	-06.9	09	01	02.0	.	.	10	02.0	13	02.0	02	02.0	05	02.2	23	01.8	04	02.0	35			
VIII	708.2	14.7	25.7	18.2	19.2	22.6	13.1	32.6	19	06.9	12	02	C1.5	02	03.0	21	01.8	13	01.6	04	01.8	15	01.8	05	02.0	31					
IX	707.3	12.6	21.4	14.8	15.9	22.4	11.1	29.6	04	02.3	28	02	01.5	.	.	13	01.7	15	01.7	06	03.5	04	01.5	14							

Mjesec	Oblačnost Nm (0-10)			Indoklizacije broj sati (Dides)	Vlažnost vazduha			Padavine R mm			Broj dana na sat																										
	7	14	21		e <sub>m</sub>	U m	t	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■										
	mm	7	14	21	mm	mm	°C	mm	mm	mm	mm	mm	mm	mm	mm	mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■										
<b>BEJELAŠNICA</b>																																					
BR. ST.141																																					
I	6.2	7.1	4.9	6.1	059.9	02.7	45	64	84	84	20	022	C17.7	01	04	30	21	•	•	•	27	12	C5	12	11	08	•	11	•	•	•	•	21	31			
II	7.4	7.7	6.8	7.3	058.5	03.1	54	56	93	93	67	047	D11.4	04	05	25	28	•	•	•	24	19	04	16	13	11	01	•	13	•	•	•	•	01	75	29	
III	6.5	6.5	5.7	6.2	151.0	03.2	74	78	80	77	33	063	C17.3	07	02	15	20	•	•	•	21	19	03	11	11	08	62	07	11	01	•	01	15	31			
IV	7.9	8.7	8.7	8.3	072.8	03.4	91	89	91	90	48	080	D18.2	10	•	16	29	•	•	•	26	20	15	02	02	18	02	•	•	•	•	•	28	30			
V	7.4	8.0	6.6	7.5	111.7	04.2	90	85	88	88	40	066	C14.0	36	•	04	18	•	•	•	27	21	01	13	19	15	02	12	12	01	•	01	03	31			
VI	7.3	7.7	7.7	7.5	115.2	05.6	61	80	86	83	21	087	C14.9	02	•	01	04	•	•	•	22	18	C7	17	19	03	16	04	•	01	•	03	04	25	10		
VII	6.4	5.5	3.8	4.5	255.4	06.0	65	68	76	70	23	016	C04.8	08	•	•	04	•	•	•	20	17	13	05	05	09	05	02	01	•	04	16	•				
VIII	3.5	5.6	3.5	4.2	279.7	06.3	52	62	71	65	20	097	C21.3	29	•	•	•	•	•	•	15	09	13	06	14	12	04	14	•	•	•	02	08	15	•		
GOD.	7.4	7.2	6.1	6.6	1553.9	04.3	82	87	85	83	20	887	D32.5	6.6	•	22	144	223	•	•	•	207	220	60	162	171	134	30	70	114	02	01	01	07	25	278	243
<b>SARAJEVO-AERODROM</b>																											$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$										
BR. ST.142																											$H_s = 510 \text{ m } H_b = 511.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
I	5.7	6.7	5.2	6.8	027.4	04.3	93	84	93	90	60	050	D15.8	18	•	03	23	•	•	•	24	15	C7	02	11	C8	01	•	•	•	•	•	21	6			
II	7.4	7.7	5.5	6.7	059.2	03.4	65	56	76	75	40	078	D35.2	04	•	15	•	•	•	07	•	03	11	09	C7	03	03	•	•	•	01	03	01	01			
III	7.3	7.1	5.8	6.7	121.1	05.3	83	52	74	72	12	025	D09.6	07	•	12	•	•	•	03	•	05	13	C8	05	•	04	04	•	•	•	01	01	01	01		
IV	7.0	8.1	6.4	7.6	121.1	05.7	83	57	76	74	34	078	D15.4	17	•	05	•	•	•	03	•	02	14	16	02	15	05	•	•	•	02	02	02	02			
V	6.7	7.3	6.4	7.6	147.7	07.7	86	54	78	73	34	092	C23.5	23	•	•	01	•	•	02	•	01	12	21	13	03	21	•	•	•	•	•	06	05			
VI	6.1	7.3	6.7	6.7	155.0	10.0	86	55	79	73	37	094	C27.7	30	•	•	08	•	•	04	•	03	10	14	12	02	04	•	•	•	07	04	•				
VII	6.3	5.1	3.5	4.7	264.6	11.0	87	53	81	74	25	057	C17.7	20	•	•	15	09	•	01	02	07	09	07	03	09	•	•	•	04	06	•					
VIII	6.0	4.9	3.8	4.6	298.6	11.9	93	51	84	76	30	055	D11.4	24	•	•	20	10	•	01	01	07	05	12	11	01	•	•	•	17	15	•					
IX	8.7	5.6	3.5	6.0	151.1	10.6	92	59	86	79	37	089	D15.4	22	•	•	08	01	•	04	01	•	05	12	10	05	12	•	•	•	01	01	14	•			
X	5.2	7.3	7.0	7.2	093.0	06.2	91	47	89	81	39	257	D06.2	24	•	06	01	•	16	20	20	10	20	02	02	•	•	•	01	14	01	01					
XI	5.2	6.7	5.5	7.1	071.3	05.0	94	70	80	85	46	073	D26.6	25	•	01	21	•	•	02	•	11	09	08	02	07	04	01	•	•	01	14	03	•			
XII	9.7	8.4	8.1	8.7	014.9	04.1	94	91	95	93	60	051	D27.1	13	02	11	29	•	•	07	24	12	07	01	09	06	01	•	•	•	22	22	27				
GOD.	7.4	7.4	5.6	6.6	1477.1	07.2	80	62	83	78	12	1005	D06.2	24	•	107	56	20	•	34	03	29	152	157	122	35	146	43	33	05	•	•	03	46	118	36	
<b>SAHAJEVAC</b>																											$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
BR. ST.143																											$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
I	6.2	6.6	7.4	8.1	033.4	04.3	94	64	92	90	62	057	C17.5	20	•	01	21	•	•	•	02	20	19	06	02	13	C5	01	•	01	•	16	15				
II	7.2	6.7	6.2	6.7	116.2	04.4	80	54	72	79	26	071	D40.7	04	•	12	•	•	06	01	03	12	09	C5	02	07	05	•	•	•	01	04	07				
III	6.4	6.8	5.2	6.1	126.2	04.6	76	74	69	64	30	018	D04.9	07	•	16	•	•	04	•	05	13	10	06	•	05	06	•	•	01	04	01	01				
IV	6.7	6.5	6.7	7.5	114.1	05.3	81	56	72	69	27	066	D12.7	17	•	02	•	•	04	•	01	14	18	15	01	18	06	05	•	02	01	07	02	02			
V	7.5	7.9	6.1	6.8	144.2	07.4	83	56	72	70	34	061	C17.0	23	•	•	01	•	•	03	10	23	16	03	23	•	•	•	•	•	07	•					
VI	7.6	7.6	7.0	6.8	175.4	09.3	81	53	73	70	28	123	C31.1	30	•	•	06	01	02	11	20	15	04	20	20	•	•	•	•	•	02	01	01				
VII	4.5	4.5	3.2	4.1	252.1	10.3	80	51	71	68	24	055	C14.9	20	•	•	16	06	•	•	14	07	08	07	03	08	•	•	•	05	•	01					
VIII	3.5</td																																				





Mesec	Vezduljani pričesak pm. min.	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, Fm (0-12)																				
		Tm		7	14	21	Sred. (dišes)	Max	Min	Dat.	Max	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
				8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.									
		$\varphi = 42^{\circ}41'N \lambda = 18^{\circ}20'E$ Gr. $\Delta G = + 1h\ 14\ min.$																												
I	-	00.3	08.8	02.9	03.7	09.3	-00.6	12.4	20	-05.6	15	*	*	03	01.0	C1	01.0	12	01.4	*	02	01.0	01	01.0	26	01.7	48			
II	-	03.4	10.8	05.1	06.1	11.5	02.0	17.0	16	-03.0	11.09	*	*	02	01.5	*	15	02.1	*	04	02.5	01	01.0	22	01.6	40				
III	-	04.3	14.7	07.5	08.5	15.4	02.5	23.6	22	-01.6	13	*	*	07	01.1	C4	01.0	12	01.4	*	*	*	*	*	28	02.5	42			
IV	-	07.8	15.1	09.6	10.5	16.1	04.9	20.6	29	-00.4	20	*	*	07	01.3	01	01.0	25	01.6	*	*	*	01	01.0	17	02.2	39			
V	-	12.0	19.2	13.7	14.6	20.0	06.1	25.6	21	04.0	11	*	*	04	01.5	04	01.2	16	01.4	*	*	*	*	*	30	02.4	39			
VI	-	15.8	23.8	18.0	18.9	24.4	11.0	29.0	27	05.0	13	*	*	05	01.0	02	01.5	09	01.3	*	02	01.0	*	*	*	38	02.3	34		
VII	-	17.5	27.7	20.1	21.4	28.8	12.3	35.6	17	07.4	09	02	02.0	02	01.5	C1	02.0	01	02.0	*	*	01	01.0	*	39	02.3	47			
VIII	-	18.1	29.3	22.5	23.1	30.4	13.6	35.0	05	08.2	14	*	*	02	01.5	*	10	01.2	*	*	*	*	*	*	33	02.6	48			
IX	-	14.1	24.2	18.2	18.6	25.3	11.7	30.4	05	04.0	28	*	*	05	01.2	*	09	01.2	*	*	02	02.0	31	02.6	43					
X	-	08.1	14.4	09.7	10.5	15.0	06.1	20.6	12	-01.0	28	*	*	08	01.5	*	02	01.0	*	08	02.5	*	43	01.8	38					
XI	-	03.2	11.8	05.5	06.5	12.3	02.1	16.0	06	-02.0	02	07	04.6	12	01.4	C3	02.7	17	01.5	*	02	01.0	01	02.0	23	02.0	36			
XII	-	00.8	08.2	02.1	03.3	08.7	-00.5	14.4	04	-05.4	24	*	*	07	04.6	12	01.4	03	01.0	*	01	01.0	01	02.0	19	01.8	36			
GOD.	-	08.8	17.3	11.2	12.1	18.1	06.1	35.6	F/V	-05.6	151	*	*	09	04.0	59	01.3	19	01.4	142	01.7	*	*	20	01.9	67	01.6	349	02.2	490
		SR SRBLJA																												
		$\varphi = 46^{\circ}06'N \lambda = 19^{\circ}46'E$ Gr. $\Delta G = + 1h\ 18\ min.$																												
I	758.5	-00.4	03.8	01.2	01.5	04.3	-01.5	10.5	20	-08.8	15	03	02.3	10	02.0	17	07.0	28	02.4	06	01.8	07	01.9	10	02.1	10	03.1	02		
II	750.8	01.9	09.9	04.7	05.3	10.6	00.8	16.4	17	-04.5	28	05	01.6	08	01.9	12	01.9	22	02.4	15	02.3	12	02.5	05	02.2	05	02.4	*		
III	754.1	03.5	13.1	06.8	07.5	14.0	02.2	26.0	21	-05.2	01	02	01.5	14	01.7	24	07.4	26	02.9	09	02.1	12	02.2	02	04.5	02	01.0	02		
IV	749.8	06.6	15.1	08.7	09.8	16.0	03.5	23.5	30	-02.9	16	17	02.7	15	02.1	10	02.5	20	02.6	05	02.0	09	01.9	07	01.9	05	02.0	02		
V	749.3	12.3	18.3	13.1	14.2	19.6	08.7	28.5	31	02.6	10	08	02.1	02	02.5	04	02.2	07	01.3	08	01.9	13	01.8	26	02.2	18	01.9	07		
VI	749.5	15.6	21.1	16.1	17.2	22.6	11.9	30.3	27	07.5	08	05	02.6	01	01.0	02	02.0	08	01.9	09	01.4	09	01.7	20	01.8	29	02.8	10		
VII	752.1	17.4	24.5	18.2	19.6	26.0	13.4	34.0	14	08.1	09	05	02.0	09	01.6	02	02.0	08	01.9	03	02.3	03	02.0	13	02.1	10	02.3	07		
VIII	752.7	18.9	27.3	20.1	21.6	28.4	15.7	35.5	04	09.6	08	05	02.0	09	01.6	02	02.0	09	01.9	07	01.9	05	02.0	13	02.1	10	02.3	07		
IX	752.2	13.1	22.3	14.9	16.3	23.6	09.9	30.5	03	00.6	28	10	07.1	15	01.6	15	01.5	05	02.4	06	01.3	08	01.0	10	01.8	14	02.4	07		
X	749.0	05.4	10.9	06.8	07.5	11.9	04.1	19.0	04	-01.3	31	10	02.1	06	02.3	09	01.8	08	01.6	14	02.0	16	01.9	20	02.0	09	01.6	01		
XI	754.0	02.3	09.7	04.3	05.2	10.3	01.5	19.1	16	-03.8	10	11	02.5	09	02.0	10	01.6	11	02.2	16	01.5	13	01.0	11	02.5	07	02.7	02		
XII	755.4	01.8	05.3	02.3	02.9	06.2	00.4	13.3	29	-04.2	24	14	07.3	03	01.9	07	01.9	05	02.4	08	01.6	19	01.9	18	02.4	20	02.4	*		
GOD.	752.3	08.2	15.1	09.8	10.7	16.1	05.9	35.5	F/V	-08.8	151	97	02.3	107	01.9	132	01.9	156	02.3	103	01.8	138	01.9	162	02.1	154	02.4	46		
		$\varphi = 45^{\circ}47'N \lambda = 19^{\circ}05'E$ Gr. $\Delta G = + 1h\ 16\ min.$																												
I	-	00.1	03.6	01.4	01.7	04.2	-00.9	09.8	20	-05.8	15	04	04.5	04	02.0	08	01.9	23	02.8	03	01.3	02	01.0	05	01.6	08	03.2	36		
II	-	01.9	09.7	04.9	05.4	10.5	01.1	16.5	17.12	-03.7	22	05	01.5	03	02.7	07	02.0	14	02.9	17	02.1	06	02.5	02	02.0	03	03.7	30		
III	-	03.4	12.9	07.0	07.6	13.6	01.9	24.8	21	-03.6	14	04	02.2	*	*	11	02.6	43	03.8	04	02.0	04	02.0	05	02.4	*	24	*		
IV	-	06.6	14.9	09.2	10.0	15.8	03.7	24.0	28	-03.5	04	12	03.0	09	03.6	05	03.0	18	03.4	04	02.2	01	02.0	06	01.9	08	02.0	25		
V	-	12.4	18.5	13.5	14.5	19.6	09.0	27.9	31	03.5	10,09	11	02.5	01	03.0	02	02.0	03	02.3	05	01.6	06	01.7	17	01.8	16	02.6	30		
VI	-	15.7	20.9	16.6	17.4	22.4	12.3	29.8	27	08.2	08	08	03.1	02	02.0	02	01.0	01	02.0	05	01.6	06	02.0	11	02.2	22	03.2	33		
VII	-	17.8	24.6	18.6	19.9	26.0	13.7	34.1	17	09.2	27	17	02.9	*	*	11	01.0	02	01.5	11	01.5	02	02.0	13	02.0	16	02.6	31		
VIII	-	18.7	27.2	20.5	21.7	28.1	15.3	34.1	03	08.7	07	02	03.0	04	01.2	07	02.9	06	04.0	04	01.5	03	01.7	07	01.8	08	02.8	55		
IX	-	13.2	21.7	15.3	16.4	22.8	10.8	28.7	03	02.0	28	11	02.5	04	01.5	05	01.4	11	01.6	02	01.5	06	02.0	01	03.0	09	02.6	44		
X	-	05.3	10.5	06.4	07.4	11.8	03.9	19.2	04	-01.3	31	11	02.6	05	02.2	02	02.0	07	02.3	11	01.8	08	02.0	13	02.1	04	02.0	32		
XI	-	02.4	09.7	04.5	05.3	10.4	01.7	19.5	16	-02.3	10	12	02.2	07	02.6	01	02.0	09	01.6	13	01.7	06	01.3	03	02.3	08	03.2	37		
XII	-	01.6	05.3	02.4	02.9	06.1	00.3	12.3	29	-04.2	24,23	17	07.3	07	01.9	*	*	05	02.2	08	01.6	10	01.5	16	01.8	07	03.7	33		
GOD.	-	08.8	15.0	10.1	10.8	15.9	06.1	34.1	F/V	-05.8	151	95	02.9	46	02.4	51	02.2	142	02.9	87	01.8	57	01.6	98	02.0	111	02.9	408		
		$\varphi = 45^{\circ}07'N \lambda = 19^{\circ}15'E$ Gr. $\Delta G = + 1h\ 17\ min.$																												
I	-	-00.3	04.1	01.6	01.7	04.9	-01.1	09.5	22	20	-08.0	15	04	01.2	03	01.7	04	03.0	57	03.2	03	01.3	02	02.0	04	02.2	16	03.1	*	
II	-	02.7	10.4	05.8	06.2	11.5	01.9	17.8	12	-02.5	28	09	02.4	04	01.5	06	03.5	55	03.4	02	03.0	02	02.5	02	01.5	04	02.2	*		
III	-	04.7	13.3	08.0	08.5	14.0	03.6	26.5	21	-02.5	01	01	03	09	01.7	18	03.2	52	04.4	04	01.5	05	02.0	05	03.0	07	02.0	*		
IV	-	06.8	14.9	09.8	10.3	16.0	05.2	24.0	28	00.5	20	06	03.4	15	02.6	07	03.1	51	02.8	04	02.5	05	01.6	04	02.8	16	02.3	*		
V	-	11.9	19.0	13.4	14.4	20.1	09.8	28.5	31	05.0	10	06	07.8	10	01.9	03	01.7	14	02.1	05	01.4	04	01.8	18	02.0	35	02.9	*		
VI	-	15.9	21.9	16.8	17.9	23.2	12.9	30.0	27	08.0	13	07	02.0	07	02.4	08	01.8	24	02.4	06	02.0	11	02.2	22	03.2	33	02.9	*		
VII	-	17.8	24.8	19.1	20.2	26.6	14.0	35.0	17	08.5	09	04																		

Meseč	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm				Broj dana na s:																
	Iznosljivo satni broj (dnev.)					Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ				
	7	14	21	Sred. (dnev.)	mm	7	14	21	Sez.	Mje	Σ	Max	Dat.	≤	<	<	≥	≥	IV	IV	IV	IV	IV			
LASTVA																										
BR. ST.151												$H_s = 295 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$														
I	3.6	4.7	3.5	3.9	-	05.0	9.0	65	88	81	40	054	018.7	04	.	.	21	*	.	.	.	.	.	01	01	
II	6.2	5.8	4.1	5.4	-	05.8	89	62	89	80	29	264	078.3	04	.	.	05	*	.	.	.	.	.	01	02	
III	3.5	4.9	3.1	3.9	-	06.1	91	48	84	74	20	118	055.2	06	.	.	06	*	.	.	.	.	.	01	02	
IV	4.9	7.1	5.2	5.7	-	07.1	86	52	85	75	24	114	025.2	17	.	.	01	*	.	.	.	.	.	03	03	
V	4.3	5.9	4.7	5.2	-	09.0	86	50	82	73	30	147	042.0	05	.	.	04	*	.	.	.	.	.	01	01	
VI	4.0	4.9	3.3	4.1	-	11.2	81	48	78	69	33	103	033.5	30	.	.	16	*	.	.	.	.	.	01	03	
VII	1.7	2.9	2.0	2.2	-	11.5	77	36	73	62	19	011	006.5	08	.	.	25	13	*	.	.	.	.	01	02	
VIII	1.5	3.4	1.2	2.0	-	12.3	73	36	74	61	17	031	011.8	29	.	.	29	18	*	.	.	.	.	05	05	
IX	4.0	4.0	3.0	3.7	-	11.4	84	52	81	72	34	355	094.2	21	.	.	18	02	*	.	.	.	.	10	01	
X	6.5	6.4	6.1	6.3	-	07.7	90	62	86	79	43	559	067.5	22	.	.	01	*	.	.	.	.	.	06	05	
XI	5.1	5.2	3.8	4.7	-	05.7	91	60	86	79	25	166	071.1	26	.	.	01	*	07	10	08	05	10	01	01	
XII	5.4	5.4	3.1	4.6	-	04.7	88	61	87	79	44	072	044.2	13	.	.	18	*	.	.	.	.	.	02	04	
GOD.	4.3	5.0	3.6	4.3	-	08.1	85	52	82	73	17	1994	094.2	20X	.	.	53	92	33	*	.	.	.	.	02	02
PALIC																										
BR. ST.152												SR SRBIJA $H_s = 102 \text{ m } H_b = 104.9 \text{ m } h_t = 2.0 \text{ m } h_r = 1.4 \text{ m}$														
I	7.8	8.1	8.4	8.1	070.6	04.4	89	76	89	85	54	029	008.7	20	.	01	20	*	.	.	.	.	.	10	01	
II	7.2	6.5	4.9	6.2	103.3	05.0	87	60	79	75	34	017	011.5	24	.	.	12	*	.	.	.	.	.	02	05	
III	6.0	6.0	4.5	5.5	184.8	05.1	81	48	72	67	22	026	007.1	12	.	.	11	01	*	.	.	.	.	01	02	
IV	5.8	7.5	5.7	6.3	-	05.5	74	42	67	61	25	028	008.0	26	.	.	04	*	.	.	.	.	.	01	02	
V	6.5	7.7	5.7	6.6	204.3	09.0	83	58	81	74	33	105	026.3	23	.	.	04	*	.	.	.	.	.	05	01	
VI	5.4	7.5	5.0	6.3	213.4	10.9	80	58	82	73	37	170	056.9	30	.	.	09	01	*	.	.	.	.	08	04	
VII	5.0	5.2	4.0	4.7	285.7	11.9	81	49	77	69	31	040	008.2	07	.	.	16	07	*	.	.	.	.	04	04	
VIII	4.1	5.0	2.8	4.0	292.1	13.7	83	49	80	71	34	073	024.6	09	.	.	26	12	*	.	.	.	.	06	07	
IX	4.2	6.0	3.7	4.6	212.6	10.4	88	53	83	75	39	014	006.9	27	.	.	12	01	*	.	.	.	.	01	04	
X	7.5	6.5	6.4	7.5	079.5	06.7	94	72	91	86	42	166	021.8	29	.	.	02	*	.	.	.	.	.	10	01	
XI	7.6	6.4	5.4	6.5	106.3	05.4	92	66	88	62	40	030	012.9	26	.	.	09	*	.	.	.	.	.	10	01	
XII	8.5	8.3	7.5	8.1	050.8	04.9	90	75	89	85	44	036	014.8	08	.	.	02	13	*	.	.	.	.	01	11	
GOD.	6.3	6.9	5.4	6.2	-	07.7	85	58	81	75	22	684	056.9	30VI	.	.	03	71	68	21	*	.	.	.	01	02
SCMBOR																										
BR. ST.153												$H_s = 88 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$														
I	8.2	7.1	6.1	7.1	058.7	04.4	88	77	87	84	60	025	010.0	20	.	01	20	*	.	.	.	.	.	04	01	
II	7.1	6.8	5.4	6.4	090.0	05.1	85	60	79	75	38	019	009.5	24	.	.	12	*	.	.	.	.	.	02	02	
III	5.3	6.0	4.5	5.2	182.9	05.0	80	50	68	66	23	021	006.6	08	.	.	10	*	.	.	.	.	.	01	02	
IV	6.0	7.2	5.3	6.2	169.0	05.7	77	45	65	62	26	033	008.6	26	.	.	05	*	.	.	.	.	.	01	02	
V	5.8	7.3	5.5	6.2	202.0	09.0	82	56	80	73	36	075	026.2	23	.	.	04	*	.	.	.	.	.	07	07	
VI	5.4	6.9	5.0	5.8	203.9	11.1	82	59	81	74	37	225	083.3	30	.	.	08	*	.	.	.	.	.	08	02	
VII	4.0	4.8	3.4	4.1	288.9	12.1	80	49	80	69	33	044	007.1	02	.	.	17	06	*	.	.	.	.	02	02	
VIII	4.0	4.5	3.1	3.8	285.8	14.1	87	52	80	73	34	077	037.6	22	.	.	26	12	*	.	.	.	.	04	02	
IX	5.1	5.8	3.6	4.8	192.4	11.0	90	59	85	78	44	013	004.9	27	.	.	11	*	.	.	.	.	.	02	01	
X	7.1	6.3	6.1	7.2	085.7	06.8	94	75	91	87	46	146	033.4	29	.	.	01	*	.	.	.	.	.	04	04	
XI	6.7	6.2	4.8	5.9	103.8	05.7	93	71	90	84	41	034	012.4	26	.	.	06	*	.	.	.	.	.	08	08	
XII	8.1	7.8	6.2	7.4	055.4	05.0	90	80	90	87	57	054	011.5	19	.	.	02	15	*	.	.	.	.	08	02	
GOD.	6.1	6.6	4.9	5.8	1918.5	07.9	85	61	81	76	23	744	062.0	49VII	.	.	02	52	76	26	06	*	.	.	32	09
BAČKI PETROVAC																										
BR. ST.155												$H_s = 85 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$														
I	6.4	6.6	5.0	6.0	073.9	04.5	90	79	89	86	54	021	009.4	20	.	01	21	*	.	.	.	.	.	10	02	
II	5.7	5.6	5.3	5.5	112.7	05.6	89	62	79	77	44	009	003.6	24	.	.	08	*	.	.	.	.	.	04	02	
III	5.0	4.9	3.8	4.6	177.8	05.8	83	55	75	71	26	023	007.6	06	.	.	10	03	*	.	.	.	.	01	02	
IV	5.2	6.5	5.9	5.9	173.9	06.7	82	55	78	71	25	035	010.1	18	.	.	02	*	.	.	.	.	.	01	02	
V	5.5	6.1	5.4	5.7	193.4	10.1	86	63	89	79	45	069	017.6	23	.	.	05	*	.	.	.	.	.	06	06	
VI	5.2	6.4	5.1	5.6	204.3	-	-	-	-	-	-	120	025.1	11	.	.	12	01	*	.	.	.	.	01	07	
VII	4.3	4.3	3.3	4.0	259.8	-	-	-	-	-	-	058	013.9	19	.	.	22	11	*	.	.	.	.	02	02	
VIII	3.5	3.6	2.7	3.2	282.3	-	-	-	-	-	-	070	023.9	12	.	.	26	12	*	.	.	.	.	03	03	
IX	4.5	5.1	3.4	4.4	181.9	12.2	92	64	89	82	44	038	015.8	27	.	.	15	02	*	.	.	.	.	02	02	
X	7.4	7.0	6.0	6.8	084.0	07.5	96	61	95	91	54	094	014.8	16	.	.	01	*	.	.	.	.	.	01	08	
XI	6.6	5.8	5.5	5.8	086.0	06.2	96	74	90	85	52	032	007.1	26	.	.	09	*	.	.	.	.	.	12	01	
XII	7.2	7.4	6.6	7.6	043.7	05.3	94	88	92	91	64	050	009.1	08	.	.	02	14	16	.	.	.	.	09	02	
GOD.	5.6	5.6	4.8	5.4	1873.7	-	-	-	-	-	-	619	025.1	KVI	.	.	03	65	83	26	*	.	.	.	01	02

Mesec	Vazdušni Pritisak Pn. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																
		7	14	21	sred. (Cles)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		V = 45°49'N λ = 19°39' E Grd. ΔGrd + 1h 18 min.										BACKA TOPOLA												BR. ST.156				
I	-	-00.2	03.8	01.4	01.6	04.5	-01.0	09.9	26 -07.5	15	.	10	01.4	.	.	48	01.6	.	10	01.0	.	.	16	02.4	09			
II	-	02.6	09.8	05.7	06.0	16.9	02.0	17.0	13 -01.8	28	.	09	01.2	.	.	48	01.7	01	01.0	13	01.2	.	.	10	01.2	06		
III	-	03.8	13.2	07.4	08.0	13.8	02.4	25.8	21 -03.0	03.02	.	10	01.0	.	.	57	02.1	.	.	13	01.5	.	.	03	01.7	10		
IV	-	06.1	15.1	09.4	10.0	16.2	04.3	23.7	26 -01.3	04	.	19	01.4	.	.	33	01.0	.	.	13	01.0	.	.	16	01.4	09		
V	-	11.8	18.4	13.9	14.5	20.0	09.3	28.6	31 04.0	10	01	01.0	04	01.0	.	.	12	01.2	.	.	27	01.1	02	01.5	32	01.2	15	
VI	-	15.5	21.7	16.9	17.7	23.1	12.7	31.4	27	06.5	08	.	07	01.0	.	.	09	01.1	.	.	30	01.1	.	.	30	02.3	14	
VII	-	17.0	24.8	19.7	20.3	26.4	14.1	34.3	17 09.0	09	01	02.0	07	01.0	.	.	20	01.1	.	.	12	01.1	.	.	41	01.8	17	
VIII	-	16.6	28.1	21.2	22.3	28.9	16.3	35.3	04	10.1	07	.	19	01.0	.	.	28	01.1	.	.	07	01.0	.	.	21	01.1	07	
IX	-	13.0	23.1	15.9	16.9	24.0	10.9	31.1	03 02.9	28	01	01.0	13	01.0	.	.	21	01.1	.	.	11	01.0	.	.	21	01.5	23	
X	-	05.7	11.0	07.4	07.9	11.9	04.2	20.4	04 -01.1	31	.	08	01.0	.	.	26	01.2	02	01.0	26	01.3	01	01.0	20	01.0	10		
XI	-	02.6	09.8	04.9	05.6	10.4	01.6	18.9	17 -02.8	10	.	15	01.1	.	.	37	01.2	01	01.0	10	01.2	.	.	14	01.4	10		
XII	-	01.4	05.0	02.6	02.9	05.7	00.4	11.6	25	.	11	01.0	.	.	17	01.1	.	.	32	01.0	.	.	31	01.6	10			
GOD.	-	06.2	15.3	10.5	11.1	16.3	06.5	35.3	04 00 -07.5	11	03	01.3	11.8	01.1	.	.	356	01.6	04	01.0	204	01.1	03	01.3	256	01.6	151	
		V = 45°34'N λ = 19°39' E Grd. ΔGrd + 1h 18 min.										VRBAS												BR. ST.157				
I	-	-00.4	03.8	00.8	01.3	04.6	-01.4	10.0	22.2	20 -08.1	15	02	01.5	09	02.6	13	02.5	22	03.5	.	.	01	02.0	12	02.4	05	05.0	19
II	-	01.5	10.4	04.6	05.3	11.5	00.8	18.0	12 -03.6	09	03	02.1	02	01.0	20	04.0	20	03.3	06	02.5	05	03.0	02	02.1	02	02.5	18	
III	-	03.9	13.1	06.9	07.7	14.0	02.2	25.8	21 -04.0	03	02	01.5	33	03.1	33	03.7	04	01.6	07	01.6	03	02.0	02	01.0	12	02.0	08	
IV	-	07.1	15.3	08.8	10.0	16.3	03.9	23.8	28 -00.8	04	06	03.7	13	03.0	14	02.4	16	03.1	04	02.2	.	.	15	02.0	08	03.4	14	
V	-	12.7	18.8	13.5	14.6	20.1	09.0	28.4	31 03.6	10	08	02.6	02	04.0	03	01.7	03	01.7	05	01.8	32	02.6	05	03.6	32			
VI	-	16.0	21.2	16.5	17.6	23.1	12.2	30.7	27 06.5	08	02	04.0	04	02.0	04	02.2	04	01.5	02	02.5	06	02.0	25	02.7	17	03.7	26	
VII	-	17.6	24.5	18.6	19.8	26.1	13.2	34.5	17 07.0	09	04	03.2	02	01.7	05	01.4	03	02.3	02	02.0	04	01.5	19	01.9	30	03.0	24	
VIII	-	19.1	27.5	20.2	21.7	28.6	15.2	34.8	04 08.4	11	02	03.5	07	02.0	15	01.8	09	02.3	02	01.5	02	01.5	08	02.4	07	01.9	41	
IX	-	13.6	23.2	15.2	16.8	24.2	10.5	30.0	03 01.6	28	04	02.5	04	01.2	16	01.4	03	02.0	02	02.0	01	02.0	12	02.6	09	02.8	39	
X	-	05.9	11.5	06.8	07.8	12.6	03.7	21.0	04 -02.0	31	04	02.8	04	02.0	14	01.6	05	03.0	06	01.7	02	01.5	27	02.7	05	02.4	36	
XI	-	02.3	10.3	03.8	05.1	11.0	01.1	20.8	16 -02.9	10	05	03.0	03	02.3	22	01.9	07	01.7	04	02.0	01	02.0	13	02.9	05	03.8	30	
XII	-	01.1	05.0	02.1	02.6	05.9	00.0	12.0	29 -04.5	23	13	03.7	01	01.3	12	01.7	03	01.4	04	01.7	02	02.0	27	02.2	13	03.4	19	
GOD.	-	08.4	15.4	09.8	10.9	16.5	05.9	34.8	04 00 -08.1	11	01	58	03.6	59	02	13	181	07.1	124	03.0	18	01.9	31	02.4	187	02.4	130	110
		V = 15°20'N λ = 19°51' E Grd. ΔGrd + 1h 18 min.										NOVI SAD-KRUMPSKI SANČEV												BR. ST.158				
I	755.8	-00.3	04.1	06.9	01.4	04.9	-01.1	10.7	22 -08.3	15	04	02.0	C5	01.3	24	02.6	37	04.0	.	.	04	02.0	12	02.4	11	02.3	05	
II	752.2	0.4	10.6	05.3	09.9	11.7	01.7	17.2	12 -03.0	28	01	02.0	04	02.2	15	02.7	57	04.4	06	02.0	02	01.5	02	01.6	03	02.7	03	
III	755.2	0.4	12.9	07.4	08.0	14.0	02.8	26.1	21 -03.2	03	07	03.6	09	02.9	10	02.5	28	04.5	03	02.0	06	01.8	12	02.3	10	02.3	03	
IV	751.0	0.6	14.9	09.1	09.9	16.0	04.4	23.6	28 -02.2	04																		
V	750.8	12.3	18.6	14.2	14.8	20.0	09.4	25.1	31 05.4	11	11	02.7	03	02.0	04	01.8	08	02.2	09	01.2	13	01.9	24	02.1	11	01.9	05	
VI	751.1	15.8	21.8	17.1	17.9	23.2	13.1	31.2	27 06.7	08	04	02.4	02	01.5	05	01.2	19	02.0	03	02.0	08	01.6	21	02.1	05	02.2	05	
VII	753.5	17.9	25.0	19.3	20.3	26.5	14.0	35.4	17 08.5	09	06	01.5	06	01.7	15	01.5	24	02.2	02	01.5	04	01.5	14	02.1	05	02.2	14	
VIII	754.0	10.7	27.8	20.8	22.0	28.9	15.8	35.3	04 11.0	07																		
IX	753.4	13.8	23.0	16.0	17.2	24.3	11.7	36.4	04 03	24.0	26	05	02.4	05	01.6	16	01.7	19	02.1	01	02.0	12	02.4	09	02.8	34		
X	756.6	0.6	11.4	07.6	08.2	13.0	04.7	21.0	04 -02.2	31	02	03.0	03	02.7	15	02.3	22	02.2	04	02.0	07	02.1	24	02.3	12	01.8	04	
XI	755.4	0.2	10.3	04.8	05.6	11.1	01.5	21.0	16 -03.0	28	04	03.7	03	02.7	06	01.0	21	02.7	01	01.0	06	02.0	16	02.1	09	02.6	19	
XII	757.1	0.1	05.3	02.8	03.1	06.3	00.5	13.0	29 -05.6	29																		
GOD.	753.7	0.8	15.5	10.4	11.2	16.7	06.5	35.4	04 00 -08.3	11	01	49	01.9	58	01.7	33	02.6	30.5	03.2	37	02.1	91	01.9	195	02.2	136	02.4	
		V = 15°15'N λ = 19°52' E Grd. ΔGrd + 1h 18 min.										NOVI SAD-PITOVARACIN												BR. ST.159				
I	755.7	0.0	4.1	01.6	01.8	04.8	-06.9	05.5	22 -06.8	15	02	03.6	11	01.5	31	02.4	17	03.7	.	.	11	02.0	11	02.2	07	02.3	03	
II	748.0	0.8	10.4	06.6	07.1	11.2	03.7	16.5	12 -02.2	28	01	02.0	04	02.0	20	02.0	25	02.8	08	02.0	11	01.6	02	02.0	06	02.0	03	
III	751.4	0.5	12.6	06.5	08.9	13.3	04.3	25.5	19 -02.6	01	09	02.2	07	01.9	26	02.2	07	03.2	02	01.5	19	02.2	08	02.6	08	02.2	01	
IV	747.3	0.7	14.6	10.4	10.7	15.3	06.7	23.4	28 02.5	09																		
V	747.3	13.0	18.4	14.8	15.2	19.7	11.1	28.2	31 07.6	09.05	04	01.4	01	01.0	10	02.0	.	08	01.9	33	02.5	22	02.4	15	02.1	.		
VI	747.6	16.3	21.7	18.1	18.5	23.0	13.8	34.5	27 06.2	12.08	05	02.2	03	01.7	12	01.6	07	02.1	03	02.0	23	02.1	20	02.6	17	02.1	05	
VII	750.0	18.4	24.7	20.8	21.2	26.3	15.8	35.7	17 10.6	09	01	02.0	06	01.7	16	02.2	11	02.2	02	01.0	20	01.9	09	02.8	11	01.9	05	
VIII	750.3	19.8	27.4	22.7	23.1	26.3	17.4	35.6	04 11.2	12																		
IX	749.7	15.0	22.3	17.7	18.2	23.5	13.1	29.8	03 07.4	27																		

Mjesec	Oblačnost Nm (0-10)			Inzolacija broj sati	Vlažnost vazduha		Padavine R mm		Broj dana nasa:																											
					em	m			Tn	Tx	Tn	Tx	Tn	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	Δ	Δ	A	A	R	T	≡	H							
	7	14	21	Sred. (danas)		mm	7	14	21	Sum mm	Max	Dan.	<	<	<	<	<	<	V	V	V	V	V	V	V	V	V	V								
<b>BR. ST.156</b>																																				
<b>BAČKA TOPOLA</b>																																				
I	7.7	7.2	7.1	7.3	-	04.5	89	79	90	86	63	024	008.8	20	+	C1	20	+	+	+	C2	01	01	13	10	06	+	07	03	-	-	-	02	01		
II	6.6	6.8	4.0	5.8	-	05.3	85	64	77	76	37	016	012.7	24	+	07	07	+	+	+	06	08	09	01	01	08	01	-	-	-	-	-	02	01		
III	4.8	5.5	3.7	4.6	-	05.5	83	52	75	70	24	024	006.2	26	+	10	01	+	+	+	G2	01	10	07	08	06	+	04	05	-	-	-	01	-		
IV	5.3	6.6	4.6	5.5	-	-	-	-	-	-	032	011.1	-	-	02	02	+	-	-	05	CE	11	04	01	11	-	-	-	-	-	01	-				
V	5.9	6.9	5.4	6.1	-	10.2	89	71	87	82	41	110	C22.5	02	+	04	04	+	+	+	05	11	15	13	05	15	-	-	-	-	-	03	-			
VI	5.3	7.0	5.2	5.8	-	11.3	63	58	62	74	37	155	076.4	30	+	09	01	+	-	-	02	08	17	12	C2	17	-	-	-	-	06	01				
VII	4.8	6.6	4.0	4.5	-	12.7	83	93	76	71	36	041	007.8	20	+	18	09	+	-	-	08	07	17	10	05	17	-	-	-	-	-	03	-			
VIII	3.9	4.2	3.7	4.0	-	14.4	86	51	79	72	33	024	019.7	12	+	26	13	01	-	-	10	04	12	10	01	12	-	-	-	-	-	06	-			
IX	4.0	5.6	3.0	4.1	-	10.7	86	54	80	74	36	015	006.0	27	+	05	16	01	+	-	09	C4	05	04	+	05	-	-	-	-	-	01	02			
X	7.3	7.8	5.8	7.0	-	07.0	93	76	91	87	40	101	021.0	29	+	01	01	+	-	-	03	12	20	18	02	20	-	-	-	-	-	03	-			
XI	7.3	6.4	5.4	6.4	-	05.7	92	69	90	83	45	028	011.5	26	+	05	05	+	-	-	04	11	09	04	02	09	-	-	-	-	-	02	-			
XII	8.5	7.9	6.4	7.6	-	05.0	91	79	90	87	42	050	014.0	08	+	01	12	+	-	-	01	16	15	11	01	14	C3	02	-	-	-	05	01			
GOD.	6.0	6.6	4.9	5.7	-	-	-	-	-	-	638	076.4	80/VI	+	02	57	74	24	01	-	-	62	109	148	99	15	139	12	02	-	-	-	-	18	-	
<b>VRBAS</b>																																				
I	7.5	7.2	5.4	6.7	075.1	04.6	93	83	93	90	67	021	009.4	20	+	01	22	+	+	+	C6	03	02	09	11	06	+	08	03	-	-	-	02	-		
II	6.4	6.0	5.7	6.0	106.5	05.5	92	65	86	81	40	013	009.2	24	+	11	05	+	+	+	07	05	06	11	09	02	+	09	01	01	-	-	01	-		
III	5.3	5.1	4.5	5.0	179.5	05.8	86	58	77	74	29	C32	016.8	06	+	10	04	+	+	+	11	06	11	C9	09	05	01	06	05	-	-	-	01	-		
IV	5.7	6.7	5.9	6.1	183.6	06.5	80	52	78	70	26	034	013.2	26	+	02	04	+	+	+	C8	04	11	09	04	01	05	-	-	-	-	-	-	-		
V	6.0	7.2	5.5	6.2	224.5	07.4	85	60	87	78	39	087	022.6	12	+	04	04	+	+	+	05	02	C2	11	16	10	04	16	-	-	-	01	04	-		
VI	5.2	7.1	6.9	6.4	223.0	11.8	64	84	77	76	30	119	C25.3	24	+	11	01	+	+	+	12	05	01	08	17	13	04	17	-	-	-	01	05	-		
VII	4.7	4.6	3.8	4.4	296.5	13.3	87	57	84	76	30	C59	016.9	20	+	16	08	+	+	+	C5	11	06	12	14	01	14	-	-	-	02	-				
VIII	4.3	3.7	2.3	3.4	301.8	14.7	87	55	83	75	41	037	017.0	12	+	27	12	+	+	+	02	13	03	10	06	01	10	-	-	-	-	-	-			
IX	4.2	5.0	3.4	4.2	199.8	11.2	90	57	84	77	43	025	011.8	27	+	15	01	+	+	+	03	01	11	C4	07	04	01	07	-	-	-	01	02	-		
X	7.7	7.4	6.6	7.0	090.9	07.1	95	75	93	88	42	090	014.0	16	+	02	02	+	+	+	03	03	15	23	18	C2	23	-	-	-	03	-				
XI	7.5	5.6	3.9	5.7	099.2	05.8	95	71	92	86	46	027	008.0	24	+	08	08	+	+	+	05	03	10	11	07	09	-	-	-	06	-					
XII	8.6	7.6	5.5	7.4	049.4	05.1	93	83	92	80	53	058	014.0	19	+	01	16	+	+	+	07	01	01	14	20	10	04	17	02	+	01	-	09	02		
GOD.	6.1	6.1	4.9	5.7	2028.6	08.4	88	65	86	80	26	602	025.3	24/IX	+	02	71	74	27	+	76	23	68	111	156	97	17	145	11	01	+	01	02	-	23	23
<b>NOVI SAD-RIMSKI ŠANČEVI</b>																																				
I	7.4	7.1	6.1	6.9	078.6	04.6	92	79	92	88	57	C17	C08.1	20	+	01	19	+	+	+	04	01	01	14	C7	05	06	02	02	01	-	-	02	01		
II	6.6	6.4	5.4	6.1	110.8	05.2	90	58	78	76	39	010	004.8	24	+	05	05	+	+	+	06	00	C9	08	02	08	01	-	-	-	-	-	01	-		
III	5.6	5.4	4.3	5.1	182.3	05.2	81	51	68	67	18	024	011.1	06	+	11	04	+	+	+	10	03	03	13	08	03	01	05	05	01	-	01	03			
IV	5.9	7.4	5.8	6.4	164.0	06.0	81	41	67	69	28	C37	011.4	17	+	04	04	+	+	+	04	01	03	11	08	02	08	02	08	01	-	01	-			
V	6.2	7.4	6.4	6.7	189.0	05.4	86	59	81	75	29	088	C26.5	23	+	03	03	+	+	+	03	01	02	15	18	12	C2	18	-	-	06	-				
VI	5.7	7.7	6.3	6.6	213.0	11.6	85	55	83	75	33	083	017.5	07	+	11	01	+	+	+	05	01	02	15	11	04	15	-	-	04	-					
VII	4.6	5.1	3.9	4.6	276.6	12.1	82	47	77	68	27	057	013.6	20	+	18	11	01	+	+	+	18	06	01	12	15	12	03	-	-	04	-				
VIII	4.4	4.0	3.1	3.8	286.1	13.8	86	47	78	71	29	056	016.4	12	+	26	12	01	+	+	14	02	10	08	02	10	-	-	05	-						
IX	4.7	5.5	3.3	4.5	193.6	11.0	91	53	84	76	36	C38	016.7	27	+	16	02	+	+	+	05	07	04	04	02	C6	-	-	02	01	-					
X	7.1	7.6	6.0	6.9	073.0	07.0	73	90	86	37	109	C44.6	16	+	01	01	+	+	+	02	04	13	23	19	03	23	-	-	04	-						
XI	7.5	6.9	4.4	6.3	091.2	05.8	93	88	90	84	39	032	007.0	29	+	07	01	+	+	+	01	03	10	06	C7	07	-	-	07	-						
XII	8.2	8.2	6.7	7.7	050.2	05.1	91	44	86	88	55	042	006.7	09	+	01	13	+	+	+	02	01	16	17	10	+	14	05	01	01	01	-	07			
GOD.	6.1	6.1	5.2	5.8	1920.5	08.1	87	60	81	76	16	593	026.9	28/IX	+	02	60	78	26	02	48	06	61	126	146	97	17	138	12	02	02	01	-	23	23	
<b>NOVI SAD-PTROVARADIN</b>																																				
I	7.2	7.2	5.9	6.8	088.6	04.3	84	73	83	80	50	019	C06.6	20	+	C1	15	+	+	+	16	05	01	12	08	04	+	C6	03	01	01	02	01			
II	6.5	6.4	5.7	6.2	108.7	04.8	72	54	66	64	33	008	005.3	07	+	02	02	+	+	+	19	05	01	11	09	01	+	08	01	01	01	-				
III	5.4	5.7	4.6	5.2	188.3	04.7	67	47	58	57</																										

Mesec	Vrstdani pritisak Em mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21						E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\varphi = 45^{\circ}38'N \lambda = 20^{\circ}02'E$ Gr. $\Delta G = +1h\ 20\ min.$																												
I	-	-00.1	04.0	01.3	01.6	04.4	-00.7	09.8	20 -07.1	15	01	04.0	07	01.4	09	01.8	35	02.7	01	01.0	05	01.0	06	01.3	12	02.3	17	
II	-	02.8	10.2	05.8	06.1	11.0	02.4	16.7	18.16 -02.9	09	04	01.5	03	01.7	13	02.2	42	02.8	06	02.2	06	02.2	05	02.6	05	02.4	07	
III	-	04.4	13.1	07.8	08.3	13.9	03.7	25.8	21 -02.3	03	01	01.0	02	01.5	31	02.5	34	03.4	08	02.4	05	02.2	04	02.5	01	05.0	07	
IV	-	06.7	15.1	09.8	10.4	15.9	04.7	23.0	28 -01.2	06	15	02.4	10	02.2	08	02.1	24	03.5	13	03.2	04	01.8	06	02.7	07	02.7	03	
V	-	12.6	18.7	14.3	15.0	19.7	10.0	29.8	31 04.2	10	10	02.5	02	01.5	04	02.2	13	02.4	10	01.9	24	02.2	23	02.7	05			
VI	-	16.0	21.5	17.2	18.0	23.0	12.9	30.3	27 07.4	08	11	02.5	01	02.0	03	01.3	07	02.3	11	02.5	05	02.2	17	02.4	23	03.0	12	
VII	-	17.9	25.1	18.9	20.2	26.1	13.9	33.4	14 07.8	09	09	02.4	01	03.0	06	01.3	12	02.0	09	01.8	04	02.0	07	02.0	32	02.6	13	
VIII	-	19.1	27.7	20.5	22.0	28.3	16.0	34.0	03 05.5	07	06	02.3	05	01.4	12	01.7	20	02.3	06	02.0	01	02.0	05	02.4	12	03.1	26	
IX	-	14.0	23.3	15.9	17.3	11.4	30.2	03 03.6	28	05	01.8	06	01.3	05	02.0	27	02.7	11	02.2	05	01.6	09	02.0	13	03.1	09		
X	-	06.4	11.3	07.8	08.3	12.4	04.9	20.1	04 -00.4	31	02	07.0	05	01.6	05	02.0	17	02.5	18	02.6	06	01.8	19	02.8	27	02.4	09	
XI	-	03.4	10.0	04.9	05.8	10.5	02.0	18.4	18 -01.8	28,10	03	03.0	05	01.6	04	01.8	23	02.5	18	02.7	07	02.1	07	03.3	13	03.1	10	
XII	-	01.4	04.6	02.4	02.7	05.5	00.4	11.5	29 -04.4	25	12	01.9	01	02.0	03	01.3	10	02.7	11	01.9	26	02.5	14	02.8	09			
GOD.	-	08.7	15.4	10.6	11.3	16.3	06.8	34.0	03 05.5	-07.1	15	79	02.4	48	01.7	101	(2.0	255	02.8	125	02.5	65	01.9	135	07.4	167	02.0	120
$\varphi = 45^{\circ}56'N \lambda = 20^{\circ}05'E$ Gr. $\Delta G = +1h\ 20\ min.$																												
I	-	-00.2	04.0	01.4	01.6	04.6	-00.9	10.4	20 -08.0	15	06	02.2	03	01.7	12	01.2	25	02.1	08	01.9	10	01.6	03	01.3	14	02.8	02	
II	-	02.6	10.3	05.9	06.2	11.0	02.1	10.1	12 -02.0	28	04	01.0	03	02.0	10	01.9	03	02.3	07	02.1	01							
III	-	04.7	13.7	08.2	08.7	14.4	03.1	27.2	21 -03.8	01	01	01.0	11	01.9	10	02.5	14	01.9	05	02.2	02	02.5	03	02.0	06			
IV	-	07.6	15.4	10.3	10.9	16.4	04.7	23.9	30 -00.5	04	14	01.3	04	02.0	06	02.2	21	02.1	06	01.7	06	02.2	10	02.2	06			
V	-	13.0	19.2	14.5	15.3	20.3	09.8	29.3	31 02.5	10	*	*	C2	C2.0	C2	C2.0	07	01.7	07	01.7	18	01.8	23	02.0	25	01.8	09	
VI	-	16.5	22.2	17.1	18.2	23.8	12.9	31.5	27 08.2	08	01	01.0	05	01.2	*	*	02	02.0	05	02.2	22	01.7	13	02.5	30	02.3	11	
VII	-	18.1	25.3	19.6	20.6	27.2	14.5	35.0	17.14 -06.5	08	05	01.8	10	01.9	05	01.8	09	01.9	06	02.0	15	02.1	40	02.4	12			
VIII	-	19.3	28.3	21.1	22.5	29.6	16.3	36.4	04.03 10.8	08	05	01.8	10	01.9	05	01.8	09	01.4	06	02.2	07	01.6	13	01.8	23	01.7	15	
IX	-	14.2	23.8	15.9	17.5	24.8	11.3	30.5	03 02.1	28	05	01.4	05	01.6	07	01.6	15	01.9	*	*	10	01.8	08	01.2	17	02.1	23	
X	-	06.3	11.5	07.8	08.3	12.5	04.9	20.1	04 -00.7	31	06	01.2	03	01.5	07	02.3	06	02.5	23	01.8	16	02.2	11	01.6	10			
XI	-	03.3	10.2	05.2	06.0	10.5	02.5	18.1	17 -02.0	28,10	07	02	02.0	06	01.5	23	02.0	11	01.9	12	04.6	11	01.6	02				
XII	-	02.0	05.3	02.8	03.2	05.8	00.7	13.4	29 -03.6	25	06	02.2	01	01.7	02	02.0	11	01.7	19	01.9	10	02.6	23	02.4	01			
GOD.	-	09.0	15.8	10.8	11.6	16.7	06.8	36.4	04 08 VIII -06.0	15	49	01.8	58	01.7	51	02.0	231	02.1	98	02.0	156	01.8	132	02.2	222	02.1	98	
$\varphi = 45^{\circ}24'N \lambda = 20^{\circ}21'E$ Gr. $\Delta G = +1h\ 22\ min.$																												
I	-	-00.3	04.0	00.9	01.4	04.7	-01.4	10.0	22 -08.7	15	01	02.4	05	01.6	14	01.5	36	02.4	21	02.9	02	01.5	06	02.5	12	02.7	06	
II	-	02.4	10.2	05.3	05.8	10.9	01.9	16.9	16 -05.8	09	04	02.0	02	02.0	24	01.5	25	03.3	33	03.2	01	04.0	05	01.8	07	02.4	01	
III	-	04.6	12.8	07.4	08.1	13.6	03.2	24.8	23.21 -02.2	03	*	*	02	02.0	09	02.2	45	03.2	22	03.5	05	02.2	03	02.0	03	02.7	*	
IV	-	07.0	14.7	08.7	09.7	15.6	04.3	23.0	28 -03.7	04	03	03.6	09	02.4	04	02.8	23	03.1	18	02.9	06	02.0	09	02.1	10	02.5	03	
V	-	12.4	18.6	13.3	14.4	19.8	09.1	28.1	31 04.1	10	07	03.4	04	01.8	02	02.0	10	02.2	14	02.5	12	02.2	23	02.5	21	02.4	*	
VI	-	15.8	21.8	16.3	17.6	23.2	12.6	30.2	27 07.8	08	06	02.8	02	02.0	03	01.8	03	02.3	03	02.8	07	02.4	22	02.6	05	02.6	05	
VII	-	17.8	25.0	18.8	20.1	26.5	13.7	34.3	17 08.3	09	09	03.0	07	01.7	02	01.5	06	01.9	15	02.1	08	01.9	17	02.4	22	03.0	05	
VIII	-	19.4	27.8	20.6	22.1	28.9	16.1	35.4	04 09.0 08.07	06	06	01.0	04	01.5	12	01.9	20	02.0	19	02.3	04	02.0	13	02.5	05	02.5	05	
IX	-	13.7	23.5	16.2	17.4	24.7	11.4	30.4	03 03.4	28	06	02.0	07	01.9	08	02.1	25	02.4	13	02.3	05	02.4	13	02.6	07	02.6	08	
X	-	06.2	11.5	07.5	08.2	12.4	05.0	19.8	04 -00.1	31	05	01.6	05	01.8	05	02.2	18	02.4	17	02.4	11	02.0	16	02.5	05</td			

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm				Broj dana na sat:																						
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	▲	△	▲	▲	■	□				
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.	Σ	Max	Dat.	≤0.00.0	0.025.0	0.020.0	0.6	8	2.0	8.0	0.1	1.00.0	●	★	▲	△	▲	▲	■	□			
<b>REČEJ</b>																																
<b>BR. ST.161</b>																																
I 6.9 7.0 6.2 6.7	073.7	04.3	85	74	85	81	53	022	006.9	20	•	01	18	•	•	01	•	03	10	09	07	•	07	04	02	•	•	04	01			
II 6.8 6.5 5.4 6.2	109.6	04.8	82	55	71	69	31	016	010.5	24	•	•	04	•	•	02	•	06	10	08	02	01	08	01	•	•	•	•	01	03		
III 5.0 4.8 3.9 4.6	192.1	04.6	76	43	61	60	12	032	012.7	06	•	•	06	02	•	06	•	11	11	07	07	01	04	05	•	•	•	•	01	03		
IV 5.4 6.7 5.0 5.7	186.9	05.4	74	42	61	59	21	039	014.4	17	•	•	01	•	•	02	01	04	09	09	05	02	09	•	•	•	•	01	03			
V 6.6 6.5 5.8 6.3	216.4	08.4	91	53	80	71	25	084	019.0	23	•	•	04	•	•	13	•	05	11	17	12	04	17	•	•	•	•	01	03			
VI 5.2 7.1 4.3 5.6	215.5	11.1	81	56	80	72	35	100	021.5	30	•	•	10	01	•	03	03	04	17	13	04	17	•	•	01	09	•	•	01	03		
VII 4.3 4.2 3.1 3.9	285.8	12.0	80	46	78	68	28	082	022.1	20	•	•	15	09	01	01	01	12	03	16	12	02	16	•	•	•	•	01	02			
VIII 3.7 3.3 1.9 3.0	307.9	13.7	81	48	79	69	29	062	029.7	12	•	•	26	11	01	01	•	•	09	08	02	09	•	•	•	•	02	03				
IX 3.6 5.0 2.6 3.7	214.9	10.2	85	48	77	70	30	024	012.8	27	•	•	15	01	•	05	15	03	07	03	01	07	•	•	•	•	01	01				
X 7.8 7.5 5.6 7.0	092.2	06.9	92	71	87	83	39	107	017.4	16	•	•	01	•	•	02	01	02	13	23	18	01	23	•	•	04	•	04	01			
XI 7.9 6.0 4.5 6.2	101.8	05.5	87	65	85	79	43	023	007.7	29	•	•	05	•	•	09	02	04	10	09	06	•	08	•	•	04	02					
XII 6.4 8.3 6.9 7.9	047.2	05.0	93	83	90	89	49	053	011.1	08	•	02	11	•	•	07	01	01	19	15	10	01	13	03	•	•	•	•	02	02		
GOD. 6.0 6.1 4.6 5.6	2044.0	07.7	83	57	77	72	12	644	029.7	10/VII	•	03	46	72	22	02	52	06	•	•	146	103	19	138	13	02	•	•	04	18	21	06
<b>SENTA</b>																																
<b>BR. ST.162</b>																																
I 7.7 7.5 6.7 7.3	-	04.4	89	75	88	84	60	024	007.0	20	•	01	18	•	•	01	01	01	15	10	06	•	08	02	•	01	01	•	•	C3	01	
II 7.0 6.9 5.4 6.4	-	05.2	86	58	76	73	31	018	013.5	24	•	•	02	•	•	•	•	03	11	08	02	01	08	01	•	•	•	•	01	01		
III 6.1 5.8 4.6 5.5	-	05.7	79	48	68	65	19	026	006.0	08	•	•	06	03	•	•	•	07	10	07	07	•	05	05	01	•	•	•	•	C2	01	
IV 5.7 7.1 5.9 6.2	-	05.7	72	44	63	60	27	028	007.2	17	•	•	01	•	•	•	•	03	09	11	06	•	11	•	•	•	•	•	•	01	01	
V 6.5 6.5 6.7 6.7	-	09.5	82	58	79	73	30	124	029.5	23	•	•	05	•	•	•	•	03	16	18	10	05	18	•	•	•	•	04	01			
VI 5.5 7.3 5.7 6.3	-	11.7	81	60	80	74	36	165	078.4	30	•	•	14	02	•	•	•	02	08	18	11	04	18	•	•	•	•	10	01			
VII 4.4 4.8 4.7 4.6	-	12.6	81	51	75	69	31	046	012.2	20	•	•	20	11	01	•	•	10	06	14	09	01	14	•	•	•	•	02	01			
VIII 4.2 4.5 3.6 4.1	-	14.4	82	51	78	70	34	064	027.7	12	•	•	26	13	01	•	•	11	04	07	07	02	07	•	•	•	•	04	06			
IX 4.1 5.4 3.6 4.2	-	10.5	86	52	80	73	37	019	015.5	27	•	•	17	01	•	•	•	10	06	06	03	•	06	•	•	•	•	C1	03			
X 7.6 6.1 6.8 7.5	-	07.2	93	75	91	86	47	115	019.9	29	•	•	01	•	•	•	•	02	16	21	19	03	21	•	•	•	•	10	01			
XI 7.1 6.2 5.6 6.3	-	05.7	91	66	86	81	45	030	013.0	29	•	•	03	•	•	•	•	02	11	09	05	02	05	•	•	•	•	07	01			
XII 6.5 8.2 7.5 8.0	-	05.0	89	79	88	85	50	040	010.3	08	•	02	11	•	•	•	•	16	19	09	01	16	05	01	03	•	•	12	01			
GOD. 6.0 6.1 6.3 5.0	-	06.1	84	59	79	74	19	699	078.4	30/VII	•	03	42	85	27	02	•	•	54	130	148	94	19	141	13	02	01	04	•	23	48	C3
<b>ZRENJANIN</b>																																
<b>BR. ST.163</b>																																
I 7.3 7.0 5.4 6.6	083.8	04.3	86	73	86	82	58	019	005.3	03	•	02	21	•	•	11	03	04	12	08	06	•	06	02	•	01	01	•	•	C3	•	
II 6.7 6.2 4.5 5.8	125.4	05.0	83	58	74	72	40	018	007.2	07	•	•	05	•	•	14	07	05	08	09	04	•	09	•	•	•	•	•	•	•	03	03
III 5.2 5.3 4.5 5.0	193.4	05.0	75	50	65	63	24	033	014.9	06	•	•	08	•	•	23	07	09	11	07	04	01	06	05	02	•	•	•	•	01	01	
IV 6.3 6.8 5.4 6.2	136.2	05.9	77	49	70	65	33	036	010.7	18	•	•	03	•	•	21	07	01	13	12	06	01	12	•	•	•	•	01	01			
V 6.6 6.5 6.0 6.4	204.9	09.5	84	61	85	77	39	088	018.1	23	•	•	02	•	•	15	01	05	01	09	18	12	03	18	•	•	•	•	05	01		
VI 6.1 7.4 6.0 6.5	213.9	11.8	84	60	86	77	43	103	022.0	30	•	•	10	01	•	15	08	01	14	13	11	04	13	•	•	02	07	02	02			
VII 4.0 4.7 4.4 4.4	291.8	12.5	82	51	79	71	36	058	004.0	07	•	•	17	11	•	14	05	11	05	15	11	•	15	•	•	•	•	04	•	06		
VIII 4.1 3.5 2.1 3.2	298.1	13.5	81	46	80	77	68	030	051.8	12																						

Mjesec	Vazdušni pritisak Pn/m <sup>2</sup>	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, fm (0-12)																	
		Tm			Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	W.									
		7	14	21								5.	12.	5.	12.	5.	12.	5.	12.	5.	12.	5.	12.						
$\phi = 45^{\circ}09'N \lambda = 21^{\circ}19' E$ Gr. $\Delta G = +1h\ 25\ min.$																													
I	760.4	00.6	03.9	01.0	01.6	04.9	-01.6	09.0	27	-12.4	15	02	C2.6	C1	C2.0	C2	C2.5	30	C5.4	11	C3.4	02	C2.0	03	C2.3	02	C3.0	40	
II	753.0	05.7	10.2	06.8	07.4	11.3	03.7	17.6	16	-04.1	09	-	-	01	02.0	-	-	38	C5.4	22	C3.6	02	C2.0	03	C2.7	-	C1.7	18	
III	756.0	06.7	13.1	09.1	09.5	14.0	04.4	26.6	21	-04.2	13	01	C2.0	04	C2.2	03	C2.0	43	C5.6	19	C3.5	04	C2.2	-	-	01	C2.0	18	
IV	751.4	08.0	14.5	09.5	10.4	15.5	04.9	22.6	30	-03.7	20	03	C1.2	06	C2.3	03	C2.7	25	C4.6	18	C2.9	03	C2.0	-	-	07	C2.3	23	
V	751.2	12.9	18.3	13.5	14.5	19.6	08.6	27.2	31	01.6	10	05	C2.4	-	-	C1	C2.0	09	C4.0	15	C2.7	02	C2.0	15	C2.5	07	C2.7	39	
VI	751.3	16.6	21.6	17.7	23.2	12.4	29.3	27	06.3	09	02	C3.0	01	C2.5	01	C2.0	07	C4.7	14	C2.7	09	C2.3	09	C2.3	11	C3.0	35		
VII	755.7	17.8	25.1	18.6	20.0	26.3	12.8	35.2	18	06.4	27	06	C2.3	06	C2.2	01	C1.0	09	C3.8	11	C2.4	03	C2.3	03	C2.7	11	C2.6	43	
VIII	754.2	20.5	27.9	20.5	22.4	28.7	15.2	34.6	04	09.1	08	06	C2.7	05	C1.8	05	C2.2	21	C4.0	08	C2.8	01	C3.0	06	C2.5	02	C3.0	39	
IX	750.7	16.8	23.9	17.4	18.9	24.8	12.3	31.1	04	01.6	28	02	C2.5	02	C3.0	C1	C2.0	34	C4.0	14	C3.1	02	C2.0	03	C2.7	05	C2.8	27	
X	751.2	08.2	12.5	09.1	09.7	14.1	05.6	21.4	05	-02.5	19	-	-	04	C2.0	C1	C2.0	20	C5.4	16	C3.1	08	C2.2	14	C2.1	03	C2.0	27	
XI	756.0	05.8	10.7	06.5	07.4	11.4	03.4	17.8	18	-02.2	30	01	C3.0	03	C2.0	C1	C2.0	26	C5.0	17	C3.2	02	C2.5	06	C3.2	03	C3.0	31	
XII	757.4	01.9	04.5	03.1	03.2	05.7	00.3	11.4	29	-05.5	23	07	C1.1	01	C1.0	-	-	07	C4.4	24	C2.8	04	C2.0	10	C2.5	02	C2.5	38	
GOD.	754.1	10.1	15.5	11.0	11.9	16.6	06.8	35.2	Tm	-12.4	H:	35	C2.7	35	C2.1	19	C2.2	269	C4.9	189	C3.1	42	C2.2	72	C2.5	54	C2.7	380	
$\phi = 44^{\circ}33'N \lambda = 19^{\circ}14' E$ Gr. $\Delta G = +1h\ 17\ min.$																													
I	757.1	00.8	04.8	01.7	02.3	05.5	-00.2	11.3	27	-05.4	15	-	-	-	C3	C2.0	-	-	-	03	C2.0	02	C1.5	09	C3.1	76			
II	749.5	03.0	10.7	05.3	06.1	11.8	02.0	19.1	12	-03.8	28	04	C2.8	-	C7	C2.0	02	C2.0	01	C3.0	03	C3.0	02	C2.0	03	C1.7	62		
III	752.1	03.6	13.6	07.7	14.2	14.3	02.5	27.6	19	-05.0	02	02	C1.5	07	C7.3	15	C2.0	02	C2.0	-	02	C1.5	01	C3.0	-	C6	55		
IV	746.3	07.0	17.2	09.2	10.1	16.4	05.0	25.6	28	-04.4	04	05	C2.7	05	C2.0	08	C2.0	02	C1.5	-	11	C1.5	01	C4.0	03	C1.7	57		
V	748.6	12.4	19.3	13.2	14.5	20.7	09.4	30.0	31	04.8	10	04	C1.6	C3	C1.0	C1	C2.0	-	C1	01.0	10	C1.8	02	C3.0	09	C2.4	58		
VI	748.0	15.8	22.6	16.9	18.0	24.0	13.6	30.8	27	08.4	13.0	09	C1.5	01	C2.0	-	C1	02.0	06	C1.8	10	C2.6	08	C2.5	60				
VII	751.3	17.2	25.4	18.6	19.9	26.5	13.9	36.9	17	09.1	27	04	C1.0	02	C1.5	07	C1.9	01	C2.0	-	08	C2.0	06	C2.3	09	C2.1	54		
VIII	751.5	16.1	28.0	19.4	21.2	29.2	15.2	36.0	04	10.7	30	07	C1.7	02	C1.5	06	C2.0	02	C1.7	-	06	C1.7	03	C2.3	07	C2.5	65		
IX	751.0	14.4	23.0	15.4	17.1	24.1	12.2	31.6	03	03.3	28	12	C1.6	02	C2.0	C4	C2.2	-	C1	02.0	01	C2.0	02	C2.5	05	C2.6	63		
X	748.2	06.2	12.6	07.4	08.4	13.9	04.6	22.7	04	-01.6	31	05	C1.6	-	C1	01.0	02	C1.5	01	C4.0	04	C2.0	05	C1.8	02	C2.4	73		
XI	752.1	03.4	11.0	04.7	06.0	12.3	02.1	22.8	16	-01.9	27	02	C1.5	-	C1	02.0	01	C1.0	06	C2.3	04	C2.0	02	C2.5	73				
XII	755.0	02.1	05.6	02.9	03.3	06.8	00.6	14.4	29	-05.4	24	01	C3.0	-	-	-	-	C1	02.0	26	C1.8	03	C1.3	07	C2.6	55			
GOD.	751.2	08.7	16.0	10.2	11.3	17.2	06.7	36.9	Tm	-05.4	H:	55	C2.0	22	C1.9	53	C2.0	02	12	C1.8	07	C2.3	86	C1.9	41	C2.3	59	C2.5	760
$\phi = 44^{\circ}11'N \lambda = 19^{\circ}21' E$ Gr. $\Delta G = +1h\ 18\ min.$																													
I	-	00.0	04.9	01.3	01.9	05.5	-00.7	10.8	22	-05.4	14	01	C1.0	C1	C1.0	C5	C2.0	C3	C3.7	01	C2.0	05	C1.4	16	C1.4	20	C1.2	41	
II	-	01.6	11.3	04.3	05.3	12.1	00.7	18.5	12	-04.0	01	07	C1.3	02	C1.0	C3	C1.0	05	C2.6	02	C1.0	01	C1.0	07	C1.2	41			
III	-	03.4	18.8	07.3	08.1	15.2	02.0	27.7	21	-03.8	13	02	C1.5	C3	C1.3	C8	C1.5	13	C3.2	-	01	C1.0	09	C1.2	16	C1.2	41		
IV	-	05.3	15.0	08.2	09.2	15.9	04.1	24.0	29	-28.0	04	04	C1.2	C2	C1.0	C3	C2.0	-	03	C1.0	17	C1.2	10	C1.4	47				
V	-	10.2	19.0	12.4	13.5	20.0	08.7	29.1	31	03.5	05	05	C1.0	C3	C1.0	C4	C1.0	04	C1.0	01	C2.0	02	C2.0	07	C1.9	12	C1.1	51	
VI	-	13.9	21.7	15.5	16.7	23.3	12.3	28.4	26.0	06.4	13	03	C1.3	C6	C1.0	C4	C1.0	05	C4.0	01	C1.0	08	C1.6	15	C1.7	09	C1.2	49	
VII	-	14.7	25.2	17.0	18.5	26.0	13.2	34.9	17	08.7	09	04	C1.0	02	C1.0	-	C3	03	C1.0	05	C1.0	07	C1.4	11	C1.5	*	C1.5	57	
VIII	-	15.7	27.4	18.1	19.8	28.5	14.7	35.0	04	10.7	09	01	C1.0	05	C1.4	-	C3	01.7	03	C1.0	10	C1.5	14	C1.1	57				
IX	-	13.4	23.2	15.0	16.6	24.6	12.5	30.5	04	03.5	28	01	C1.0	C3	C1.0	C4	C1.0	03	C1.3	01	C1.0	06	C1.2	03	C1.0	20	C1.3	51	
X	-	05.6	13.0	07.1	08.2	14.4	04.8	22.0	08	-01.5	26	07	C1.4	-	-	C3	03	C3.3	02	C1.0	02	C1.0	23	C1.5	15	C1.3	41		
XI	-	02.0	10.0	03.7	04.8	10.9	01.0	18.1	16	-01.6	30	07	C1.3	-	-	C1	01.0	03	C2.7	01	C1.0	17	C1.2	43					
XII	-	-00.9	02.8	00.4	00.7	03.9	-01.0	09.5	10	-11.6	25	06	C1.0	04	C1.0	03	C1.0	01	C1.0	24	C1.6	16	C1.6	24	C1.6	38			
GOD.	-	07.0	15.7	09.2	10.3	16.7	06.0	35.0	Tm	-11.6	H:	48	C1.2	31	C1.1</														

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm	Broj dana na se:																												
	Insekticija broj sati						Tn	Tx	Tn	Tx	Tn	F(O-12)	Nm(0-10)	R mm	•	*	Δ	▲	■	□															
	7	14	21	Sred. (Dles)	7	14	21	Sred.	Mn	Σ	Max	Dat.	=	<	≤	IV	V	VI	≥	>	≥	≤													
<b>VRBAC</b>																																			
I	7.4	7.1	6.5	7.0	073.5	03.9	77	67	79	74	30	019 005.2	18	01	.	19	.	.	18	10	02	15	10	06	10	03	.	.	.	.	05	.			
II	6.7	6.4	4.3	5.8	113.9	04.7	66	52	65	61	28	028 010.8	21	.	.	05	.	.	25	15	04	07	06	03	01	06	.	.	.	.	01	.			
III	5.4	5.4	4.3	5.0	184.8	04.4	62	42	53	52	18	015 004.8	07	.	.	07	05	.	22	16	10	10	05	04	05	02	.	.	.	.	01	01			
IV	6.8	6.9	5.2	6.3	159.5	05.4	66	46	61	58	24	039 009.7	16	.	.	03	.	.	21	10	.	06	12	08	12	12	.	.	.	.	02	.			
V	7.0	6.0	6.7	7.1	6.9	191.3	05.0	81	57	80	73	29	117 020.3	23	.	.	03	.	.	12	04	02	13	19	15	05	19	.	.	.	.	01	06	02	
VI	5.9	6.7	5.7	6.1	191.3	11.2	80	59	79	73	36	065 016.1	30	.	.	11	.	01	12	09	01	09	14	11	02	14	.	.	.	.	01	06	.		
VII	4.5	4.5	3.9	4.1	279.8	12.0	80	50	76	69	32	089 021.5	23	.	.	16	10	02	07	02	11	04	16	11	03	16	.	.	.	.	07	01	.		
VIII	3.8	4.0	1.7	3.1	286.0	12.5	71	45	72	67	29	057 024.2	13	.	.	28	12	02	17	11	12	02	08	05	02	08	.	.	.	.	05	02	.		
IX	4.6	5.1	4.1	4.6	203.8	09.9	68	47	69	61	28	083 035.2	27	.	.	16	02	01	22	13	06	04	06	04	03	06	.	.	.	.	02	03	.		
X	7.0	7.8	6.6	7.1	098.0	07.0	82	62	78	71	39	172 023.2	16	.	.	02	.	.	18	12	02	15	20	17	08	20	02	01	.	.	.	.	01	04	01
XI	6.0	6.1	6.0	6.3	107.2	05.5	78	62	76	72	32	054 019.4	29	.	.	03	.	.	21	11	04	09	12	07	01	12	01	01	.	.	.	.	05	02	.
XII	8.3	8.2	7.9	8.1	040.9	04.9	87	82	84	84	26	084 015.9	09	.	02	12	.	.	13	03	01	19	19	11	04	18	06	.	.	.	.	12	04	.	
GOD.	6.2	6.2	5.2	5.9	1930.0	07.5	75	56	72	68	18	822 035.2	270	01	02	51	79	24	06	210	116	55	115	147	103	29	146	14	02	.	.	02	33	36	04
<b>LGZNICA</b>																																			
BR. ST.167															H = 121 m H <sub>b</sub> = 122.2 m h <sub>t</sub> = 2.1 m h <sub>r</sub> = 1.2 m																				
I	8.4	7.2	5.8	7.1	061.0	04.7	92	78	90	87	49	042 019.6	20	.	.	15	.	.	02	01	01	15	14	06	01	12	04	.	.	.	.	12	.		
II	6.8	4.8	4.6	6.2	111.8	05.3	88	58	79	75	32	028 008.0	07	.	.	06	.	.	03	02	03	10	12	08	01	12	01	.	.	.	.	03	.		
III	6.0	6.7	4.8	5.8	143.7	05.4	84	51	71	69	18	008 002.6	08	.	.	07	04	.	06	11	09	02	09	04	.	.	.	.	02	01	.				
IV	6.5	7.0	5.9	6.5	177.2	06.1	80	47	73	67	24	062 016.2	17	.	.	01	01	.	03	01	06	14	15	09	02	15	.	.	.	.	01	.			
V	6.3	7.2	5.6	6.4	206.3	09.1	82	55	83	73	29	089 012.6	13	.	.	05	02	.	04	01	05	09	18	15	02	18	.	.	.	.	01	10	.		
VI	5.4	7.3	6.2	6.3	204.8	11.4	81	56	81	73	34	113 027.7	25	.	.	13	01	.	04	03	04	05	15	12	04	15	.	.	.	.	14	.			
VII	4.5	4.3	3.9	4.2	276.1	12.4	81	51	81	71	28	034 010.3	20	.	.	19	13	.	03	01	13	05	12	08	01	12	.	.	.	.	05	.			
VIII	3.1	3.6	2.9	3.2	297.4	13.7	85	49	83	72	31	060 020.1	12	.	.	26	15	01	04	01	16	03	08	07	02	08	.	.	.	.	08	03			
IX	5.9	5.7	4.1	5.2	177.6	11.8	91	58	91	80	29	074 026.5	05	.	.	17	03	.	07	01	05	06	09	09	02	05	.	.	.	.	05	05			
X	7.4	7.0	6.5	6.9	132.3	06.9	92	66	90	83	35	146 022.2	24	.	.	02	.	.	03	02	03	13	20	19	04	20	02	.	.	.	.	06	.		
XI	6.4	6.4	4.5	5.6	097.5	05.7	91	63	70	81	34	065 017.9	08	.	.	05	.	.	02	01	03	08	10	07	03	10	01	.	.	.	.	05	.		
XII	7.7	7.9	5.8	7.1	046.9	05.0	88	76	86	83	46	065 014.1	13	.	01	11	.	.	02	01	05	17	13	02	12	06	01	.	.	.	.	07	07		
GOD.	6.2	6.2	5.1	5.9	1912.6	08.1	86	59	83	76	18	786 027.7	251	.	01	47	85	32	01	37	14	68	122	159	116	25	153	18	02	.	.	01	45	42	07
<b>LJUBOVCIJA</b>																																			
BR. ST.168															H = 170 m H <sub>b</sub> = - m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.2 m																				
I	8.4	6.5	5.5	6.8	-	04.7	94	78	92	88	42	080 034.7	20	.	.	17	.	.	03	14	18	07	03	18	04	03	.	.	.	.	13	.			
II	6.6	5.6	4.6	5.7	-	05.2	90	56	82	77	36	019 009.4	07	.	.	12	.	.	01	04	09	11	05	01	12	02	.	.	.	.	01	05	01		
III	6.3	6.5	3.7	5.5	-	05.5	87	49	76	70	19	008 003.7	07	.	.	08	05	.	01	06	05	09	02	07	04	01	.	.	.	.	01	04	01		
IV	6.6	7.0	5.4	6.5	-	06.1	90	49	79	72	20	064 016.7	19	.	.	06	.	.	03	11	16	11	02	16	01	01	.	.	.	.	02	05	.		
V	7.6	7.0	6.6	6.4	-	09.5	94	61	90	82	33	116 019.5	16	.	.	03	.	.	04	01	05	09	18	12	04	22	.	.	.	.	06	12	.		
VI	8.3	7.0	6.1	7.2	-	-	-	-	-	-	-	138 026.5	30	.	.	12	.	.	01	11	21	13	05	21	.	.	.	.	01	12	06				
VII	6.7	5.7	3.1	3.5	5.7	-	12.8	94	56	91	80	35	054 012.0	01	.	.	15	10	.	01	04	08	02	15	09	02	15	.	.	.	.	03	17	.	
VIII	8.9	4.3	2.9	5.4	-	13.8	96	54	89	80	32	082 025.8	28	.	.	24	15	.	02	05	20	08	03	14	.	.	.	.	12	21	.				
IX	9.1	5.9	4.4	6.5	-	-	-	-	-	-	-	070 020.5	08	.	.	15	02	.	01	08	16	08	02	16	.	.	.	.	07	16	.				
X	9.1	7.4	7.0	7.8	-	07.1	97	68	93	86	38	130 018.0	24	.	.	02	.	.	04	04	15	22	20	05	22	.	.	.	.	01	01	01			
XI	8.9	6.4	5.3	6.9	-	05.6</td																													

Meseč	Vazdušni pritisak Pm (mb)	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																		
		Tm				Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Srednji (Dnev.)							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	C						
$\varphi = 44^{\circ}37'N \lambda = 19^{\circ}47'E$ Gr. $\Delta G = 1h\ 14\ min.$																								VLACIMIRCI						
I	-	-00.1	04.5	01.6	01.9	05.0	-00.9	10.2	31	-07.2	15	.	.	.	.	10	02.9	.	.	.	.	06	02.2	10	03.6	67				
II	-	03.0	10.6	05.8	06.3	11.3	02.1	17.2	12	-04.0	28	.	.	.	.	16	02.1	02	03.5	.	.	01	02.0	04	02.5	61				
III	-	03.9	13.8	07.9	08.4	14.1	02.9	26.6	23	-03.0	01	.	.	.	.	27	03.5	09	07.3	.	.	01	02.0	*	01	03.0	55			
IV	-	06.7	15.2	09.3	10.1	16.0	05.2	23.5	29	-28	01.5	04	.	.	.	.	09	04.4	.	.	.	.	03	02.3	19	03.2	59			
V	-	12.8	19.3	13.4	14.7	20.1	09.6	30.0	31	06.0	11.0	06	02	02.0	.	.	02	03.5	.	.	.	.	03	02.7	15	03.3	71			
VI	-	15.6	21.9	17.1	17.9	23.3	19.0	25.0	27	07.5	13	03	02.0	.	.	.	.	01	03.0	.	.	.	.	23	03.5	61				
VII	-	18.0	25.3	18.7	20.2	26.6	13.8	35.0	14	05.5	27	01	03.0	.	.	.	.	.	.	.	.	04	01.5	07	02.7	79				
VIII	-	18.1	28.6	20.7	22.0	29.3	19.6	36.0	03	10.2	30	01	03.0	.	.	02	02.5	.	.	.	.	02	01.5	18	03.6	70				
IX	-	13.6	23.4	16.3	17.4	24.1	12.1	31.6	04	03.5	28	03	02.0	.	.	04	02.0	.	.	.	.	02	03.0	17	03.3	64				
X	-	06.0	11.9	07.5	08.2	13.0	04.6	21.5	04	-00.5	31	05	02.2	.	.	09	02.7	.	.	.	.	02	03.0	06	02.7	71				
XI	-	03.2	10.7	05.5	06.2	11.2	02.3	20.0	16	-01.0	11	04	02.2	.	.	07	02.7	.	.	.	.	04	02.5	06	04.0	69				
XII	-	02.0	05.3	02.9	03.3	06.3	00.2	17.0	29	-06.8	25	*	.	.	.	01	02.0	.	.	.	.	01	01.0	21	03.6	70				
GOD.	-	08.6	15.9	10.6	11.4	16.7	06.7	36.0	03	08	-07.2	45	1	19	02.2	.	.	87	03.0	11	06.6	01	03.0	01	02.0	30	02.2	147	03.4	707
$\varphi = 44^{\circ}17'N \lambda = 19^{\circ}55'E$ Gr. $\Delta G = + 1h\ 18\ min.$																									VALJEVO					
BR. ST.172																														
I	752.0	-00.1	04.9	01.1	01.8	05.7	-01.5	10.8	27	-07.0	15	01	04.0	03	01.3	06	02.2	01	03.0	.	.	01	02.0	07	02.7	04	02.8	70		
II	744.8	01.6	10.7	04.5	05.4	12.1	00.5	18.3	17	-06.4	28	*	.	05	01.2	07	02.1	04	03.0	02	02.5	02	03.5	07	01.6	*	.	57		
III	747.3	03.3	13.6	07.5	08.0	14.4	01.7	27.9	19	-04.7	02	02	01.0	06	01.2	20	02.0	06	03.0	01	02.0	*	.	02	01.5	55				
IV	743.5	06.5	14.2	08.4	09.4	15.4	04.0	23.3	28	-02.7	04	04	02.2	04	02.0	10	02.3	03	02.3	*	.	*	.	12	01.4	05	C1.8	57		
V	743.8	12.7	18.1	13.3	14.3	19.8	08.9	28.7	31	03.4	11	09	01.4	04	01.5	C4	01.8	*	.	05	02.6	.	.	14	01.4	01	C1.0	56		
VI	744.2	16.1	21.6	16.5	17.7	23.3	12.5	28.8	27	06.7	13	05	C2.0	*	.	01	02.0	.	.	04	02.2	.	.	16	01.9	05	C2.4	59		
VII	746.6	17.7	25.0	18.3	19.8	26.4	13.3	37.6	17	06.9	28	06	02.0	02	02.0	08	01.9	01	02.0	.	.	.	.	17	02.1	04	02.7	55		
VIII	746.7	16.1	26.2	19.7	21.4	29.1	14.9	34.8	05	04	10.0	08	04	01.8	05	02.4	16	02.1	02	01.5	*	.	.	.	11	01.9	02	03.4	53	
IX	746.1	13.6	23.6	15.8	17.2	25.0	11.3	32.0	04	00.7	28	04	01.5	05	01.6	C5	01.8	*	.	01	03.0	01	02.0	03	01.7	07	02.6	64		
X	743.4	05.6	12.6	07.3	08.2	13.8	03.9	21.5	12	-02.6	31	03	01.7	03	02.0	C4	01.8	02	02.0	04	02.2	02	02.0	05	01.6	04	01.8	67		
XI	748.2	02.0	11.0	04.2	05.4	11.8	00.8	20.2	16	-03.9	27	01	02.0	*	.	04	01.5	01	03.0	02	02.0	*	.	09	01.9	02	02.5	71		
XII	749.9	00.7	05.3	02.2	02.6	06.8	-01.4	13.0	29	-10.0	24	01	02.0	01	02.0	*	.	*	.	01	02.0	01	01.0	17	01.7	08	02.4	64		
GOD.	746.4	08.2	15.7	09.9	10.9	17.0	05.7	37.6	47	VII	-10.0	24	XL	40	01.8	38	01.7	05	02.0	20	02.6	20	02.3	08	02.2	118	01.8	44	02.3	722
$\varphi = 44^{\circ}48'N \lambda = 20^{\circ}28'E$ Gr. $\Delta G = + 1h\ 22\ min.$																									BEOGRAD					
BR. ST.173																														
I	756.1	00.5	04.2	01.6	02.0	04.8	-00.2	09.7	27	-06.3	15	*	.	01	02.0	22	C3.0	36	03.2	*	.	07	01.3	12	01.9	04	02.4	05		
II	748.8	04.5	10.8	06.5	07.0	11.6	03.9	17.6	12	-01.8	28	.	02	01.0	18	03.1	42	02.8	04	01.5	08	01.5	05	01.6	04	01.5	01			
III	751.6	05.6	12.9	08.5	08.9	13.7	04.6	26.6	19	-02.0	01	*	.	03	01.3	25	03.6	53	03.2	03	02.3	04	01.5	01	02.0	02	02.0	04		
IV	747.4	07.8	15.0	10.4	10.9	15.7	06.7	23.6	28	-02.7	15	01	02.0	06	01.8	18	02.7	28	02.8	01	01.0	14	01.8	11	02.2	02				
V	747.4	13.0	19.1	14.3	15.2	20.1	10.8	29.4	31	07.4	10	02	02.0	03	02.0	03	01.7	17	01.7	12	01.8	10	01.7	23	02.1	18	01.9	05		
VI	747.8	16.6	21.9	17.4	18.4	23.4	14.1	29.5	06	08.7	13	04	01.5	05	01.4	04	01.5	17	01.8	10	01.3	07	01.1	24	02.3	16	02.2	03		
VII	750.1	18.4	25.2	20.1	20.9	26.6	15.6	35.3	18	10.7	09	08	02.2	05	01.8	10	01.5	18	01.8	04	01.2	08	01.4	24	02.3	15	02.2	01		
VIII	750.5	20.3	27.9	21.7	22.9	28.7	17.9	34.9	04	12.8	12	04	01.8	03	01.7	22	02.0	33	01.9	02	01.0	14	01.9	09	02.4	05				
IX	749.9	15.6	23.2	17.2	18.3	24.3	13.9	30.2	04	05.5	28	05	02.4	02	02.0	10	01.9	39	02.2	01	02.0	07	01.6	16	02.0	07	02.1	03		
X	747.2	07.0	12.2	08.8	09.2	13.3	06.0	21.0	04	00.4	30	01	01.0	03	01															

Meseč	Oblačnost Nm (0-10)				Isolacija broj sati (Dana)	Vlažnost vazduha				Padavine K mm		Broj dana nesa:																		
	7	14	21	Srednji Srednji Srednji Min.		em	7	14	21			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	▲	■	□		
						mm	7	14	21	Srednji Srednji Srednji Min.	Σ	Max	Min		30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.0	0.0	•	*	*	Δ	▲	■
<b>VLADIMIRCI</b>																														
BR. ST.171																														
I	-	-	-	-	-	04.6	92	79	90	87	57	025	011.0	20	-	01	19	-	-	-	10	04	01	10	01	01	-	-		
II	-	-	-	-	-	05.4	87	62	79	76	37	028	009.1	07	-	-	05	-	-	-	-	06	05	-	08	-	-	04	-	
III	-	-	-	-	-	05.6	84	54	70	70	27	008	003.0	07	-	-	09	04	-	-	03	03	-	04	03	-	04	02		
IV	-	-	-	-	-	06.8	82	59	78	73	33	075	014.5	17	-	-	01	-	-	-	03	-	-	11	10	03	11	-		
V	-	-	-	-	-	10.0	86	63	87	79	38	068	011.0	23	-	-	02	01	-	-	01	01	-	16	16	02	16	-		
VI	-	-	-	-	-	-	-	-	-	-	-	146	053.7	30	-	-	13	-	-	-	-	13	13	04	13	-	-	-		
VII	-	-	-	-	-	12.9	81	54	81	72	23	046	006.0	24	-	-	19	13	-	-	-	11	11	-	11	-	-	-		
VIII	1.4	1.4	2.1	1.6	-	-	-	-	-	-	-	042	C19.5	12	-	-	27	16	-	-	-	21	01	08	-	-	-	-		
IX	4.7	2.2	2.3	3.1	-	11.9	80	61	86	79	35	060	015.5	27	-	-	14	02	-	-	01	-	15	04	10	09	03	10	-	
X	5.4	5.6	5.3	5.5	-	07.0	93	72	90	85	38	157	031.4	24	-	-	01	-	-	-	-	10	11	15	19	05	19	-		
XI	6.7	3.5	3.7	4.6	-	05.9	92	68	87	83	39	060	014.5	09	-	-	03	-	-	-	-	08	06	09	01	09	01	12		
XII	7.2	5.5	5.2	6.1	-	05.1	88	61	87	85	53	066	015.0	15	-	-	02	15	-	-	-	06	12	14	10	01	13	05		
GOD.	-	-	-	-	-	-	-	-	-	-	-	781	053.7	30.0	-	-	03	53	80	32	-	08	04	-	-	133	113	21	132	05
<b>VALJEVO</b>																														
BR. ST.172																														
I	6.1	7.4	5.4	6.9	064.8	04.6	92	75	91	86	46	050	024.1	20	-	-	20	-	-	-	01	02	13	12	09	01	12			
II	6.2	6.4	5.2	6.1	110.1	04.9	89	53	81	74	30	C19	006.2	07	-	-	12	-	-	-	04	06	11	10	05	04	02			
III	5.9	6.1	4.2	5.4	160.9	05.1	84	47	69	66	18	010	004.1	07	-	-	09	03	-	-	02	01	11	06	03	C2	05			
IV	5.8	7.3	5.3	6.1	162.3	05.8	78	47	75	67	21	081	017.2	17	-	-	03	-	-	-	04	05	10	15	03	15	01			
V	6.0	7.1	6.4	6.7	187.1	09.1	80	56	84	74	29	144	020.8	08	-	-	01	-	-	-	04	01	02	11	20	16	05			
VI	6.2	7.6	6.7	6.8	183.2	11.6	82	57	88	75	35	177	054.1	19	-	-	13	-	-	-	03	13	20	17	05	20	-			
VII	3.9	4.6	3.9	4.1	276.1	12.3	80	50	84	71	25	042	011.4	01	-	-	19	11	-	-	01	11	08	11	01	11	-			
VIII	3.5	3.6	2.6	3.1	296.5	13.2	82	44	81	69	31	036	020.3	12	-	-	27	15	-	-	01	16	03	06	04	02	06			
IX	4.7	5.5	4.4	4.9	182.5	11.5	90	54	90	78	32	047	015.3	05	-	-	16	03	-	-	03	07	06	08	06	02	08			
X	6.3	7.2	6.6	6.7	114.0	06.9	92	66	92	84	36	175	049.0	24	-	-	04	-	-	-	05	14	19	15	05	19	02			
XI	6.7	6.6	4.8	6.0	107.6	05.5	92	62	91	81	34	057	023.4	09	-	-	13	-	-	-	02	05	09	11	04	11	01			
XII	7.0	8.0	5.6	7.0	054.6	04.7	89	73	88	83	46	078	013.2	15	01	01	20	-	-	-	01	03	15	16	13	05	01			
GOD.	5.9	6.5	5.1	5.8	1899.7	07.9	85	57	84	75	18	958	054.1	Hv	01	01	81	79	29	-	27	01	70	124	154	115	31	146		
<b>BEGGRAC</b>																														
BR. ST.173																														
I	7.5	6.6	5.5	6.5	083.4	04.3	85	71	82	79	48	026	010.0	20	-	-	15	-	-	-	17	03	04	10	09	07	01	08		
II	6.2	6.0	5.2	5.8	120.1	05.1	78	54	69	47	37	024	009.8	07	-	-	03	-	-	-	16	02	04	10	09	06	05	01		
III	4.9	5.1	4.5	4.8	179.8	04.7	68	47	59	58	19	022	010.4	06	-	-	06	04	-	-	22	12	09	10	07	04	01			
IV	6.3	6.7	6.1	6.4	169.9	05.6	69	45	62	59	23	046	009.5	17	-	-	03	-	-	-	16	02	06	10	13	10	12	01		
V	6.0	6.5	5.8	6.2	202.5	08.8	77	53	77	69	32	080	012.4	16	-	-	03	-	-	-	06	01	02	09	20	18	01	26		
VI	5.9	7.0	5.5	6.1	197.3	11.3	79	58	78	71	38	175	043.8	30	-	-	13	-	-	-	02	06	01	04	18	16	01			
VII	3.6	4.3	3.5	3.8	289.1	11.9	75	50	70	65	27	041	019.2	24	-	-	18	12	04	06	03	13	04	10	06	01				
VIII	4.0	3.0	2.9	3.3	296.4	12.9	71	46	66	62	30	059	017.4	13	-	-	27	13	07	07	-	13	03	07	06	03				
IX	4.5	5.3	4.0	4.6	206.7	10.9	79	53	76	69	33	099	039.4	27	-	-	16	01	-	-	12	04	07	04	07	03	04			
X	5.4	7.3	7.2	7.1	104.3	07.2	51	65	86	82	30	185	037.4	14	-	-	03	-	-	-	14	02	04	15	21	20	21	02		
XI	6.1	5.8	5.3	5.8	095.9	05.9	88	65	83	78	37	063	016.0	29	-	-	18	-	-	-	09	03	03	08	09	02	09			
XII	7.5	8.0	7.2	7.6	051.0	05.0	87	79	82	83	45	090	022.5	16	-	-	01	10	-	-	07	02	16	15	10	03</td				

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, fm (0-12)																		
		Tm			Sred. (dies)			Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21										6	3	8	3	8	3	6	3	8	3	8						
$\varphi = 44^{\circ}18'N \lambda = 20^{\circ}33'E$ Grd. AG + 1h 22 min.														BUKOVICA BANJA																
I	-	-00.4	03.8	00.5	01.1	04.6	-02.6	10.1	31	-09.7	15	01	02.0	05	02.2	09	01.9	28	01.9	14	01.6	*	*	14	02.2	21	01.9	02		
II	-	02.3	05.8	04.3	05.2	10.7	01.3	16.4	02	-06.0	26	07	01.0	03	01.0	14	01.7	23	01.6	11	01.8	05	02.0	05	02.2	12	02.7	09		
III	-	03.7	12.3	06.0	07.0	12.9	02.6	26.0	19	-06.0	01	01	03.0	03	02.8	10	03.0	23	02.1	06	01.5	02	03.5	*	*	02	02.0	07		
IV	-	06.4	13.7	07.8	08.9	14.7	03.9	22.5	28	-02.5	04	02	01.5	02	02.0	10	01.4	20	02.1	03	01.3	01	03.0	17	02.1	12	02.9	13		
V	-	12.5	17.6	12.4	13.7	19.3	09.3	26.9	31	04.7	11	02	01.0	02	01.0	*	*	02	01.0	09	01.2	03	02.1	44	01.9	14	03.1	17		
VI	-	15.9	21.2	15.5	17.0	22.5	12.5	25.5	06	07.5	09	01	01.0	01	01.0	04	01.0	01	01.0	08	01.4	05	07.0	34	01.6	08	02.9	28		
VII	-	17.5	23.8	17.0	18.8	25.6	13.2	34.7	18	08.5	27	01	01.0	01	01.0	05	01.0	02	01.0	04	01.7	05	01.6	33	01.4	08	02.1	34		
VIII	-	17.8	27.8	18.4	20.6	28.5	14.8	34.5	04	10.5	30.0	04	01.0	01	01.0	15	01.3	01	01.0	05	01.0	*	*	17	01.9	08	02.8	47		
IX	-	13.9	23.5	15.0	16.8	24.7	11.5	33.0	04	02.5	28	*	*	01	01.0	10	01.1	07	01.3	05	01.2	02	01.0	20	02.4	04	02.0	41		
X	-	06.0	12.0	06.8	07.9	13.0	04.1	21.0	12	-02.0	31	01	01.7	01	02.0	09	01.0	02	01.0	12	01.2	*	*	19	01.7	14	02.1	33		
XI	-	02.9	10.6	04.6	05.2	11.4	01.4	18.5	19	-02.2	04	02	01.5	01	01.0	14	01.4	09	01.2	06	01.0	02	02.0	17	02.0	06	02.5	31		
XII	-	02.1	05.0	02.7	03.1	06.8	-00.4	16.0	29	-07.5	25.2	04	01.0	02	01.0	*	*	02	01.5	05	01.2	03	01.7	06	01.8	47	01.5	15	01.5	14
GOD.	-	08.4	15.1	09.2	10.5	16.2	06.0	34.7	28	-09.7	01	20	01.4	19	01.6	132	01.5	113	01.8	03	01.4	31	01.2	27	02.3	124	02.6	301		
$\varphi = 44^{\circ}51'N \lambda = 20^{\circ}40'E$ Grd. AG + 1h 22 min.														PANČEVO												BR. ST. 177				
I	-	-00.4	03.8	00.3	01.0	04.4	-01.9	09.4	20	-10.2	15	01	02.0	01	02.0	04	02.0	41	03.0	04	02.8	*	*	67	02.4	09	02.8	26		
II	-	01.7	10.7	04.1	05.0	11.1	00.4	16.6	12	-06.2	05	*	*	*	*	06	02.2	42	03.0	05	02.8	*	*	66	01.8	04	02.0	21		
III	-	03.4	12.6	06.5	07.3	13.8	01.8	25.9	19	-05.0	01	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
IV	-	06.7	15.0	09.0	09.9	16.0	04.5	22.6	28	-02.6	03	05	03.2	01	02.0	18	04.1	14	03.1	02	02.0	*	*	11	02.8	05	02.8	34		
V	-	12.5	19.0	13.6	14.7	20.4	09.7	29.3	31	04.5	11	02	07.5	*	*	04	01.5	05	02.7	03	01.0	27	01.6	10	02.7	40				
VI	-	16.4	22.1	16.9	18.1	23.7	12.9	30.2	27	08.0	09	*	*	01	02.0	01	02.0	04	02.5	04	02.2	02	01.0	24	01.1	10	02.4	43		
VII	-	17.8	25.3	19.0	20.3	26.6	13.6	34.5	17.14	08.5	27	06	01.8	*	*	02	02.5	02	03.0	01	01.0	*	*	21	01.8	10	01.2	51		
VIII	-	19.1	28.2	20.4	22.0	28.9	15.5	35.5	04	16.4	08	01	04.0	02	02.5	11	03.0	06	02.3	*	*	62	03.0	13	01.0	59				
IX	-	14.1	23.5	16.8	17.8	24.7	11.7	31.2	04	02.2	27	03	02.0	*	*	09	02.7	12	02.5	01	02.0	*	*	12	02.3	03	01.7	51		
X	-	05.9	12.2	07.9	08.5	13.3	04.6	20.0	12	-01.0	31	*	*	01	02.0	07	02.3	08	02.0	01	02.0	02	01.5	19	01.5	07	01.0	51		
XI	-	03.1	10.3	05.1	05.9	11.2	02.0	17.6	13	-01.5	30	01	03.3	01	02.0	11	02.8	11	02.9	*	*	01	02.0	11	02.8	02	02.6	50		
XII	-	01.2	04.4	02.3	02.6	05.7	-00.2	12.1	29	-06.2	25	*	*	05	03.0	05	02.8	*	*	02	02.9	71	01.8	04	02.8	49				
GOD.	-	08.5	15.8	10.2	11.1	16.6	06.2	35.5	28	-10.2	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
$\varphi = 44^{\circ}39'N \lambda = 20^{\circ}57'E$ Grd. AG + 1h 24 min.														SMEĐEVREVO												BR. ST. 178				
I	-	00.2	03.9	00.8	01.4	04.5	-01.0	05.8	27	-07.5	14	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
II	-	03.9	10.5	05.4	06.3	11.2	02.4	17.1	12	-03.5	27	27	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
III	-	05.1	13.2	07.9	08.5	13.9	03.5	26.5	21.19	-05.0	01	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
IV	-	07.1	14.8	09.4	10.2	15.9	04.9	23.2	28	-01.7	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
V	-	13.0	19.0	13.3	14.6	20.1	05.8	27.5	31	05.0	10	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
VI	-	15.7	22.7	16.4	17.4	23.8	12.7	29.2	27	08.5	13	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
VII	-	17.6	25.7	17.7	17.7	26.8	14.1	35.2	18.14	09.5	27	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
VIII	-	18.1	28.1	18.9	21.0	28.7	15.7	34.5	05.04	10.0	08	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
IX	-	14.5	23.5	16.1	17.6	24.5	12.4	31.5	04	03.0	28	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
X	-	06.5	12.5	08.1	08.8	13.9	04.8	20.0	12	-02.0	31	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
XI	-	04.2	10.6	05.7	06.5	11.2	02.4	16.2	16	-01.8	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
XII	-	01.2	04.8	02.5	02.8	06.0	-00.6	12.5	29	-06.4	25	*	*	*	*	*	*	*	*	*	*	*	*	*	*					
GOD.	-	08.5	15.8	10.2	11.1	16.9	05.8	35.6	28	-10.4	01	58	02.2	24	01.8	06	01.5	139	02.3	90	01.9	02	01.0	128	02.7	515				
$\varphi = 44^{\circ}02'N \lambda = 20^{\circ}56'E$ Grd. AG + 1h 24 min.														SMEĐEVRSKA PALANKA												BR. ST. 180				
I	757.1	-00.4	03.5	00.6	01.1	04.3	-01.7	09.0	27	-10.2	15	05	01.0	03	01.0	26	02.0	29	02.4	05	02.0	01	02.0	12	02.6	10				



Mesec	Vrstdusni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednje jačina veta mD, fm (0-12)																
		Tm			Sred. (danes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21								E.	J.	S.	D.	E.	J.	S.	D.	E.	J.	S.	D.	E.	J.	C		
$\psi = 44^{\circ}56'N \quad \varphi = 21^{\circ}05'E \quad E.G. = +1h 24 min.$																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	02.8	04.5	03.6	04.9	10.4	06.1	16.2	12 -11.9	09	0.1	02.0	01	02.0	-	-	43	04.0	13	02.2	01	02.0	01	02.0	03	02.3	20	
III	-	04.2	12.0	05.7	07.0	13.2	02.2	25.8	21 -05.2	15	-	-	-	-	01	03.0	65	04.0	03	02.2	01	03.0	01	02.0	03	02.0	23	
IV	-	05.8	14.5	06.3	08.2	15.4	01.2	23.0	30 -08.2	04	31	01.7	01	01.0	-	-	26	04.0	12	07.3	01	02.0	04	02.5	03	03.0	31	
V	-	12.1	18.7	11.7	13.5	19.7	06.1	27.8	31 -01.8	11	0.6	02.0	-	-	02	02.5	09	02.8	14	02.4	03	03.3	16	02.6	15	02.9	28	
VI	-	15.7	21.7	14.7	16.7	23.0	10.2	29.4	27 -02.0	09	0.5	01.6	-	-	07	02.7	10	02.4	05	03.0	12	02.6	12	03.4	35			
VII	-	17.2	24.8	16.2	18.6	25.9	10.1	35.0	18 -01.8	27	11	02.4	-	-	05	02.0	06	03.7	08	02.2	-	08	07.1	14	02.5	41		
VIII	-	18.3	26.9	16.8	19.7	27.6	11.5	33.0	04.0,07	04.0	08	0.6	02.6	-	-	03	02.3	16	02.6	10	02.9	03	03.0	02	02.5	06	03.6	46
IX	-	13.5	23.3	13.8	16.1	24.2	09.8	30.8	04 -02.0	28	0.2	01.0	01	04.0	05	02.2	20	03.4	15	02.5	01	03.0	03	01.3	09	03.1	34	
X	-	05.6	12.4	06.3	07.7	13.6	02.5	20.8	06 -05.5	19	0.2	01.7	-	-	05	02.8	14	03.3	18	02.7	06	02.3	08	02.6	05	02.6	34	
XI	-	02.5	10.5	03.7	05.1	11.3	00.3	19.0	17 -05.5	30	0.1	01.4	-	-	29	03.0	14	02.3	01	02.0	02	02.0	09	03.4	36			
XII	-	-00.2	04.5	01.8	05.4	-02.4	11.5	29 -11.0	23,10	16	0.1	01.1	-	-	02	02.0	20	02.5	-	10	01.2	07	02.1	16				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\psi = 44^{\circ}56'N \quad \varphi = 21^{\circ}05'E \quad E.G. = +1h 24 min.$																												
I	-	-00.8	03.1	-00.3	00.4	03.7	-02.5	09.2	22 -12.2	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	02.0	09.0	04.3	05.1	09.9	01.2	16.0	12 -05.2	09	-	-	02	01.0	47	03.6	13	02.5	01	01.0	-	-	04	02.0	-	-	17	
III	-	04.2	12.0	06.8	07.6	13.0	03.1	25.8	19 -03.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	06.9	13.9	08.2	09.3	15.2	02.3	21.0	28,12 -02.0	23,22	-	-	03	01.0	26	02.4	06	01.0	-	-	-	11	01.6	06	03.3	24		
V	-	11.8	18.7	13.0	14.2	19.9	06.6	28.0	31 04.0	24,08	01	03.0	06	02.0	10	02.0	15	01.6	-	02	01.5	17	02.4	10	02.1	32		
VI	-	15.5	22.1	15.7	17.2	23.3	11.7	29.2	27 07.0	08	0.1	01.0	04	01.5	12	01.5	12	02.1	-	02	01.5	25	02.9	11	01.4	23		
VII	-	17.7	25.1	17.7	19.5	26.4	12.5	36.2	18 06.2	09	-	03	01.0	16	01.5	05	01.8	01	01.0	03	02.0	20	02.0	17	01.8	20		
VIII	-	19.4	27.6	19.4	21.5	28.4	14.7	34.7	03 09.2	07	-	-	03	01.0	22	01.7	22	01.5	-	-	-	11	02.0	07	02.6	26		
IX	-	15.0	23.4	15.4	17.3	24.3	11.1	31.0	04 01.2	28	-	-	01	01.0	19	02.2	25	02.4	02	01.5	02	01.0	10	01.1	07	03.2	24	
X	-	06.1	11.9	07.6	08.3	13.3	02.2	20.2	08 -01.2	28,27	-	-	02	01.0	03	02.7	20	03.0	-	08	01.5	05	01.2	09	01.4	46		
XI	-	03.4	09.4	04.5	05.6	10.4	02.2	17.0	18,17 -02.2	20	0.4	02.0	-	-	05	01.6	36	02.5	-	01	01.0	02	02.5	10	01.7	32		
XII	-	00.4	04.0	01.7	02.0	04.7	-00.8	10.0	29 -07.0	25	0.4	01.2	02	01.0	03	01.0	14	01.7	02	01.0	01	01.0	21	02.0	10	02.2	36	
GOD.	-	03.6	15.0	09.5	10.7	16.0	05.7	36.2	04,01 -12.2	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\psi = 44^{\circ}54'N \quad \varphi = 21^{\circ}23'E \quad E.G. = +1h 25 min.$																												
I	-	00.3	03.7	04.9	01.5	04.4	-01.2	05.4	27 -05.5	15	-	-	-	-	04	02.0	26	02.0	07	02.3	03	02.0	07	01.1	17	01.4	29	
II	-	03.8	16.0	05.9	06.4	10.8	02.1	17.0	12 -04.2	05	-	-	01	05.0	04	03.0	34	02.1	-	13	01.7	08	01.1	07	01.6	17		
III	-	05.9	13.0	08.6	09.0	13.9	04.2	26.0	21 -02.9	12	01	01.0	-	-	18	04.1	36	03.3	04	02.0	06	01.3	02	01.0	01	01.0	25	
IV	-	07.9	14.8	10.2	10.8	16.3	05.2	22.3	30 -01.2	22,20	05	01.6	-	-	11	02.9	16	03.2	06	01.8	04	01.0	06	01.8	13	01.5	29	
V	-	12.4	18.8	13.4	14.5	19.6	09.1	27.5	31 04.0	11	0.4	01.2	-	-	02	01.5	-	02	02.5	08	01.6	18	01.7	20	02.4	39		
VI	-	16.5	22.1	17.0	18.2	23.8	12.8	29.2	27 08.0	09	-	-	01	01.0	03	02.0	34	02.7	03	01.3	06	02.0	24	01.4	36			
VII	-	17.7	25.5	18.8	20.2	26.9	13.2	35.4	14 08.0	23	-	-	01	02.0	01	02.0	36	02.6	01	03.0	06	01.7	11	01.8	35			
VIII	-	20.0	28.5	20.8	22.5	29.6	15.7	35.7	04 11.2	07	0.2	01.5	03	01.0	03	02.0	05	02.0	08	02.2	05	01.6	10	01.4	19	02.1	36	
IX	-	15.8	23.9	16.8	16.4	25.4	12.3	32.6	04 02.1	28	0.1	01.0	-	-	04	01.8	18	02.7	06	01.8	09	02.7	09	02.6	36			
X	-	07.6	13.1	08.7	09.4	14.0	05.2	20.5	05 -00.6	31,28	-	-	01	03.0	02	01.5	14	02.9	08	01.9	03	02.0	15	01.4	09	01.3	41	
XI	-	04.1	11.0	06.5	07.1	11.7	02.9	18.8	18 -01.1	14	0.1	01.0	-	-	03	02.0	15	02.7	07	01.9	02	01.0	06	01.5	12	02.2	44	
XII	-	01.0	04.3	02.5	02.6	05.7	-00.4	12 -04.6	23	0.1	02.0	-	-	02	02.0	07	01.0	06	01.5	22	01.6	06	01.5	22	01.6	53		

Mesec	Oblastnost Nm (0-10)	Insolacije broj sati (Gles)	Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm			Broj dana na sa:																												
				Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■												
	7	14	21	Sred.	7	14	21	Sred.	Max	Dat.	≤	<	<	≤	IV	IV	IV	IV	≥	<	>	≤	≥	•	Δ	Δ	▲	▲	R	T	≡	■			
<b>BR. ST.181</b>																																			
<b>FLAMUNDA</b>																																			
I	-	-	-	062.3	-	-	-	-	-	024	007.4	20	-	-	-	-	-	-	-	07	07	-	05	02	-	-	-	-	02	01					
II	5.7	5.8	4.5	5.3	119.0	04.8	80	59	79	73	36	024	009.8	21	01	-	11	-	-	06	07	07	04	-	07	-	-	-	-	-					
III	4.5	3.7	3.1	3.6	182.0	04.6	75	46	69	64	17	024	009.5	06	-	-	12	04	-	13	08	16	09	05	04	-	03	02	-	-					
IV	7.0	6.3	5.0	6.1	164.1	05.3	75	45	75	65	23	048	010.6	18	-	-	12	-	-	04	01	04	07	10	09	01	10	-	-	02	-				
V	6.4	6.1	6.5	6.6	178.1	08.9	86	57	84	76	03	072	013.2	01	-	-	03	02	-	01	01	03	09	16	13	03	18	-	-	04	01				
VI	6.1	6.7	4.2	5.6	166.7	11.4	86	60	88	78	38	081	025.6	30	-	-	11	-	-	01	05	07	15	12	02	15	-	-	06	-					
VII	3.9	4.2	3.1	3.7	-	12.3	84	54	86	75	32	134	106.5	24	-	-	15	07	-	11	04	11	06	02	11	-	-	-	-	VIII	3.3	2.7	1.5	2.5	
VIII	3.3	2.7	1.5	2.5	253.6	12.7	83	47	90	73	27	084	036.2	13	-	-	24	12	01	02	-	20	03	08	05	03	06	-	-	01	-				
IX	4.3	4.7	2.8	3.9	201.9	10.3	83	54	84	74	32	076	035.7	27	-	-	01	15	01	-	02	09	04	06	05	03	06	-	-	02	06				
X	7.3	7.8	6.1	7.1	102.6	-	-	-	-	-	175	030.2	16	-	-	10	-	-	01	03	16	20	17	08	20	02	-	-	03	02					
XI	6.4	5.5	5.2	5.7	110.7	05.3	89	64	85	79	39	076	021.2	29	-	-	14	-	-	04	07	11	09	09	04	08	01	-	-	04	02				
XII	8.2	7.4	7.1	7.5	043.7	04.8	92	83	90	88	52	087	018.5	15	02	-	16	-	-	03	19	16	13	04	13	05	-	-	-	-	14				
GOD.	-	-	-	-	-	-	-	-	-	-	905	106.5	94.7	-	-	-	-	-	-	30	10	-	-	130	104	30	122	12	-	-	-	-	19		
<b>BR. ST.182</b>																																			
<b>SUSARA</b>																																			
I	7.2	7.2	6.4	7.1	-	-	-	-	-	-	020	004.5	18	01	01	23	-	-	03	01	14	07	06	-	07	04	04	-	-	08	01				
II	6.0	5.8	5.1	5.6	-	-	-	-	-	-	026	011.5	21	-	-	09	-	-	03	03	07	07	04	01	07	-	-	-	-	01					
III	4.9	5.6	4.1	5.0	-	-	-	-	-	-	014	006.0	07	-	-	11	04	-	06	05	07	10	07	04	-	06	04	03	-	-	01				
IV	6.7	6.4	5.1	6.1	-	05.9	7.6	53	74	67	26	049	008.7	18	-	-	06	-	-	02	02	01	07	12	08	-	12	-	-	01	01				
V	6.5	5.9	6.1	6.2	-	09.1	88	57	84	76	30	084	C14.0	23	-	-	04	-	-	01	02	09	18	14	03	18	-	-	02	03					
VI	5.8	6.1	4.9	5.6	-	11.7	89	60	88	79	39	075	027.5	30	-	-	14	-	-	01	05	09	15	12	02	15	-	-	06	02					
VII	4.6	3.8	3.2	3.9	-	12.4	84	53	82	73	27	072	C38.2	24	-	-	17	11	01	-	11	05	10	07	02	10	-	-	04	01					
VIII	3.7	3.4	2.3	3.1	-	12.6	77	44	79	67	26	070	039.6	13	-	-	27	13	01	-	14	C2	06	05	02	06	-	-	04	01					
IX	4.6	4.9	3.1	4.2	-	10.5	80	51	82	71	31	086	C49.2	27	-	-	15	03	-	-	05	04	06	04	02	06	-	-	02	05					
X	6.3	7.6	6.4	6.7	-	-	-	-	-	-	187	027.5	30	-	-	04	-	-	02	13	20	18	16	07	22	02	-	-	02	04	02				
XI	6.4	5.7	5.1	5.7	-	-	-	-	-	-	061	C14.4	29	-	-	04	-	-	06	07	09	09	01	05	01	-	-	02	02						
XII	9.0	8.1	8.2	8.4	-	04.9	95	85	90	90	67	080	015.0	15	02	-	17	-	-	-	18	17	13	04	16	06	02	-	-	10	11				
GOD.	6.0	5.9	5.0	5.6	-	-	-	-	-	-	819	046.2	2711	-	01	01	74	81	27	02	15	08	57	105	134	105	25	132	17	09	-	01	21	37	17
<b>BR. ST.183</b>																																			
<b>BELA CRKVA</b>																																			
I	7.5	7.0	6.5	7.0	-	04.5	92	76	92	87	51	020	003.8	19	-	-	20	-	-	01	-	04	16	12	08	-	11	05	04	-	01	-	06		
II	6.1	5.2	4.3	5.2	-	05.7	86	68	83	79	41	035	C17.0	08	-	-	04	-	-	05	04	08	04	01	08	-	-	-	-	02					
III	4.9	4.8	4.1	4.6	-	-	-	-	-	-	002	001.3	06	-	-	05	03	-	05	01	09	07	05	01	-	04	02	01	-	-	01				
IV	6.4	6.5	6.1	6.3	-	06.3	73	54	67	65	33	038	009.6	27	-	-	02	-	-	03	02	02	08	14	09	-	-	-	-	01					
V	6.5	6.3	6.4	6.4	-	-	-	-	-	-	126	020.6	16	-	-	04	-	-	01	-	01	08	18	14	05	18	-	-	07	01					
VI	5.9	5.8	5.8	5.8	-	-	-	-	-	-	121	025.7	17	-	-	15	-	-	03	-	03	05	12	03	16	-	-	02	08						
VII	4.2	4.7	3.8	4.3	-	-	-	-	-	-	100	037.2	23	-	-	18	11	01	-	-	10	07	13	07	04	13	-	-	05	-					
VIII	3.6	3.5	2.7	3.3	-	-	-	-	-	-	048	015.5	12	-	-	26	16	03	-	-	11	C1	07	06	02	07	-	-	04	-					
IX	4.3	4.3	3.7	4.1	-	-	-	-	-	-	072	048.2	27	-	-	17	03	-	02	-	04	05	02	06	-	-	04	01							
X	6.5	7.5																																	

Mesec	Vazdušni pritisak Pn mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																	
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.			
$\varphi = 44^{\circ}12'N \lambda = 21^{\circ}47'E$ Gr. $\Delta G = +1h\ 27\ min.$											ZAGURICA												BR. ST.186						
I	-	-02.0	01.6	-00.8	-00.5	02.4	-02.7	09.0	27 -12.0	15	.	.	.	.	31	02.4	11	02.7	.	.	.	.	10	01.9	.	.	41		
II	-	00.9	06.9	02.9	03.4	08.1	00.0	17.4	12 -06.4	01	.	.	09	02.6	21	03.0	08	02.8	02	02.5	.	.	04	01.2	.	.	41		
III	-	02.3	05.5	05.6	05.8	10.4	01.4	25.0	19 -03.0	01	.	.	22	02.5	26	02.3	34	02.0	.	.	01	02.0	03	01.3	.	.	27		
IV	-	05.1	12.9	08.3	08.6	14.0	03.4	21.4	13 -01.0	04	.	.	01	04.0	22	01.7	09	01.9	.	.	04	01.0	07	01.6	01	01.0	44		
V	-	09.8	17.2	12.9	13.2	18.5	08.5	24.6	31 02.4	11	.	.	.	.	02	02.0	02	02.5	.	.	.	.	21	01.5	06	01.0	62		
VI	-	13.7	20.1	16.9	16.9	22.1	12.3	27.2	27 06.0	09	.	.	.	.	01	02.0	09	01.8	01	02.0	01	04.0	27	01.8	05	01.2	46		
VII	-	14.3	23.1	17.9	18.2	24.5	12.0	34.0	18 06.0	27	.	.	.	.	02	02.0	01	01.0	03	01.3	28	01.5	05	01.4	52				
VIII	-	16.3	26.3	18.9	20.1	27.2	13.8	34.4	03 04.6	08	.	.	03	01.3	22	01.7	04	01.5	02	01.0	.	.	12	01.8	.	.	50		
IX	-	12.2	22.3	15.6	16.4	23.1	10.7	30.0	04 02.2	28	.	.	01	01.0	24	02.5	04	01.0	.	.	.	.	14	02.3	01	01.0	46		
X	-	05.9	13.2	08.4	09.0	14.9	04.8	23.0	08 -03.0	28	.	.	.	.	10	01.9	11	01.9	.	.	02	02.5	13	01.2	.	.	57		
XI	-	01.5	07.7	04.0	04.8	10.5	00.8	18.0	18.17 -03.0	30.21	.	.	.	.	18	02.4	07	01.1	.	.	01	01.0	08	02.4	02	02.0	54		
XII	-	-01.4	03.3	00.6	00.7	04.3	-02.5	09.0	29 -13.8	25	.	.	.	.	.	.	.	.	.	01	02.0	17	01.2	01	01.0	74			
God.	-	06.5	13.8	09.3	09.7	15.0	05.2	34.4	02.0 -13.8	45	.	.	.	.	15	02.3	179	02.3	101	02.0	06	01.7	13	01.7	14	01.6	21	01.2	596
$\varphi = 44^{\circ}22'N \lambda = 21^{\circ}57'E$ Gr. $\Delta G = +1h\ 26\ min.$																								DEBELI LUG					
BR. ST.187																									BR. ST.187				
I	-	-02.2	00.3	-01.5	-01.2	01.2	-03.7	06.0	22 -14.2	15	.	.	10	04.5	26	03.2	05	02.4	.	.	.	.	04	02.9	18	02.5	25		
II	-	00.8	05.7	01.5	02.4	06.8	-00.8	16.2	11 -04.0	11.0	.	.	08	04.8	23	02.6	17	02.6	.	.	.	02	02.5	04	02.6	30			
III	-	01.1	08.7	03.7	04.3	09.7	00.0	24.8	19 -05.0	02	01	01.0	06	04.7	47	03.4	11	02.8	.	.	.	.	01	01.0	02	03.0	25		
IV	-	04.0	11.7	06.5	07.2	13.1	01.8	26.5	13 -02.5	04.0	03	.	04	02.8	29	02.4	09	02.9	.	.	.	.	03	02.0	15	02.1	30		
V	-	10.0	17.2	11.2	12.4	18.5	08.3	24.7	31 03.0	12	.	.	07	01.1	01	06.0	02	01.5	.	.	.	06	01.3	22	02.5	55			
VI	-	13.4	20.7	14.3	15.8	22.0	11.0	27.0	29 05.1	09	.	.	03	02.3	04	01.8	.	.	.	.	01	01.0	30	02.1	52				
VII	-	15.1	24.8	16.3	16.2	25.8	11.8	.	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	15.3	26.3	17.6	19.2	27.1	13.1	34.2	03 10.1	29	01	03.0	.	09	01.6	09	02.2	.	.	.	.	.	.	11	02.4	63			
IX	-	11.3	21.9	13.3	14.9	22.6	10.0	29.5	03 06.0	20	.	.	02	02.0	10	02.2	07	02.7	.	.	.	.	.	12	01.9	59			
X	-	05.3	12.4	06.8	07.9	13.4	03.7	26.7	08 -02.8	28	.	.	03	02.7	05	02.0	14	01.5	.	.	.	.	26	01.7	45				
XI	-	-	-	-	-	-	-	-	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-				
God.	-	-	-	-	-	-	-	-	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 44^{\circ}05'N \lambda = 22^{\circ}06'E$ Gr. $\Delta G = +1h\ 28\ min.$																								BCK					
BR. ST.188																									BR. ST.188				
I	-	-02.1	-00.2	-01.9	-01.5	01.1	-04.4	08.0	28 -12.5	15	19	03.3	07	01.4	26	01.9	04	01.5	06	01.5	.	.	02	02.5	.	.	29		
II	-	01.2	05.4	01.7	05.2	06.6	-00.9	17.4	12 -05.6	28	05	01.4	05	02.4	23	01.8	06	01.7	06	01.7	01	04.0	02	01.5	03	02.0	23		
III	-	02.8	08.3	04.1	04.8	09.1	00.3	23.2	20 -05.8	28	07	01.0	07	01.0	51	02.4	06	01.5	05	02.2	.	.	02	02.0	20	.	20		
IV	-	06.2	12.2	07.4	08.3	13.3	03.1	22.0	13 -00.4	15	20	02.4	08	01.6	20	02.4	09	01.9	04	02.2	01	01.0	02	01.5	04	01.5	22		
V	-	12.9	17.8	12.7	14.0	19.2	08.7	26.2	31 04.0	11	40	02.2	01	02.0	02	02.0	02	03.5	08	01.9	06	01.5	05	02.8	04	01.2	25		
VI	-	16.5	21.4	15.6	17.3	22.6	12.1	26.3	29 06.9	14	17	02.3	03	02.7	04	01.8	04	02.2	06	02.5	01	01.0	06	02.1	17	04.1	35		
VII	-	19.1	24.7	17.5	19.7	26.0	13.3	33.8	14 05.4	09	20	02.5	01	03.0	03	01.7	04	01.5	03	02.0	05	01.8	17	02.9	37				
VIII	-	19.6	27.0	19.6	21.4	27.8	15.1	34.2	03 11.4	11	13	02.5	06	07.0	11	01.6	16	01.6	04	02.8	01	02.0	.	.	19	02.3	23		
IX	-	14.3	21.1	15.9	17.2	23.4	11.1	30.0	03 05.9	28	13	02.8	03	01.7	14	02.1	02	04.2	02	02.5	.	.	10	03.2	31				
X	-	07.6	13.3	08.0	09.2	14.6	07.8	20.8	08 -02.6	28	11	02.9	07	01.6	25	02.4	07	02.0	07	01.9	06	02.0	03	01.2	34				
XI	-	02.4	06.7	03.5	04.0	07.5	00.5	15.5	17 -04.6	27	10	01.9	04	02.8	08	01.9	09	01.8	07	01.6	02	02.5	03	02.0	35				
XII	-	01.2	04.6	02.4	02.6	05.8	-01.3	12.0	27 -06.2	25	24	02.2	01	02.0	00	01.3	06	01.2	03	02.0	01	03.0	05						

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm			Broj dana na sat																										
										Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	T	III	II							
	7	14	21	Sed.	(Dnev.)	Inopacijalna broj sati	em	m	mm	7	14	21	Sed.	Min	Σ	Max	Dat.	≤	<	≤	IV	≤	IV	<	>	IV	IV	IV	IV	IV	IV	IV	IV			
ZAGUBICA																																				
BR. ST.186																																				
I	8.6	7.6	6.5	7.6	0.62±1	-	-	-	-	012	004.0	18	02	07	24	-	-	-	02	18	07	05	06	03	02	-	-	-	-	-	01	-				
II	7.3	7.0	5.8	6.7	0.90±6	04.4	85	64	78	78	24	039	020.2	21	-	01	12	-	-	04	13	09	05	02	09	01	-	-	-	-	-	01	-			
III	6.4	6.1	4.8	5.8	1.50±9	04.5	78	54	67	66	12	005	002.2	07	-	01	14	01	-	-	08	12	05	02	04	03	02	-	-	-	-	-	01	-		
IV	7.0	7.0	5.7	6.7	1.31±8	05.9	86	56	72	72	29	070	024.5	15	-	01	04	-	-	04	12	12	09	02	12	-	-	-	-	-	02	01				
V	6.5	6.0	6.5	7.0	1.54±6	09.1	97	62	86	81	32	152	033.0	13	-	-	-	-	-	02	15	25	19	04	25	-	-	-	-	-	03	06				
VI	7.1	7.3	5.9	6.8	1.71±3	11.4	93	64	85	81	34	090	015.9	22	-	-	08	-	-	08	10	16	13	04	16	-	-	-	-	-	04	-				
VII	4.4	5.3	3.5	4.4	2.56±1	12.4	94	60	85	80	33	067	016.2	23	-	-	14	09	-	09	06	10	07	03	10	-	-	-	-	-	03	-				
VIII	4.5	4.5	2.0	3.7	2.72±2	12.8	89	51	83	74	26	081	047.8	10	-	-	24	09	02	10	04	05	04	02	05	-	-	-	-	-	02	04				
IX	5.7	5.8	3.1	4.9	1.73±2	10.3	89	53	81	74	28	039	021.4	27	-	-	11	01	-	01	05	06	06	04	02	06	-	-	-	-	-	05	-			
X	7.8	7.3	5.0	6.7	1.06±3	07.1	94	66	88	83	34	134	032.6	15	-	-	05	-	-	12	18	16	04	18	-	-	-	-	-	01	01					
XI	7.1	6.3	4.8	6.1	0.87±1	05.4	94	66	91	83	34	056	013.0	09	-	-	15	-	-	05	11	10	09	02	09	01	-	-	-	-	-	07	01			
XII	9.0	7.0	7.0	7.7	0.24±9	04.5	93	82	94	91	01	108	024.6	09	02	01	21	-	-	02	17	15	11	05	12	06	02	-	-	-	-	-	07	18		
GOD.	6.8	6.6	5.0	6.2	1.68±1	-	-	-	-	853	047.8	40	NP	04	10	95	58	19	02	01	-	51	136	138	104	30	132	14	06	-	-	01	-	44	20	
DEBELI LUG																																				
BR. ST.187																																				
I	9.1	8.6	8.4	8.7	-	03.8	87	86	86	86	65	-	-	02	09	28	-	-	-	02	25	-	-	-	-	-	-	-	-	-	-	-				
II	8.0	6.9	6.8	7.2	-	05.1	88	75	88	87	-	038	017.5	21	-	01	14	-	-	03	16	08	06	01	06	02	-	-	-	-	-	01	-			
III	6.2	5.9	4.9	5.7	-	04.7	83	66	81	77	22	-	-	02	15	-	-	09	01	08	11	-	-	-	-	-	-	-	-	-	-	02	09			
IV	7.0	6.7	6.5	6.7	-	05.4	82	57	73	71	29	086	034.7	15	-	01	09	-	-	03	13	11	11	02	11	06	06	-	-	-	-	-	01	-		
V	7.3	7.1	6.1	6.8	-	08.9	92	63	90	82	31	123	022.0	03	-	-	-	-	01	01	-	12	19	18	04	19	-	-	-	-	-	01	08			
VI	7.0	6.0	6.5	6.5	-	11.0	88	63	89	80	43	118	038.0	30	-	-	10	-	-	01	11	18	16	03	18	-	-	-	-	-	01	03				
VII	9.1	3.4	2.1	2.9	-	11.9	87	52	87	75	-	-	-	-	-	-	-	-	01	-	-	-	-	-	-	-	-	-	-	01	-					
VIII	3.3	3.3	2.5	3.0	-	12.6	90	52	86	76	30	062	023.1	13	-	-	24	09	-	02	16	04	04	03	04	-	-	-	-	-	01	08				
IX	6.7	4.5	3.9	5.0	-	10.0	92	52	91	78	33	084	050.0	27	-	-	06	-	-	04	04	06	05	02	06	-	-	-	-	-	02	10				
X	8.4	6.6	7.1	7.4	-	06.7	93	63	90	82	33	142	022.6	14	-	-	01	-	-	01	14	18	16	07	18	-	-	-	-	-	01	12				
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
SCR																																				
BR. ST.188																																				
I	8.3	8.0	7.2	7.8	-	03.7	89	84	87	87	66	034	013.4	03	03	15	27	-	-	01	-	02	17	15	08	01	14	01	01	-	12	19				
II	7.1	7.4	7.0	7.2	-	04.6	86	73	87	62	17	023	011.8	21	-	02	18	-	-	02	15	16	03	01	11	06	01	-	-	11	-					
III	5.8	5.6	6.1	5.9	-	04.6	79	62	75	72	23	068	023.0	07	-	04	16	-	-	11	15	11	08	02	11	-	-	-	-	-	02	11				
IV	6.1	6.9	5.5	6.2	-	05.2	72	51	69	64	24	096	021.4	17	-	-	05	-	-	05	12	19	09	05	12	04	04	-	-	-	01	-				
V	5.4	6.2	6.0	5.9	-	08.1	71	53	77	67	30	107	023.4	09	-	-	01	-	-	05	05	15	14	04	15	-	-	-	-	-	02	-				
VI	5.5	6.0	3.3	4.9	-	10.5	75	56	79	70	30	030	015.0	30	-	-	09	-	-	02	07	06	15	12	02	15	-	-	-	-	-	02	-			
VII	3.0	2.9	2.1	3.0	-	10.8	64	47	74	62	17	019	011.0	07	-	-	17	11	-	01	17	03	04	01	04	04	-	-	-	-	-	01	-			
VIII	2.7	2.7	1.4	2.3	-	11.2	63	43	66	58	25	071	032.8	24	-	-	25	12	-	01	20	03	06	06	02	06	-	-	-	-	-	03	-			
IX	3.5	4.0	3.0	3.6	-	09.6	69	52	71	64	30	021	017.1	27	-	-	13	01	-	10	02	05	02	01	05	-	-	-	-	-	01	-				
X	5.5	5.6	4.8	5.7	-	06.7	79	61	81	73	23	122	018.9	30	-	-	03	-	-	01	07	11	15	12	06	15	01	-	-	-	-	-	03	-		
XI	8.7	7.6	6.7	7.7	-	04.9	86	71	85	81	27	095	020.2	09	-	-	15	-	-	01	18	18	10	04	14	06	01	-	-	12	09					
XII	6.7	6.8	7.5	7.0	-	04.2	80	69	78	76	26	056	016.8	16	-	01	21	-	-	01	03	15	10	07	03	08	05	-	-	-	-	-	06	12		
GOD.	5.7	6.0	5.1	5.6	-	07.0	76	60	77	71	17	785	032.8	04	NP	03	22	105	65	24	-	04	02	90	122	142	95	32	108	47	05	02	-	01	11	46
TERIJA																																				
BR. ST.189																																				
I	8.9	7.6	8.3	8.3	-	04.1	86	80	87	84	55	014	004.8	03	-	0																				

Mesec	Vazdušni Pritisak Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																
		Tm				Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred.	č.	j.	č.	j.	č.	j.	č.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		
$\varphi = 43^{\circ}55'N \lambda = 19^{\circ}26'E$ Gr. $\Delta G = +1h\ 18\ min.$																												
I	-	-03.9	00.5	-03.0	-02.4	01.0	-05.0	05.0	00.0	04.03	-14.0	14	51	01.1	+	+	+	+	+	06	C1.2	+	+	+	+	+	36	
II	-	-02.4	03.6	-01.7	-00.6	04.1	-03.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	06.4	10.9	06.9	07.8	12.0	03.5	19.0	31	-01.5	10.05	35	C1.1	+	+	+	+	+	56	01.2	+	+	+	+	+	02		
VI	-	10.1	14.5	10.5	11.4	15.9	06.9	23.4	27	03.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	11.6	17.2	11.1	12.8	18.6	07.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.1	16.4	10.6	11.7	17.8	07.0	26.0	04	-01.6	28	32	C1.2	+	+	+	+	+	29	01.2	+	+	+	+	+	29		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}44'N \lambda = 19^{\circ}43'E$ Gr. $\Delta G = +1h\ 17\ min.$																												
MITROVAC-TARA													BR. ST.191															
I	-06.7	02.8	-00.3	-01.9	-01.7	00.9	-04.2	07.8	01	-09.2	14	19	C1.9	C8	01.5	C2	C1.5	C7	01.7	04	C2.2	42	C2.6	C3	C4.0	C4	C1.5	08
II	670.9	-00.1	04.2	01.5	01.8	05.4	-01.2	12.4	12	-07.8	29	06	C1.3	18	02.1	C3	C1.3	C8	02.1	15	C0.1	30	C3.7	01	C1.0	02	C1.5	01
III	673.5	01.5	07.0	03.5	03.9	07.8	-00.3	19.3	23	-07.9	01	11	C1.5	26	01.8	C4	C1.2	C10	10	02.6	19	C2.6	01	C2.0	01	C2.0	01	
IV	670.6	03.0	07.6	04.0	04.7	08.8	01.2	17.2	29	-3.7	21	19	C1.6	24	01.9	C3	C2.0	C4	02.0	12	C2.8	22	C2.7	03	C1.7	02	C1.5	02
V	671.9	08.2	12.1	09.1	09.6	13.8	05.5	23.0	31	02.0	10	22	C1.8	08	01.9	07	01.9	03	01.7	09	C3.3	34	C2.8	04	C7.5	05	C1.2	01
VI	674.2	12.3	16.0	12.7	13.4	18.0	09.5	25.5	27	03.1	13	23	C0.0	09	01.9	C4	C1.8	C3	01.7	07	C3.4	33	C2.8	05	C2.2	04	C1.8	07
VII	676.0	14.5	18.7	15.1	18.8	20.2	11.3	30.4	17	05.1	09	18	C1.7	15	01.9	C6	C1.7	C6	02.0	05	C2.4	34	C2.5	03	C1.7	07	C2.0	07
VIII	676.4	15.6	21.4	17.2	17.8	22.4	13.3	27.7	03	06.7	12	12	C2.1	26	02.1	14	C2.2	07	01.9	06	C2.0	15	C2.1	02	C1.5	05	C1.6	06
IX	675.1	11.8	17.3	13.2	13.9	18.6	10.0	28.2	04	01.8	28	12	C1.8	19	01.7	C4	C1.8	C2	01.5	13	C2.9	30	C2.7	07	C1.7	07	C1.5	03
X	670.7	04.3	05.0	05.6	10.0	12.2	15.6	08	-04.8	31	09	01.6	17	C1.8	C4	C1.2	C3	01.7	07	03.5	38	C3.2	05	C2.4	02	C1.5	02	
XI	674.5	01.0	05.6	02.2	02.7	07.2	-00.2	14.1	16	-08.2	30	12	C1.4	09	01.4	C1	C3.0	C2	02.0	09	C2.9	50	C2.8	05	C2.6	07	C2.0	02
XII	675.1	-02.5	-00.1	-01.2	-01.3	01.6	-04.4	07.4	12.11	-13.8	24	25	C0.2	01	02.0	02	01.5	03	06	03.2	50	03.1	04	02.5	02	C2.0	01	
GOD.	673.7	05.6	09.8	06.7	07.2	11.2	03.6	30.4	77M	-13.8	94M	187	C1.8	190	01.9	54	C1.8	51	01.9	111	C2.9	397	C2.8	43	C2.1	31	C1.6	31
$\varphi = 43^{\circ}52'N \lambda = 19^{\circ}51'E$ Gr. $\Delta G = +1h\ 21\ min.$																												
TITCWC UZICE												BR. ST.193																
I	-	-00.7	03.3	01.2	04.0	-01.2	09.8	22	-07.2	15	+	+	*	*	*	*	*	*	02	01.0	03	01.0	02	C1.0	C6	C1.2	08	
II	-	00.9	03.9	03.4	04.6	10.8	00.4	17.8	12	-05.0	09	+	+	02	02.0	C2	C1.5	C5	01.6	01.0	09	C1.7	01	C1.0	*	44		
III	-	02.3	12.4	06.4	06.9	13.0	01.8	25.5	21.19	-05.4	02	+	+	*	*	C2	C1.0	08	01.5	*	05	C1.2	*	04	C1.0	04		
IV	-	05.8	13.3	07.7	08.6	14.7	03.7	23.0	29	00.2	05	+	+	02	02.0	C1	C1.0	03	01.7	02	01.0	06	C1.3	04	C1.0	04		
V	-	10.7	18.0	12.2	13.3	19.2	07.9	28.7	31	04.0	11	+	+	03	01.3	*	*	03	01.7	C1	0.0	08	C1.1	12	C1.1	03	C1.3	43
VI	-	14.0	21.6	16.0	17.1	23.0	12.1	29.3	27	07.0	14.13	+	+	*	*	04	01.5	*	07	01.6	15	C1.2	01	C1.0	61			
VII	-	15.9	24.4	17.7	18.9	25.6	12.8	35.2	17	07.5	09	+	+	03	01.0	C1	C1.0	03	01.0	*	03	C1.3	18	C1.1	01	C1.0	64	
VIII	-	16.3	27.4	18.9	20.4	26.3	14.3	34.0	03	10.3	08	+	+	07	01.0	01	02.0	07	01.1	05	04	C1.5	60	C1.4	07	C1.5	60	
IX	-	12.3	22.6	15.1	16.3	24.0	11.2	33.0	04	02.0	28	+	+	02	01.0	01	01.0	02	01.0	*	07	01.1	C8	01.1	*	70		
X	-	04.7	12.2	07.0	07.8	13.0	03.8	20.0	04	-02.6	31	+	+	03	01.0	*	*	02	01.0	*	11	01.1	01	01.0	04	C1.2	72	
XI	-	01.7	08.6	03.5	04.4	09.4	00.8	15.6	19	-01.8	29	+	+	01	01.0	01	01.0	05	01.2	*	04	01.5	79	C1.5	04	C1.5	04	
XII	-	-00.1	04.4	01.7	01.9	05.4	-01.1	12.0	29	-08.7	24	+	+	01	02.0	*	*	01	01.0	*	03	01.3	16	C1.0	07	C1.3	66	
GOD.	-	07.0	14.8	09.3	10.1	15.9	05.5	35.2	77M																			

Meseč	Oblačnost Nm (0-10)				Vlažnost vzdušna e <sub>m</sub> mm	Temperatura vzdušna T <sub>m</sub> °C	Precip. R mm	Broj dana na mesečno																		
	Broj sati (Dias.)							Padavine R mm		Broj dana na mesečno																
	7	14	21	Seč. (Dias.)				Tn	Tx	Tn	Tx	T <sub>x</sub>	Tn	F(0-12)	Nm(0-10)	R mm	•	*	♦	Δ	▲	▲				
MITROVAC-TARA																										
BR. ST. 191																										
I	7.9	7.5	9.0	8.1	055.3	-	-	-	-	-	-	-	078	024.4	20	04	08	31	*	*	*	*	*			
II	6.5	4.3	7.8	6.2	067.8	-	-	-	-	-	-	-	030	010.4	07	-	-	-	-	-	-	-	31			
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15			
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	7.2	6.7	8.6	7.5	142.4	06.9	89	74	92	85	41	138	022.4	16	*	02	*	*	*	*	15	19	18	05	19	
VI	6.8	7.0	8.8	7.5	151.2	08.5	86	73	87	82	-	149	031.2	30	*	*	*	*	*	*	13	16	16	05	16	
VII	5.5	5.4	6.3	5.7	236.7	09.1	87	68	87	81	-	074	021.7	01	-	-	-	-	-	-	10	09	03	10	-	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	02	03		
IX	-	-	-	-	167.9	09.0	92	68	94	85	47	103	032.2	11	*	02	01	*	*	*	*	12	11	03	12	*
X	-	-	-	-	-	-	-	-	-	-	-	-	258	051.2	14	-	-	-	-	-	-	20	20	09	16	04
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.																										
ZLATIBOR																										
BR. ST. 192																										
I	7.2	7.4	5.6	6.7	053.8	03.7	93	85	91	91	60	054	014.1	18	*	11	30	*	*	04	05	15	16	11		
II	6.1	4.4	4.5	5.8	110.2	04.0	85	65	79	73	30	022	006.5	05	*	04	17	*	*	12	03	05	12	05		
III	5.8	7.1	4.8	5.9	135.0	04.3	80	65	75	74	21	023	006.6	28	*	06	17	*	*	05	01	04	12	10		
IV	6.6	7.8	5.3	6.6	139.1	04.4	77	61	73	70	26	085	015.1	19	*	02	09	*	*	Cf	02	10	17	12		
V	6.4	7.7	6.2	6.8	166.5	06.7	81	65	78	74	20	086	012.3	16	*	*	*	*	*	12	02	02	10	24		
VI	6.3	7.0	5.7	6.6	173.0	08.5	78	64	73	74	30	081	021.7	30	*	*	01	*	*	13	04	02	10	17		
VII	5.8	5.1	3.9	4.3	266.5	09.4	76	60	74	70	30	074	026.0	08	*	*	09	01	*	C7	01	12	09	08		
VIII	3.5	4.5	2.3	3.4	287.1	10.1	75	55	68	66	37	046	014.6	10	*	*	10	*	*	04	01	15	C3	08		
IX	4.6	5.9	3.3	4.6	175.6	09.0	81	64	81	75	39	174	116.0	11	*	11	02	*	*	11	06	03	12	11		
X	6.6	7.4	5.5	6.5	114.0	05.3	82	69	82	78	41	175	039.7	29	*	*	01	*	*	20	07	04	12	20		
XI	5.9	6.0	5.0	5.6	109.6	04.5	89	72	83	81	45	096	022.1	29	*	*	01	14	*	10	03	05	07	10		
XII	6.6	7.3	6.6	6.8	060.1	03.8	91	86	87	88	60	080	017.1	16	*	03	09	26	*	16	02	15	11	03		
GOD.																										
TITOVČE LIZICE																										
BR. ST. 193																										
I	7.4	7.7	7.7	7.6	-	04.4	92	81	86	87	40	039	021.0	20	*	17	*	*	*	04	20	17	C6	01		
II	5.8	5.6	5.4	5.6	-	04.9	92	56	84	77	29	018	004.4	05	*	12	*	*	*	06	11	10	07	*		
III	5.5	5.1	3.8	4.8	-	05.7	65	59	80	76	28	023	006.0	07	*	12	04	*	*	11	10	11	05	*		
IV	5.7	6.5	5.7	5.9	-	06.4	84	60	84	76	14	055	012.4	15	*	*	07	*	*	05	12	18	10	02		
V	5.9	6.3	5.3	5.8	-	09.4	89	65	88	80	45	068	016.3	13	*	*	03	*	*	01	04	09	19	16		
VI	5.8	5.7	5.4	5.6	-	-	-	-	-	-	-	076	023.4	02	*	*	10	*	*	05	09	13	11	03		
VII	3.4	4.3	3.2	3.6	-	12.8	85	62	85	77	34	046	013.4	01	*	*	15	11	*	16	07	10	06	02		
VIII	3.3	3.1	1.6	2.7	-	13.5	67	59	84	77	24	026	013.7	25	*	*	27	14	*	16	02	08	05	01		
IX	5.7	4.9	4.9	5.2	-	12.1	94	68	92	85	40	062	019.2	27	*	*	13	02	*	05	08	12	05	02		
X	6.6	7.4	6.7	6.4	-	07.0	96	73	92	87	50	151	034.1	16	*	*	03	*	*	05	14	19	14	08		
XI	5.0	5.2	4.6	5.3	-	05.6	94	76	94	88	48	077	025.1	08	*	*	07	*	*	07	09	11	06	02		
XII	6.9	7.2	6.9	7.0	-	04.8	93	83	90	89	59	063	012.0	09	*	*	18	*	*	05	16	15	14	01		
GOD.																										
SJENICA																										
BR. ST. 194																										
I	8.8	3.6	7.2	7.9	058.8	03.4	93	85	92	90	63	030	007.6	20	*	10	15	29	*	02	03	21	13	C8		
II	6.9	6.8	5.7	6.5	117.7	03.9	91	77	87	85	60	028	011.7	05	*	04	02	21	*	03	01	03	18	06		
III	6.7	7.0	4.2	6.0	151.8	04.4	91	80	82	78	19	020	007.2	28	*	01	24	*	*	04	03	12	10	07		
IV	6.7	7.9	5.6	6.7	140.2	04.7	88	61	81	77	31	037	008.7	15	*	*	17	*	*	04	02	02	11	17		
V	6.9	5.5	5.4	6.6	154.6	06.7	86	63	81	76	34	120	019.8	09	*	*	02	*	*	08	01	02	13	06		
VI	7.8	7.4	6.2	7.1	185.5	08.8	84	63	82	77	42	055	016.6	30	*	*	01	*	*	1						

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																
		Tm			Sred. (Dices)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\psi = 43^{\circ}35'N \lambda = 20^{\circ}14'E$ Gr. $\Delta G = + 1h 21 min.$																												
I	-	-01.2	03.3	00.3	00.7	04.2	-02.0	16.0	27	-08.5	15	14	C1.2	C3	01.3	C5	C2.0	12	01.2	C4	01.6	01	04.0	03	03.0	11	01.6	39
II	-	01.1	09.8	03.4	04.4	11.5	00.2	18.0	12	-06.8	09	10	C1.5	C3	01.0	C9	01.9	13	02.2	C13	02.3	•	•	03	01.0	10	02.6	23
III	-	01.6	12.4	05.1	06.0	13.6	00.6	25.7	20	-07.2	02	13	C1.7	C3	01.7	15	01.7	06	02.4	C8	04.9	•	•	02	01.5	12	02.5	29
IV	-	04.5	12.9	06.5	07.6	14.6	02.6	24.5	04	10	01.4	06	C1.5	15	01.9	17	02.0	04	04.5	•	•	03	02.7	14	02.1	21		
V	-	10.3	17.5	11.2	12.6	19.5	07.1	28.6	31	03.0	11	12	C1.7	C5	07.0	C8	C1.8	22	02.0	C7	C4.4	01	02.0	02	01.5	06	02.8	29
VI	-	15.1	21.2	14.7	16.4	23.3	11.4	30.2	29	06.0	14.09	12	C1.8	C7	03.0	C13	C1.5	19	01.8	C3	02.7	01	02.0	01	04.0	08	03.6	26
VII	-	15.8	24.3	15.9	17.9	25.7	11.5	36.2	17	06.1	09	07	C1.7	C2	04.0	C19	C1.5	24	02.0	C8	04.5	02	01.5	01	01.0	09	02.0	21
VIII	-	15.2	27.1	16.5	18.9	26.5	12.7	33.6	04	08	04.6	14	04	C2.0	06	C1.8	17	C1.5	19	C9	C2.4	•	•	03	02.3	07	02.7	26
IX	-	12.1	22.7	14.1	15.7	24.2	10.6	30.6	03	01.5	28	04	C1.1	C1	02.0	C4	01.8	22	02.0	C6	C1.7	01	03.0	06	02.7	05	02.2	37
X	-	05.4	12.9	06.5	07.8	14.6	03.6	21.5	08	-01.3	31	14	C1.9	C1	01.0	C17	C1.7	08	02.1	C4	C2.0	01	04.0	09	02.1	06	02.3	33
XI	-	01.6	09.8	03.3	04.5	11.4	00.2	18.5	19	-04.0	26	14	C1.1	C3	01.5	C16	C1.3	20	01.8	C4	C2.4	•	•	04	02.5	13	01.3	15
XII	-	-01.1	04.1	00.5	01.0	05.7	-02.4	12.6	05	-12.8	24	11	C1.6	C4	01.3	C10	C1.5	22	01.9	C7	C1.6	01	01.0	•	•	04	02.8	26
GOD.	-	06.7	14.8	08.2	09.5	16.4	04.7	36.2	MVII	-12.8	24	141	C1.6	47	01.6	C52	01.6	C20	01.9	77	C2.6	08	02.4	37	02.2	105	02.3	325
$\psi = 43^{\circ}25'N \lambda = 20^{\circ}17'E$ Gr. $\Delta G = + 1h 21 min.$																												
BELE VODE-GELIJA																												
BR. ST. 197																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	10.2	13.9	09.3	10.7	15.3	07.2	22.0	27.06	01.0	13.11	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	12.4	16.5	11.5	13.0	16.0	08.7	27.1	17	02.2	08.07	24	C1.1	C2	01.0	•	•	C1	01.0	•	•	12	01.8	07	01.1	33	02.1	14
VIII	-	13.4	19.1	12.7	14.5	20.1	10.2	26.0	04.03	04.0	12	31	C1.3	15	01.8	14	01.8	•	•	•	•	03	02.7	06	01.9	21	01.7	03
IX	-	09.4	15.6	09.8	11.1	16.3	07.4	24.0	04	00.0	27	18	C1.6	04	02.2	C7	02.6	•	•	06	C3.7	05	03.0	14	02.1	30	02.3	06
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	07.8	15.5	09.2	10.4	16.3	05.4	34.5	MVII	-09.0	24	15	C2.1	14	01.6	31	02.2	37	02.3	37	01.9	70	C2.3	128	02.1	13	02.3	750
$\psi = 43^{\circ}08'N \lambda = 20^{\circ}31'E$ Gr. $\Delta G = + 1h 21 min.$																												
NOVI PAZAR																												
BR. ST. 199																												
I	-	-01.2	03.7	00.1	00.7	04.3	-02.4	05.4	03	-05.4	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	-00.1	06.1	02.5	03.3	09.0	-01.2	15.5	17	-06.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	58			
III	-	02.7	12.4	06.9	07.2	12.9	01.7	25.5	19	-06.0	02	-	-	-	-	10	C0.5	21	C2.3	09	C0.2	02.1	C2.0	04	02.2	47		
IV	-	05.9	14.3	07.9	09.0	15.2	03.4	23.0	30	-02.0	04	04	02.0	01	02.0	04	C2.0	01	03.0	02.0	07	02.4	16	02.0	02	02.0	51	
V	-	12.0	18.6	12.3	18.5	19.8	08.1	29.0	31	03.5	11	93	C2.0	01	03.0	•	•	03	01.7	08	02.2	18	02.1	01	04.0	59		
VI	-	15.7	22.1	15.6	17.3	23.3	12.2	26.8	06	07.4	09	03	C2.0	•	01	02.0	01	02.0	01	02.0	09	02.2	17	02.1	01	03.0	57	
VII	-	17.1	25.4	17.2	19.2	26.3	13.0	34.5	18	08.5	27	-	04	01.2	•	01	01.0	•	06	01.8	07	02.0	01	03.1	03	01.3	63	
VIII	-	17.4	28.8	18.6	20.4	29.1	14.5	34.1	04	11.0	31.08	03	C2.3	•	04	02.0	01	02.0	05	02.4	13	02.1	03	02.3	63	02.4	63	
IX	-	13.4	24.1	15.7	17.2	24.6	11.2	31.8	04	02.0	28	01	C0.2	01.7	C1	02.0	C2	01.5	C3	02.0	03	02.7	03	C2.3	•	•	74	
X	-	05.5	14.3	07.1	08.1	13.8	04.0	21.5	08	-02.5	24	•	03	C1.3	C1	01.0	•	02	02.0	05	02.4	08	01.9	•	•	74		
XI	-	02.5	09.4	03.7	04.8	10.1	00.8	14.7	17	-02.0	30	•	03	01.3	06	C2.3	07	02.3	03	01.3	06	02.3	07	02.3	03	01.3	74	
XII	-	-02																										



Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																			
		Tm			Sred. (Dnes)	Max	Min	Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21										E.	J.	S.	J.	E.	J.	S.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 43^{\circ}37'N \quad \lambda = 20^{\circ}54' E$ Gr. AG = + 1h 22 min.															VRNJAČKA BANJA												BR. ST. 201				
I	-	-00.9	03.0	-00.1	00.4	03.8	-02.2	05.5	22	-16.7	16	09	02.1	20	02.0	10	02.8	C3	01.0	20	01.4	02	01.5	.	.	15	02.2	14			
II	-	01.5	09.4	03.5	04.5	10.6	00.3	15.8	12	-05.5	28	11	01.6	20	02.2	11	02.5	C2	01.5	20	01.4	.	01	02.0	05	C1.4	14				
III	-	02.9	11.7	05.6	06.3	12.7	02.5	25.5	19	-03.7	01	08	02.0	19	02.2	29	02.8	C6	01.7	12	01.8	01	03.0	.	.	02	01.5	16			
IV	-	05.7	13.4	07.7	08.6	14.8	03.5	22.8	28	-01.2	04	19	01.9	10	01.6	C5	02.8	05	01.6	12	01.6	.	.	01	01.0	11	02.3	27			
V	-	11.4	18.1	12.4	13.5	19.8	08.5	27.6	31	04.5	11	31	01.8	C4	01.8	.	C3	01.0	13	01.8	02	01.5	.	.	08	02.1	31				
VI	-	15.6	21.6	15.9	17.2	23.3	12.3	28.9	27	06.8	14.13	37	01.6	04	01.5	C1	02.0	01	01.0	18	01.7	01	01.0	01	02.0	11	02.8	16			
VII	-	16.8	24.4	17.5	19.1	26.1	13.1	35.2	18	07.5	09	32	01.7	C5	01.6	C3	02.7	02	02.0	20	02.0	01	03.0	01	02.0	09	02.7	20			
VIII	-	17.1	27.6	18.7	20.5	28.4	14.8	33.5	04	11.4	08	24	02.0	14	02.4	C3	02.3	.	22	01.7	.	.	.	.	05	01.6	25				
IX	-	13.1	22.9	15.2	16.6	23.9	11.7	30.3	03	02.8	28	16	02.1	10	02.0	C5	02.0	C3	02.0	08	01.6	02	02.5	.	.	12	02.2	34			
X	-	05.9	13.4	07.6	08.6	14.8	04.5	22.0	08	-03.1	28	28	01.9	C5	01.2	.	.	.	13	01.7	02	02.5	.	.	04	C2.0	41				
XI	-	02.0	09.0	04.1	05.0	10.8	01.0	16.9	17	-02.1	27	12	01.8	C4	02.5	C5	02.6	02	02.0	18	01.4	01	02.0	02	01.0	09	02.1	37			
XII	-	-00.2	04.8	01.6	01.9	06.0	-01.3	11.8	29	-11.0	24	26	01.8	02	02.0	.	05	01.4	15	01.5	01	02.0	01	02.0	14	02.0	29				
500.	-	07.6	15.0	09.1	10.2	16.2	05.7	35.2	PM		-11.0	PM		253	01.8	118	02.0	72	02.6	32	01.6	191	01.6	13	02.1	07	01.6	105	C2.2	304	
$\varphi = 43^{\circ}27'N \quad \lambda = 21^{\circ}04' E$ Gr. AG = + 1h 21 min.															ALFKSANDREVAC												BR. ST. 202				
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	03.6	11.0	05.6	06.4	11.7	01.9	24.5	19	-06.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	07.4	13.2	07.8	09.1	14.5	03.2	23.4	30	-02.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	13.1	17.9	13.0	14.2	19.4	08.8	27.3	31	05.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	17.0	21.4	15.8	17.5	23.0	12.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	18.4	24.0	17.4	19.3	25.8	13.0	35.0	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	19.3	26.9	19.1	21.1	27.7	15.0	33.3	04	10.8	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	14.9	22.5	15.2	17.0	23.8	12.0	31.1	04	04.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	07.6	13.9	07.8	09.2	15.9	05.0	22.0	08	-03.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	03.8	10.5	05.3	06.2	12.0	01.8	16.2	18	-06.6	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	01.3	05.7	02.5	03.0	06.8	-00.2	13.5	29	-05.4	25.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
500.	-	07.7	15.6	09.3	10.5	16.6	05.1	35.6	PM		-10.8	45.1	17	02.0	10	01.7	25	01.4	27	01.7	85	01.5	09	01.6	45	02.1	116	C2.2	761		
$\varphi = 43^{\circ}52'N \quad \lambda = 21^{\circ}06' E$ Gr. AG = + 1h 24 min.															REKEVAC												BR. ST. 203				
I	-	-00.2	03.3	00.3	00.9	03.9	-01.9	08.8	22	-16.8	15	-	-	-	-	C1	01.0	C4	01.0	23	01.3	.	.	.	.	12	03.2	53			
II	-	01.8	09.4	03.7	04.6	10.3	-00.2	16.0	16.12	-07.1	28	02	01.0	C2	02.5	C2	02.0	05	02.2	17	01.5	.	.	.	.	01	C2.0	55			
III	-	02.2	12.1	05.6	06.4	12.7	01.1	25.3	23.21	-05.5	01	-	-	C2	02.0	C4	01.2	06	01.5	12	01.5	.	.	.	.	01	02.0	6R			
IV	-	05.4	14.1	08.0	08.9	15.2	02.6	23.4	28	-02.2	04	02	0.0	.	.	05	01.6	06	02.0	05	02.2	.	.	.	.	04	C1.8	13	C2.4	55	
V	-	11.8	18.4	13.1	14.1	19.7	08.1	27.7	31	02.5	11	03	03.3	.	.	C1	01.0	01	01.0	02	02.0	01	01.0	12	02.0	61					
VI	-	15.5	22.2	16.0	17.4	23.6	12.0	29.4	29	06.8	13	02	01.5	C2	01.0	C1	03.0	.	04	01.5	.	09	02.1	63							
VII	-	17.0	24.0	17.4	19.2	26.2	12.7	35.6	18	07.5	09	01	01.0	01	01.0	.	C1	01.0	02	04.5	15	01.5	66								
VIII	-	17.5	26.3	19.0	20.9	28.7	14.0	34.0	04.03	09.0	08	02.3	01.0	01.0	07	01.1	01	01.0	02	01.5	07	C3.1	69								
IX	-	13.2	24.0	15.0	16.8	24.8	10.2	31.4	04	06.8	28	-	-	C2	02.0	C1	01.0	.	C6	01.5	03	01.7	01	01.0	09	C2.4	68				
X	-	05.7	13.8	07.3	08.5	15.4	03.6	22.0	08	-03.6	28	02	01.0	.	.	C2	01.5	02	02.5	63	01.7	01	01.0	04	02.2	12	C1.2	67			
XI	-	02.7	11.1	04.4	05.6	11.9	00.8	16.5	17	-02.5	04	-	-	C1	01.0	02	02.0	10	01.5	02	02.5	04	02.2	12	04.5	69					
XII	-	00.0	05.4	01.9	02.1	05.5	-01.3	10.1	11	-06.9	24	-	-	C1	01.0	.	.	01	01.0	.	.	.	.	01	01.0	23	C7.1	67			
500.	-	07.8	16.0	10.8	11.3	17.0	05.8	36.1	PM		-10.8	45.1	03	01.7	02	02.0	.	.	155	02.5	.	.	01	01.0	.	.	152	C2.4	782		
$\varphi = 43^{\circ}08'N \quad \lambda = 21^{\circ}16' E$ Gr. AG = + 1h 25 min.																															



Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																										
		Tm			Sred. (Dnev.)		Max		Min		Max		Dat.		Min		Max		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21			Max	Min	Max	Min	Dat.	Max	Min	Dat.	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min								
$\varphi = 43^{\circ}34'N \lambda = 21^{\circ}21' E$ Gr. $\Delta G = +1h\ 25\ min.$																									KRUSEVAC		BR. ST. 206											
I	-	-00.7	03.1	00.3	00.8	03.8	-01.8	09.6	31	-09.4	15	01	C2.0	06	03.4	22	03.0	02	02.5	01	01.0	.	.	06	02.3	06	04.0	49										
II	-	01.7	09.6	04.1	04.9	10.8	00.4	17.6	12	-06.1	28	02	C3.0	04	03.0	17	02.3	06	03.3	10	03.4	.	.	03	03.0	01	02.0	38										
III	-	02.6	11.8	07.2	07.2	12.7	01.8	25.4	23	-06.0	01	C3	C2.3	C9	03.6	31	03.4	06	03.0	02	03.0	.	.	03	02.0	.	.	39										
IV	-	05.7	14.0	08.8	09.3	15.3	03.2	23.1	28	-03.0	03	05	C2.2	05	03.4	10	03.4	06	02.7	07	03.1	01	03.0	08	03.1	05	03.6	43										
V	-	11.9	18.4	13.7	14.4	19.9	09.1	28.3	31	04.1	11	13	C3.2	C2	03.0	03	C2.6	03	03.3	17	02.8	01	02.0	07	03.0	05	03.8	42										
VI	-	16.0	21.9	16.8	17.9	23.7	12.8	30.2	27	07.6	14	08	C2.9	C3	03.3	02	C2.5	07	03.0	02	02.5	08	03.6	03	04.0	57												
VII	-	16.6	24.8	18.5	19.6	26.4	13.3	35.4	17	08.6	27	05	C5.2	C1	C2.0	C3	C2.0	01	02.3	03	03.0	13	02.8	09	03.6	48												
VIII	-	16.8	26.1	19.8	21.1	26.9	13.9	34.6	04	10.2	08	04	C3.0	06	02.8	C6	C2.7	04	02.5	06	02.5	03	02.3	03	03.0	56												
IX	-	13.2	23.8	16.3	17.4	24.9	11.0	32.7	04	02.2	28	02	C2.5	02	03.0	C7	C2.7	03	02.7	11	03.0	01	03.0	04	05.5	05	04.0	55										
X	-	06.7	15.2	09.4	10.2	16.9	05.0	25.1	08	-02.7	28	11	C2.5	C6	C2.5	C1	C2.5	13	03.6	.	.	04	02.5	06	02.5	46												
XI	-	02.2	11.1	05.1	05.9	12.3	01.1	17.6	17	-01.8	15	02	C4.0	03	03.0	C9	C3.2	05	03.4	01	04.0	01	04.0	09	04.2	02	04.0	58										
XII	-	-00.6	04.3	01.4	01.6	05.3	-01.6	10.0	05	-11.6	25	03	C3.3	01	02.0	C3	C2.7	04	03.0	03	03.7	08	03.1	03	04.0	69												
GOD.	-	07.7	15.5	10.1	10.9	16.7	05.7	35.4	FVII	-11.6	25	59	C2.9	47	03.0	117	C3.1	43	02.9	88	02.9	15	02.9	76	03.2	50	03.6	600										
$\varphi = 43^{\circ}56'N \lambda = 21^{\circ}23' E$ Gr. $\Delta G = +1h\ 25\ min.$																									CUPRIJA		BR. ST. 207											
I	757.1	-00.9	02.9	00.0	00.5	03.9	-02.1	09.6	27	-11.3	15	+	.	01	C2.0	24	C3.0	20	02.8	06	02.0	01	02.0	03	02.0	04	02.5	34										
II	756.2	02.7	09.1	03.7	04.8	10.4	01.1	16.4	12	-05.6	09	.	.	C1	C3.0	34	C3.3	13	02.6	02	03.5	.	.	.	01	03.0	33											
III	752.8	03.4	12.3	07.1	07.5	13.5	02.0	26.4	20	-04.4	14	.	04	01.5	41	C3.3	05	02.4	02	02.5	.	.	.	.	.	41												
IV	748.2	06.2	14.5	08.4	09.4	15.4	03.1	23.8	13	-04.7	04	02	C2.0	C1	02.0	18	C3.0	05	03.0	04	01.8	01	02.0	05	02.6	06	03.0	48										
V	748.2	12.2	18.8	12.9	14.2	20.3	06.6	28.2	31	02.5	11	07	C2.3	.	.	C1	C2.0	07	02.1	15	02.1	03	02.3	04	01.8	14	01.9	42										
VI	748.5	16.2	22.0	16.3	17.7	23.7	12.2	30.0	27	07.0	09	17	C2.6	03	02.0	.	C2	03.0	07	C2.1	05	02.2	01	01.0	05	02.6	50											
VII	750.8	17.4	24.8	17.9	19.5	26.2	12.5	34.3	14	06.4	09	25	C2.3	C2	02.0	C2	C1.0	01	02.0	03	02.0	09	03.0	01	02.0	39												
VIII	751.1	18.4	28.2	19.7	21.5	28.8	14.2	34.5	03	05.3	C8	13	C2.4	C1	02.0	01	C3.0	13	02.6	06	02.0	07	02.3	01	02.0	05	02.2	46										
IX	750.8	14.3	24.1	15.5	17.4	25.1	11.3	32.6	04	01.4	28	14	C2.4	.	.	C9	C2.6	19	02.4	05	02.0	02	01.0	02	04.0	39												
X	748.1	06.4	14.0	00.5	09.4	15.4	04.5	23.2	08	-02.3	28	18	C2.3	C3	02.0	.	C6	03.3	14	02.6	05	03.0	.	.	47													
XI	753.1	03.1	10.7	05.2	06.0	11.8	01.6	16.8	18	-02.6	21	11	C2.7	.	.	C6	C2.7	22	02.6	06	02.0	.	.	03	C2.0	36												
XII	754.5	-00.3	04.3	01.4	01.7	05.1	-01.5	10.1	05	-11.6	24	20	C2.7	01	01.0	.	C11	01.9	04	02.2	.	.	01	03.0	56													
GOD.	751.1	08.3	15.5	09.7	10.8	16.7	05.6	34.5	FVII	-11.6	04	01.0	127	02.5	17	01.9	121	C3.1	92	02.7	121	02.3	45	02.2	17	02.0	44	02.4	511									
$\varphi = 43^{\circ}14'N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = +1h\ 26\ min.$																									PRKUPLJE		BR. ST. 208											
I	-	-00.5	03.5	00.5	01.0	04.4	-01.5	08.6	31	27	-10.3	16	.	.	C9	02.2	.	.	C2	C1.0	.	.	.	.	C7	02.4	02	03.0	73									
II	-	01.1	09.4	04.2	04.7	10.8	-00.1	17.0	17	-07.1	28	08	C2.6	05	02.2	.	C8	02.2	03	03.7	C3	03.7	02	02.0	04	03.0	51											
III	-	02.3	12.1	06.5	06.8	13.0	01.5	26.0	21	-07.6	01	02	C2.0	18	C3.1	C1	C1.0	02	01.5	01	04.0	02	02.5	09	02.0	02	C1.0	62										
IV	-	05.1	14.1	08.5	09.1	15.4	03.1	23.9	30	-02.9	03	10	C2.9	03	02.3	.	C7	02.6	02	01.5	05	03.0	06	02.0	03	02.0	54											
V	-	11.0	18.2	12.9	13.7	19.8	08.7	28.0	31	03.0	11	05	C2.4	C1.0	01	01.0	C9	02.2	02	03.0	02	03.5	04	02.5	06	03.2	66											
VI	-	15.1	22.1	16.8	17.7	23.9	12.5	29.6	29	05.0	14	01	C3.0	03	01.7	.	C4	02.5	02	01.0	08	02.0	03	02.3	05	02.8	64											
VII	-	15.8	25.1	17.4	18.9	26.5	12.8	34.9	17	09.0	10	07	C3.9	07	01.7	.	C6	01.7	03	03.0	02	02.4	03	04.0	66													
VIII	-	16.3	28.3	19.4	20.9	29.1	14.3	34.0	04	10.9	08	01	C2.0	03	03.0	07	C1.0	01.0	01	02.0	05	02.8	06	03.0	66													
IX	-	12.3	23.7	15.6	16.8	24.7	10.7	33.0	04	01.8	28	01	C3.0	C2	02.0	C3	C2.3	07	02.3	.	.	04	01.2</td															

Mjesec	Oblačnost Nm (0-10)				Indeks broj sati (dnev.)	Vlažnost vazduha				Padavine R mm		Broj dana na sata:																										
						Um s						Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	•	Δ	▲	▲	R <sub>t</sub>	•	■							
	7	14	21	Sred. (dnev.)		mm	7	14	21	U S	Min	Σ	Max	Dat.	≤	<	<	≤	≤	≤	≤	>	≤	≤	W	P	Δ	•	Δ	•	Δ	▲	▲	T	•	■		
<b>KRUŠEVAC</b>																												$H_s = 166 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$										
I	8.1	7.8	7.2	7.7	032.2	04.1	89	74	86	83	48	028	008.8	21	.	02	18	.	.	C2	.	02	19	13	08	.	02	08	.	01	.	01	.	03	05			
II	5.8	6.3	4.7	5.6	107.0	04.9	89	58	81	76	37	048	022.5	21	.	•	13	.	.	01	.	07	09	05	04	02	05	01	01	.	01	.	01	.	01	05		
III	5.8	5.6	4.8	5.4	146.3	04.9	89	86	50	66	68	028	010.3	07	.	•	13	03	.	.	01	.	09	12	09	05	01	04	06	01	.	01	.	01	.	01	05	
IV	6.0	7.1	5.0	6.0	154.0	05.8	86	47	72	68	23	061	014.7	15	.	•	06	.	.	02	01	04	08	12	07	04	12	01	.	01	.	01	.	01	02			
V	6.5	7.3	6.3	6.7	183.2	09.0	86	54	84	75	26	112	023.1	09	.	•	02	.	.	01	.	02	11	20	17	04	20	.	.	.	02	01	06	02				
VI	6.4	6.8	5.9	6.4	165.7	11.4	83	59	86	75	32	162	C52.2	20	.	•	13	01	.	01	.	01	11	18	11	05	16	.	.	01	01	06	02					
VII	5.6	4.7	3.2	5.8	189.3	12.2	82	85	48	84	73	27	052	013.3	11	.	•	17	12	.	14	01	11	07	11	02	11	.	.	02	.	02	.					
VIII	5.3	3.9	2.5	3.2	272.7	12.5	88	39	80	69	22	048	018.4	10	.	•	25	14	.	07	13	04	08	07	02	06	.	.	01	03	03	.						
IX	5.0	5.3	3.5	4.6	168.7	10.6	89	45	84	73	28	027	012.5	27	.	•	17	02	.	12	02	08	07	03	01	07	.	.	.	02	02	.						
X	6.5	7.3	4.7	6.2	115.7	07.1	91	55	84	77	29	094	021.6	14	.	•	06	01	.	06	02	03	10	16	12	04	16	01	.	.	06	.						
XI	6.5	5.7	4.8	5.7	059.6	05.6	94	61	88	81	31	082	018.2	08	.	•	14	.	.	04	02	05	10	08	07	04	06	01	.	.	08	.						
XII	7.5	7.5	6.7	7.2	030.7	04.6	95	78	91	88	49	086	022.5	16	02	01	18	.	.	05	03	15	16	12	03	13	07	.	.	06	18							
GOD.	5.9	6.3	4.9	5.7	1745.1	07.7	88	55	82	75	22	828	052.2	20	W	02	03	88	78	29	.	55	08	69	123	143	100	32	130	25	02	01	03	02	22	32	28	
<b>CUPRIJA</b>																											$H_s = 123 \text{ m } H_b = 124.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$											
BR. ST. 207																																						
I	8.3	7.2	6.6	7.3	058.7	04.1	89	76	87	84	52	034	010.4	20	02	01	19	.	.	03	16	14	09	01	11	06	C1	01	01	.	04	07						
II	5.7	5.8	4.4	5.3	138.4	05.0	80	82	81	76	41	047	029.6	21	.	•	13	.	.	01	.	07	09	05	02	01	01	.	01	01	.	01	03					
III	5.2	5.5	5.0	5.2	176.3	04.9	78	50	66	65	22	013	004.3	07	.	•	09	04	.	01	08	11	06	04	03	05	G1	.	.	.	01	03						
IV	6.8	6.8	5.5	6.4	167.0	05.8	81	48	72	67	22	046	011.0	19	.	•	08	.	.	01	04	10	12	07	02	12	.	.	.	01	02							
V	6.2	7.1	6.8	6.7	269.2	05.6	87	59	86	77	22	143	026.8	30	.	•	02	.	.	01	03	12	24	15	06	24	.	.	.	01	01	09	01					
VI	6.0	6.5	5.8	6.1	203.5	11.9	85	61	86	77	36	107	027.6	25	.	•	13	01	.	01	03	06	16	16	03	18	.	.	.	01	11	02						
VII	3.4	4.0	3.1	3.5	291.7	12.6	83	56	83	74	34	066	029.8	24	.	•	17	11	.	04	15	06	12	08	02	12	.	.	.	02	.							
VIII	3.4	3.1	2.4	3.0	366.0	13.1	81	47	77	69	28	048	024.5	10	.	•	28	12	.	C3	01	16	03	05	05	01	05	.	.	03	.							
IX	5.4	4.5	3.1	4.4	200.3	10.5	83	49	80	70	31	030	022.6	27	.	•	18	02	.	02	08	04	04	03	01	C4	.	.	.	01	02							
X	6.8	6.9	5.5	6.4	127.1	07.3	93	64	88	82	35	121	024.2	15	.	•	05	.	.	04	11	17	14	05	17	02	02	.	.	01	06							
XI	6.3	5.7	5.5	5.9	114.5	05.7	90	66	85	80	40	078	016.8	29	.	•	08	.	.	C6	06	12	04	07	04	06	01	.	.	04	02							
XII	7.5	7.5	6.6	7.3	052.0	04.4	97	81	91	88	48	098	025.4	09	02	•	19	.	.	01	04	17	13	12	03	16	04	.	.	01	19							
GOD.	5.9	5.9	5.1	5.6	2050.8	01.9	85	55	81	75	22	831	079.8	24	W	04	01	81	82	26	.	30	02	81	117	147	105	30	139	24	04	02	02	01	02	30	21	31
<b>PREKUPLJE</b>																												$H_s = 265 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$										
BR. ST. 208																																						
I	8.7	7.1	6.2	7.3	-	04.2	86	75	86	83	58	031	010.2	20	01	03	21	.	.	02	01	-	10	04	.	06	06	03	.	.	.	12	15					
II	5.5	5.5	4.5	5.2	-	04.8	85	52	78	74	34	024	010.4	21	.	•	15	.	.	C1	.	09	10	08	04	01	08	06	.	.	06							
III	5.5	5.0	3.7	4.7	-	05.0	85	52	70	69	23	046	C18.2	07	.	•	13	03	.	01	08	11	06	07	C7	04	03	.	.	01	06	02						
IV	5.9	6.7	3.6	5.4	-	05.5	82	47	67	67	15	048	016.8	15	.	•	08	.	02	06	08	06	06	02	08	06	.	.	03	01								
V	5.8	6.3	3.3	5.1	-	08.8	86	58	81	75	34	084	020.0	16	.	•	01	.	.	01	07	05	16	11	03	16	.	.	06	02								
VI	6.2	4.0	3.6	5.3	-	11.2	85	55	79	74	38	058	022.8	23	.	•	14	.	.	01	01	01</td																

Meseč Vazdušni pritisak mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
	Tm			Sred. (dies)	Mn	Mn	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C	č.	j.	č.	j.					
	7	14	21								č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 43^{\circ}01'N \lambda = 21^{\circ}57' E$ Gr. $\Delta G = +1h\ 26\ min.$											LESKOVAC												BR. ST. 211					
I	748.0	-00.4	03.6	01.2	01.4	04.4	-01.3	08.8	03	-08.8	16	04	01.5	01	02.0	.	.	02	02.0	13	01.6	14	01.3	07	01.4	06	02.2	46
II	741.4	01.3	09.8	04.5	05.0	11.0	00.2	16.1	16	-05.6	28	08	02.8	01	03.0	07	02.9	07	02.0	14	01.8	12	01.3	04	02.0	02	02.0	29
III	743.6	02.9	12.9	06.8	07.4	13.8	01.8	25.9	23	-06.2	02	07	02.1	03	01.3	07	02.1	16	02.1	03	01.3	13	01.5	03	01.7	06	02.2	35
IV	739.4	05.6	14.1	08.5	09.2	15.1	03.1	24.2	30	-02.3	03	10	02.4	08	02.6	05	02.2	12	02.1	10	01.5	07	02.6	04	02.2	08	02.8	26
V	739.7	11.6	18.3	13.3	14.1	19.8	08.7	27.4	31	02.4	11	12	02.5	04	02.5	06	01.5	09	01.6	16	01.5	09	02.2	02	02.0	01	02.0	34
VI	740.0	15.8	22.2	16.9	17.9	24.1	12.2	30.1	29	04.3	14	16	02.9	01	02.0	02	01.5	09	01.6	16	01.6	06	02.0	05	03.6	06	02.8	29
VII	742.2	16.1	25.2	17.9	19.3	26.7	12.1	35.4	17	07.6	27	15	03.1	.	*	02	01.5	11	01.6	14	01.3	07	01.4	04	01.5	06	02.2	34
VIII	742.3	16.2	28.1	19.5	20.9	29.0	13.0	34.5	04	08.3	14	15	02.3	03	02.0	02	01.3	11	01.4	11	01.5	02	01.7	03	01.7	33		
IX	742.4	12.2	24.1	15.9	17.0	25.0	10.0	32.5	04	00.3	28	13	02.7	01	02.0	02	01.5	06	01.7	10	01.5	08	02.2	04	02.5	06	03.7	40
X	739.4	06.4	16.5	09.0	10.3	17.6	04.4	25.3	08	-03.7	28	08	03.1	08	02.4	03	02.0	16	02.1	08	03.0	03	03.3	02	04.0	02	02.5	43
XII	744.5	01.8	10.7	04.7	05.5	11.7	00.7	17.0	05	-04.1	30	07	03.7	03	02.7	01	01.0	05	02.2	08	01.0	01	02.0	05	02.0	01	01.0	59
GOO.	742.4	07.4	15.7	09.9	10.7	16.9	05.2	35.4	07.VII	-11.9	24.VII	127	C2.8	37	02.3	37	02.0	112	01.9	127	01.7	96	01.7	44	02.1	50	02.5	465
$\varphi = 43^{\circ}34'N \lambda = 22^{\circ}16' E$ Gr. $\Delta G = +1h\ 29\ min.$																								BR. ST. 212				
I	-	-02.3	01.9	-01.2	-00.7	02.4	-04.3	09.6	27	-12.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-00.2	07.4	01.8	02.7	08.5	-02.4	16.8	11	-10.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	00.4	10.3	04.1	04.7	11.3	-02.0	25.9	20	-11.2	02	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	04.6	13.7	07.2	08.2	14.7	00.3	22.2	13	-07.6	03	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	11.6	19.0	12.3	13.8	20.4	06.9	28.7	31	01.1	11	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	15.6	23.0	15.9	17.6	24.2	10.6	30.7	27	04.9	09	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	16.5	26.0	17.0	19.1	27.2	10.3	35.4	14	04.5	27	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	14.8	28.1	18.1	19.8	29.0	11.4	34.4	04.03	07.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	10.7	24.4	13.8	15.7	25.2	08.0	32.8	04	00.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	05.3	15.6	07.8	09.1	16.3	03.8	24.7	08	-04.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	01.5	08.2	02.7	03.8	09.2	00.1	19.6	17	-03.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	00.1	05.6	02.0	02.4	06.7	-01.4	11.5	29	-07.2	25	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOO.	-	06.6	15.3	08.5	09.7	16.3	03.4	35.4	44.VII	-12.6	44.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}53'N \lambda = 22^{\circ}18' E$ Gr. $\Delta G = +1h\ 29\ min.$																								ZAJECAR				
I	-	-02.3	01.2	-01.1	-00.9	02.0	-04.1	10.0	28	-16.0	15	06	02.3	37	02.9	06	02.7	06	02.5	*	21	02.2	10	02.6	07	03.4	*	
II	-	00.7	06.2	02.0	02.8	07.2	-00.7	18.0	12	-04.7	28	03	02.0	38	02.8	08	03.2	06	02.7	01	03.0	21	02.7	05	01.8	02	04.0	*
III	-	01.7	09.3	04.9	05.2	10.1	00.2	25.0	19	-06.5	13	04	02.0	51	03.0	14	03.2	02	03.5	01	03.0	18	02.2	03	01.7	*	*	*
IV	-	05.4	13.3	08.4	08.9	14.6	01.9	23.0	13	-05.5	03	05	02.6	25	02.7	09	03.2	03	03.0	01	02.0	37	02.6	03	03.0	*	*	*
V	-	12.3	19.4	13.7	14.8	20.8	08.6	27.4	31	03.6	11	01	03.0	08	02.5	02	03.0	03	03.0	06	03.0	58	02.3	08	02.9	07	03.0	*
VI	-	16.1	22.7	16.8	18.1	24.2	11.9	29.0	27	06.7	09	02	02.5	10	02.2	04	02.8	02	03.0	04	02.5	48	02.5	13	03.0	07	03.3	*
VII	-	17.7	25.8	17.7	19.7	27.1	12.0	35.5	14	07.1	27	02	02.0	13	02.4	03	01.7	*	03	01.7	51	02.2	17	02.4	04	03.2	*	
VIII	-	17.1	28.2	19.8	21.2	29.1	13.0	34.0	03	06.5	28	-	16	02.4	07	03.0	03	02	02.0	54	02.2	08	02.9	03	03.7	*		
IX	-	12.4	24.0	16.4	17.3	25.1	09.8	31.0	04	04.0	29	02	02.0	14	02.8	13	02.9	02	03.0	*	48	02.4	11	02.6	*	*	*	
X	-	06.1	14.9	08.6	09.5	16.0	04.1	23.3	08	-03.0	28	03	03.3	16	02.6	06	03.0	03	02.0	04	02.2	49	02.6	07	02.3	05	02.4	*
XI	-	02.6	07.7	03.8	04.4	08.3	01.0	16.0	13	-05.4	27	02	02.5	33	02.6	05	02.8	01	01.0	03	02.3	36	02.2	07	03.0	03	02.0	*
XII	-	-02.1	03.9	-00.2	00.4	05.1	-03.4	12.5	04	-13.5	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOO.	-	06.4	14.9	08.4	09.5	16.0	04.4	33.4	48.VII	-13.5	25.X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 43^{\circ}09'N \lambda = 22^{\circ}36' E$ Gr. $\Delta G = +1h\ 29\ min.$																								PIRTY				
I	-	-00.8	02.9	00.6	00.8	03.9	-02.4	08.5	27	-12.9	16	14	01.9	01	02.0	01	01.0	14	02.5	*	*	*	*	*	16	01.6	47	
II	-	01.2	08.5	03.5	04.2	10.0	-00.6	16.4	17.12	-07.4	28	04	02.0	*	01	03.0	24	02.4	*	*	*</							

Mjesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha		Padavine R mm		Broj dana na mjesecu:																					
	7	14	21	Srednji (dnev.)		U <sub>m</sub>	t	T <sub>n</sub>	T <sub>x</sub>	T <sub>n</sub>	T <sub>x</sub>	T <sub>x</sub>	T <sub>n</sub>	F(0-12)	Nm(0-10)	R mm	•	*	Δ	▲	▼	▲	▼	T	≡	■					
	mm	mm	mm	mm		Σ	Max	Dat.	≤	<	<	≥	≥	≥	≥	≥	<	>	≥	≥	≥	≥	≥	≥	≥						
LESKOVAC																															
$H_s = 224 \text{ m } H_b = 225.5 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$																															
I 8.2 8.3 7.0 7.8	-	04.5	53	79	91	88	53	C46	G07.2	20	.	02	20	.	.	.	03	18	11	10	.	05	06	03	.	.	.	00	01		
II 5.5 6.6 4.5 5.5	-	05.0	86	60	80	77	39	C30	C12.5	24	.	.	16	.	.	.	03	06	05	07	03	02	07	01	01	.	.	.	01	02	
III 6.0 5.9 5.1 5.7	-	05.3	88	54	76	72	25	C32	C13.6	07	.	.	14	04	.	.	01	06	12	10	05	01	08	04	02	.	.	.	01	02	
IV 6.9 7.3 5.6 6.6	-	06.0	87	50	72	76	27	C62	C19.5	18	.	.	08	.	.	.	04	03	11	14	07	04	14	.	.	.	.	02	01		
V 6.9 7.5 6.0 6.8	-	09.2	86	58	83	76	32	C116	C35.1	16	.	.	03	.	.	.	02	02	10	21	17	04	21	.	.	.	.	01	08		
VI 6.6 7.0 6.7 6.8	-	11.7	86	60	81	76	41	C67	C13.7	14	.	.	15	04	.	.	05	01	01	07	16	11	03	04	.	.	.	11	04		
VII 4.0 4.6 3.0 3.8	-	12.3	88	51	84	74	31	C56	C23.2	08	.	.	18	11	.	.	04	14	06	08	06	02	08	.	.	.	.	03	06		
VIII 3.2 4.3 3.6 3.7	-	12.5	90	43	77	70	26	C44	C18.4	25	.	.	27	14	.	.	03	08	C3	08	06	01	08	.	.	.	.	08	03		
IX 4.4 4.9 3.6 4.3	-	10.7	93	45	82	75	32	C18	G07.6	27	.	.	20	03	.	.	03	06	03	06	03	.	06	.	.	.	.	03	07		
X 7.6 8.5 4.8 6.5	-	07.4	93	57	85	78	33	C056	C010.3	16	.	.	03	01	.	.	08	03	01	10	16	10	01	16	.	.	.	.	02	06	
XI 7.4 6.6 4.7 6.0	-	05.8	95	69	84	79	39	C055	C019.7	08	.	.	16	.	.	.	05	04	08	08	07	05	07	01	.	.	.	.	12	07	
XII 7.4 7.2 7.0 7.2	-	04.5	94	84	94	91	54	C071	C14.6	16	03	01	01	.	.	.	03	03	15	16	14	03	10	01	.	.	.	.	12	06	
God. 6.2 6.4 5.1 5.9	-	07.9	90	55	82	77	25	C681	C025.1	KV	03	03	97	88	30	.	41	04	57	112	141	95	26	131	22	07	.	.	01	39	66
KNJAZEVAC																															
$H_s = 280 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																															
I 11.0 0 B-010.0 9.3	-	-	-	-	-	-	-	041	C17.6	03	03	69	36	.	.	.	.	09	06	01	02	07	01	.	.	.	.	01	15		
II 6.4 6.5 7.2 6.7	-	-	-	-	-	-	-	C28	C016.6	21	01	.	20	.	.	.	C6	13	05	03	01	05	.	.	.	.	.	01	.		
III 5.7 5.9 5.7 5.6	-	-	-	-	-	-	-	C23	C07.2	09	01	.	23	01	.	.	08	13	05	05	01	01	.	.	.	.	.	.	.		
IV 5.7 6.1 5.2 5.6	-	-	-	-	-	-	-	C087	C027.6	18	.	.	12	.	.	.	07	11	08	07	03	08	02	.	.	.	.	01	.		
V 6.7 7.4 6.5 6.9	-	-	-	-	-	-	-	120	C23.0	13	.	.	04	.	.	.	03	12	15	13	05	15	.	.	.	.	02	.			
VI 5.2 5.8 5.5 5.5	-	-	-	-	-	-	-	C77	C017.6	02	.	.	15	01	.	.	C3	C5	18	12	03	18	.	.	.	.	03	.			
VII 2.8 3.6 3.1 3.2	-	-	-	-	-	-	-	C14	C006.4	06	.	.	15	12	.	.	17	C4	06	02	06	02	.	.	.	.	01	.			
VIII 2.4 2.8 1.9 2.4	-	-	-	-	-	-	-	C018	C006.0	24	.	.	27	13	.	.	06	04	06	04	06	06	.	.	.	.	01	02			
IX 3.5 3.3 2.6 3.2	-	-	-	-	-	-	-	C12	C08.0	27	.	.	18	02	.	.	12	04	02	04	02	04	.	.	.	.	01	.			
X 6.3 6.6 4.6 6.2	-	-	-	-	-	-	-	C089	C045.5	30	.	.	08	.	.	.	15	12	03	15	01	06	.	.	.	.	01	06			
XI 6.9 6.4 6.7 6.7	-	-	-	-	-	-	-	C255	C13.5	27	.	.	13	.	.	.	05	14	09	06	02	09	01	.	.	.	.	10	.		
XII 6.0 7.8 8.0 7.9	-	-	-	-	-	-	-	C057	C017.2	14	.	.	18	.	.	.	01	18	07	07	02	07	05	02	.	.	.	.	06	-	
God. 5.8 5.8 5.6 5.8	-	-	-	-	-	-	-	C672	C027.6	KV	05	06	124	84	29	.	02	-	107	84	21	97	76	06	.	.	.	11	-		
ZAJEĆAR																															
$H_s = 137 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$																															
I 8.6 8.3 7.5 8.1	038.2	03	8.8	91	78	88	85	58	C28	C11.2	03	03	10	30	.	.	18	09	06	01	04	06	.	.	.	02	16				
II 7.8 6.8 6.5 7.0	077.7	04.8	51	72	88	84	25	C26	C024.7	21	.	.	16	.	.	.	01	03	15	12	03	01	12	.	.	.	03	.			
III 7.0 6.1 6.2 6.4	142.5	05.1	90	64	79	77	29	C38	C012.7	07	.	.	02	13	01	.	.	06	15	11	07	01	05	05	03	.	.	06	08		
IV 6.4 7.1 6.0 6.5	158.0	06.1	67	56	74	72	32	C75	C016.7	15	.	.	08	.	.	.	03	13	12	06	04	12	02	03	.	.	01	02			
V 6.6 6.2 5.5 6.1	209.7	09.4	66	56	83	75	38	C111	C23.1	13	.	.	04	.	.	.	01	05	20	14	05	20	.	.	.	.	06	02			
VI 5.7 5.9 5.4 5.7	231.6	11.9	P4	57	85	75	39	C87	C016.6	02	.	.	15	01	.	.	03	C4	16	12	03	18	.	.	.	.	03	02			
VII 3.1 3.6 3.5 3.4	326.6	12.3	80	50	85	71	31	C206	C006.6	23	.	.	15	12	.	.	01	12	03	07	05	07	.	.	.	.	01	.			
VIII 2.5 3.3 2.6 2.8	325.6	12.7	P4	44	76	63	23	C19	C09.8	10	.	.	28	13	.	.	01	16	C1	04	04	06	.	.	.	.	02	03			
IX 4.4 4.7 4.2 4.3	226.5	10.3	88	48	76	71	32	C021	C016.8	27	.	.	18	02	.	.	02	08	C5	04	02	01	.	.	.	.	02	.			
X 6.8 6.4 4.9 6.1	151.1	07.2	92	60	89	80	33	C70	C13.9	30	.	.	06	.	.	.	02	04	08	16	10	03	16	.	.	.	.	03	.		
XI 6.1 7.2 6.6 7.3	074.9	05.4	91	75	89	85	47	C085	C020.5	09	.	.	11	01	01	.	.	05	15	13	09	04	13	01	01	.	.	06	01		
XII 7.2 6.2 6.5 6.6	085.9	04.8	89	72	85	82	49	C080	C030.5	15	01	01	21	.	.	.	02	04													

Mesec	Vazdušni pritisak Pm (hPa)	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Pm (0-12)																											
		Tm			Sred. (dnev.)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C																	
		7	14	21								8.	3.	8.	3.	8.	3.	8.	3.	8.	3.																
$\varphi = 41^{\circ}20'N \lambda = 22^{\circ}41'E$ Gr. - AG = + 1h 30 min.												TOPLI DU										BR. ST. 216															
I	-	-02.5	01.4	-01.5	-01.0	02.6	-03.9	06.5	22	-12.1	16	-	-	-	-	-	-	-	-	-	-	-															
II	-	00.2	06.8	01.5	02.5	07.6	-01.3	13.8	17.12	-08.1	28	-	-	-	-	-	-	-	-	-	-	-															
III	-	01.5	09.7	03.7	04.7	10.3	00.1	23.0	20	-08.2	01	-	-	-	-	-	-	-	-	-	-	-															
IV	-	04.4	10.4	05.8	06.6	11.3	02.1	22.0	30	-03.9	03	-	-	-	-	-	-	-	-	-	-	-															
V	-	09.1	14.0	09.7	10.9	16.0	06.7	23.8	31	02.6	11	-	-	-	-	-	-	-	-	-	-	-															
VI	-	14.0	18.0	13.2	14.8	20.3	10.0	27.8	27	04.3	14	-	-	-	-	-	-	-	-	-	-	-															
VII	-	15.0	22.0	15.1	16.8	23.0	11.5	31.8	17	06.7	27	-	-	-	-	-	-	-	-	-	-	-															
VIII	-	16.2	24.1	17.2	18.7	25.2	13.1	30.9	05	09.1	28	-	-	-	-	-	-	-	-	-	-	-															
IX	-	11.6	21.0	13.8	15.1	22.3	09.6	29.6	04	04.1	28	-	-	-	-	-	-	-	-	-	-	-															
X	-	07.6	14.1	08.8	09.8	15.3	05.4	20.5	08	-03.4	28	-	-	-	-	-	-	-	-	-	-	-															
XI	-	01.9	08.6	03.6	04.4	09.6	00.5	15.6	19	-03.2	30	-	-	-	-	-	-	-	-	-	-	-															
XII	-	-01.0	07.6	-00.3	00.2	03.6	-02.6	08.9	13	-08.0	10	-	-	-	-	-	-	-	-	-	-	-															
GOD.	-	06.5	12.9	07.6	08.6	13.9	04.2	31.8	Pm	-12.1	M	-	-	-	-	-	-	-	-	-	-	-															
$\varphi = 43^{\circ}01'N \lambda = 22^{\circ}45'E$ Gr. - AG = + 1h 29 min.												DIMITREVGRAD										BR. ST. 217															
I	727.6	-01.6	02.7	-00.3	00.1	03.4	-02.6	08.1	23	-13.6	16	-	-	-	-	-	-	-	-	-	-	-															
II	722.0	00.6	08.4	02.5	03.5	09.0	-00.5	15.4	17	-07.1	28	-	-	-	-	-	-	-	-	-	-	-															
III	724.4	01.7	11.6	05.3	06.0	12.4	04.8	25.1	20	-07.9	01	-	-	01	03.0	13	02.8	61	01.1	04.0	-	04															
IV	719.0	04.6	12.7	07.0	07.8	13.8	02.2	20.5	30	-03.5	03	-	-	03	01.3	15	02.7	33	02.6	-	04	02.2	19	03.0	14												
V	720.2	10.3	17.0	11.4	12.5	18.4	06.9	25.2	31	-00.4	11	01	C1.6	-	-	13	C1.7	18	01.9	-	-	13	01.9	23	03.0	25											
VI	726.9	14.6	20.9	15.4	16.6	23.1	10.7	25.9	27	04.8	14	07	02.0	01	01.0	08	02.5	22	02.0	-	01	01.0	06	03.7	27	03.3	23										
VII	723.1	15.6	24.7	16.7	18.4	25.5	11.1	34.4	18.17	06.2	10	01	C1.0	01	02.0	05	01.6	24	02.1	-	04	01.8	04	02.6	36	03.4	16										
VIII	723.7	15.8	27.0	17.8	19.6	28.0	12.1	34.2	05	09.3	29	-	-	03	07.3	15	02.3	38	02.3	02	01.5	01	02.0	03	02.7	17	02.6	14									
IX	723.4	11.6	23.7	15.0	16.3	24.8	08.9	31.7	04	01.4	28	01	02.0	02	01.0	09	02.1	40	02.5	01	02.0	02	02.5	06	01.8	18	03.7	11									
X	726.2	07.8	16.6	05.9	10.8	17.4	05.1	24.5	14	-04.3	28	-	-	01	02.3	12	02.3	41	02.2	02	01.5	01	04.0	08	01.8	17	02.6	06									
XI	724.8	02.1	08.6	03.4	04.3	09.4	00.7	15.0	06	-03.7	30	-	-	-	10	02.7	52	07.9	-	-	07	02.0	12	02.9	09	-	-	-	-								
XII	725.1	-01.4	03.5	00.5	00.8	04.3	-02.6	08.6	13	-05.6	24	-	-	-	06	C1.5	26	02.2	-	-	02	01.5	22	01.6	23	02.9	14	-	-	-							
GOD.	722.9	06.8	14.8	08.7	09.7	15.8	04.4	34.4	Pm	-13.6	M	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
$\varphi = 42^{\circ}10'N \lambda = 20^{\circ}18'E$ Gr. - AG = + 1h 21 min.												PEC										BR. ST. 218															
I	722.2	00.1	04.5	02.2	02.2	05.2	-00.5	05.9	20	-06.4	14	04	C2.0	10	01.8	06	01.7	C7	01.7	05	01.6	17	01.6	Q3	C2.3	34	-	-									
II	712.8	01.9	9.9	04.3	04.3	07.4	01.2	14.2	17	-03.0	01	14	C1.9	05	01.6	04	01.7	04	01.4	09	01.6	12	02.1	01	04.0	75	-	-	-	-							
III	716.2	04.5	11.4	07.9	07.9	12.3	03.6	22.6	21	-04.0	01	17	C1.0	08	01.8	05	01.4	07	01.3	05	01.2	08	02.3	03	01.7	72	-	-	-	-							
IV	714.5	07.1	12.8	08.9	09.4	13.6	05.1	20.9	30	01.0	19	10	C2.3	11	02.0	10	01.9	C5	01.6	08	01.9	10	02.4	08	01.9	07	02.1	19	-	-	-	-					
V	715.6	11.0	16.8	12.9	13.4	18.2	08.4	25.3	31	04.4	11	15	C1.1	16	07.2	10	01.6	06	02.5	14	01.6	11	01.5	05	02.2	03	02.3	13	-	-	-	-					
VI	716.2	16.1	21.6	17.3	18.1	22.8	12.7	28.2	27	04.4	14	03	C2.3	14	07.1	C8	04	02.0	12	01.6	07	02.4	16	03.0	07	03.1	19	-	-	-	-						
VII	718.4	17.9	24.7	20.0	20.6	26.1	14.5	32.9	17	09.7	10	06	C2.5	07	02.9	15	01.7	04	02.6	22	02.6	09	02.2	17	02.4	02	03.5	11	-	-	-	-					
VIII	716.6	19.0	26.6	21.1	22.0	27.7	16.3	32.8	05	09.9	14	10	02.0	00	02.4	12	02.0	10	01.9	15	02.2	14	03.4	-	-	-	-	-	-	-	-	-					
IX	718.4	14.0	21.9	16.8	17.4	22.8	11.7	30.7	04	01.8	28	03	C1.7	09	07.1	06	02.0	07	02.3	C9	01.7	11	01.9	17	02.8	02	03.0	16	-	-	-	-	-	-	-	-	-
X	716.9	07.5	13.7	09.6	10.1	14.7	05.9	19.4	01	-03.0	28	04	C1.2	17	01.8	C4	01.5	04	01.5	08	02.4	11	01.7	13	02.4	-	-	34	-	-	-	-	-	-	-	-	-
XI	719.6	02.9	9.9	05.6	05.6	09.6	02.1	12.8	17	-07.6	19	03	01.3	06	01.5	08	01.5	03	02.0	07	01.6	10	01.6	10	01.8	02	02.0	41	-	-	-	-	-	-	-	-	-
XII	726.4	06.0	04.0	01.6	01.6	05.2	-01.0	12.6	04	-07.6	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	07.4	15.2	09.6	10.4	16.4	05.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}26'N \lambda = 20^{\circ}21'E$ Gr. - AG = + 1h 22 min.												SKIVJANJE-ĐAKOVICA										BR. ST. 219															
I	-	-00.6	05.0	01.3	01.7	05.7	-01.4	10.5	22.21	-07.5	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	01.0	07.6	03.6	03.9	08.9																															

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine mm	Broj dana na nra:																														
							Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡												
	7	14	21	Sred. (Dnev.)			mm	7	14	21	Sred.	Mn	Dat.	=	<	>	≥	≤	≥	≤	≥	≤	≥	≤	≥												
<b>BR. ST.216</b>																																					
I	7.5	7.3	6.4	7.1			048	C13.6	03	03	07	27	•	•	•	•	02	16	14	09	01	06	12	04	•	•											
II	5.9	5.9	5.0	5.6			035	C12.0	08	•	•	19	•	•	•	•	06	11	07	05	02	06	03	02	•	02											
III	6.9	6.4	7.7	6.0			027	C07.0	09	•	•	17	•	•	•	•	06	14	11	05	•	03	09	01	•	01											
IV	6.7	7.5	6.2	6.8			126	027.3	18	•	•	07	•	•	•	•	01	11	14	11	06	14	03	03	•	01											
V	7.3	7.6	6.6	7.3			139	C27.4	16	•	•	•	•	•	•	•	14	22	16	03	22	•	•	•	01	04	•										
VI	6.8	7.4	6.0	6.7			121	C19.3	07	•	•	•	05	•	•	•	02	•	01	08	19	14	05	19	•	•	01										
VII	6.4	6.3	3.4	4.4			074	C06.6	24	•	•	14	04	•	•	•	09	09	07	06	03	07	•	•	01	01	•										
VIII	2.7	2.7	3.1	4.0			035	C17.4	13	•	•	•	17	02	•	•	10	04	05	05	01	05	•	•	06	•											
IX	3.7	5.4	3.2	4.1			073	C04.1	27	•	•	•	05	•	•	•	05	01	06	05	01	06	•	•	03	01	•										
X	7.1	6.6	5.6	6.5			090	C21.3	22	•	•	03	•	•	•	•	01	11	17	13	02	14	02	01	•	02											
XI	6.1	5.4	4.9	5.5			082	C30.9	27	•	•	04	•	•	•	•	08	11	11	08	02	09	05	01	•	01											
XII	6.6	6.6	6.4	6.7			058	C27.0	09	•	03	26	•	•	•	•	06	13	14	11	01	07	11	03	•	24											
GOD.	-	6.1	6.4	5.1	5.9		-	-	908	C04.1	27	x	03	10	105	39	06	•	00	-	55	123	147	110	27	120	45	15	•	01	01	24	06	44			
<b>BR. ST.217</b>																																					
<b>DIPITREVGRAD</b>																																					
I	7.3	7.6	6.5	7.2			064.5	C03.8	86	70	84	80	48	037	C10.3	03	03	04	23	•	•	C2	•	C3	16	15	08	01	08	10	01	•	•	06			
II	6.4	6.0	5.5	6.0			117.7	C04.3	85	55	77	72	25	028	C12.2	21	•	•	13	•	•	05	04	12	05	04	01	03	01	•	01	02					
III	6.4	5.5	5.0	5.6			154.0	C04.5	82	47	70	66	17	019	C005.5	07	•	•	11	01	•	04	08	14	10	04	•	09	06	03	•	01					
IV	7.0	7.0	4.4	6.1			152.3	C05.3	82	45	70	67	22	072	C26.4	19	•	08	•	•	06	04	09	13	08	03	12	01	•	C1	04						
V	6.3	6.7	5.7	6.2			197.1	C08.1	86	57	82	75	34	128	C04.5	16	•	01	01	•	01	02	08	20	15	03	20	•	•	01	06	02					
VI	6.3	6.6	5.1	6.0			212.1	C10.5	53	58	80	74	38	083	C22.6	08	•	•	12	•	•	05	02	03	06	15	03	15	•	•	11	C1					
VII	3.7	4.0	3.1	3.4			316.7	C10.6	79	46	78	68	23	050	C13.8	24	•	•	19	11	•	04	14	C3	08	07	03	06	•	03	01	•	03				
VIII	2.7	4.7	4.0	3.2			252.3	C10.4	80	36	74	64	24	035	C13.6	26	•	•	24	10	•	02	01	C1	07	04	02	07	•	•	07	01	•				
IX	3.2	4.6	2.2	3.4			240.4	C09.4	84	40	76	67	25	022	C07.4	27	•	•	17	01	•	03	01	12	•	06	06	06	•	•	04	04	•				
X	7.0	7.1	3.9	6.0			158.0	C07.1	81	51	82	72	26	065	C15.0	25	•	•	05	•	•	01	01	08	16	10	02	16	•	•	04	01	•				
XI	7.6	5.8	4.3	5.9			115.5	C05.2	89	68	87	82	20	078	C17.5	09	•	•	11	•	•	02	05	11	08	07	03	07	03	01	01	02					
XII	6.5	6.2	6.4	6.4			087.5	C04.0	89	77	86	82	26	057	C13.0	15	•	01	24	•	•	01	05	10	05	03	10	10	02	01	•	01	19				
GOD.	-	5.8	6.0	4.5	5.5		2108.5	C06.9	P4	54	78	72	17	674	C041.5	Kv	-	03	96	73	22	-	38	04	76	58	141	93	24	172	35	04	01	01	40	20	32
<b>PEČ</b>																											<b>H<sub>s</sub> = 498 m H<sub>b</sub> = 500.8 m H<sub>r</sub> = 2.0 m h<sub>t</sub> = 1.5 m</b>										
BR. ST.218	-	-	-	-	-	-	087.1	C04.4	E7	73	83	81	45	028	C004.5	03	-	16	-	-	02	02	14	12	07	-	10	04	01	-	-	03	-	-			
II	7.7	7.4	6.7	7.4			068.2	C05.0	87	70	80	79	45	066	C22.0	05	-	11	-	-	04	18	11	05	03	11	01	-	-	-	05	-					
III	7.1	6.4	5.5	6.4			144.6	C05.2	79	57	68	68	29	056	C17.0	29	-	06	-	-	04	13	13	10	01	11	05	02	-	C2	07						
IV	7.3	7.9	6.1	7.1			136.7	C05.4	72	50	64	62	27	062	C030.8	18	-	05	-	-	02	04	10	12	07	03	12	-	-	C3	02	-					
V	7.0	6.5	6.6	6.6			174.2	C07.5	80	57	70	69	40	11	C29.3	16	-	01	-	-	03	01	11	17	14	04	17	-	-	04	01	-					
VI	6.0	6.7	6.7	6.5			212.9	C09.5	70	49	64	61	27	073	C26.7	17	-	05	-	-	06	12	07	02	12	-	-	-	-	04	01	-					
VII	5.6	5.6	3.6	4.1			300.4	C10.1	67	45	56	56	23	044	C31.0	21	-	06	-	-	17	07	01	C7	02	11	05	07	05	01	07	-	03				
VIII	2.9	4.9	4.1	3.9			295.1	C10.4	63	41	55	53	29	012	C06.1	30	-	04	-	-	24	10	03	05	•	10	02	04	•	06	04	-	04				
IX	5.0	5.2	2.7	4.3			201.9	C10.0	61	52	69	68	36	042	C24.7	27	-	01	-	-	03	04	08	06	06	01	08	-	-	07	01	-					
X	7.1	6.9	5.3	6.4			147.6	C07.0	86	61	76	74	35	284	C06.2	16	-	01	-	-	03	10	17	17	09	17	01	01	-	06	02	-					
XI	6.5	6.5	5.4	6.3			090.4	C05.5	89	69	81	80	37	107	C030.6	01	-	05	-	-	02	04	12	13	C8	04	11	01	01	-	01	09	-	01			
XII	7.1	7.3	6.2	6.9			068.7	C04.8	88	74	82	81	44	023	C006.7	13	-	03	20	-	-	02	03	15	11	07	07	08	05	01							

Mesec	Vazdušni Pritisak hPa mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 42^{\circ}38'N \lambda = 20^{\circ}34' E$ Gr. $\Delta G = + 1h\ 22\ min.$																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	00.9	08.3	03.9	04.3	09.3	00.2	16.9	16 -05.0	28.12	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	02.8	13.1	07.2	07.5	14.0	01.6	25.0	21 -05.8	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	05.7	13.9	08.5	09.2	15.1	03.8	21.8	30 -02.0	71	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	10.8	18.4	12.3	13.4	19.9	07.6	27.0	31 01.1	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	15.9	22.8	17.0	18.2	24.3	11.8	29.0	27 04.2	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	16.8	26.2	18.5	20.0	27.5	12.6	34.4	17 07.4	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	17.0	28.5	19.6	21.1	29.7	13.2	34.7	05 09.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	11.9	23.8	15.4	16.6	25.1	09.9	32.7	04 -00.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	05.9	15.2	08.7	09.7	16.7	04.5	22.0	23 -03.6	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	01.9	09.8	04.6	05.2	11.0	01.3	16.4	15 -02.2	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	-01.2	04.5	01.2	01.4	06.0	-01.6	13.5	04 -07.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 42^{\circ}04'N \lambda = 20^{\circ}39' E$ Gr. $\Delta G = + 1h\ 23\ min.$																												
I	-	-02.0	01.8	-01.2	-00.5	03.3	-03.4	-	-	-	19	02.0	08	02.0	26	01.2	04	02.2	02	02.0	03	01.7	02	01.0	19	02.4	10	
II	-	00.3	04.5	01.3	01.8	06.0	-01.2	12.1	12 -06.1	28.09	10	02.2	06	01.5	20	01.4	20	02.1	10	02.4	04	03.0	01	03.0	13	03.5	*	
III	-	01.8	07.3	03.4	04.0	08.3	00.8	19.0	23 -07.1	01	17	02.1	C5	01.8	33	01.2	05	02.0	02	03.0	01	05.0	01	02.0	25	02.9	04	
IV	-	03.5	08.1	04.7	05.2	09.7	01.6	18.0	30 -01.1	24	24	02.4	02	02.5	17	01.3	07	02.7	11	02.4	C2	02.5	06	02.5	18	02.7	01	
V	-	04.4	12.8	09.1	09.8	14.6	-	22.0	31	-	17	C2.6	06	01.8	15	01.1	12	01.4	16	02.8	14	03.1	*	*	05	02.4	08	
VI	-	13.6	17.7	13.2	14.4	19.5	-	27.0	27	-	10	02.8	02	01.0	21	01.4	08	01.6	14	02.1	15	02.7	C6	03.5	10	02.3	04	
VII	-	15.3	21.2	14.8	16.5	23.0	-	32.1	17	-	22	C3.0	05	02.2	26	C1.5	14	01.1	05	02.4	05	03.8	02	03.0	08	02.8	06	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	12.0	18.4	12.6	13.9	19.7	09.3	28.1	04 -03.0	28	12	C3.0	04	02.0	31	01.2	15	02.3	10	02.1	05	04.0	01	04.0	06	03.0	06	
X	-	06.3	11.6	07.2	08.1	13.1	04.3	19.1	05 -03.4	28	10	02.6	03	02.3	17	01.2	15	02.7	22	03.1	18	03.8	05	02.2	03	04.0	*	*
XI	-	02.2	07.5	03.2	04.0	08.7	06.9	16.0	19 -05.1	02	24	02.3	04	01.8	17	01.2	11	01.5	12	02.5	12	03.4	03	01.7	03	02.0	04	*
XII	-	-00.3	03.4	00.3	00.9	05.1	-02.2	12.0	29 -07.1	20.19	13	02.7	13	01.9	13	01.2	23	02.2	07	02.0	08	02.9	02	02.0	11	04.5	03	*
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\varphi = 42^{\circ}13'N \lambda = 20^{\circ}44' E$ Gr. $\Delta G = + 1h\ 23\ min.$																												
I	-	00.3	04.7	02.3	02.4	05.6	-00.4	11.8	23 -06.0	16	05	C1.6	09	02.1	C3	01.3	03	01.3	02	01.5	01	01.0	01	01.0	02	01.0	67	
II	-	01.7	07.4	04.6	04.6	08.8	01.2	14.7	17 -03.1	28	04	02.8	07	02.9	02	01.5	04	01.5	01	02.0	04	02.2	06	02.2	*	*	56	
III	-	04.1	12.0	08.8	08.4	13.2	03.6	23.6	23 -04.1	01	02	C1.5	08	01.1	C1	02.0	06	01.7	*	03	02.3	01	02.0	02	03.5	70		
IV	-	06.8	13.6	09.8	10.0	14.7	05.6	22.4	30 -01.6	21	07	C1.3	03	02.3	06	01.7	04	01.8	01	02.0	05	01.6	06	02.5	03	C1.3	55	
V	-	11.8	18.1	13.8	14.4	20.0	09.6	26.6	31 05.4	11	07	C2.1	05	C1.6	C1	02.0	06	01.8	09	01.6	11	01.8	12	02.5	02	01.5	40	
VI	-	17.1	23.5	18.4	19.4	25.3	14.1	32.5	27	07.0	14	08	01.8	08	01.9	04	01.2	05	01.6	07	01.3	14	02.1	21	02.7	02	01.0	21
VII	-	19.1	27.0	21.4	22.0	28.9	14.9	37.6	17	09.5	09	18	C1.5	09	01.4	12	02.1	15	01.7	05	01.2	05	01.6	08	02.1	03	01.7	18
VIII	-	16.9	26.4	22.1	22.7	29.6	16.2	36.1	05 11.8	31	16	C1.8	19	01.9	06	01.8	09	01.3	06	01.3	07	01.1	01	01.0	20	*	*	*
IX	-	14.3	24.0	17.8	18.5	25.4	13.0	34.1	04 -03.7	28	05	C2.4	11	01.6	06	01.3	11	01.8	08	01.9	08	01.8	07	02.3	03	01.3	31	
X	-	08.4	15.7	10.9	11.4	17.0	07.0	23.0	23 -02.0	28	04	01.2	08	01.6	04	01.5	07	01.9	11	02.0	13	02.8	16	02.6	04	01.2	26	
XI	-	03.1	09.1	05.6	05.8	10.2	02.5	15.1	29.28	-01.4	18	11	01.3	12	02.2	05	01.8	06	01.3	07	01.1	09	01.7	05	02.2	07	01.1	28
XII	-	00.4	03.7	01.7	01.9	04.7	-00.7	12.2	04 -06.1	24	11	01.5	20	02.3	04	01.2	04	01.0	11	01.5	06	02.0	07	01.7	04	01.2	26	
GOD.	-	08.7	15.6	11.4	11.8	17.0	07.2	27.6	07.0 -06.1	24.0	08	C1.7	11.9	01.9	54	01.7	80	01.7	71	01.5	85	02.0	97	02.3	33	01.4	458	
$\varphi = 42^{\circ}53'N \lambda = 20^{\circ}52' E$ Gr. $\Delta G = + 1h\ 24\ min.$																												
I	-	-00.2	04.0	00.9	01.4	04.3	-01.2	08.0	02.01	-08.3	16	14	C2.0	C2	01.0	C5	01.4	05	01.6	04	01.5	08	01.1	06	01.5	13	01.8	36
II	-	01.0	07.7	03.3	03.8	08.3	-00.1	14																				

Mjesec	Oblačnost Nm (0-10)				Insolacije broj sati (dnevi)	Vlažnost vazduha				Padavine R mm		Broj dana na sata:																
	e <sub>m</sub>	7	14	21		7	14	21	Sred. Sred. (dnevi)			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	♦	▲	▲	■		
	mm	mm	mm	mm		mm	mm	mm	mm			mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm			
KLINA																												
BR. ST.221																												
I	-	-	-	-	-	-	-	-	-	013 003.0	11	-	-	-	-	-	-	-	-	11 07	11 01	-	-	-	-	-		
II	7.3	5.8	6.0	6.4	-	-	-	-	-	048 C18.0	05	-	-	11	-	-	-	05	14 13	05 02	12	-	-	-	-	15		
III	-	-	-	-	-	-	-	-	-	015 007.2	09	-	09	01	-	-	-	-	08 04	07 03	02	-	-	-	-	09		
IV	6.3	4.8	4.6	5.9	-	-	-	-	-	048 017.1	18	-	-	02	-	-	-	01	08 11	09 01	11	-	-	-	-	05		
V	6.4	4.5	4.2	5.7	-	-	-	-	-	129 064.4	16	-	-	02	-	-	06	03	06 17	11 03	17	-	-	-	-	03		
VI	5.9	5.9	6.4	5.9	-	-	-	-	-	080 044.5	17	-	-	16	-	-	07	01	07 11	10 01	11	-	-	-	-	02		
VII	3.2	4.1	3.0	3.4	-	-	-	-	-	035 011.7	08	-	-	23	12	-	07	13	04 09	07	02 09	-	-	-	-	02		
VIII	2.5	4.5	2.8	3.3	-	-	-	-	-	014 006.3	24	-	-	27	17	-	08	13	02 06	03	06	-	-	-	-	02		
IX	5.1	4.4	2.0	3.8	-	-	-	-	-	043 024.3	27	-	-	01	19	02	05	10	02 07	05 01	07	-	-	-	-	06		
X	6.1	6.1	4.9	5.7	-	-	-	-	-	191 025.4	16	-	-	06	-	-	05	05	C9 16	14 06	16	01	-	-	-	03		
XI	7.0	5.9	5.5	6.1	-	-	-	-	-	092 026.2	26	-	-	15	-	-	04	12	10	09	04	10	-	-	01			
XII	6.9	7.5	6.7	7.7	-	-	-	-	-	026 007.5	15	-	03	24	-	-	-	01	16	09	07	07	03	01	01	12		
GOD.	-	-	-	-	-	-	-	-	-	734 064.4	Kv	-	-	-	-	-	-	-	128 91	22 125	08 03	01	-	-	-	24		
DRAGAS																												
BR. ST.222																												
I	6.5	6.5	6.4	6.5	-	-	-	-	-	044 020.1	24	-	-	-	-	-	01	01	07 16	12 12	01	07	10	02	-	-		
II	6.2	6.6	5.6	6.1	-	04.0	80	69	79	76	38	048 G19.7	05	-	03	16	-	-	01	06	11	06	02	07	04	-	02	
III	5.8	6.3	6.0	6.0	-	-	-	-	-	030 015.1	09	-	01	15	-	-	-	09	15	10	03	01	07	08	-	01		
IV	7.4	6.8	6.8	7.5	-	04.8	82	62	74	73	22	043 013.6	17	-	05	-	-	02	01	15	13	10	01	12	04	-	01	
V	6.8	7.4	6.9	7.0	-	06.7	78	64	77	73	30	164 041.1	16	-	-	-	-	01	-	02	13	17	16	05	17	-	04	
VI	5.6	5.9	6.0	5.9	-	08.3	70	58	73	67	32	077 C20.0	20	-	-	-	01	-	06	11	13	10	03	13	-	01		
VII	3.2	3.9	3.1	3.1	-	09.1	70	50	73	64	21	027 010.0	21	-	-	-	16	03	-	02	01	15	04	05	-	02		
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	4.5	4.8	3.0	4.1	-	08.4	74	57	76	69	39	038 016.5	27	-	-	03	-	-	01	-	08	05	03	02	05	-	03	
X	5.9	6.9	4.9	5.9	-	05.8	75	60	74	70	30	168 033.2	15	-	-	02	-	-	02	-	09	10	19	17	08	18	03	
XI	5.5	5.7	5.6	5.6	-	-	-	-	-	100 040.5	02	-	-	06	-	-	01	-	07	08	09	07	04	06	-	01		
XII	6.2	5.6	7.3	6.4	-	-	-	-	-	039 013.4	19	-	03	24	-	-	05	-	06	13	14	07	01	07	-	23		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
PRIZREN																												
BR. ST.223																												
I	7.0	7.0	6.4	6.8	084.1	04.6	91	74	84	83	46	052 018.6	24	-	-	15	-	-	05	-	06	15	15	07	02	12	05	
II	7.1	6.9	6.0	6.6	092.4	05.0	92	67	81	80	37	041 020.0	05	-	-	09	-	-	05	02	04	15	08	06	02	08	-	
III	6.0	6.4	5.8	6.1	149.7	05.6	87	57	69	71	26	029 008.9	09	-	-	04	-	-	04	07	14	10	06	08	04	01	02	
IV	7.3	7.6	5.6	6.8	140.2	05.8	77	50	65	64	24	051 013.5	17	-	-	05	-	-	06	01	12	15	10	02	15	-	01	
V	6.5	7.0	5.1	6.2	184.4	07.9	77	54	67	66	27	159 048.7	16	-	-	04	-	-	08	01	02	09	17	16	04	17	-	
VI	5.5	5.4	4.7	5.2	234.1	05.8	68	47	62	59	29	061 025.0	20	-	-	18	03	01	1C	03	04	07	11	08	02	11	-	
VII	2.9	3.7	2.7	3.1	319.0	10.4	70	39	55	55	21	024 013.6	08	-	-	24	15	01	05	01	16	02	07	04	01	07	-	
VIII	2.7	3.9	2.1	2.9	296.8	10.9	70	40	54	55	22	024 007.5	23	-	-	27	16	01	10	-	12	02	07	04	07	-	06	
IX	4.9	4.1	1.9	3.6	214.0	09.8	80	44	65	63	27	031 015.1	27	-	-	20	03	-	09	-	10	02	06	04	02	06	-	
X	6.8	6.5	4.5	6.0	158.9	04.9	83	52	72	69	27	155 025.4	15	-	-	01	-	-	16	05	02	07	21	18	05	21	-	
XI	8.3	6.2	5.0	6.5	080.9	05.6	88	71	83	81	39	059 022.6	01	-	-	08	-	-	07	03	02	13	13	06	02	13	01	
XII	8.3	7.8	7.8	8.0	052.2	04.6	90	81	89	87	54	060 033.0	19	-	04	20	-	-	09	02	02	20	12	08	02	09	06	
GOD.	6.1	6.0	4.8	5.6	6.1	-	-	-	-	-	-	413 034.8	Kv	-	-	86	70	25	-	01	-	56	142	120	94	23	110	17
PRISTINA																												
BR. ST.225																												
I	8.0	7.5	6.0																									

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm			Sred. (Dles)	Max	Min	Max	Dat.	Min	Det.	N		NE		E		SE		S		SW		W		NW			
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.				
$\varphi = 42^{\circ}23'N \lambda = 21^{\circ}10' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	-	-01.5	02.5	-00.5	00.0	03.1	-02.5	08.0	03 -08.8	25	18	C1.1	*	*	C2	C2.5	12	02.7	03	01.7	07	01.9	11	01.8	39	C2.1	01		
II	-	00.9	05.4	03.2	03.4	07.3	-00.1	14.0	17 -06.3	28	05	C1.4	05	02.0	C4	C1.5	21	03.4	07	02.5	08	02.0	15	01.9	22	C2.1	01		
III	-	01.6	10.9	05.5	05.9	11.6	01.1	22.9	23.22 -06.8	01	06	C1.3	06	01.7	02	02.0	26	03.5	04	02.0	09	01.7	09	01.7	31	02.0	*		
IV	-	05.2	11.9	06.9	07.7	12.9	02.7	20.0	29 -02.0	21	14	C1.6	09	01.6	04	01.8	26	03.5	01	02.0	12	02.6	05	02.0	19	02.4	*		
V	-	10.0	16.5	11.6	12.4	18.3	07.2	25.0	31 03.0	14	10	C1.6	C8	02.0	05	02.0	05	02.2	04	01.8	07	02.7	24	01.8	32	C2.1	*		
VI	-	14.4	21.0	15.6	16.7	22.7	11.3	28.5	29 04.4	14	13	C1.2	04	02.0	01	02.0	11	01.8	04	01.0	18	02.6	19	02.3	20	02.0	*		
VII	-	15.6	24.6	17.5	18.8	26.0	11.9	33.8	17 07.1	10	09	C1.7	04	02.0	02	02.5	01	02.0	06	01.5	13	02.4	25	02.2	33	02.6	*		
VIII	-	16.0	27.2	18.6	20.1	27.7	13.2	33.2	05 09.3	11	03	C1.3	G7	07.5	*	*	05	02.0	03	01.3	18	01.4	25	02.1	37	02.1	*		
IX	-	11.7	22.6	14.5	15.8	23.3	10.0	30.0	04 00.6	28	16	C1.5	C3	02.3	*	*	08	02.4	06	01.5	09	02.2	23	01.8	25	02.2	*		
X	-	06.3	15.2	09.0	09.9	16.5	04.6	22.6	23.08 -03.2	28	14	C1.6	C4	07.0	C1	C2.0	14	02.6	03	02.7	11	02.4	15	03.3	33	C2.5	*		
XI	-	01.4	07.9	03.7	04.2	08.8	00.4	14.1	06 -04.9	30	21	C1.8	04	02.0	*	*	11	03.1	07	01.4	08	02.5	14	01.5	23	01.9	02		
XII	-	-02.2	03.3	-00.1	00.3	04.3	-03.5	09.6	04 -14.6	25	27	C1.7	C3	02.7	*	*	07	01.9	01	02.0	09	01.8	16	01.9	30	02.2	*		
GOD.	-	06.6	14.2	08.8	09.6	15.2	04.7	33.8	Pm	-14.6	25	00	156	C1.5	47	00.0	21	02.0	147	03.0	44	01.7	129	G2.7	201	02.0	344	C2.2	04
$\varphi = 42^{\circ}47'N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-00.3	03.6	00.6	01.1	04.6	-01.9	09.0	01 -10.3	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	02.0	08.5	04.0	04.6	09.7	00.2	15.4	11 -07.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	02.1	11.4	05.3	06.0	12.3	00.7	24.9	23.21 -07.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	04.7	12.6	07.2	07.9	17.0	02.7	-	-	-	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	09.5	17.0	10.9	12.1	18.8	06.9	25.9	28 01.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	13.9	21.3	15.0	16.3	22.9	10.7	28.2	29 03.9	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	14.0	24.2	15.9	17.5	25.4	11.4	33.4	17 07.0	09	04	C1.2	-	*	*	*	01	02.0	03	01.7	*	*	*	*	*	05			
VIII	-	14.4	26.7	17.0	18.8	27.5	12.3	32.0	05.04	05.2	11	02	C1.0	-	*	*	05	02.0	04	01.2	*	*	*	*	*	02			
IX	-	11.7	21.9	14.3	15.6	22.8	09.5	30.4	04 00.4	28	02	C1.0	-	*	*	*	C1	01.0	14	02.1	*	*	*	*	*	73			
X	-	07.3	14.8	08.3	09.7	16.7	04.6	22.9	08 -03.5	28	09	C1.6	-	*	*	*	03	02.0	23	02.5	*	*	*	*	*	58			
XI	-	02.3	10.0	03.9	05.0	10.9	00.8	16.9	17 -02.1	30	04	C1.5	-	*	*	*	04	01.0	14	02.1	*	*	*	*	*	68			
XII	-	-00.6	04.9	01.2	01.6	05.7	-01.7	10.0	04 -07.3	24	03	C1.3	-	*	*	*	10	02.7	*	*	*	*	*	*	*	*	80		
GOD.	-	06.6	14.7	08.6	09.7	16.2	04.7	-	-	-	10.3	K1	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 42^{\circ}27'N \lambda = 21^{\circ}47' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-00.3	03.6	01.5	01.6	04.5	-	08.8	29	-	-	08	C2.0	C2	03.0	10	C2.4	05	01.8	17	02.3	04	03.0	C2	01.5	01	C2.0	44	
II	-	01.8	08.3	04.2	04.6	09.4	-	13.8	17	-	-	02	C2.5	C2	02.5	04	C2.8	03	03.0	37	02.7	01	01.0	02	02.0	*	*	33	
III	-	02.9	11.8	06.2	06.8	12.6	-	23.5	22	-	-	*	02	C2.5	C5	02.4	08	02.5	23	02.7	05	01.8	01	02.0	*	*	49		
IV	-	05.3	13.0	07.9	08.5	14.4	03.2	21.9	30 -02.0	03	02	C2.0	06	02.0	11	01.7	02	02.5	30	02.7	*	*	01	01.0	02	02.5	36		
V	-	09.7	17.5	12.0	12.8	19.1	07.1	25.7	31 01.9	11	01	C1.0	07	02.4	08	C2.1	05	02.2	12	02.6	06	02.2	05	02.4	02	02.0	47		
VI	-	14.8	21.8	16.2	17.3	24.1	11.3	29.3	29 06.4	14	12	C2.5	01	04.0	06	C1.5	01	03.0	18	02.8	14	02.4	07	03.4	*	*	41		
VII	-	15.3	25.4	17.0	18.7	26.7	11.5	34.9	17 06.8	10	03	C3.3	06	02.8	07	02.0	01	02.0	08	01.8	06	02.0	04	02.2	03	04.3	55		
VIII	-	16.0	28.0	18.8	20.4	28.8	12.5	34.5	05 09.0	11	*	*	03	02.7	09	C2.1	02	02.5	15	02.0	*	*	08	02.6	*	*	56		
IX	-	11.8	23.3	14.7	16.2	24.2	09.8	30.9	04 00.2	28	03	C2.0	02	02.0	06	C2.3	02	03.5	19	02.4	05	02.4	03	03.0	01	01.0	49		
X	-	07.0	16.2	10.4	10.8	17.3	04.4	23.1	24.08 -04.3	28	01	C3.0	-	*	*	03	02.0	01	03.0	41	02.5	06	02.3	02	02.5	*	*	39	
XI	-	01.8	09.4	03.8	04.7	10.4	00.6	15.0	06 -03.0	30	01	C3.0	16	02.1	C5	01.8	*	*	03	02.0	01	01.0	17	02.2	02	02.0	03	03.0	43
XII	-	-01.4	04.1	03.7	01.1	01.2	05.1	-02.2	10.7	13 -08.5	25	01	04.0	35	02.7	03	02.3	*	*	03	01.7	08	02.1	03	02.7	01	03.0	39	
GOD.	-	07.1	15.2	09.3	10.2	16.4	-	34.9	-	27	02.7	39	02.6	85	02.1	37	02.3	248	0										

Mesec	Oblačnost Nm (0-10)			Incidenca ljetnih satih (%)	Vlažnost vazduha			Padavine mm	Broj dana na mjesec																										
					Umjer.				Nm (0-10) P mm																										
	7	14	21		7	14	21		7	14	21	Tn	Tx	In	Tz	Iz	In	F (0-12)	Nm (0-10)	P mm	●	★	◆	▲	▲	A	▲	■	■						
<b>BR. SI.226 URESEVAC</b>																																			
I	8.2	7.2	5.6	7.1	061.2	04.2	91	83	91	88	63	030	C12.4	18	•	03	23	•	•	•	03	14	11	07	01	04	•	•	•	05	12				
II	7.2	6.6	5.6	6.6	101.0	04.9	92	83	84	83	10	025	C12.7	21	•	02	16	•	•	•	01	05	13	07	04	06	01	02	•	•	02	03			
III	6.1	5.7	4.5	5.6	104.9	05.4	93	61	81	78	31	015	C03.3	06	•	01	16	•	•	•	01	05	10	09	06	03	01	01	01	01	04				
IV	6.4	7.	3.7	5.9	106.2	05.7	E5	55	74	73	30	032	C12.0	17	•	•	03	•	•	•	04	01	•	13	07	03	02	02	•	•	02	•			
V	6.3	6.2	4.3	5.6	109.0	05.2	97	61	80	76	33	125	C06.7	16	•	•	01	•	•	•	04	08	18	15	08	15	•	•	•	•	05	01			
VI	6.0	6.3	4.0	5.6	104.7	10.5	83	60	77	74	37	075	C17.2	17	•	•	11	•	•	•	01	07	13	09	07	13	•	•	•	•	01	01			
VII	3.2	4.4	3.5	3.7	105.8	10.9	62	50	71	65	32	049	C14.3	21	•	•	16	07	•	•	01	14	05	07	06	13	•	•	•	•	02	•			
VIII	3.2	3.2	2.4	2.7	100.3	11.6	84	87	83	84	14	021	C04.2	25	•	•	26	11	•	•	12	01	05	02	01	05	•	•	•	•	03	•			
IX	5.2	3.5	1.5	4.4	235.5	10.5	93	55	84	78	24	024	C10.1	08	•	•	08	01	•	•	10	01	08	04	01	06	•	•	•	•	02	•			
X	6.5	5.4	3.3	5.1	100.1	07.4	90	62	84	75	36	095	C18.2	16	•	•	04	•	•	•	01	05	19	19	02	19	•	•	•	•	01	•			
XII	7.2	6.3	5.2	6.2	077.9	04.2	91	79	80	87	59	049	C17.0	19	02	01	25	•	•	•	01	10	06	02	04	07	•	•	•	•	01	07			
GOD.	6.2	5.8	3.9	5.3	2113.6	07.4	85	64	81	78	10	017	C01.2	5.9	•	07	67	110	66	19	•	08	01	•	17	01	05	01	01	01	01				
<b>BR. SI.227 SJEJARINSKA BARJA</b>																										H <sub>b</sub> = 375 m H <sub>p</sub> = m h <sub>b</sub> = 2,0 m h <sub>p</sub> = 1,0 m									
I	8.1	8.0	7.0	7.7	-	-	-	-	-	-	-	036	C08.8	18	02	02	24	•	•	05	26	04	07	07	01	04	03	•	•	03	02				
II	6.7	6.7	5.5	6.4	-	-	-	-	-	-	-	026	C11.5	08	-	-	14	•	•	07	04	05	15	06	02	01	06	•	•	03	•				
III	6.1	6.7	5.3	5.2	-	-	-	-	-	-	-	047	C14.6	09	-	-	13	•	•	01	05	15	09	07	02	07	06	•	•	05	•				
IV	7.4	7.6	6.7	7.7	-	-	-	-	-	-	-	053	C15.0	15	-	-	67	•	•	07	01	02	15	09	04	03	05	•	•	•	•				
V	7.1	7.4	7.4	7.3	-	-	-	-	-	-	-	102	C05.4	16	-	-	02	•	•	04	03	16	15	13	01	16	•	•	•	•	05	•			
VI	7.0	7.0	6.6	7.1	-	-	-	-	-	-	-	104	C17.5	26	-	-	16	•	•	01	02	14	11	11	04	11	•	•	01	07	•				
VII	3.6	4.6	3.5	3.8	11.8	52	56	89	79	85	45	032	C14.6	08	-	-	15	04	•	06	14	07	06	06	01	06	•	•	02	•					
VIII	2.9	4.9	5.1	4.7	12.3	94	50	56	77	51	024	C11.6	12	-	-	24	10	•	03	10	08	03	05	03	05	•	•	01	01	01	01				
IX	5.6	6.6	6.1	6.1	-	10.2	93	54	86	76	19	030	C16.4	23	-	-	07	01	•	04	10	05	04	01	04	•	•	•	•	02	01				
X	6.8	6.6	4.6	6.0	-	07.4	92	60	90	51	83	092	C17.9	22	-	-	04	•	•	01	05	11	11	14	04	15	•	•	02	•					
XI	6.1	6.6	5.2	5.9	-	05.6	94	67	92	84	39	081	C02.7	08	-	-	14	02	•	02	08	12	17	07	04	05	02	01	•	•	03	01			
XII	7.0	6.5	7.2	7.6	-	04.5	94	73	89	75	24	075	C21.0	15	-	-	25	•	•	02	03	17	11	06	03	07	02	•	•	01	16				
GOD.	6.2	6.7	5.9	6.2	-	-	-	-	-	-	-	720	C04.5	40	-	-	62	-	-	01	06	74	140	177	92	28	93	21	12	•	•	01	24	14	24
<b>BR. SI.228 BUJANOVAC</b>																										H <sub>b</sub> = 400 m H <sub>p</sub> = m h <sub>b</sub> = 2,0 m h <sub>p</sub> = 1,5 m									
I	7.4	7.3	5.5	5.6	-	04.4	52	77	86	85	57	027	C05.7	20	-	-	12	•	•	06	16	13	12	11	07	04	•	•	•	01	04	•			
II	7.3	6.1	4.0	5.8	-	05.2	90	66	85	80	41	040	C13.0	21	-	-	14	•	•	02	07	09	07	02	07	01	•	•	•	03	•				
III	6.0	5.5	5.4	5.4	-	05.6	93	59	77	71	27	038	C11.5	09	-	-	13	•	•	03	10	08	06	01	06	02	•	•	01	01	01	01			
IV	6.0	6.7	4.5	5.7	-	05.9	86	57	75	71	43	074	C03.6	16	-	-	06	•	•	02	06	10	06	02	10	•	•	01	02	•					
V	6.1	7.0	5.2	6.1	-	08.6	91	82	86	85	76	090	C01.6	16	-	-	02	•	•	02	07	16	14	02	18	•	•	•	•	05	•				
VI	5.6	6.0	4.2	5.3	-	11.7	89	64	89	79	43	100	C17.0	24	-	-	15	•	•	01	05	16	14	12	05	14	•	•	01	06	02				
VII	3.2	3.8	1.9	3.0	-	11.8	86	52	79	72	37	025	C17.0	01	-	-	20	12	•	03	17	04	04	06	04	01	06	•	•	02	02				
VIII	2.3	2.6	0.8	2.0	-	11.2	87	42	79	68	25	014	C07.5	25	-	-	26	14	•	01	21	01	06	02	06	•	•	01	01	01	01				
IX	4.5	3.6	1.7	3.2	-	10.3	92	50	85	74	36	027	C10.0	08	-	-	08	01	•	01	10	02	05	05	01	05	•	•	•	•	02	03			
X	5.6	6.3	2.4	5.0	-	07.4	91	56	82	76	33	055	C14.8	30	-	-	04	•	•	01	07	17	12	11	12	04	06	•	•	01	01				
XI	6.1	6.2	5.3	6.5	-	05.7	92	72	87	85	42	084	C16.8	08	-	-	12	•	•	02	12	06	06	02	04	01	01	•	•	01	07				
XII	6.4	6.1	5.3	6.0	-	04.3	93	75	91	86	84	034	C02.5	15	-	-	27	•	•	04	06	04	06	01	06	05	02	•	•	05	12				
GOD.	6.3	6.5	5.1	6.0	2028.1	07.4	86	58	75	73	23	721	C04.3	48	-	-	02</																		

Mesec	Vardulni pritisak Pm, mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Fm (0-12)																		
		Tm			Sred. (Dnes)		Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21									8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 42^{\circ}58'N \lambda = 22^{\circ}08' E$ Gr. $\Delta G = +1h\ 29\ min.$																														
I	-	00.5	03.8	01.7	01.9	04.7	69.4	09.5	31.03	-08.6	16	-	-	-	-	-	-	-	-	-	-	-	-	-						
II	-	03.6	09.8	05.1	05.9	11.2	01.7	16.4	11	-03.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-						
III	-	05.0	12.9	08.2	08.6	13.9	03.0	26.4	27	-05.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	07.9	14.0	09.6	10.0	15.3	04.4	25.9	30	-00.1	04	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	12.0	16.3	13.1	14.1	20.1	09.6	28.4	31	05.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	16.4	22.2	16.7	18.0	24.3	13.0	29.9	29	06.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	16.8	25.5	17.9	19.5	26.6	13.4	34.9	17	08.5	04	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	17.2	26.0	19.7	21.2	29.3	14.3	35.4	04	11.0	07.06	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	14.0	24.4	16.1	17.7	25.2	11.9	32.4	04	02.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	09.7	16.9	10.4	11.8	17.9	06.1	25.1	08	-00.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	03.5	11.2	05.8	06.5	12.2	02.0	17.4	19	-01.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	00.3	04.6	01.7	02.0	05.3	-01.1	10.0	05	-05.5	25	-	-	-	-	-	-	-	-	-	-	-	-	-						
GOD.	-	08.9	16.0	10.5	11.4	17.2	601.7	35.4	04M	-09.5	25 VII	-	-	-	-	-	-	-	-	-	-	-	-	-						
$\varphi = 42^{\circ}50'N \lambda = 22^{\circ}08' E$ Gr. $\Delta G = +1h\ 29\ min.$																														
I	-	-00.4	03.6	01.0	01.3	04.5	-01.4	10.0	03	-05.7	16	36	C1.8	C6	01.7	C4	01.0	10	C1.9	13	C2.0	C2	C2.5	-	02	C3.0	20			
II	-	01.7	09.8	04.0	04.9	10.9	00.5	16.9	17.16	-06.1	28	11	C2.1	C2	01.5	C5	01.8	22	C1.8	27	C2.1	C3	C2.7	-	06	C1.8	11			
III	-	02.0	12.2	06.3	06.7	13.1	01.5	25.9	23	-06.4	01	18	C1.7	C7	02.1	C5	01.6	15	C1.9	17	C1.9	04	C2.2	C2	C2.0	10	C2.4	15		
IV	-	05.2	13.1	07.6	08.4	14.5	03.2	25.1	30	-02.8	03	17	C2.0	C4	01.3	11	C1.3	17	C1.9	14	C2.2	C1	C2.0	-	07	C2.6	17			
V	-	10.8	18.1	12.1	13.3	19.2	08.5	27.2	31	03.1	11	11	C1.9	C6	01.8	13	C1.6	15	C1.8	16	C1.8	C3	C2.3	-	05	C2.2	24			
VI	-	15.0	21.0	15.7	16.9	23.3	11.8	29.4	29	05.9	14	16	C2.1	C5	01.8	03	01.7	12	C1.9	16	C1.7	04	C1.8	02	C2.0	11	C2.4	21		
VII	-	15.8	24.5	16.9	18.5	25.7	12.2	33.9	17.14	08.6	10	15	C2.6	C1	02.0	20	C1.2	09	C1.4	15	C1.9	C1	C1.0	01	C1.0	11	C1.7	20		
VIII	-	15.5	26.8	17.8	19.5	28.0	13.4	33.1	03	10.0	11	13	C1.8	C10	01.5	07	C1.0	25	C1.6	07	C2.0	C1	C1.0	02	C2.0	06	C1.8	22		
IX	-	12.4	23.5	14.3	16.1	24.4	10.7	32.4	04	02.5	28	13	C2.4	C3	01.3	04	C1.0	21	C2.0	09	C2.0	C5	C2.4	-	09	C2.2	26			
X	-	07.2	17.1	08.6	10.5	18.0	05.4	25.0	08	-02.6	28	13	C2.2	C5	01.6	12	C1.2	20	C1.9	10	C2.1	04	C2.2	-	06	C2.3	23			
XI	-	02.4	10.7	04.0	05.3	11.5	01.1	17.7	06	-03.6	30	09	C1.4	C9	02.2	10	C1.2	21	C2.0	20	C2.2	04	C2.5	-	06	C2.0	11			
XII	-	-00.3	04.7	01.2	01.7	05.7	-01.2	11.4	13	-06.6	24	12	C2.7	C5	02.2	C6	01.3	17	C1.8	20	C2.2	-	02	C3.0	31					
GOD.	-	07.3	15.4	09.1	10.3	16.6	05.5	33.9	F7	14.7	07.07	46.1	184	02.0	65	C1.8	C10	01.3	204	C1.9	179	C2.0	32	C2.2	C7	01.9	81	C2.2	24	
$\varphi = 42^{\circ}41'N \lambda = 22^{\circ}11' E$ Gr. $\Delta G = +1h\ 29\ min.$																														
I	-	-00.5	03.6	01.0	01.3	04.3	-01.3	08.8	29	-09.6	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	01.8	07.9	03.9	04.4	09.3	00.4	15.0	16	-05.4	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	04.0	12.0	07.2	07.6	13.1	02.7	25.1	21	-05.9	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	06.3	12.8	07.7	08.6	14.2	04.2	23.4	30	-00.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	11.3	17.5	12.2	13.1	18.7	08.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	15.9	21.0	15.9	17.2	22.9	12.3	29.5	29	05.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	16.8	24.3	17.9	19.2	25.8	12.9	33.9	17	08.5	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	17.6	26.7	16.3	20.7	27.6	14.8	33.9	05	10.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	13.2	22.7	15.8	16.9	23.7	11.0	31.5	04	04.1	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	07.9	15.7	10.3	11.1	17.1	06.2	24.0	08	-03.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	01.8	05.3	04.6	05.1	10.6	00.8	15.2	06	-03.3	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-01.1	03.8	01.1	01.2	04.9	-02.0	06.5	05.03	-08.2	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	07.9	14.8	09.7	10.5	16.0	05.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\varphi = 42^{\circ}44'N \lambda = 22^{\circ}21' E$ Gr. $\Delta G = +1h\ 29\ min.$																														
I	-	-06.9	-01.6	-04.7	-04.5	-00.2	-08.4	06.6	17	-20.4	16	13	C2.2	C7	02.0	08	01.2	09	01.0	05	01.0	01	01.0	17	C1.4	32				
II	-	-03.7	02.0	-02.4	-01.6	03.3	-05.5	08.8	18	-13.7	11	-	-	04	02.0	13	C1.5	10	C1.4	03	C1.3	05	C1.8	08	C1.4	31				
III	-	-01.9	05.5	00.6	01.2	06.4	-03.6	17.8	23	-14.5	02	-	-	07	C1.9	20	C1.6	16	C1.3	C8	C1.4	01	01.0	-	03	C1.3	36			
IV	-	01.4	06.7	01.9	03.0	04.4	-01.2	15.3	30	-05.6	05	04	C1.2	C1	03.0	04	02.2	14	C											

Meseč	Oblačnosť Nm (0-10)			Temperatúra dielo satí (Sred. dňa)	Vlažnosť vzduchu			Padaviny R mm			B r o j d a n a n r a :																									
	7	14	21		e mm	m mm	s mm				Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	□									
					7	14	21	Σ	M	Σ	20.00.0	0.025.0	0.20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	*	•	Δ	○	▲	■	□								
<b>V L A S T I N E C</b>																																				
<b>BR. ST.231</b>																																				
I	7.7	6.6	7.6	7.8	-	-	-	-	-	-	055	C13.0	20	-	03	16	-	-	-	03	20	11	1C	01	10	05	04	-								
II	5.5	5.7	6.8	5.3	-	-	-	-	-	-	038	C14.5	21	-	03	10	-	-	-	06	10	07	04	02	07	-	-	02								
III	5.6	5.4	5.6	5.5	-	-	-	-	-	-	026	C10.2	07	-	03	08	04	-	-	07	11	08	04	01	06	03	-	05								
IV	6.4	6.4	5.9	6.2	-	-	-	-	-	-	068	C16.5	19	-	03	01	-	-	-	01	09	11	10	03	11	01	-	04								
V	6.4	6.9	6.5	6.7	-	-	-	-	-	-	122	C36.2	16	-	03	-	-	-	04	12	18	15	05	18	-	-	02									
VI	5.5	6.1	5.2	5.7	-	-	-	-	-	-	083	C20.2	12	-	03	13	-	-	-	03	05	14	09	04	14	-	-	05								
VII	3.6	4.0	3.7	3.8	-	-	-	-	-	-	075	C45.4	01	-	03	18	11	-	-	13	04	07	05	02	07	-	-	01								
VIII	3.1	3.5	3.2	3.3	-	-	-	-	-	-	043	C25.5	13	-	03	26	14	-	-	12	04	08	05	01	08	-	-	01								
IX	5.0	4.3	3.5	4.3	-	-	-	-	-	-	048	C25.0	27	-	03	17	02	-	-	06	05	02	06	-	-	-	-	03								
X	5.6	5.6	5.0	5.4	-	-	-	-	-	-	057	C09.0	30	-	03	01	01	-	-	03	06	16	11	16	-	-	-	-								
XI	5.9	5.6	5.0	5.6	-	-	-	-	-	-	076	C17.0	06	-	03	04	-	-	-	05	1C	07	07	05	06	01	-	-	01							
XII	6.9	7.0	6.4	6.8	-	-	-	-	-	-	095	C28.0	15	-	03	17	-	-	-	05	13	15	13	02	12	09	05	-								
GOD.	5.6	5.7	5.2	5.5	-	-	-	-	-	-	786	C45.4	01M	-	03	56	E3	27	-	-	-	128	9P	28	121	19	10	-	01	-	13	22	22			
<b>P R E D E J A N E</b>																																				
<b>BR. ST.232</b>																																				
I	6.3	6.1	7.3	7.9	-	044	3	B6	73	88	F3	45	074	C24.1	21	-	02	19	-	03	C3	1F	15	12	03	11	08	02	-	01	06					
II	5.5	5.9	3.1	5.2	-	049	9	B9	57	77	T2	31	040	C14.7	21	-	03	12	-	01	06	C7	C5	07	04	02	08	C1	C1	-	01	01				
III	6.3	5.5	5.2	5.7	-	051	91	B3	72	72	T2	24	024	C09.5	07	-	03	12	02	-	01	06	10	07	04	04	04	-	-	02	02					
IV	6.7	6.6	5.7	6.4	-	061	90	B5	78	74	T2	29	09.	C23.3	18	-	03	05	01	-	C1	03	11	15	08	04	15	01	01	-	02	03	01			
V	6.5	6.6	6.1	6.4	-	063	95	E6	89	E1	33	140	C37.5	16	-	03	-	-	-	04	12	22	15	05	21	01	-	-	07	03	-					
VI	5.8	6.3	6.4	6.2	-	114	9	H9	64	H1	82	39	158	C34.2	20	-	03	13	-	02	01	01	06	16	17	05	16	-	-	01	11	03	-			
VII	3.8	3.6	3.3	3.6	-	126	6	H6	56	H8	78	40	109	C06.0	07	-	03	16	08	-	C1	14	C5	07	04	07	04	-	-	02	03	-				
VIII	3.1	3.7	2.8	3.2	-	129	9	H4	57	H6	77	24	047	C30.7	13	-	03	25	12	-	C3	14	04	08	04	01	08	-	-	05	03	-				
IX	5.3	4.6	3.3	4.6	-	109	4	H9	54	H2	80	30	048	C31.3	27	-	03	15	02	-	01	08	C4	06	04	01	06	-	-	04	07	-				
X	5.6	6.1	4.3	5.8	-	086	0	H5	60	H2	63	31	071	C01.2	30	-	03	02	01	-	-	03	07	15	14	02	15	01	-	01	01	-				
XI	7.0	5.8	4.5	5.7	-	058	8	H5	66	H3	85	39	094	C02.8	29	-	03	07	-	-	-	06	10	09	07	06	07	04	02	-	-	03				
XII	7.1	7.0	6.4	6.8	-	046	6	H4	77	H3	88	41	131	C30.0	15	-	03	23	-	-	-	04	15	17	16	05	12	11	04	-	-	04				
GOD.	6.1	5.8	4.9	5.6	-	088	0	H2	60	H1	86	79	24	1030	C60.7	01M	-	03	80	76	22	-	C4	72	111	145	105	36	130	31	10	-	03	33	37	32
<b>S U R D U L I C A</b>																																				
<b>BR. ST.233</b>																																				
I	6.9	7.4	6.7	7.0	-	-	-	-	-	-	051	C10.5	18	-	01	21	-	-	-	04	15	15	10	01	06	07	-	-	01	11	31					
II	5.6	5.2	4.4	5.1	-	-	-	-	-	-	039	C19.0	08	-	01	13	-	-	-	01	C7	C5	07	04	02	07	01	-	-	02	01	-				
III	4.6	5.1	4.8	4.8	-	-	-	-	-	-	024	C08.2	07	-	03	11	01	-	-	11	09	08	04	08	03	03	-	-	01	01	-					
IV	6.2	6.5	5.2	6.0	-	-	-	-	-	-	065	C29.0	15	-	03	-	-	-	03	09	13	11	04	13	01	-	-	02	01	01						
V	5.8	6.5	5.7	6.1	-	-	-	-	-	-	128	C37.4	16	-	-	-	-	-	-	21	21	02	21	-	-	-	-	01	-	01						
VI	-	-	-	-	-	-	-	-	-	-	173	C33.2	08	-	03	13	-	-	-	-	13	13	06	13	-	-	-	-	02	-	02					
VII	3.0	3.0	2.4	2.8	-	-	-	-	-	-	072	C35.4	01	-	03	17	10	-	-	01	16	C3	08	06	02	08	-	-	01	02	-					
VIII	2.1	3.7	2.6	2.8	-	-	-	-	-	-	044	C18.0	13	-	03	24	12	-	-	14	C2	07	07	01	07	-	-	01	02	-						
IX	3.3	4.5	2.9	3.6	-	-	-	-	-	-	034	C17.5	27	-	03	14	01	-	-	11	C1	07	06	01	07	06	-	-	01	01	-					
X	5.5	5.4	4.1	5.0	-	-	-	-	-	-	079	C23.8	25	-	03	-	-	-	-	04	C8	14	13	03	14	-	-	01	01	-						
XI	5.6	5.0	5.0	5.5	-	-	-	-	-	-	056	C17.2	27	-	03	10	-	-	-	05	C6	07	01	03	06	01	-	-	06	02	-					
XII	5.3	4.4	4.6	6.3	-	-	-	-	-	-	087	C22.2	15	-	03	23	-	-	-	07	13	15	13	02	08	11	02	-	-	04	19	-				
GOD.	-	-	-	-	-	-	-	-	-	-	874	C37.4	01M	-	-	-	-	01	-	-	135	115	27	121	24	05	-	-	05	-	15	34				
<b>V L A S I N A</b>																																				
<b>BR. ST.234</b>																																				
I	7.8	7.5	7.3	7.6	001.2	-	-	-	-	-	063	C15.0	20	09	16	31	-	-	-	03	18	19	11	01	04	17	03	-	-	11	31					
II	6.2	6.4	5.1	5.9	003.0	7.3	97	91	87	36	044	C23.5	08	04	05	26	-	-	-	02	C7	C5	07	04	02	07	01	-	-	04	28					
III	6.7	5.8	5.7	6.1	146.4	0.1	91	73	86	30	021	G06.5	07	02	07	24	-	-	-	05	14	10	06	02	C9	01	-	-	07	21						
IV	6.7	7.0	4.9	6.2	151.0	0.4	3	84	55	81	75	30	075	C16.4	15	-	03	21	-	-	01	01	07	15	10</td											

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
		Tm			Sred. (Diss)	Max	Min	Dat.	Min	Dat.		N	NE	E	SE	S	SW	W	NW	C									
		7	14	21							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
<b>SR CRNA GORA</b>																													
$\varphi = 43^{\circ}00'N \lambda = 18^{\circ}44'E$ Gr. $\Delta G = +1h\ 15\ min.$																													
I	-	-00.7	04.4	00.7	01.3	04.8	-02.1	09.6	22	-06.8	15	04	04.5	15	03.3	08	03.5	23	01.8	08	01.9	11	01.5	04	01.8	06	01.8	14	
II	-	00.3	04.9	01.1	01.8	05.7	-00.7	11.4	16	-05.6	28	01	02.0	19	05.1	02	03.0	25	01.9	15	02.6	11	02.2	02	02.5	03	02.2	07	
III	-	02.5	10.2	03.9	05.2	10.5	01.9	11.2	22	-04.4	12	02	01.0	13	03.1	01	03.0	33	01.9	04	01.6	18	01.8	*	04	01.2	14		
IV	-	04.7	09.1	05.2	06.0	09.7	04.0	19.0	30	-01.6	18	*	*	23	02.4	01	01.0	28	02.0	08	01.9	18	01.7	01	02.0	05	01.6	06	
V	-	08.9	13.5	09.2	10.2	14.4	08.0	21.0	27	03.6	15	04	02.0	20	02.2	01	02.0	15	01.9	03	02.0	16	02.8	03	03.3	21	01.6	10	
VI	-	12.8	17.6	13.3	14.3	11.8	26.0	05	06.4	12	02	13	01.9	08	01.6	14	01.9	08	01.5	14	01.9	*	*	16	02.1	15			
VII	-	15.4	22.3	16.8	17.8	23.4	19.9	30.4	17.16	09.0	20	07	02	04.0	24	03.1	01	01.0	22	01.5	01	01.0	06	01.5	*	08	01.2	29	
VIII	-	16.1	23.8	19.0	19.5	25.5	14.9	30.6	05	10.4	31	01	02.0	21	03.0	02	04.5	16	01.6	03	02.3	08	01.5	04	01.8	04	01.7	34	
IX	-	12.5	19.1	10.0	15.4	20.2	-	27.4	04	*	*	*	*	09	04.3	C1	03.0	25	03.3	*	*	27	03.2	*	*	*	*	26	
X	-	05.5	09.8	07.5	07.6	11.2	-	15.0	24.12	-	*	*	*	*	*	*	*	36	03.3	*	*	46	03.9	*	*	*	*	11	
XI	-	01.6	07.6	05.5	05.1	09.0	-	16.4	12	-	*	01	03.0	05	04.0	*	*	29	02.9	*	*	37	03.3	*	*	01	02.0	17	
XII	-	-01.8	03.4	01.2	01.0	05.3	-	12.4	30	-	*	*	*	05	06.4	*	*	38	03.7	*	*	27	03.6	*	*	*	*	23	
GOD.	-	06.5	12.1	08.2	06.8	13.2	-	30.6	-	*	17	02.6	167	03.2	25	02.5	304	02.5	54	02.0	239	02.8	14	02.2	AB	C1.7	207		
<b>KRSTAC</b>																										BR. ST. 236			
$\varphi = 43^{\circ}09'N \lambda = 19^{\circ}08'E$ Gr. $\Delta G = +1h\ 17\ min.$																										FABLJAK			
																										BR. ST. 237			
I	+46.4	-04.5	01.1	-03.2	-02.5	01.7	-07.8	06.2	22	-14.8	14	04	03.5	03	02.0	02	02.0	09	02.1	*	*	*	01	02.0	12	02.1	67		
II	634.8	-03.7	01.1	-02.2	-01.7	02.6	-06.2	08.8	12	-13.5	09	05	01.8	01	02.0	C1	02.0	09	02.2	11	02.7	03	02.0	*	*	53			
III	637.8	-01.9	05.6	00.2	01.1	06.6	-04.2	15.0	22.1	-11.5	13	*	*	02	02.0	05	01.2	07	02.1	12	02.5	04	02.0	*	01	02.0	62		
IV	635.4	00.8	04.6	00.6	01.7	06.3	-02.5	15.4	30	-08.0	20	06	C1.8	05	01.6	01	01.0	09	02.0	04	03.8	01	02.0	*	06	02.2	59		
V	637.3	05.9	09.3	05.5	06.5	11.7	01.2	18.6	31	-02.5	17	09	02.3	03	02.0	C1	01.0	05	02.4	13	02.0	09	02.9	03	02.3	04	02.0	46	
VI	639.0	10.1	13.9	09.8	10.9	15.5	05.5	21.4	05	-01.5	14	08	01.9	01	02.0	C2	01.5	04	04.0	17	02.5	08	02.0	01	04.0	08	02.5	41	
VII	641.9	12.7	17.8	12.3	13.8	19.5	07.6	21.0	17	02.2	08.0	07	07	02.0	*	*	09	01.2	06	02.7	05	01.6	05	02.0	01	07.0	14	02.1	66
VIII	643.1	12.9	19.9	12.8	14.6	21.6	08.6	27.5	04	03.5	14.12	04	02.0	04	02.0	07	01.6	06	02.3	*	03	02.0	02	02.0	08	02.0	59		
IX	642.0	08.9	15.5	09.9	11.1	16.8	06.9	24.0	06	-01.0	28	05	02.7	*	*	06	01.3	05	02.2	18	02.6	06	03.0	*	*	02	02.5	48	
X	636.2	02.4	08.3	02.7	03.5	08.1	00.5	13.5	10	-05.7	31	03	C1.7	*	*	*	*	02	02.5	34	03.0	07	03.6	02	01.0	*	45		
XI	639.6	-02.0	03.8	-01.3	-00.2	05.2	-03.9	10.7	18.16	-06.6	30	04	01.2	*	*	*	*	03	02.0	25	02.8	*	*	01	01.0	02	01.5	56	
XII	640.1	-04.0	01.1	-03.3	-02.4	02.3	-03.3	10.2	29	-14.0	19	14	02.3	*	*	*	05	02.4	02	02.0	01	02.0	09	01.7	09	02.2	53		
GOD.	-	05.3	14.1	07.9	08.8	15.5	04.1	33.0	05.0	04.0	25.0	01	02.0	80	01.7	15	01.3	142	01.3	36	01.3	362	01.5	12	01.2	54	01.5	384	
<b>RIJELO POLJE</b>																										BR. ST. 231			
$\varphi = 43^{\circ}02'N \lambda = 19^{\circ}45'E$ Gr. $\Delta G = +1h\ 19\ min.$																													
I	-	-02.0	03.8	00.2	00.6	05.0	-02.4	09.6	03	-08.2	14	*	*	06	01.2	C1	01.0	12	01.0	*	*	15	01.0	*	*	01	01.0	58	
II	-	-00.2	01.1	02.5	03.3	10.4	-00.9	15.6	17	-06.9	01	*	*	13	01.9	C2	01.0	13	01.0	*	*	15	01.5	03	01.3	05	01.2	33	
III	-	00.8	13.0	05.7	06.3	14.3	05.0	22.8	22	-06.2	01	01	02.0	06	02.5	01	02.0	14	01.4	01	03.0	39	01.4	01	01.0	06	01.5	24	
IV	-	03.6	12.3	06.6	07.3	13.6	02.4	22.3	30	-02.4	21	*	*	10	01.8	C1	01.0	17	01.2	01	01.0	34	01.7	*	*	06	01.7	21	
V	-	07.9	16.9	10.8	11.6	18.3	06.0	25.3	31	00.9	11	*	*	04	01.8	02	02.0	14	01.9	03	01.3	44	01.5	*	*	07	01.1	19	
VI	-	12.4	20.9	14.6	15.6	22.5	10.0	27.4	05	02.9	14	*	*	05	02.0	02	02.0	08	01.2	05	01.6	45	01.7	02	02.0	03	01.3	22	
VII	-	13.0	24.2	19.5	25.7	17.1	10.8	33.0	17	04.5	09	*	*	08	01.9	01	01.0	13	01.5	05	01.2	24	01.6	01	01.0	05	02.2	32	
VIII	-	13.2	26.9	16.3	18.1	26.1	11.7	33.0	05.04	05.9	14	*	*	01	02.0	02	02.0	07	01.3	05	01.2	35	02.0	*	*	02	01.0	36	



Mjesec	Vardušni pritisak Pn, cm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																				
		Tm				Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C											
		7	14	21	Spred. (Dies)						8.	1.	8.	1.	8.	1.	8.	1.	8.											
$\phi = 42^{\circ}49'N \lambda = 12^{\circ}41'E$ Gr. $\Delta G = +1h\ 15\ min.$																														
I	-	-00.9	06.9	06.8	01.9	07.8	-03.0	12.0	22.12	-06.2	15	02	03.0	02	02.0	*	*	02	01.0	05	01.2	03	01.3	06	02.3	04	02.5	09		
II	-	01.2	07.3	02.3	03.3	08.8	-00.8	14.5	16	-07.0	09	01	02.0	05	02.5	11	02.5	10	01.9	05	02.0	02	02.0	01	01.0	02	01.5	06		
III	-	01.7	11.9	03.3	05.0	13.1	-01.2	22.5	21	-06.2	10	02	04.5	03	02.3	10	03.3	09	02.0	06	02.5	*	*	*	*	02	02.5	04	02.5	01
IV	-	06.1	11.9	05.8	07.2	13.0	01.4	20.0	30	-03.2	24	*	*	03	01.3	15	02.0	12	02.2	04	02.5	*	*	*	*	01	01.0	02	01.5	05
V	-	11.0	15.6	09.4	11.3	17.3	04.0	23.2	20	00.0	11	01	03.0	04	02.0	14	01.9	09	01.6	08	02.0	01	01.0	*	*	02	02.0	04		
VI	-	14.7	20.3	12.9	15.2	22.2	07.2	26.0	05	00.5	14	*	*	04	03.0	09	01.9	11	01.6	05	01.0	02	01.5	*	*	02	03.0	05		
VII	-	17.0	25.4	16.1	18.7	27.3	09.1	34.0	16	04.2	09	05	01.0	03	01.7	01	02.0	07	01.7	06	01.3	*	*	04	01.8	06	01.8	01		
VIII	-	18.2	27.1	17.7	20.2	29.7	10.2	35.5	04	05.8	14	01	01.0	*	*	05	01.6	04	01.5	09	01.3	*	*	05	01.6	02	01.5	07		
IX	-	13.7	21.8	13.7	15.7	23.4	08.1	26.0	14.10	-00.5	28	*	*	01	02.0	15	01.4	09	01.6	04	01.2	03	01.3	*	*	02	02.5	06		
X	-	05.9	11.9	07.2	08.1	13.6	02.2	18.5	05	-04.0	28	*	*	02	03.0	07	01.1	09	01.8	09	01.3	02	03.5	01	02.0	*	*	03		
XI	-	06.6	09.7	03.6	04.4	10.9	-01.0	17.4	17	-04.8	02	*	*	01	01.0	01	01.0	*	*	01	01.0	*	*	05	01.6	01	03.0	03		
XII	-	-01.7	06.9	00.1	01.3	07.9	-03.7	13.0	04	-05.8	24	12	03.0	04	07.5	03	02.0	02	01.9	03	01.0	01	01.0	02	02.0	04	02.0	04		
GOD.	-	07.3	14.7	07.7	09.4	16.2	02.7	35.5	07	-06.8	24	*	*	02.7	21	02.6	51	02.0	08	01.8	65	01.6	14	01.7	24	01.8	26	02.1	74	
$\phi = 42^{\circ}26'N \lambda = 18^{\circ}41'E$ Gr. $\Delta G = +1h\ 15\ min.$																														
I	765.3	04.8	11.8	05.7	07.0	13.1	01.6	17.4	20	-03.0	15	05	02.2	09	01.9	*	*	07	02.0	04	01.5	06	02.2	01	02.0	06	02.2	55		
II	751.7	07.3	13.2	08.3	09.3	14.8	04.5	18.8	18.16	-00.5	10	01	02.0	12	03.8	01	01.0	12	02.8	05	03.0	09	02.1	*	*	06	02.0	36		
III	760.6	06.8	15.5	09.7	10.2	16.4	04.1	22.0	21	00.4	13.10	*	*	03	02.0	*	*	13	02.3	03	02.7	21	02.2	*	*	04	02.0	49		
IV	756.9	11.1	15.6	12.0	12.7	17.5	07.4	24.9	30	02.8	24	02	03.0	08	02.5	03	02.3	10	01.9	08	02.5	10	02.5	03	02.8	05	02.8	41		
V	751.1	19.6	15.6	16.5	20.4	26.9	11.1	26.4	20	06.2	11	05	04.6	02	04.0	*	*	02	01.0	16	02.4	19	02.3	01	01.0	02	02.5	46		
VI	755.4	20.3	24.9	20.6	21.3	26.0	14.8	30.2	27	07.9	14	05	02.7	07	01.7	03	01.0	04	03.0	17	02.1	04	02.8	05	01.8	39				
VII	760.4	22.0	28.6	21.9	23.6	29.9	16.0	36.0	15	12.4	24	03	03.7	09	02.8	00	01.0	01	01.0	02	02.5	22	02.2	01	01.0	03	01.7	50		
VIII	759.8	23.6	30.3	22.4	24.6	31.5	17.8	35.7	31	03	13.6	01	02.1	05	02.4	*	*	*	01	02.0	24	02.1	01	02.0	11	02.0	48			
IX	760.5	18.2	25.7	18.5	20.2	27.0	14.8	32.6	11	06.6	28	*	*	04	03.2	05	01.4	05	01.8	03	01.1	22	02.2	02	02.9	02	03.0	42		
X	758.3	11.6	17.5	13.8	19.0	08.2	02.3	22.5	05	01.8	28	02	01.0	03	00.0	05	01.0	03	02.0	13	02.7	11	02.6	04	01.7	01	01.0	49		
XI	763.3	07.4	14.9	6.2	10.0	16.2	07.3	19.0	07	-	-	05	01.4	08	04.6	01	01.0	03	01.0	02	02.6	09	02.2	03	01.7	*	*	56		
XII	764.3	05.0	12.4	06.7	13.9	01.7	19.1	04	-	-	-	08	05.1	11	02.9	03	01.3	02	01.5	03	01.0	05	01.8	06	01.8	04	02.0	34		
GOD.	760.5	12.8	19.2	13.5	14.7	20.5	09.0	36.0	08	-	-	40	03.2	81	02.0	72	01.3	64	02.1	72	02.4	176	02.2	23	01.9	50	02.2	567		
$\phi = 42^{\circ}17'N \lambda = 18^{\circ}51'E$ Gr. $\Delta G = +1h\ 15\ min.$																														
I	766.5	06.8	12.9	07.9	08.9	13.3	04.0	17.5	21	01.7	14	*	*	04	02.4	*	*	*	20	01.6	*	*	*	*	*	*	*	*	64	
II	760.1	08.4	13.4	09.2	10.1	13.8	07.5	18.5	16	03.0	09	*	*	08	02.4	03	02.0	06	02.0	37	02.0	*	*	*	*	*	*	*	31	
III	762.1	08.6	15.0	09.7	10.8	15.2	05.0	20.0	30.25	03.5	10	*	*	01	02.0	01	02.0	07	02.3	37	02.3	*	*	*	*	*	*	56		
IV	758.2	12.2	15.8	11.9	13.0	16.5	10.6	21.5	30	07.5	23	*	*	01	02.0	04	02.2	13	02.4	28	02.0	*	*	*	*	*	*	44		
V	755.0	16.1	19.4	15.3	16.5	19.4	13.8	27.3	20	10.2	14	02	02.0	01	03.0	01	02.0	07	03.4	27	02.5	07	01.4	01	02.0	02	02.5	47		
VI	760.0	21.6	24.9	19.5	21.1	25.4	16.1	29.6	30	12.5	15	01	05.0	*	*	*	*	31	02.0	04	02.5	*	*	*	*	07	02.0	39		
VII	760.8	23.3	28.4	21.7	23.8	29.3	19.0	33.6	17	16.0	25.09	*	*	09	02.0	01	02.0	06	26.17	03	01.7	06	02.5	*	*	54				
VIII	760.3	24.0	30.3	23.1	25.1	31.0	20.3	35.0	21	18.2	31.14	*	*	01	02.0	02	02.5	02	01.0	24	01.9	03	02.0	03	02.3	01	03.0	57		
IX	761.1	26.3	25.9	20.0	21.6	26.6	17.6	32.0	11	12.0	28.27	*	*	*	*	*	*	04	02.8	33	02.2	06	03.3	01	03.5	*	*	45		
X	758.6	13.4	17.8	13.6	14.7	18.9	11.5	23.6	05	06.0	28	*	*	02	02.0	*	*	03	02.3	53	02.8	04	02.5	*	*	31				
XI	762.3	09.7	15.4	10.6	11.4	16.1	09.1	20.4	08	04.0	02	*	*	02	04.6	01	02.0	03	02.1	02	02.0	*	*	*	*	46				
XII	764.5	07.1	12.9	08.4	09.2	13.2	06.4	17.4	04	03.7	22	11	05.1	*	*	01	02.0	01	05.0	29	01.9	*	*	*	*	51				
GOD.	761.3	14.2	19.3	-14.2	15.5	19.9	12.2	35.0	07	01.7	41	14	04.6	20	07.															

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha em mm	Padavine R mm	Broj dana u mjesecu:																																
	7	14	21			Sred. (Dnev.)	Inkolacija broj sati	Tn	Tx	Tn	Tx	Tn	Tx	Tn	F (0-12)	Nm (0-10)	R mm	≤	<	<	≥	>	>	≥	≤	≥	●	★	▲	△	▲	■	■					
								mm	7	14	21	Sred. Min.	Max.	Dat.	mm	6	8	2.0	8.0	0.1	1.10.0	6	8	2.0	8.0	0.1	1.10.0	6	8	2.0	8.0	0.1	1.10.0	6	8	2.0	8.0	0.1
GRADOVAC																																						
BR. ST.241																																						
I 4.5 5.3 3.3 4.4	-	04.9 88 86 90 86 40	154 059.6	02	*	*	24	*	*	*	*	*	*	*	11	06	06	06	04	06	01	01	*	*	*	*	*	*	*	*	02	*						
II 7.1 6.1 4.9 6.1	-	05.3 90 82 93 88 64	526 139.2	04	*	*	12	*	*	*	01	*	03	08	13	12	08	13	03	03	*	*	*	*	*	*	*	*	*	04	*							
III 4.8 4.8 3.2 4.3	-	05.9 85 74 90 83 14	268 108.4	06	*	*	20	*	*	*	03	*	15	09	07	07	05	07	05	*	*	*	*	*	*	*	*	*	05	*								
IV 5.6 7.5 5.2 6.1	-	04.7 87 77 91 85 52	192 052.6	18	*	*	06	*	*	*	*	*	*	03	11	16	14	03	16	*	*	*	*	*	*	*	*	*	*	*	*							
V 4.9 6.3 4.2 5.1	-	08.6 83 75 87 82 49	206 069.2	05	*	*	*	*	*	*	*	*	*	07	09	12	09	05	12	*	*	*	*	*	*	*	*	*	*	01	*							
VI 4.6 5.5 3.2 4.4	-	10.3 76 70 79 75 47	071 038.2	12	*	*	05	*	*	*	*	*	*	04	03	08	07	02	08	*	*	*	*	*	*	*	*	*	*	*	*							
VII 2.0 3.0 1.2 2.0	-	12.9 81 65 80 75 39	011 011.0	08	*	*	24	10	*	*	*	*	*	20	01	02	01	01	01	*	*	*	*	*	*	*	*	*	*	*	*							
VIII 1.5 3.7 1.1 2.1	-	12.5 71 53 77 67 31	053 023.6	30	*	*	26	17	*	*	*	*	*	20	05	04	02	01	01	*	*	*	*	*	*	*	*	*	*	*	*							
IX 3.9 4.6 2.9 3.8	-	10.5 82 62 83 76 28	399 084.6	72	*	*	01	16	*	*	*	*	*	11	04	09	09	07	05	*	*	*	*	*	*	*	*	*	*	*	*							
X 6.5 6.5 5.4 6.2	-	07.2 51 77 88 85 45	933 127.4	24	*	*	09	*	*	*	*	*	*	06	11	19	18	16	15	01	*	*	*	*	*	*	*	*	*	02	01							
XI 5.4 4.8 4.0 4.8	-	05.6 92 74 91 86 41	198 096.6	26	*	*	19	*	*	*	*	*	*	09	08	13	07	04	12	01	*	*	*	*	*	*	*	*	*	01	04							
XII 4.9 4.9 2.6 4.0	-	04.5 90 71 92 84 40	094 045.6	13	*	*	25	*	*	*	03	02	10	05	05	04	02	05	02	01	*	*	*	*	*	*	*	*	02	01								
GOD. 4.6 5.2 3.4 4.4	-	07.9 84 72 86 81 14	3107 139.2	0.0.0.	*	*	116	73	27	*	07	02	119	71	115	98	59	114	14	04	*	*	*	*	*	*	*	*	08	16								
TIVAT																																						
BR. ST.242																																						
I 5.1 5.0 3.0 4.3	-	05.9 85 63 84 77 29	056 013.6	18	*	*	10	*	*	*	*	*	*	10	06	10	09	02	10	*	*	*	*	*	*	*	*	*	07	*								
II 7.3 6.7 5.5 6.5	-	06.7 80 61 85 75 31	202 050.4	07	*	*	01	*	*	*	01	*	04	11	14	11	07	14	*	*	*	*	*	*	*	*	*	02	*									
III 4.9 5.3 3.3 4.5	-	07.7 91 62 93 82 44	148 049.4	06	*	*	*	*	*	*	*	*	06	07	09	08	04	05	*	*	*	*	*	*	*	*	*	02	02									
IV 6.0 7.0 6.3 6.4	-	08.4 81 64 86 77 34	138 028.2	17	*	*	*	*	*	*	*	*	01	01	01	11	16	13	*	*	*	*	*	*	*	*	*	02	07									
V 5.1 5.5 5.2 5.2	-	10.5 81 63 89 78 33	295 101.0	02	*	*	04	*	*	01	*	07	08	18	14	08	18	*	*	*	*	*	*	*	*	*	02	05										
VI 4.3 4.7 3.5 4.2	-	12.5 71 50 75 65 34	047 025.1	20	*	*	24	01	01	01	01	07	02	10	07	01	10	*	*	*	*	*	*	*	*	*	04	*										
VII 1.8 2.2 1.4 1.8	-	13.3 67 43 72 61 26	004 003.7	71	*	*	30	17	01	*	*	20	*	03	01	03	03	*	*	*	*	*	*	*	*	*	02	*										
VIII 1.9 2.7 1.3 2.0	-	14.0 66 42 73 60 24	028 026.2	24	*	*	31	20	03	*	*	21	01	04	02	01	04	*	*	*	*	*	*	*	*	*	07	*										
IX 3.8 4.1 2.5 3.6	-	13.9 86 57 89 77 26	447 165.7	23	*	*	22	05	*	01	01	11	02	09	09	07	09	*	*	*	*	*	*	*	*	*	11	*										
X 7.2 6.4 5.8 6.5	-	05.7 92 62 90 63 34	494 077.2	08	*	*	*	*	*	01	*	03	12	21	16	13	21	*	*	*	*	*	*	*	*	*	01	06										
XI 5.2 5.7 4.2 5.0	-	07.5 88 66 89 80 27	047 008.0	28	*	*	*	*	*	07	*	04	14	12	14	12	*	*	*	*	*	*	*	*	*	*	01	*										
XII 4.5 4.9 3.1 4.2	-	05.9 82 58 82 74 30	072 057.2	13	*	*	*	*	*	03	01	07	03	04	02	04	*	*	*	*	*	*	*	*	*	*	02	*										
GOD. 4.8 5.0 3.6 4.5	-	09.7 80 57 83 73 24	1978 165.7	23.9.0.	*	*	11	112	43	05	09	04	06	106	72	132	107	81	132	*	*	*	*	*	*	*	*	01	05	02								
BUCVA																																						
BR. ST.243																																						
I 5.4 6.1 3.5 5.0	-	129.1 06.8 82 68 83 78 34	049 009.6	18	*	*	*	*	*	*	*	*	*	10	07	13	06	13	*	*	*	*	*	*	*	*	*	*	01	*								
II 7.5 6.9 5.9 6.4	-	105.1 07.0 77 67 71 55 35	177 042.1	07	*	*	12	*	*	*	01	*	04	11	12	10	08	12	*	*	*	*	*	*	*	*	*	07										
III 5.4 5.3 3.7 4.5	-	106.6 06.1 83 73 85 80 45	116 044.1	06	*	*	*	*	*	*	*	*	10	09	08	08	03	08	*	*	*	*	*	*	*	*	*	04	01									
IV 6.4 7.5 5.6 6.5	-	135.0 06.3 73 73 68 73 36	188 045.7	17	*	*	*	*	*	*	*	*	02	11	15	12	06	15	*	*	*	*	*	*	*	*	*	02	03									
V 5.7 6.0 5.0 5.6	-	166.1 11.0 77 71 83 77 36	214 046.6	02	*	*	02	*	*	01	*	06	10	17	16	07	17	*	*	*	*	*	*	*	*	*	03	*										
VI 3.9 4.2 3.5 3.2	-	274.8 15.5 71 64 77 71 59	022 008.8	17	*	*	24	*	*	*	*	*	12	01	07	05	07	*	*	*	*	*	*	*	*	*	*	01	*									
VII 1.7 2.5 1.5 1.9	-	316.6 15.7 70 61 73 68 33	019 010.0	22	*	*	30	16	13	*	*	21	02	02	02	01	02	*	*	*	*	*	*	*	*	*	01	*										
VIII 3.1 2.8 2.0 2.7	-	284.6 16.0 67 57 71 65 28	011 006.0	24	*	*	31	20	24	*	*	18	01	04	02	04	04	*	*	*	*	*	*	*	*	*	02	*										
IX 5.0 5.1 2.6 4.3	-	218.3 15.5 82 71 82 78 33	434 187.9	23	*	*	21	05	01	*	*	09	05	09	06	07	09</																					

Mjesec	Vardulski Pratiski Pm. num.	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																									
		Tm				Max		Min		Max		Min		Dat.		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (dies)	Max	Min	Max	Min	Dat.	Min	Dat.	Min	Dat.	E.	J.	E.	J.																			
$\lambda = 42^{\circ}14'N \lambda = 19^{\circ}05'E$ Gr. $\Delta G = +1h\ 16\ min.$														VIRPAZAR												BR. ST.246											
I	-	02.2	09.2	04.2	04.9	00.2	14.0	04	-03.0	29	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*									
II	-	05.0	10.6	06.3	07.1	11.2	03.0	16.0	17	-01.0	28	03	01.0	27	02.6	*	*	*	*	10	02.2	C2	C1.0	30	01.6	06	01.0	*	*								
III	-	06.4	14.7	08.6	09.7	15.0	03.9	26.0	22	-00.5	01	*	*	21	01.1	*	*	03	01.7	02	C1.0	37	01.5	15	01.1	06	C1.3	09									
IV	-	09.0	15.5	11.2	11.7	15.9	05.5	19.0	28.27	02.0	20	*	*	08	02.0	02	01.0	03	01.3	03	C1.0	50	01.5	18	01.4	01	C1.0	05									
V	-	14.5	20.0	15.0	16.1	20.4	10.2	26.4	30.27	06.5	16	*	*	12	02.2	*	*	13	02.4	01	C1.0	49	01.8	07	01.3	04	C1.0	07									
VI	-	22.8	26.7	22.1	23.4	27.0	14.7	30.0	29	11.5	04	*	*	27	02.0	*	*	01	02.0	02	C1.0	39	02.3	14	01.0	03	C1.3	09									
VII	-	24.5	31.0	23.9	25.9	31.5	15.3	40.0	17.16	12.0	23	*	*	33	02.6	*	*	02	03.0	02	C1.0	28	01.4	13	01.1	*	*	15									
VIII	-	25.9	34.5	26.2	28.4	34.8	16.5	35.8	09	13.5	30	02	C1.0	37	01.8	*	*	01	02.0	07	C1.0	18	01.2	04	01.0	03	01.0	21									
IX	-	21.4	27.1	20.3	22.3	27.5	11.6	33.6	04	06.5	28	*	*	18	01.8	*	*	05	03.0	C5	C1.0	33	02.2	09	01.1	05	C1.6	15									
X	-	10.0	14.6	10.8	11.8	15.0	06.6	20.0	16	01.5	28	*	*	11	02.0	*	*	11	02.0	03	C2.3	46	02.8	05	01.0	11	C1.8	06									
XI	-	05.3	12.7	06.6	07.6	12.9	03.0	16.6	13	01.0	30	02	C1.0	19	02.0	01	01.0	01	01.8	C3	C1.0	30	01.8	14	01.0	05	G3.0	11									
XII	-	01.6	10.4	03.8	04.9	10.6	00.0	13.0	10.02	-02.5	24	01	C3.6	33	02.9	*	*	06	01.5	04	C1.0	21	01.3	08	01.0	06	C1.2	10									
GOD.	-	12.5	18.9	13.3	14.5	19.3	07.6	40.0	KRK-VII	-03.0	29	*	11	02.1	241	02.3	03	01.0	60	02.1	34	01.1	301	01.6	113	01.1	44	C1.6	114								
$\lambda = 42^{\circ}06'N \lambda = 19^{\circ}06'E$ Gr. $\Delta G = +1h\ 16\ min.$														RAR												BR. ST.247											
I	756.3	C7.4	12.3	07.7	08.8	13.2	03.9	16.9	01	-01.3	15	08	02.4	49	02.4	16	01.4	04	01.8	06	02.0	06	01.8	08	01.9	05	C2.4	01									
II	756.6	09.1	13.9	09.9	10.7	14.9	06.1	20.2	18	01.2	10	04	C5.2	38	01.6	12	C2.0	11	03.5	05	02.0	06	02.4	05	02.2	03	C3.0	*									
III	766.9	08.9	14.8	09.9	10.9	15.8	05.8	20.2	29	01.2	02	03	C7.0	42	02.0	19	01.7	*	03	02.7	07	01.9	16	01.1	03	01.7	*										
IV	757.2	12.9	15.9	12.4	13.4	17.7	08.7	26.2	30	04.0	21	11	C6.6	37	02.2	15	01.7	07	02.6	03	02.7	04	02.0	15	0.5	01	C4.0	02									
V	756.7	16.1	18.8	15.1	16.3	19.8	11.5	25.8	20	07.9	11	07	C2.1	36	01.7	68	01.5	05	03.4	10	02.7	10	02.1	14	02.4	*	*	03									
VI	756.9	20.6	23.5	19.3	20.7	24.7	15.2	29.6	27	09.1	14	05	C3.2	28	02.0	13	01.5	07	01.6	06	03.0	10	02.0	14	0.9	05	C2.6	02									
VII	766.0	22.8	26.2	21.0	22.0	27.4	16.6	34.7	18	12.4	10	*	*	28	01.7	26	01.5	02	01.5	03	02.3	C9	01.8	16	0.1	05	C2.0	04									
VIII	759.5	24.3	27.4	22.5	24.2	29.1	18.6	32.3	23	15.3	31	03	04.0	28	02.2	22	07.0	C2	01.0	03	01.7	08	02.1	21	02.3	05	01.6	01									
IX	766.1	20.8	24.7	20.0	21.1	26.1	16.0	31.4	11	10.2	27	03	03.0	26	02.3	23	01.7	06	02.3	06	03.0	05	01.8	16	0.7	05	C2.8	*									
X	756.1	13.9	16.3	14.6	15.4	19.4	10.4	23.7	12	03.2	28	02	01.5	19	02.6	23	01.8	04	02.2	16	03.6	13	04.0	15	02.9	01	C4.0	*									
XI	762.8	05.8	15.1	11.0	11.7	16.2	06.9	19.8	06	03.8	30	04	01.8	36	02.6	22	01.5	03	03.0	10	03.8	04	01.8	09	01.9	01	C3.0	01									
XII	763.7	07.1	12.3	08.1	08.9	13.2	03.8	17.8	04	01.1	23,21	05	C3.0	30	03.8	27	02.1	03	02.0	07	02.9	08	01.5	08	01.6	03	02.3	02									
GOD.	766.4	14.5	18.6	14.3	15.4	19.8	10.3	34.7	48	07	-01.3	51	55	C2.7	382	02.4	226	01.8	54	02.5	78	02.9	90	02.2	157	02.5	37	C2.5	16								
$\lambda = 42^{\circ}26'N \lambda = 19^{\circ}17'E$ Gr. $\Delta G = +1h\ 17\ min.$														TITCGRAD												BR. ST.248											
I	762.0	C3.9	10.8	05.6	06.5	11.4	02.8	15.0	04	-02.1	15	03	02.3	16	03.9	C3	04.0	*	*	11	01.9	06	01.8	01	C1.0	*	*	53									
II	755.6	06.6	12.6	08.0	08.8	13.0	05.4	19.4	16	-01.4	21	07	C2.1	19	04.7	C4	C1.2	02	02.0	11	03.2	06	02.3	03	02.7	*	*	C2.0	31								
III	757.3	07.6	16.6	10.6	11.4	17.3	06.4	26.0	22	01.1	02	04	C2.0	11	04.0	C2	C1.5	*	*	13	02.5	14	02.7	*	*	01	C3.0	48									
IV	752.6	11.0	16.4	12.2	12.9	18.2	09.0	24.1	30	05.3	23	11	C3.0	27	03.1	C1	05.0	03	02.3	12	03.2	05	03.4	04	02.5	*	*	27									
V	754.8	15.0	20.1	15.6	16.6	21.6	12.1	28.2	20	05.3	11	13	03.2	08	02.9	02	02.5	04	04.0	14	04.5	09	03.2	01	02.0	03	C2.0	39									
VI	754.9	19.9	25.6	20.5	21.7	27.0	16.5	31.6	27	05.5	12	11	04.5	18	03.4	C2	02.5	03	02.7	17	03.8	12	03.2	02	01.5	03	C1.3	27									
VII	755.9	23.2	31.1	24.7	25.9	32.4	19.9	38.9	16	15.0	24	23	03.1	22	03.4	C1	03.0	01	03.0	15	03.6	09	03.1	02	02.0	01	C2.0	19									
VIII	755.5	24.9	32.9	26.2	27.5	33.9	22.6	36.6	05	17.0	13,13	27	03.3	01	03.6	18	03.6	01	07.0	27	03.6	01	03.6	02	03.0	*	*	24									
IX	756.4	15.5	26.7	21.0	22.0	28.2	17.8	35.6	14	07.5	27	14	03.4	07	03.1	C1	04.0	17	03.6	07	03.7	*															

Mesec	Oblačnost Nm (0-10)			Temperatura hod. (t) (°C)	Vlažnost vazduha U m t	Padavine R mm		Broj dana na sat:																									
	7	14	21			mm	7	14	21	28	Min	Σ	Max	Cat.	Tn	Tx	In	Tx	Tx	Tn	F (0-12)	Nm (0-10)	R mm	•	*	♦	Δ	▲	■	□			
	≤	<	=	≥	≥	IV	V	VI	VI	VI	V	IV	III	II	I	II	III	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV						
<b>BR. ST.246 VIRPAZAR</b>																																	
I 5.0 5.5 5.4 4.4 5.4 -	-	04.9	89	57	79	75	22	101	025.6	06	.	.	16	.	.	.	10	09	11	11	06	04	11	.	.	.	.	.	07				
II 7.0 7.4 7.4 5.8 6.9 -	-	05.9	87	63	82	78	38	271	125.0	07	.	.	01	.	.	.	01	04	15	08	06	08	.	.	.	.	.	01	.	02			
III 5.5 5.6 5.4 4.2 5.1 -	-	06.4	86	52	76	71	24	110	028.6	05	.	.	01	01	.	.	14	11	07	07	05	07	.	.	.	.	.	02	.	.			
IV 7.0 7.2 7.2 7.1 7.1 -	-	08.1	66	61	81	78	26	204	055.4	18	.	.	.	.	.	.	01	03	14	13	12	06	13	.	.	.	.	.	02	.	.		
V 6.2 6.6 5.8 6.2 -	-	11.5	86	72	85	81	50	407	096.4	02	.	.	01	.	.	.	02	02	03	14	17	17	11	17	.	.	.	.	.	01	.	.	
VI 3.0 4.0 4.2 2.4 3.2 -	-	17.3	75	74	82	77	37	039	014.0	11	.	.	26	01	.	.	02	03	13	01	06	06	02	06	.	.	.	.	.	01	.	.	
VII 1.3 2.4 1.4 1.1 1.6 -	-	17.6	72	58	80	70	32	019	010.0	19	.	.	29	21	03	01	21	03	02	01	02	01	02	.	.	.	.	.	01	.	.		
VIII 1.1 1.7 0.9 1.2 1.2 -	-	18.3	71	48	71	63	29	035	025.6	29	.	.	31	27	.	.	25	01	03	03	01	03	.	.	.	.	.	01	.	.			
IX 4.2 4.3 3.4 4.0 C -	-	15.7	77	62	82	73	48	546	130.6	26	.	.	20	15	.	.	03	01	15	06	08	08	08	08	.	.	.	.	.	01	.	.	
X 8.6 8.6 8.6 8.6 -	-	08.6	85	71	87	81	51	746	118.4	08	.	.	01	.	.	.	04	02	07	20	23	23	17	23	.	.	.	.	.	01	.	.	
XI 4.5 5.8 3.9 4.8 -	-	05.9	88	50	85	74	31	155	070.4	26	.	.	01	.	.	.	02	01	06	05	07	07	02	07	.	.	.	.	.	01	.	11	
XII 5.3 4.9 3.8 4.7 -	-	04.2	86	39	76	67	23	069	025.6	13	.	.	14	.	.	.	02	02	09	08	07	07	03	07	.	.	.	.	.	01	01	.	
GOD. 5.0 5.4 4.2 4.9 -	-	10.4	82	55	80	74	22	2724	130.6	26	X	.	.	32	115	64	03	19	12	123	104	113	111	66	113	.	.	.	.	01	06	.	21
<b>BR. ST.247 BAR</b>																																	
I 5.6 6.0 3.6 5.1 -	142.2	05.5	70	60	76	69	37	052	017.6	18	.	.	01	.	.	.	01	07	07	11	10	01	11	.	.	.	.	.	04	.	.		
II 7.2 6.5 5.2 6.4 -	127.3	06.0	70	66	73	67	33	125	037.5	07	.	.	01	.	.	.	04	06	11	12	10	05	12	.	.	.	.	.	05	.	.		
III 5.1 5.5 4.2 5.3 -	195.6	07.4	77	65	78	74	45	057	020.5	06	.	.	01	.	.	.	06	05	03	05	03	08	.	.	.	.	.	02	01	.			
IV 6.6 6.7 7.2 6.9 -	163.5	08.0	67	64	74	68	23	124	021.7	19	.	.	01	.	.	.	04	02	14	13	11	05	13	.	.	.	.	.	01	06	.		
V 5.8 5.5 5.1 5.8 -	223.9	10.8	74	82	76	44	270	066.2	02	.	.	01	.	.	.	02	06	12	16	15	04	16	.	.	.	.	.	04	.	.			
VI 4.3 3.2 2.5 3.5 -	327.5	12.5	68	62	70	66	28	026	009.6	13	.	.	14	01	.	.	02	01	16	02	07	03	06	.	.	.	.	.	04	.	.		
VII 1.9 2.0 1.2 1.7 -	375.9	14.1	60	64	70	65	30	009	006.4	20	.	.	25	03	01	04	03	21	02	02	02	02	02	.	.	.	.	.	01	.	.		
VIII 2.1 2.4 1.7 2.1 -	330.7	14.4	57	62	66	72	30	016	014.0	29	.	.	30	13	04	01	20	03	02	01	03	03	.	.	.	.	.	05	.	.			
IX 4.7 4.1 3.6 3.9 -	237.2	14.1	72	68	76	72	31	275	064.5	24	.	.	21	01	01	01	10	06	10	04	09	09	08	09	.	.	.	.	.	06	.	.	
X 7.2 6.6 5.9 6.4 -	157.3	09.7	76	62	76	72	39	342	087.5	16	.	.	01	.	.	.	16	05	04	11	21	17	07	21	.	.	.	.	.	03	13	.	
XI 4.7 5.6 4.3 4.9 -	141.3	07.6	71	73	73	73	36	070	016.6	30	.	.	06	.	.	.	06	07	08	14	09	03	14	.	.	.	.	.	05	.	.		
XII 4.6 5.3 3.6 4.5 -	149.5	05.8	70	59	69	66	33	056	024.6	13	.	.	01	.	.	.	08	05	07	05	04	07	01	08	.	.	.	.	.	01	02	01	
GOD. 5.1 5.5 4.3 5.0 -	2558.6	06.5	72	50	70	64	15	1681	097.0	16	X	.	.	12	114	64	55	171	46	84	131	107	51	130	.	.	.	.	01	46	04	.	
<b>BR. ST.248 KOLASIN</b>																																	
I 5.2 5.5 3.5 4.7 -	154.2	05.5	83	61	81	75	36	047	017.4	11	.	.	05	.	.	.	10	09	06	01	11	.	.	.	.	.	03	.	.				
II 7.0 6.5 5.9 6.5 -	126.9	06.0	76	57	77	70	31	152	052.6	07	.	.	01	.	.	.	14	04	06	12	11	04	11	.	.	.	.	.	01	.	.		
III 5.5 5.2 4.1 4.9 -	107.0	06.9	81	51	75	69	28	039	024.3	06	.	.	02	.	.	.	05	09	08	06	06	02	06	.	.	.	.	.	03	06	.		
IV 6.4 7.4 5.9 6.6 -	159.3	07.5	73	56	73	67	31	151	040.0	17	.	.	01	.	.	.	16	02	02	12	16	11	06	16	.	.	.	.	.	02	02	.	
V 5.7 6.5 6.1 6.1 -	219.1	09.7	74	58	75	69	32	188	033.0	02	.	.	08	01	.	.	13	01	04	11	19	17	07	19	.	.	.	.	.	07	01	.	
VI 4.7 5.5 3.4 4.5 -	279.7	11.8	68	48	65	61	33	044	010.7	12	.	.	24	02	04	04	16	02	04	04	11	09	01	11	.	.	.	.	.	04	.	.	
VII 2.3 2.3 2.4 2.5 -	368.7	12.0	54	36	53	48	25	011	006.4	08	.	.	01	.	.	.	25	02	22	14	16	07	15	02	04	.	.	.	.	.	01	.	.
VIII 2.5 4.0 3.4 3.0 -	335.6	11.7	49	31	50	43	15	016	007.2	29	.	.	31	26	24	21	21	06	12	01	04	03	04	.	.	.	.	.	05	.	.		
IX 4.2 4.2 3.1 3.8 -	247.9	12.0	69	47	68	62	29	249	061.6	26	.	.	20	14	13	21	04	11	04	08	08	07	09	.	.	.	.	.	02	.	.		
X 7.2 7.1 6.3 6.8 -	157.1	08.3	79	56	80	71	29	533	097.0	16	.	.	01	.	.	.	16	06	02	13	20	18	15	70	.	.	.	.	.	01	12	.	
XI 4.8 5.5 5.0 5.6 -	150.4	06.5	62	55	81	73	30	157	062.3	26	.	.	16	02	04	04	01	11	05	10	06	01	10	.	.	.	.	.	03	12	.		
XII 4.9 5.1 4.1 4.7 -	153.9	04.0	76	48	70	65	30	075	024.2	13	.	.	07	.	.	.	14	08	05	04	08	06	03	07	.	.	.	.	.	02	02	.	
GOD. 5.1 5.5 4.3 5.0 -	2558.6	06.5	72	50	70																												

Mesec	Vazdušni pritisak pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Br. (1-12)																	
		Tm			Sred. (Dnes)	Max	Min	Dat.	Max	Min	Dat.	U	NE	E	SE	S	SW	N	NW	C									
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.								
$\varphi = 41^{\circ}55'N \lambda = 19^{\circ}13'E$ Gr. AG = + 1h 17 min.																													
I	756.9	06.1	10.7	07.6	08.0	11.5	04.8	15.6	21	06.9	14	.	.	12	02.4	72	02.5	02	01.5	.	.	03	01.7	02	C1.5	02			
II	750.6	07.7	12.5	09.2	09.7	13.4	06.3	18.6	16	02.2	28	.	.	19	02.5	46	07.5	05	02.8	06	02.1	03	02.7	02	C3.5	01			
III	752.7	09.3	15.4	10.8	11.6	16.0	07.8	23.2	25	02.4	09	.	.	71	02.5	37	02.4	05	02.6	02	02.5	02	C2.0	09	02.7	08	C2.4	09	
IV	749.4	11.6	15.8	12.0	12.9	17.0	09.2	24.6	30	05.6	20	01	03.0	17	02.2	33	02.2	04	02.0	05	01.8	06	02.3	12	02.8	09	C2.6	03	
V	750.7	15.1	19.0	15.2	16.2	19.9	12.1	24.4	21.20	06.8	01	01	02.0	12	02.2	20	01.8	01	02.0	09	03.4	02	02.0	18	03.1	17	C2.8	04	
VI	750.9	12.6	24.3	19.3	20.6	25.3	16.3	26.8	27	16.0	01	02.0	16	01.8	24	02.0	05	01.8	03	02.0	05	03.4	09	02.6	23	03.1	03		
VII	751.8	22.6	26.7	22.6	24.1	30.1	17.8	36.6	17	14.6	22.08	01	02.0	19	02.0	29	01.9	01	02.0	02	01.5	02	01.0	07	02.9	28	C3.3	04	
VIII	751.5	24.2	31.1	24.3	26.0	32.1	20.7	37.3	04	16.4	29.28	.	.	10	02.2	26	02.0	03	01.3	01	02.0	02	02.5	13	02.8	22	03.1	06	
IX	752.1	20.4	25.8	21.4	22.2	27.1	17.6	31.4	16	11.2	27	.	.	25	02.1	27	02.0	03	02.0	06	03.5	06	03.0	12	02.4	09	C3.6	02	
X	749.7	13.1	16.0	14.8	15.2	19.1	10.9	23.2	05	04.9	28	01	01.0	17	02.1	23	02.1	03	02.3	10	04.2	03	05.0	19	04.1	13	C2.8	04	
XI	754.4	05.4	14.4	11.7	15.5	15.7	07.5	18.4	15	04.3	02	.	.	20	02.3	48	02.2	01	02.0	08	02.6	02	03.5	05	03.4	06	02.7	.	
XII	755.2	06.2	11.4	08.0	08.4	12.4	04.5	17.3	04	01.9	25.21	01	02.0	26	02.3	51	02.3	02	01.0	06	02.8	02	02.0	01	02.0	04	02.5	.	
GOD.	752.2	13.8	16.9	14.7	15.6	20.0	11.4	37.3	08	06.9	41.1	08	01.8	224	02.2	436	02.3	35	02.1	58	03.0	34	02.7	111	03.0	143	C3.0	34	
SR MAKEDONIJA																													
$\varphi = 42^{\circ}01'N \lambda = 20^{\circ}53'E$ Gr. AG = + 1h 24 min.																													
I	-	-04.4	-02.0	-04.6	-03.9	00.4	-07.0	06.6	23	-12.0	13	03	03.7	01	01.0	.	.	02	02.0	02	02.0	05	01.8	01	04.0	38	C3.2	41	
II	-	-03.2	-01.1	-03.1	-02.6	01.0	-05.1	06.5	11	-12.6	28	.	.	.	.	.	.	01	03.0	11	02.7	11	04.2	.	.	19	C2.6	42	
III	-	-01.2	01.8	-00.3	00.0	03.4	-02.9	11.5	27	-13.0	01	01	02.0	.	.	06	01.0	07	02.1	11	04.2	03	02.0	10	C1.7	55			
IV	-	-30.3	01.8	-00.2	00.5	03.6	-02.5	08.8	20	-06.9	20	02	02.5	01	02.0	02	01.5	11	02.2	08	02.2	06	02.2	05	03.4	18	02.7	37	
V	-	04.8	06.8	05.1	05.4	06.6	02.0	15.2	31	-02.0	10	03	02.7	.	.	02	02.0	13	01.9	06	02.8	05	02.6	04	04.5	27	C2.5	34	
VI	-	04.9	11.8	09.6	10.2	13.5	06.4	19.8	27	-00.2	13	.	03	01.3	03	01.0	12	01.9	03	03.3	01	01.0	05	04.4	26	C3.2	36		
VII	-	13.3	14.9	12.2	13.2	16.4	09.1	24.5	17	01.6	08	04	02.8	01	04.0	.	.	13	01.5	02	02.0	05	01.6	23	02.4	40			
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	10.2	12.6	10.3	10.8	13.9	06.9	21.5	04	-00.6	27	01	01.0	01	01.3	05	01.4	15	01.5	10	01.6	07	02.1	01	05.0	07	C2.7	42	
X	-	04.0	06.1	03.6	04.3	07.7	06.9	14.0	04	-07.5	28	01	02.0	02	03.0	.	.	11	01.8	12	03.2	18	03.6	05	04.6	08	02.8	36	
XI	-	-00.2	02.5	00.4	00.6	04.7	-01.7	11.7	16	-0.6	02	.	01	03.0	.	.	01	01.0	01	04.0	06	03.0	04	03.8	17	01.9	40		
XII	-	-02.1	-00.5	-02.1	-01.7	02.1	-04.9	10.5	24	-16.4	07	03	02.7	02	03.5	.	.	01	02.0	03	02.3	.	05	04.6	42	02.8	37		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 12^{\circ}00'N \lambda = 20^{\circ}58'E$ Gr. AG = + 1h 24 min.																													
I	-	-01.5	C3.5	00.5	00.7	04.6	-02.1	12.0	20	-08.0	16	02	C1.0	C2	06.0	C1	01.0	C3	01.7	03	01.0	04	01.5	.	.	02	C2.5	7	
II	-	01.5	07.0	04.3	04.3	08.3	01.1	13.5	11	-04.5	02.01	03	01.3	C9	02.0	C2	01.0	.	04	C1.2	03	01.7	.	.	.	.	13	01.0	
III	-	03.2	11.6	07.9	07.6	12.9	02.8	23.5	23	-03.5	02	04	01.5	06	01.2	C1	01.0	02	01.0	01	01.0	01	01.0	01	01.0	01	01.0		
IV	-	05.7	13.0	09.4	09.4	14.2	04.6	20.0	29	-06.5	10	07	01.9	09	01.2	C6	01.3	03	01.7	04	02.2	02	02.5	01	04.0	.	58		
V	-	10.3	17.4	13.1	13.5	19.3	06.0	25.5	31	02.5	11	11	01.5	05	01.0	.	.	02	01.0	02	C2.0	06	02.7	01	01.0	01	01.0	01	01.0
VI	-	15.2	22.9	17.6	18.4	24.4	12.0	30.0	29	06.0	13	05	01.6	01	01.0	C1	01.0	02	03.0	05	02.2	06	03.2	09	04.0	09	03.2	09	
VII	-	16.1	27.0	20.4	21.0	28.3	12.6	35.0	17	06.5	10	17	01.9	08	01.4	.	.	03	01.3	04	02.2	07	01.5	01	01.0	02	01.0	02	01.0
VIII	-	15.6	27.9	21.1	21.4	28.9	13.5	34.5	05	05.5	14	08	02.4	04	01.8	C6	01.0	05	01.2	02	02.5	01	01.0	04	01.2	01	01.0		
IX	-	11.5	23.2	15.6	16.5	24.0	10.2	36.0	04	01.6	28	09	01.6	04	01.5	.	.	01	01.0	01	03.0	.	.	01	01.0	01	01.0	01	01.0
X	-	C6.7	16.2	10.1	10.8	17.1	05.4	22.5	08	-03.8	28	07	01.6	03	01.3	C2	01.0	.	06	03.7	07	02.9	.	.	03	01.7	65	.	
XI	-	02.4	09.0	04.9	05.3	05.3	10.2	01.8	15.5	29	-01.5	30.15	01	02.0	03	01.0	C2	01.0	02	01.0	03	01.0	02	01.0	03	01.0	02	01.0	
XII	-	-00.8	05.0	01.1	01.6	06.4	-01.8	12.0	04																				



Mesec	Vazdušni pritisak mm Hg	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)															
		Tm	7	14	21	Sred. Dneš	Max	Min	Dat.	Min	Max	N	NE	E	SE	S	SW	W	NW	C					
										8.	9.	10.	11.	12.	13.	14.	15.	16.	17.						
$\gamma = 42^{\circ}12'N \lambda = 22^{\circ}20'E$ Gr. AG = + 1h 23 min.																									
I	709.3	-01.4	02.9	-00.4	00.2	03.6	-02.2	07.5	01	-08.0	15	02	02.5	03	03.1	01	04.0	*	*	01	03.0	22			
II	708.1	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	-01.0	28	3	3	3	03.5	*	*	01	05.3	20	03.0	01			
III	702.3	02.4	10.0	02.4	00.1	41.7	02.2	45.0	22	-02.0	01	01	01	01	01	01	01	01	01	01	01	01			
IV	698.4	05.6	11.8	07.0	07.9	13.3	03.2	22.0	30	-00.8	03	04	02.9	01	04.0	02	03.5	01	03.0	22	03.0	04			
V	699.4	10.6	16.1	11.1	12.2	17.9	07.4	24.7	31	02.7	06	01	03.0	47	02.5	01	03.0	*	01	05.0	21	03.2	01		
VI	706.3	15.2	20.5	15.0	16.4	23.0	11.2	29.1	29	06.1	13	02	02.5	49	02.7	*	01	04.0	*	01	04.0	01	02.0	01	
VII	702.5	16.7	25.1	17.3	19.1	26.6	12.5	33.8	17	07.0	10	01	02.0	57	02.9	*	*	*	*	01	02.6	01	05.0	01	
VIII	702.8	17.0	26.1	18.2	19.9	27.0	14.1	33.3	05	10.6	31	01	03.0	70	03.2	01	03.0	*	*	01	02.7	*	02	03.0	
IX	702.6	12.8	22.4	14.5	16.1	24.0	10.6	30.6	04	02.8	28	01	03.0	56	03.0	01	06.0	*	*	02	03.2	02	04.5	*	
X	695.9	08.4	16.4	10.0	11.2	17.2	06.4	23.2	14.0	-03.8	28	01	03.0	44	03.4	*	*	02	04.0	06	05.5	34	04.0	*	
XI	703.2	02.6	05.4	04.1	05.1	10.5	01.6	14.1	17	-02.4	03	01	03.0	51	03.7	*	*	*	02	04.5	26	02.6	*	02	01.5
XII	703.1	-00.7	04.9	00.3	01.2	05.9	-02.2	11.1	30	-05.6	18	01	03.0	53	03.3	*	*	*	*	01	01.9	*	01	04.0	
GOD.	-	07.6	14.4	08.7	09.9	15.8	05.4	33.8	Fm VII	-08.0	41	09	02.7	647	03.1	06	03.8	05	03.8	13	05.1	248	03.0	11	
$\gamma = 41^{\circ}31'N \lambda = 20^{\circ}32'E$ Gr. AG = + 1h 23 min.																									
I	-	-01.7	04.7	01.9	01.7	05.5	-02.6	09.5	22	-07.5	25	01	01.0	*	*	02	04.5	*	*	37	01.5	*	*	41	
II	-	01.8	07.5	04.1	04.4	08.0	-00.2	14.0	14	-05.5	28	07	01.7	*	*	16	05.1	*	*	43	02.1	*	*	15	
III	-	03.9	11.6	06.7	07.2	12.8	01.3	23.0	24.2	-05.0	02.0	01	01.4	*	*	20	05.2	*	*	28	02.1	*	*	18	
IV	-	06.8	12.7	08.0	08.9	13.7	03.6	20.0	30.2	00.0	24	04	02.2	*	*	14	03.7	*	*	40	01.9	*	*	22	
V	-	05.0	16.6	11.7	12.5	18.3	06.4	26.0	31	01.5	11	*	*	*	*	01	03.0	*	*	56	02.0	*	*	19	
VI	-	15.6	22.4	16.1	17.6	23.8	10.7	30.5	27	05.5	12	*	*	*	*	*	*	*	55	01.9	*	*	21		
VII	-	17.1	26.9	19.2	20.6	28.3	11.7	36.0	17	06.0	10	07	02.5	*	*	*	*	54	01.9	*	*	22			
VIII	-	17.8	27.7	21.0	21.9	29.0	13.6	34.5	06	08.0	14	*	*	*	*	04	03.2	*	*	47	01.9	*	*	26	
IX	-	13.9	23.0	16.9	17.7	24.1	10.8	31.5	04	04.0	29.2	*	*	*	*	*	*	*	52	01.5	*	*	25		
X	-	07.9	15.0	16.0	10.7	16.7	05.6	23.0	12.0	-03.0	28	*	*	*	*	*	*	*	66	02.0	*	*	14		
XI	-	03.2	10.9	05.8	06.4	11.8	01.8	16.5	20	-04.0	30	*	*	*	*	*	*	*	63	01.9	*	*	14		
XII	-	-06.4	06.1	01.8	02.3	07.3	-01.8	12.5	04	-05.0	25.20	*	*	*	*	*	*	*	58	01.9	*	*	21		
GOD.	-	08.0	15.4	10.3	11.0	16.7	05.1	36.0	Fm VII	-07.5	21	10	01.8	*	*	57	04.6	*	*	599	01.9	*	*	258	
$\gamma = 41^{\circ}11'N \lambda = 20^{\circ}41'E$ Gr. AG = + 1h 23 min.																									
I	-	-00.3	05.6	01.9	02.3	06.3	-00.9	10.3	04	-05.6	16	09	C2.0	C2	02.5	*	*	*	18	01.9	06	01.7	01		
II	-	02.3	07.0	04.0	04.3	08.0	01.1	12.4	18	-02.2	02	13	C2.0	C14	04.2	*	*	23	02.4	02	03.0	04			
III	-	03.2	10.6	06.4	06.7	11.6	01.9	20.8	24	-02.5	02	14	C1.5	C12	02.8	C1	02.0	02	05.2	03	01.0	29			
IV	-	06.2	11.2	07.8	08.3	12.6	04.3	20.0	30	00.6	10	11	C1.8	C5	03.4	C1	02.0	03	01.0	27	01.7	01			
V	-	10.4	15.7	11.8	12.4	17.3	07.1	23.0	31	02.0	11	12	C1.8	C2	02.5	C2	01.5	02.5	05	01.2	20	01.3			
VI	-	15.3	21.2	16.8	17.5	22.9	10.8	28.4	27	04.6	15	14	C1.9	C3	07.3	C1	03.0	02	01.5	18	02.2	12			
VII	-	17.1	25.6	19.2	20.6	26.8	12.0	33.5	17	06.2	10	12	C2.7	C1	02.0	C1	03.0	*	24	02.1	01	01.0	07		
VIII	-	17.4	26.4	19.2	20.5	27.6	13.7	31.6	04	08.8	13	12	C2.0	*	*	C1	02.0	*	19	02.2	06	01.0	37		
IX	-	12.9	22.4	15.6	16.6	23.3	10.3	29.5	04	02.4	28	15	C2.0	C4	02.0	*	*	01	03.0	24	02.0	02	03.5		
X	-	07.9	15.2	09.8	10.7	16.2	05.9	21.4	23	-02.1	28	06	02.2	*	*	01	03.0	*	*	28	02.7	12	03.4		
XI	-	03.6	09.9	04.5	05.6	10.6	01.8	14.5	20	-01.6	04	13	C1.1	C2	03.0	*	*	23	02.2	04	03.0	02			
XII	-	-06.4	06.4	01.4	02.2	07.3	-01.7	12.5	04	-05.1	21	18	C2.1	*	*	01	03.0	16	02.2	01	01.0	45			
GOD.	-	00.0	14.8	09.9	10.6	15.9	05.5	33.5	Fm VII	-05.6	41	157	C2.0	45	02.9	C8	C2.2	12	01.9	271	02.2	58	02.8	46	
$\gamma = 41^{\circ}32'N \lambda = 20^{\circ}42'E$ Gr. AG = + 1h 23 min.																									
I	-	052.4	-04.1	00.8	-03.0	-02.3	02.0	-05.4	06.5	22	-12.1	14	07	C2.0	C2	01.5	16	C1.5	15	01.6	07	01.7	*		
II	-	047.9	-01.8	02.2	-00.7	-00.2	03.5	-02.9	11.1	12	-11.8	09	02	01.5	01	01.0	08	C1.8	26	01.6	15	01.0	03	02.0	
III	-	050.2	00.5	06.5	01.9	02.7	07.4	-00.8	18.1	21	-08.7	02	01	01.0	01	01.0	07	C1.6	03	01.7	21	01.6	10	01.4	02.8
IV	-	047.2	01.7	06.0	02.4	03.2	08.1	00.0	14.6	30	-03.2	09	06	01.7	04	00.0	08	C1.4	10	01.4	14	01.8	09	01.0	07
V	-	045.5	07.3	11.2	07.7	08.5	12.8	04.2	18.8	20	00.6	11	11	C2.9	C5	02.6	C4	C2.0	11	02.3	08	02.3	04	01.8	07
VI	-	051.4	12.0	16.5	12.2	13.2	18.5	07.7	24.4	27	00.6	12	17	C2.5	C9	02.5	C5	C3.2	16	01.8	05	01.4	02	02.0	07
VII	-	053.5	13.7	21.0	14.8	16.1	22.2	09.8	29.6	16	02.0	09	09	C2.8	C9	02.7	C1	C2.6	11	02.2	03	01.7	07	02.1	10
VIII	-	053.6	13.8	22.1	15.7	16.8	23.5	10.8	28.2	06	04.9	13	04	02.2	12	02.2	C8	C2.2	09	02.6	08	02.2	02	02.2	07
IX	-	053.2	10.2	17.7	11.6	12.7	18.6	07.8	25.5	04	01.0	28	07	C2.9	C2	02.0	16	C2.1	08	02.5	05	02.0	06	03.2	02
X	-	045.0	04.8	09.7	05.4	06.3	11.0	02.4	17.7	04	-07.0	28	10	C3.0	09	02.1	C5	C2.6	21	02.2	07	03.1	11	02.3	09
XI	-	051.9	00.5	06.7	01.7	02.5	07.2	-00.7	13.3	21	-06.8	30	01	02.1	02	07.0	13	C2.5	13	02.1	05	02.2	11	01.9	08
XII	-	051.6	-02.8	02.5	-02.4	-01.3	04.2	-04.8	09.9	25	-12.6	20	14	01.9	0.1	02.0	18	C2.2	06	02.5	05	02.4	04	02.4	11
GOD.	-	051.0	04.6	10.2	05.6	06.5	11.6	02.3	29.6	Fm VII	-12.6	41	95	C2.4	79	02.2	129	C2.1	161	02.0	95	02.0	82	01.9	84
$\gamma = 41^{\circ}42'N \lambda = 20^{\circ}45'$ E Gr. AG = + 1h 23 min.																									
I	-	-03.0	01.6	-02.1	-01.4	02.4	-04.8	08.0	17	-11.6	14	*	*	17	C2.2	*	*	*	*	10	02.4	*	*	*	
II	-	-00.7	03.1	00.6	00.9	03.8	-02.2	12.1	12</td																

Mjesec	Oblažnost Nm (0-10)				Temperatura °C mm	Vlažnost vazduha				Padavine mm				Broj dana n s a:																					
	7	14	21	Sred. (Dnev.)		7	14	21	Spec.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	□	■	■									
						mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	•	Δ	▲	□	■	■	■										
<b>KRIVA PALANKA</b>																																			
BR. ST.256																																			
I	7.4	7.4	6.0	6.9	084.6	03.7	62	67	80	76	31	025	006.6	24	•	01	24	•	•	02	•	05	16	16	09	06	04	06							
II	6.5	6.7	5.5	6.2	125.9	04.3	80	63	71	73	36	060	023.4	08	•	0	14	•	•	04	•	04	13	07	05	07	01	01	02						
III	6.9	6.3	5.5	6.2	150.5	04.6	77	55	71	68	19	937	033.2	9!	+	3	93	+	3	97	+	93	18	19	96	91	06	01	01	02					
IV	4.4	4.0	3.4	4.8	164.7	05.2	75	51	60	65	20	029	033.0	15	+	0	92	•	•	02	+	17	09	05	01	09	•	•	02	02					
V	6.2	7.2	5.6	6.4	198.0	07.6	80	55	78	71	34	134	C39.0	16	•	•	•	•	•	06	•	03	09	23	20	02	23	•	•	06					
VI	4.6	6.7	5.8	5.7	244.7	10.0	76	57	77	70	39	124	C25.2	02	•	•	08	•	•	04	02	02	06	14	11	06	14	•	•	12					
VII	2.5	4.0	2.5	3.1	335.5	10.1	71	43	67	60	25	023	012.9	01	•	•	•	21	09	•	•	14	03	07	03	01	07	•	•	05					
VIII	2.4	4.4	2.0	3.1	305.2	10.4	73	42	66	60	28	049	C13.7	12	•	•	24	09	•	04	01	13	02	10	06	03	10	•	•	01	05				
IX	3.5	5.0	2.4	3.6	243.4	05.2	80	48	74	67	29	019	C13.2	27	•	•	•	16	01	•	04	•	14	02	05	04	01	05	•	•	02				
X	6.5	7.2	4.8	6.2	191.9	06.9	81	49	73	68	30	065	C26.1	22	•	•	03	•	•	14	03	01	08	14	10	03	14	•	•	06					
XI	5.7	5.7	4.7	5.4	129.2	05.1	85	62	82	76	43	040	C19.2	01	•	•	04	•	•	06	07	06	01	06	06	01	06	01	05	•					
XII	5.7	6.4	6.1	6.1	105.5	03.8	83	61	81	75	20	045	C14.5	15	•	•	27	•	•	02	•	05	11	13	06	01	08	05	02	•	•	01	12		
GOD.	5.4	6.2	4.8	5.5	2279.1	06.8	78	54	74	69	18	640	C39.0	Ns.V	•	01	81	65	19	•	45	06	76	106	135	91	27	117	30	07	•	02	47	05	21
<b>DEBAR</b>																																			
BR. ST.257																																			
I	6.0	6.1	6.2	6.1	-	04.2	91	68	84	81	28	038	C20.0	18	•	•	23	•	•	01	•	09	14	05	05	01	C2	02	•	•	02	01			
II	6.9	6.7	7.5	7.3	-	04.7	83	63	79	75	38	126	C42.0	07	•	•	15	•	•	05	01	04	16	07	07	04	07	•	•	•	•	01	02		
III	6.3	6.2	6.7	6.4	-	05.1	82	55	72	69	26	054	C15.0	09	•	•	10	•	•	04	02	07	14	07	C7	C2	05	03	•	•	01	02			
IV	6.7	7.3	7.1	7.0	-	06.3	82	62	78	74	48	083	C24.4	17	•	•	•	•	•	01	•	01	14	10	10	04	10	•	•	•	•	•			
V	6.5	6.9	6.5	6.6	-	07.6	85	55	76	72	26	233	C32.0	05	•	•	01	•	•	•	•	04	13	15	15	09	15	•	•	•	•	•	02		
VI	5.2	6.5	6.4	6.1	-	09.9	76	49	72	66	17	062	C32.0	17	•	•	14	01	•	•	•	04	10	07	07	01	07	•	•	•	•	•	02		
VII	1.6	3.5	2.8	2.6	-	09.8	69	35	63	56	20	-	-	-	•	•	25	19	•	•	19	02	•	•	•	•	•	•	•	•	•	•	02		
VIII	3.7	4.6	4.6	4.3	-	10.1	71	34	59	55	19	032	C13.0	25	•	•	25	17	•	•	12	06	05	05	01	05	•	•	•	•	•	02			
IX	4.3	4.7	4.7	4.6	-	10.3	87	49	73	70	25	038	C10.0	08	•	•	18	01	•	•	09	08	06	08	01	06	•	•	•	•	•	02			
X	6.5	6.5	7.1	6.7	-	07.3	86	60	80	75	15	192	C31.0	31	•	•	02	•	•	03	17	17	17	08	17	•	•	•	•	•	03				
XI	5.8	6.5	6.0	6.1	-	05.8	91	64	84	80	46	078	041.0	01	•	•	05	•	•	05	14	05	15	C4	05	•	•	•	•	•	03				
XII	5.1	4.9	5.6	5.2	-	04.5	89	67	90	82	52	029	012.0	19	•	•	24	•	•	08	09	04	04	01	02	02	01	•	•	•	•	03			
GOD.	5.4	5.5	5.9	5.8	-	07.1	83	55	76	71	15	965	C42.0	07.0	•	•	93	70	31	•	11	03	85	137	90	90	35	85	07	01	•	•	06	07	
<b>STRUGA</b>																																			
BR. ST.258																																			
I	6.4	5.9	4.9	5.7	-	04.4	51	67	84	81	36	046	C14.1	18	•	•	20	•	•	06	09	11	09	01	11	03	C1	•	•	•	•	02			
II	7.2	7.2	7.2	7.2	-	05.6	67	82	79	36	101	027.8	05	•	•	11	•	•	C1	•	03	16	13	10	12	03	01	•	•	02					
III	6.1	6.6	5.8	6.1	-	05.4	88	59	76	75	27	063	C12.0	31	•	•	06	•	•	07	15	13	11	01	13	04	•	•	•	01	02				
IV	6.9	7.9	7.2	7.3	-	06.4	88	65	82	78	31	091	C19.5	16	•	•	•	•	•	C1	•	01	12	18	14	04	18	•	•	02	04				
V	6.0	7.6	5.7	6.4	-	08.0	84	63	77	75	33	090	C16.6	02	•	•	05	•	•	02	14	16	13	04	16	•	•	•	•	•	02				
VI	4.4	5.9	4.3	4.9	-	10.0	78	24	70	67	25	044	C20.3	17	•	•	05	•	•	C4	05	09	C7	C1	05	•	•	•	•	07					
VII	1.2	3.5	1.7	2.2	-	10.1	70	39	63	58	22	010	C05.0	01	•	•	22	06	•	20	02	03	05	02	05	05	•	•	02	02					
VIII	2.5	4.1	3.3	3.3	-	10.6	74	40	66	60	21	094	C27.0	29	•	•	25	06	•	14	02	09	07	01	09	•	•	•	•	10					
IX	3.2	4.9	3.4	3.6	-	10.0	88	48	78	71	26	038	C17.0	27	•	•	11	•	•	12	04	07	04	02	07	•	•	•	•	06					
X	6.4	6.4	5.0	6.1	-	07.5	89	60	81	77	34	195	C29.4	22	•	•	01	•	•	C2	02	08	06	19	19	•	•	•	•	04					
XI	5.7	6.2	6.6	5.3	-	05.7	92	66	85	82	38	094	C26.8	01	•	•	04	•	•	02	12	10	C8	05	10	06	10	01	02						
XII	5.2	4.5	4.2	4.6	-	04.4	88	67	80	84	45	023	008.6	19	•	•	25	•	•	C8	07	07	06	06	03	01	•	•	•	02					
GOD.	5.2	4.0	4.8	5.3	-	07.3	84	58	78	73	21	849	C29.4	22.X	•	•	67	67	12	•	05	•	81	108	137	111	28	125	13	03	•	02	37	02	
<b>LAZAROPCLE</b>																																			
BR. ST.259																																			
I	6.6	6.4	6.7	5.9	-	03.2	85	68	83	79	30	056	C24.2	18	04	07	28	•	•	02	•	05	11	11	07	01	11	03	01	•	•	02			
II	7.5	8.0	6.0	7.8	-	073.4	03.7	71	83	70	25	122	031.7	05	01	03	23	•	•	C2	03	20	17	C8	C5	15	02	•	•	01	01	28			
III	6.4	6.8	6.1	6.3	-	132.8	04.3	85	64	80	77	21	052	012.9	09	•	01	19	•	•	07	14</													

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																	
		Tm			Sred. (Siles)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21									8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.						
$\varphi = 41^{\circ}07'N \lambda = 20^{\circ}48'E$ Gr. $\Delta G = +1h\ 23\ min.$																													
I	694.0	00.2	05.6	C1.9	02.4	04.2	-01.0	09.3	22	-06.4	16	37	C1.5	CR	01.9	C1	C2.0	02	02.0	10	01.7	09	01.2	01	01.0	13	C1.7	12	
II	693.9	02.7	07.0	04.2	04.5	08.3	01.0	12.6	17	-04.0	09	26	C2.0	09	02.4	CR	C2.5	04	02.8	16	02.7	08	01.5	03	02.3	09	C1.4	01	
III	696.0	04.0	10.4	06.9	07.1	11.7	02.7	20.9	23	-02.5	02	34	C1.7	08	02.2	C7	C2.4	04	03.0	16	01.9	11	01.9	06	01.5	08	01.5	09	
IV	692.5	06.1	11.3	07.7	08.2	12.7	04.0	26.0	30	06.3	09	17	C1.6	64	01.5	02	C2.0	04	02.5	20	02.3	14	02.1	10	02.3	06	C1.0	13	
V	694.2	10.8	15.9	12.0	12.6	17.5	07.5	23.3	28	03.1	11	08	C1.6	C4	02.5	C1	C2.0	01	02.0	34	02.3	22	02.0	06	02.5	02	01.5	15	
VI	695.2	15.5	21.0	16.8	17.6	22.9	11.4	27.4	27	06.3	15	17	C2.3	*	*	*	*	04	01.2	32	01.9	14	02.4	11	02.2	04	02.2	08	
VII	694.9	17.4	25.2	19.9	20.6	26.9	13.7	32.0	18	17	07.6	09	26	C1.8	04	01.2	*	*	01	01.0	23	01.6	14	01.9	04	02.8	08	01.2	13
VIII	697.0	17.6	26.2	19.7	20.8	27.9	14.9	32.3	30	05.3	13	43	C1.8	07	01.7	01	01.0	*	*	11	02.1	13	01.9	04	01.8	10	01.4	04	
IX	697.0	13.7	22.2	18.7	17.3	23.6	11.8	28.2	24	03.9	28	36	C1.8	C4	02.2	03	C3.0	01	01.0	16	02.0	09	01.9	09	01.9	11	01.5	01	
X	694.9	08.8	14.8	10.7	11.2	16.1	06.8	21.4	28	24	02.1	01	07	C1.7	01	01.0	C2	C1.0	03	02.0	26	03.0	21	C2.7	07	02.4	10	02.1	01
XI	697.5	04.6	09.8	05.7	06.5	10.8	03.0	14.7	20	-06.7	30	34	C1.9	05	01.2	*	*	*	*	14	02.1	11	02.4	12	02.0	08	01.6	06	
XII	697.4	00.7	06.5	02.1	02.6	07.4	-01.1	14.0	04	-05.7	20	46	C2.3	07	07.5	*	*	*	*	09	02.0	12	01.5	C7	02.7	13	C1.7	04	
GOD.	696.0	08.5	14.7	10.4	11.0	16.0	C1.6	06.2	32.3	CXVII	-06.4	46	336	C1.9	56	01.9	25	02.3	24	02.2	227	02.2	158	02.0	80	02.2	102	01.6	87
$\varphi = 41^{\circ}48'N \lambda = 20^{\circ}57'E$ Gr. $\Delta G = +1h\ 24\ min.$																													
I	-	-02.6	03.4	-01.1	-00.3	04.7	-05.6	10.0	21	-13.0	15	06	C2.0	05	C2.4	*	*	*	*	*	08	02.4	*	*	08	C2.6	66		
II	-	01.6	C6.6	02.6	03.4	07.7	-00.8	11.4	12	11	-08.0	02	01	C2.0	03	C2.3	*	*	01	02.0	*	14	03.6	*	*	21	C2.6	43	
III	-	03.8	11.0	05.4	06.4	12.1	01.3	22.4	23	21	-03.8	02	02	C2.0	08	C2.5	*	*	01	07.0	*	12	02.7	*	*	22	C2.3	48	
IV	-	07.0	12.6	08.2	09.0	13.9	03.1	26.0	27	06.0	04	06	C2.5	08	C2.4	*	*	*	*	*	12	03.5	*	*	24	C2.5	40		
V	-	12.8	17.2	12.2	13.6	19.4	06.2	25.0	31	03.5	16	01	C2.0	11	C2.3	*	*	04	04.2	*	34	C3.9	*	*	18	02.7	25		
VI	-	17.2	22.6	16.4	18.4	24.0	10.1	28.4	46	07.2	13	03	C2.3	13	C2.4	*	*	01	03.0	29	C3.9	*	*	22	C2.5	22			
VII	-	18.9	26.3	20.6	27.5	10.9	34.6	17	07.2	09	05	C2.4	13	C2.2	*	*	01	03.0	00	C3.1	*	*	31	C2.3	34				
VIII	-	18.4	26.3	18.8	20.6	27.7	12.5	33.0	04	08.6	13	*	16	05.5	*	*	03	03.0	*	10	02.6	*	*	24	C2.4	40			
IX	-	13.7	21.3	15.7	16.7	22.9	08.4	27.6	04	01.0	29	28	05	C2.2	08	C2.2	*	*	01	C2.0	*	*	10	03.0	*	*	17	C2.3	49
X	-	05.7	15.7	10.2	11.2	17.1	02.2	22.4	24	01	-04.2	28	35	C2.2	06	C2.5	*	*	01	05.0	*	39	C4.3	*	*	15	C2.2	27	
XI	-	02.0	09.0	C3.7	04.6	10.1	-00.9	15.2	28	-04.3	19	*	08	02.5	*	*	*	*	15	03.5	*	*	18	02.4	49				
XII	-	-01.0	05.0	01.1	01.6	06.4	-02.7	11.6	30	-08.4	25	10	C4.8	06	C2.3	*	*	*	*	02	03.5	*	*	15	C2.3	60			
GOD.	-	08.3	14.8	C9.3	10.4	16.1	03.6	34.8	MAY	-13.0	151	45	C2.6	105	C2.4	*	*	11	03.3	02	03.0	194	03.6	*	*	235	C2.4	503	
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}58'E$ Gr. $\Delta G = +1h\ 24\ min.$																													
I	-	-00.9	04.7	C1.5	01.7	05.6	-01.7	09.5	22	21	-08.5	16	29	C1.1	12	C1.8	14	C1.4	16	C1.8	15	01.7	02	01.0	07	02.1	01	C2.0	07
II	-	01.7	C7.1	04.1	04.2	08.0	00.7	14.0	12	-04.6	01	30	02.1	05	C1.8	13	C2.3	*	*	14	02.0	04	02.0	07	01.6	02	C2.6	09	
III	-	02.9	11.9	07.5	07.4	12.6	C2.2	23.8	22	-03.6	02	32	C2.0	07	C2.3	16	C1.6	C5	C6.2	14	01.4	06	01.5	11	01.5	03	C2.3	09	
IV	-	04.9	13.2	08.7	08.9	14.0	04.0	19.5	30	29	-01.0	10	33	C2.5	07	C3.0	C5	C4.2	01	C3.0	34	C2.5	02	01.5	06	C1.7	07		
V	-	68.5	17.5	12.9	13.0	18.9	07.2	26.0	31	01.8	11	22	C2.3	C2	01.0	11	C1.8	02	02.0	24	C3.2	03	01.7	11	C1.8	08	01.5	10	
VI	-	12.8	23.6	17.7	18.0	24.7	11.1	30.8	27	05.0	13	12	C2.8	10	C2.4	11	C1.6	02	02.8	20	C3.0	11	01.5	07	C1.6	04			
VII	-	14.2	28.3	20.1	20.7	29.1	12.0	36.5	17	06.2	10	36	C2.1	17	C2.3	06	C1.6	02	02.5	07	01.7	04	02.2	07	01.4	07			
VIII	-	14.3	27.8	20.2	20.6	28.9	13.2	35.0	06.05	07.6	13	34	C1.7	08	C2.5	C5	C2.4	02	01.5	06	01.5	09	C1.2	08	C1.6	13			
IX	-	16.9	23.3	15.4	16.5	24.1	16.1	31.5	04	01.2	28	21	C1.9	05	C1.8	C6	C1.2	01	01.0	08	C1.6	02	01.5	19	C1.4	10			
X	-	07.0	15.7	09.7	10.5	16.8	05.2	23.4	04	-05.3	28	20	C1.4	08	C6	C1.3	C1.0	01	03.5	10	C1.4	16	C1.3	07	C1.3	06			
XI	-	02.3	10.4	05.4	05.4	11.6	01.3	15.2	20	-02.5	30	24	C1.6	06	C1.8	C8	C1.4	04	01.2	20	C2.0	03	01.3	08	C1.6	06			

Meseč	Oblažnost mm (0-10)					Vlažnost vazduha			Padavine R mm			Broj dana na sat:																				
	Temperatura °C		Uvijet m s		Precipitation mm			mm			Tn	Tx	In	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	□	■	■				
	7	14	21	Sred. Sred. Sred.	Dnev. Dnev. Dnev.	Uvijet m s	Σ	X	Σ	X	Σ	X	Σ	X	Σ	N	Σ	N	Σ	N	Σ	N	Σ	N	Σ	N						
CHRD																																
BR. ST.261																																
I 6.2 5.8 5.5 5.8	113.3	04.5	86	70	82	80	47	035	C09.7	18	•	•	21	•	•	•	05	11	11	C5	•	11	03	01	•	•	•	04				
II 7.5 6.8 7.0 7.1	085.4	04.9	83	66	77	76	47	090	C30.6	05	•	•	10	•	•	•	05	01	03	15	12	10	04	12	02	02	•	02				
III 6.5 6.6 5.5 6.2	141.6	05.4	83	60	75	73	32	040	C11.2	31	•	•	03	•	•	•	07	06	13	12	10	01	12	06	04	•	•	01				
IV 7.0 6.1 6.6 7.3	133.1	06.1	85	63	77	75	36	083	C15.2	16	•	•	•	•	•	•	04	01	•	12	18	16	02	18	•	•	•	01	04			
V 5.5 7.7 5.1 6.1	197.7	08.1	82	63	78	74	36	098	C34.0	05	•	•	•	•	•	•	03	11	15	10	04	15	•	•	•	•	01	04				
VI 4.3 6.1 4.6 5.0	265.1	10.5	78	58	72	69	42	042	C25.5	17	•	•	06	•	•	•	01	04	07	10	06	10	01	08	•	•	•	08				
VII 1.2 3.4 1.5 2.0	347.9	11.0	72	47	62	61	32	004	C01.8	01	•	•	22	07	•	•	19	C2	C3	03	•	03	•	•	•	•	03	•				
VIII 2.3 3.9 2.9 3.0	303.3	11.2	74	47	63	61	32	049	C14.4	28	•	•	26	08	•	01	•	15	C2	08	07	01	06	•	•	•	01	11				
IX 3.2 5.1 3.1 3.8	225.9	10.2	83	53	72	70	36	033	C14.7	26	•	•	11	•	•	01	01	10	C2	C7	02	02	07	•	•	•	06	•				
X 6.4 6.8 5.6 6.2	157.5	07.7	86	64	78	76	41	150	C26.0	22	•	•	01	•	•	07	03	01	08	21	19	07	21	•	•	•	05	•				
XI 7.0 6.2 4.9 6.0	109.8	06.0	90	68	85	81	50	077	C31.8	01	•	•	02	•	•	03	03	09	06	02	05	05	01	02	•	•	01					
XII 5.4 4.8 3.8 4.7	129.1	04.5	85	69	81	78	43	023	C08.6	19	•	•	23	•	•	01	•	08	07	05	05	03	01	•	•	•	01	02				
GOD. 5.2 5.9 4.7 5.3	2209.7	07.5	62	60	75	72	32	724	C04.0	65	V	•	•	60	65	15	•	25	06	77	98	133	106	24	131	15	08	•	03	45	03	
GOSTIVAR																																
BR. ST.262																																
H = 525 m H <sub>b</sub> = - m h = 2.1 m h <sub>r</sub> = 1.5 m																																
I 6.2 5.6 5.2 5.7	-	03.2	62	73	64	66	-	09	C22.0	24	04	•	31	•	•	•	07	11	11	16	04	05	06	•	•	•	03	31				
II 6.6 6.8 6.2 6.5	-	04.5	74	71	76	74	43	174	C30.0	05	•	•	16	•	•	•	02	•	06	14	18	17	08	18	•	•	02					
III 5.5 6.2 5.8 5.8	-	05.3	79	62	77	72	33	134	C17.0	09	•	•	08	•	•	•	08	12	11	11	09	08	06	04	•	•	04					
IV 6.5 7.4 6.9 6.9	-	06.2	79	59	76	71	26	664	C16.0	17	•	•	•	•	•	01	01	•	10	13	11	02	12	•	•	•	•	•				
V 5.5 7.1 5.4 6.0	-	08.2	72	59	72	68	39	088	C29.0	16	•	•	01	•	•	01	01	07	07	13	11	C3	13	•	•	•	•	•				
VI 4.6 6.1 5.6 5.4	-	10.4	70	54	68	64	32	052	C30.0	17	•	•	14	•	•	01	01	02	03	06	04	03	06	•	•	•	•	•				
VII 1.6 3.8 1.7 2.4	-	10.6	63	44	63	57	30	005	C03.0	08	•	•	25	09	•	•	15	•	02	07	•	02	•	•	•	•	•	•				
VIII 2.3 4.5 2.5 3.1	-	11.2	69	42	65	61	31	033	C18.0	25	•	•	25	10	•	•	13	03	05	05	01	04	•	•	•	•	01					
IX 3.8 5.4 C4.0 4.2	-	09.4	76	55	74	68	11	042	C11.0	27	•	•	08	•	•	04	06	C3	05	02	C5	•	•	•	•	•	01	•				
X 5.2 5.6 4.3 5.1	-	07.0	76	56	72	68	10	13	C25.0	21	•	•	04	•	•	05	02	C5	C8	17	16	04	17	•	•	•	•	•	03			
XI 5.6 5.8 5.4 5.6	-	04.8	75	67	75	73	41	069	C30.0	27	•	•	20	•	•	01	01	C8	C8	08	02	08	•	•	•	•	•	16				
XII 4.8 4.3 4.5 4.5	-	03.6	65	71	71	69	32	018	C07.0	19	•	•	31	•	•	01	01	C8	C6	06	04	C2	04	•	•	•	•	•	01			
GOD. 4.6 5.7 4.8 5.1	-	07.1	72	60	71	68	-	516	C03.0	07XII	04	•	110	73	19	•	12	06	R3	E5	115	106	36	102	16	•	•	•	02	05		
KICEVO																																
BR. ST.263																																
H = 620 m H <sub>b</sub> = - m h = 2.1 m h <sub>r</sub> = 1.5 m																																
I 6.8 6.1 6.2 6.4	-	04.4	92	72	88	84	48	055	C11.6	11	•	•	19	•	•	•	06	16	11	08	C3	C7	05	•	•	05	06	•	02			
II 7.7 7.1 7.2 7.4	-	05.0	90	67	84	80	21	094	C29.0	05	•	•	09	•	•	•	04	18	15	12	05	15	02	02	01	02	01	01				
III 6.9 6.4 6.7 6.9	-	05.4	90	57	72	73	20	053	C13.5	09	•	•	06	•	•	•	03	17	10	C9	01	05	07	06	•	•	01	08	02			
IV 7.9 8.5 8.1 8.2	-	06.0	88	55	73	71	29	111	C18.2	15	•	•	01	•	•	•	02	01	•	18	14	04	14	01	•	•	02	01				
V 5.5 6.3 7.0 6.9	-	06.0	87	60	74	74	28	095	C10.4	22	•	•	01	•	•	01	01	11	12	12	05	12	12	•	•	04	01	01				
VI 5.0 6.8 5.7 5.9	-	10.1	84	50	66	67	13	058	C16.3	19	•	•	16	01	•	•	01	06	11	10	02	11	•	•	01	07	03					
VII 2.0 2.9 3.2 3.4	-	10.7	80	39	64	61	27	001	C01.1	02	•	•	26	16	•	•	17	01	01	01	01	01	01	•	•	01	06					
VIII 2.3 4.9 3.0 4.2	-	11.2	84	43	66	55	27	076	C03.7	25	•	•	26	15	•	•	12	02	08	08	03	06	•	•	08	06	06					
IX 4.7 4.9 3.0 4.2	-	10.4	91	54	78	74	39	064	C02.5	27	•	•	13	01	•	01	09	04	06	06	01	06	•	•	03	07	•					
X 6.6 6.9 5.2 6.3	-	07.5	89	61	82	77	29	124	C18.0	22	•	•	02	•	•	02	02	C2	04	02	04	02	04	•	•	04	03	•				
XI 5.5 6.0 5.0 5.3	-	05.5	90	63	84	75	48	076	C02.5	01	•	•	11	•	•	03	03	10	09	06	03	09	•	•	01	12	•					
XII 6.1 5.6 5.0 5.3	-	04.0	86	62	84	77	37	010	C03.9	15	•	•	24	•	•	01	09	11	04	03	•	03	02	01	•	•	01					
GOD. 5.7 6.2 5.4 5.8	-	07.4	88	57	76	74	13	817	C04.7	25XVII	0	•	72	62	33	•	05	02	68	122	120	116	32	116	19	14	•	01	01	32	56	06
RESEN																																
BR. ST.264																																
H = 881 m H <sub>b</sub> = - m h = 1.9 m h <sub>r</sub> = 1.7 m																																
I 6.2 6.4 5.4 6.0	-	04.1	80	75	83	81	37	046	C10.3	03	•	01	24	•	•	•	01	01	16	11	09	01	06	01	01	•	•	06				
II 7.3 7.7 7.5 7.1	-	04.6	81	73	87	81	23	109	C32.2	05	•	•	13	•	•	•	02	•	05	15	12	10	03	11	04	03	•	01	03			
III 7.0 6.3 6.0 6.5	-	05.0	87	60	83	77	26	058	C16.2	05	•	•	09	•	•	•	03	17	11	01	05											

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, fm (0-12)																		
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21							8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.
$\varphi = 41^{\circ}22'N \lambda = 21^{\circ}15'$ E Gr. AG = + 1h 25 min.																												
I	-	-02.3	00.7	-01.5	-01.1	01.9	-03.9	07.5	18.17	-11.4	14	17	02.2	25	01.8	18	01.6	19	01.8	03	02.7	05	02.6	C6	02.2	C1	66.6	14
II	-	-00.1	02.4	01.0	01.0	03.6	-01.5	08.4	12.11	-07.0	29	02	01.0	30	01.8	11	01.2	15	02.7	01	01.0	09	03.9	05	04.0	03	01.7	08
III	-	02.2	05.9	03.5	03.8	06.4	00.8	16.4	19	-06.6	01	05	02.0	27	01.7	15	01.5	27	02.0	05	02.0	02	01.5	02	04.5	04	02.2	06
IV	-	03.8	06.8	04.5	04.9	08.1	01.4	14.5	29	-01.7	20	.	.	21	07.4	28	01.9	19	02.6	02	02.0	09	05.3	09	03.4	01	03.0	01
V	-	09.2	11.7	09.0	09.7	13.2	05.9	19.4	31	01.1	05	03	03.3	25	02.6	10	01.5	12	02.2	03	02.7	15	03.7	19	03.9	04	03.0	02
VI	-	14.0	17.8	13.4	14.6	19.0	05.8	24.5	27	02.2	11	09	05.0	13	01.7	12	01.9	08	01.0	01	01.0	29	03.3	12	03.7	16	03.8	.
VII	-	17.7	21.9	16.7	18.3	22.7	12.4	28.8	16	04.8	23	01	04.0	24	07.4	22	01.7	09	01.3	01	03.0	05	03.6	06	02.8	07	03.1	04
VIII	-	17.4	22.5	17.0	16.5	23.6	13.8	28.6	06	08.5	13	05	03.6	39	01.3	21	01.7	12	02.2	03	01.7	05	03.4	03	04.0	.	05	
IX	-	13.5	18.0	13.8	14.8	19.0	10.4	26.0	04	01.9	27	04	02.2	23	01.8	16	02.0	16	02.2	01	02.0	13	02.8	08	03.0	C5	03.6	02
X	-	07.0	11.2	08.2	08.5	12.3	05.1	18.5	28	03	04.0	06	01.8	C7	02.4	06	03.7	45	04.8	08	03.6	02	02.0	.	02	.	02	.
XI	-	02.6	06.4	03.8	04.2	07.1	01.5	13.7	19	-03.2	02	04	02.2	19	02.2	16	01.7	06	03.0	06	04.5	18	03.2	14	03.9	03	03.0	04
XII	-	-00.4	03.2	00.4	00.9	04.3	10.5	10.5	20	08.3	20	08	02.5	47	02.4	06	01.8	07	02.5	02	03.1	07	04.0	04	04.0	05	05	
GOD.	-	07.0	10.7	07.4	08.2	11.8	04.4	28.8	4-17	-11.4	06.1	05	02.8	30.9	02.7	16.2	01.7	16.4	02.2	36	02.5	15.3	03.7	59	03.5	50	03.3	57
$\varphi = 41^{\circ}03'N \lambda = 21^{\circ}23'$ E Gr. AG = + 1h 25 min.																												
I	714.3	-00.1	04.3	01.2	01.5	04.9	-01.3	08.0	21	-06.7	16	17	01.8	16	01.9	C2	01.5	04	01.2	11	02.9	05	04.0	02	02.0	11	01.4	21
II	705.0	01.9	06.9	03.8	04.1	08.3	02.9	13.1	12	-03.6	01	02	01.5	21	01.3	C5	01.6	02	01.5	20	03.9	05	03.4	C2	03.0	05	03.2	21
III	711.0	03.9	11.0	06.8	07.1	11.7	02.9	21.4	21	-04.0	02	10	01.6	18	02.1	C4	01.8	03	02.3	26	03.8	10	03.9	05	C4.2	04	01.0	13
IV	707.2	06.2	12.0	08.6	08.6	13.4	04.0	20.1	29	-00.3	10	01	02.0	17	02.8	C6	02.0	02.5	17	03.7	11	02.7	02	01.5	03	04.3	12	
V	708.3	11.5	17.4	12.9	13.6	19.2	07.4	24.2	31	02.0	11	14	02.1	14	02.1	C1	02.0	07	02.1	17	02.8	08	02.4	05	02.6	07	03.9	20
VI	705.0	16.1	23.0	17.6	18.5	24.5	11.6	30.2	27	05.6	15	13	02.8	15	02.1	C5	02.2	15	02.7	14	01.8	C5	03.8	14	04.3	10		
VII	710.9	17.4	27.8	20.2	21.4	29.1	12.0	36.9	17	05.6	10	19	02.1	22	01.5	C3	01.7	06	02.0	08	01.9	05	02.2	04	01.8	09	03.9	15
VIII	711.2	16.8	28.0	20.3	21.4	29.2	13.1	34.7	06	07.1	13	12	02.2	14	02.6	C1	01.0	05	02.8	06	02.5	02	02.0	04	03.3	24		
IX	711.4	12.5	24.0	16.6	17.4	25.0	10.3	32.2	04	03.4	28	18	02.2	07	02.0	C1	01.0	03	03.3	18	02.7	07	02.3	04	02.5	09	02.9	23
X	706.1	08.3	17.0	11.4	12.1	18.5	05.5	24.9	05	-03.6	28	11	02.5	C1	01.0	14	02.4	27	04.0	10	03.4	C9	03.2	07	02.4	12		
XI	712.3	02.2	09.4	05.4	05.6	10.2	01.4	16.2	28	-03.3	04	16	01.9	05	01.8	C4	01.5	07	02.0	10	03.5	04	01.0	07	02.6	07	03.3	30
XII	712.6	-03.8	02.0	-02.2	-01.6	03.1	-05.8	12.2	04	-15.7	18.17	29	01.9	08	01.6	C2	01.0	05	02.2	07	02.1	01	02.0	04	01.7	05	01.7	32
GOD.	710.4	07.7	15.2	10.2	10.8	16.4	05.2	36.9	ITM	-15.2	18.17	177	02.1	16.4	04.2	22	01.6	63	03.3	195	03.2	76	02.9	54	02.7	91	03.1	24.3
$\varphi = 41^{\circ}57'N \lambda = 21^{\circ}38'$ E Gr. AG = + 1h 27 min.																												
I	746.9	00.3	05.6	01.6	02.3	06.5	-00.9	10.1	22	-07.7	15	14	03.1	C8	02.0	C7	01.4	12	01.8	01	01.0	04	01.0	11	02.4	25		
II	746.7	C2.3	08.9	04.6	05.1	10.4	01.1	14.6	11	-06.5	02	12	02.9	00	02.4	C7	01.0	19	02.1	10	02.9	02	01.0	03	01.6	08	02.0	18
III	742.6	03.9	13.0	07.6	08.6	14.0	02.2	22.6	22	-05.4	01	10	02.3	13	02.2	C6	01.5	22	02.3	14	02.4	02	02.0	05	01.6	06	01.6	16
IV	738.4	07.0	14.9	10.1	15.8	22.0	04.5	22.0	27	-06.4	04	10	03.0	14	07.6	C7	01.3	21	02.6	11	02.5	01	01.0	06	01.0	06	01.0	16
V	738.8	11.8	19.2	13.9	14.7	21.0	08.5	26.7	31	01.8	11	16	02.6	C9	02.3	C6	01.3	13	02.4	03	01.0	03	01.0	03	02.0	00	01.9	22
VI	735.6	16.9	24.2	19.3	20.6	26.4	17.7	32.1	29	05.2	15	16	02.5	C5	02.5	C7	01.9	14	01.9	10	01.9	01	01.0	06	03.0	10	02.8	18
VII	741.0	18.3	26.5	20.4	22.2	29.6	13.3	37.0	17	06.9	10	11	03.4	11	07.7	C7	01.3	10	01.5	09	01.3	01	01.2	01	02.0	05	02.2	25
VIII	741.2	16.5	24.6	22.1	23.1	30.8	15.0	36.2	05	11.0	14	15	01.0	14	06.6	C6	01.7	08	01.5	08	02.1	06	01.5	08	02.4	21		
IX	741.5	13.6	25.1	17.3	18.3	26.1	11.4	33.0																				

Mjesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm		Broj dana u nizu:																										
	7	14	21		e <sub>m</sub>	U <sub>m</sub>	%		Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	R	T	M								
					mm	7	14	21	Stred.	Min							≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV									
<b>KRUŠEVO</b>																																				
<b>BR. ST.266</b>																																				
I	7.1	7.2	6.6	6.3	-	03.8	90	87	88	88	55	C65	C15.7	03	01	07	28	•	•	C3	•	09	12	16	09	03	05	14	•							
II	7.0	7.8	7.1	7.3	-	04.3	89	84	87	87	43	132	C30.4	05	•	05	20	•	•	03	01	05	18	17	13	04	07	15	02	•						
III	6.9	7.1	6.4	6.8	-	04.9	86	77	81	81	40	067	C12.5	28	•	01	18	•	•	05	16	16	13	01	02	14	•	•	02	20	•					
IV	6.6	6.4	5.9	7.0	-	05.3	84	78	79	80	51	u94	C16.5	16	•	•	05	•	•	02	•	•	13	17	12	06	04	•	•	01	03	12	01			
V	5.6	7.1	5.6	6.2	-	07.1	75	74	79	77	55	130	C33.7	06	•	•	•	•	•	07	•	C3	06	15	15	04	15	•	•	•	03	05	•			
VI	4.7	6.2	4.3	5.1	-	08.9	72	66	71	76	43	085	C023.5	19	•	•	•	•	•	03	•	C3	06	12	07	04	12	•	•	•	01	04	C3			
VII	1.2	4.5	1.1	2.3	-	10.5	66	57	67	63	25	006	G02.8	18	•	•	09	•	01	01	•	15	03	02	03	02	•	•	•	02	•	•				
VIII	2.7	4.5	2.4	3.2	-	13.4	63	78	83	81	98	051	C23.2	26	•	•	14	•	•	02	•	11	C1	07	05	02	07	•	•	•	11	•	•			
IX	3.5	4.6	2.2	3.4	-	09.2	78	62	72	71	35	049	C21.0	27	•	•	01	•	•	03	•	11	01	06	04	02	06	•	•	•	02	C1	•			
X	6.2	6.9	4.4	5.9	-	06.4	79	69	74	74	42	116	C031.5	22	•	•	04	•	•	13	02	C2	08	19	17	03	17	04	•	•	•	01	04	•		
XI	5.5	5.7	4.6	5.2	-	05.0	86	74	82	81	38	097	C031.3	08	•	•	05	•	•	03	•	06	10	12	08	03	10	02	•	•	•	08	01	•		
XII	5.2	5.0	4.5	4.9	-	03.6	76	71	75	74	35	058	C19.4	15	•	03	25	•	•	02	•	05	08	08	07	01	02	07	•	•	•	05	•	•		
GOD.	5.2	6.3	4.4	5.3	-	06.9	81	73	78	77	25	950	C033.7	00/V	01	16	105	24	•	01	43	03	75	101	148	112	30	103	60	07	•	•	02	34	160	•
<b>BITOLA</b>																																				
<b>BR. ST.267</b>																																				
I	6.6	6.8	5.2	6.3	09C.5	04.4	89	75	87	84	48	049	C010.1	25	•	•	20	•	•	C7	•	06	11	10	09	01	08	06	04	•	•	•	C3	C3		
II	7.0	7.2	6.4	6.9	082.4	05.0	89	69	84	81	37	119	C027.1	18	•	•	11	•	•	11	01	05	•	•	09	04	15	05	04	•	•	03	01	01	01	
III	6.7	6.5	5.7	6.3	139.0	05.6	87	60	78	75	31	051	C11.0	15	•	•	03	•	•	11	•	06	11	01	13	02	01	•	•	01	•	•	01			
IV	6.7	6.2	6.3	7.0	158.5	06.2	85	60	74	73	33	050	C06.4	19	•	•	01	•	•	11	01	01	11	16	13	•	14	•	•	•	03	•	•			
V	5.5	7.1	6.2	6.2	233.7	08.3	81	57	74	71	34	066	C024.8	30	•	•	•	•	•	14	01	C3	09	13	10	02	13	•	•	•	04	•	•			
VI	5.8	6.2	4.6	5.2	288.0	10.5	78	52	69	66	27	048	C029.8	17	•	•	16	01	•	19	01	03	08	06	01	08	06	04	•	•	07	01	•	•		
VII	1.7	4.0	2.6	2.8	369.3	10.1	71	35	57	55	24	001	C000.7	22	•	•	26	17	•	11	•	14	01	01	•	01	•	•	•	•	•	C2	•	•		
VIII	3.2	4.4	3.6	3.7	316.5	11.7	79	65	61	62	24	044	C25.4	25	•	•	25	16	•	05	•	09	02	05	04	02	05	•	•	•	04	•	•			
IX	3.4	4.5	2.9	3.7	245.2	09.8	88	64	70	67	31	015	C008.8	27	•	•	17	03	•	C9	01	10	C1	03	03	01	•	•	•	04	•	•				
X	5.5	6.0	4.5	5.5	166.0	07.4	86	52	71	70	25	055	C12.5	21	•	•	03	•	•	21	05	04	06	16	15	01	16	•	•	02	•	•				
XI	6.7	6.6	6.4	6.4	101.6	05.9	85	70	86	81	25	070	C036.6	08	•	•	07	02	05	11	15	08	02	11	06	04	03	01	•	•	12	01	•			
XII	7.1	5.2	6.4	6.2	098.7	03.7	90	77	88	85	51	059	C021.2	15	09	08	26	•	•	05	01	03	12	07	05	03	16	04	02	01	11	17	•			
GOD.	5.7	5.1	5.5	5.5	2291.4	07.3	84	57	75	72	24	627	C034.8	08/R	05	08	75	84	37	•	135	13	68	103	123	93	17	123	17	12	•	•	34	27	73	•
<b>SKOPJE-Petrovac</b>																																				
<b>BR. ST.268</b>																																				
I	6.9	7.2	6.2	6.7	075.4	04.5	88	70	86	81	48	036	C015.8	24	•	•	15	•	•	05	•	04	13	11	06	01	11	03	02	•	•	02	01	•		
II	7.6	6.9	6.2	6.9	096.5	05.3	88	66	81	81	41	080	C036.3	16	•	•	09	•	•	10	•	05	14	06	06	02	04	06	04	02	•	04	•			
III	6.6	6.2	6.0	6.3	137.2	05.7	87	64	77	72	28	030	C005.6	07	•	•	05	02	•	07	•	05	15	12	07	02	03	01	01	•	07	•	07	•		
IV	6.7	7.0	5.9	6.8	154.8	06.3	82	72	71	76	25	055	C016.4	15	•	•	01	•	•	12	01	01	12	14	06	02	14	•	•	01	04	•	04	•		
V	5.7	7.3	5.6	6.0	195.9	08.9	86	53	76	72	30	092	C025.8	16	•	•	04	•	•	10	02	03	05	17	13	03										

Mesec	Vazdušni Pritisak Fm mb	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																
		Tm			Max	Min	Mx	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21							8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.		
$\varphi = 41^{\circ}43'N \lambda = 21^{\circ}46'E$ Gr. $\Delta G = + 1h 27 min.$																												
I	-	01.7	06.5	02.8	03.5	07.4	00.4	10.8	29 -07.0	15	.	.	C1	02.0	.	.	11	02.8	.	.	07	01.4	.	.	46	02.3	28	
II	-	03.2	10.1	05.7	06.2	10.9	02.4	14.8	06 -04.8	02	01	02.0	04	01.5	.	.	19	02.5	.	.	09	01.8	.	.	32	01.9	19	
III	-	05.2	13.8	09.0	09.2	14.5	04.2	25.6	21 -04.8	02	.	.	11	01.6	.	.	27	03.4	.	.	05	03.0	.	.	31	02.4	19	
IV	-	08.0	15.5	10.7	11.2	16.8	06.0	22.6	29 06.6	10	01	01.0	09	01.9	.	.	21	02.7	.	.	11	01.8	.	.	32	02.4	17	
V	-	13.5	20.4	15.4	16.2	22.0	10.4	26.2	31 05.5	06	.	.	03	01.7	.	.	C5	02.2	.	.	11	02.7	.	.	35	02.9	14	
VI	-	18.4	25.6	19.9	20.9	26.9	14.3	33.0	29 07.5	15	.	.	03	04.2	.	.	12	07.6	.	.	08	04.0	.	.	26	03.4	41	
VII	-	19.9	29.4	22.0	23.3	30.5	15.1	37.6	16 10.2	09	.	.	04	02.0	.	.	C5	01.8	.	.	02	01.5	.	.	32	02.9	40	
VIII	-	20.4	30.7	25.0	24.3	31.6	11.0	37.5	05 13.2	13.11	.	.	03	01.0	.	.	08	01.5	.	.	06	02.3	.	.	31	02.6	45	
IX	-	15.6	25.9	18.4	19.6	26.8	13.0	33.6	04 04.8	29	.	.	04	01.0	.	.	11	01.9	.	.	06	02.0	.	.	20	02.4	44	
X	-	10.1	19.7	12.7	13.8	20.7	07.2	30.0	08 -02.5	28	.	.	01	01.0	.	.	14	02.7	.	.	16	02.6	.	.	14	02.9	44	
XI	-	04.2	11.4	06.2	07.0	12.1	02.9	17.2	06 -03.0	30	.	.	03	01.0	.	.	C6	01.7	.	.	16	01.9	.	.	18	02.8	40	
XII	-	00.0	06.8	02.1	02.8	07.9	-01.2	12.6	13 -07.0	25	.	.	02	01.0	.	.	03	01.3	.	.	05	02.4	.	.	26	03.6	47	
GOD.	-	10.0	18.0	12.3	13.2	19.0	01.6	37.6	le VII -07.0	25	00	02	01.5	45	01.6	.	.	146	02.6	.	.	102	02.2	.	.	343	02.6	457
$\varphi = 41^{\circ}50'N \lambda = 22^{\circ}02'E$ Gr. $\Delta G = + 1h 28 min.$																												
I	-	C1.0	06.0	02.2	02.8	06.9	-00.9	10.5	22 -09.0	16	.	.	C1	02.0	.	.	02	02.0	.	.	02	02.5	.	.	19	03.5	69	
II	-	03.3	10.1	04.8	05.7	10.9	01.4	14.5	06 -06.4	02	01	02.0	01	02.0	01	03.0	09	02.6	01	06.0	01	03.0	.	.	11	02.5	59	
III	-	05.2	13.6	07.3	08.4	14.4	02.8	24.6	21 -05.0	02	.	.	02	01.5	.	.	19	01.9	.	.	02	02.5	.	.	12	02.8	60	
IV	-	07.9	15.1	09.0	10.3	16.3	04.3	22.5	29 -01.5	10	.	.	02	01.5	.	.	17	02.6	.	.	02	01.0	.	.	17	02.0	54	
V	-	12.8	20.1	13.8	15.1	21.2	09.1	28.0	31 02.5	11	.	.	02	01.0	.	.	05	02.4	.	.	03	02.3	.	.	25	03.3	40	
VI	-	17.7	25.8	17.8	19.8	26.5	11.7	32.2	28 05.5	15	01	04.0	01	04.0	01	03.0	07	03.7	01	02.0	.	.	.	.	22	04.8	57	
VII	-	18.2	28.9	20.6	22.1	25.9	13.4	37.4	17 06.8	10	05	04.0	01	04.0	01	03.0	01	03.0	03	02.0	.	.	.	.	20	04.8	49	
VIII	-	18.8	30.5	21.0	23.2	31.3	15.2	36.8	05 10.6	31	04	02.5	01	03.0	.	.	01	03.0	03	02.0	.	.	.	.	14	03.5	70	
IX	-	14.1	26.2	17.3	18.7	26.8	11.2	34.0	04 03.0	28	.	.	01	01.0	.	.	17	04.6	C2	04.0	01	03.0	.	.	01	02.0	63	
X	-	10.6	19.1	12.0	13.4	20.0	06.5	26.0	08 -04.5	26	.	.	C1	05.0	.	.	C3	04.3	.	.	01	03.0	.	.	07	05.4	74	
XI	-	04.2	10.3	06.5	06.9	10.8	01.6	15.0	13 -03.5	30	.	.	01	01.0	.	.	-	-	-	-	-	-	-	-	-	-		
XII	-	01.1	06.6	03.6	03.8	07.4	-00.3	12.5	13 -07.0	24	.	.	02	01.0	.	.	-	-	-	-	-	-	-	-	-	-		
GOD.	-	09.6	17.7	11.4	12.5	18.5	06.3	37.4	le VII -05.0	00.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 41^{\circ}26'N \lambda = 22^{\circ}02'E$ Gr. $\Delta G = + 1h 26 min.$																												
I	-	01.1	06.1	03.0	03.3	06.4	-00.7	09.8	03 -07.5	16	05	02.4	17	01.1	C1	01.0	01.0	C1	01.0	.	.	27	01.0	47				
II	-	04.5	10.3	05.9	06.6	10.6	02.2	15.2	17 -02.3	11	07	04.0	05	01.4	05	02.8	13	01.5	04	01.0	11	01.2	02	01.5	16	01.6	26	
III	-	06.7	13.5	09.2	09.6	13.8	04.3	24.5	21 -03.5	02	01	01.7	16	01.5	10	04.0	11	01.5	05	01.0	04	01.0	03	03.3	23	01.1	30	
IV	-	09.0	15.4	11.0	11.6	16.3	05.6	23.0	30.27 01.8	04	02	01.5	11	02.0	08	01.2	01	01.0	02	01.0	.	.	27	01.7	22			
V	-	14.5	20.7	15.8	16.7	21.8	09.4	27.0	31 05.8	17	02	03.5	07	01.4	C4	02.2	02	01.0	04	01.0	07	01.6	.	.	32	01.6	47	
VI	-	19.3	26.0	20.5	21.6	27.1	14.6	33.1	29 08.5	13	02	03.0	08	01.5	05	02.0	06	01.2	07	01.8	.	.	29	01.4	57			
VII	-	21.3	30.0	23.2	24.4	30.6	15.3	37.6	17 10.0	10	02	01.0	05	01.8	C3	02.0	03	01.0	05	01.0	03	02.0	01	01.0	25	01.7	47	
VIII	-	21.0	31.0	23.9	25.0	31.4	17.4	36.8	04 11.9	13	01	01.0	03	02.0	C2	03.0	04	01.0	02	01.0	06	01.0	.	.	23	02.1	54	
IX	-	16.2	25.7	18.8	19.9	26.2	12.8	29.6	10 06.5	28	.	.	08	02.2	.	.	06	01.6	01.0	01.0	03	01.7	01	01.0	20	01.6	51	
X	-	12.3	20.7	14.7	15.6	21.1	09.3	26.6	23 -01.1	28	.	.	12	01.3	C2	01.5	01.5	02	01.3	12	01.5	01	01.0	18	01.2	37		
XI	-	05.4	11.2	07.3	07.8	11.7	04.1	16.0	06 -00.6	04	02	01.0	10	01.4	C5	01.8	04	01.0	03	01.3	06	01.2	.	.	19	01.4	41	
XII	-	01.1	06.1	02.0	03.2	04.2	-01.3	12.0	04 -06.4	25.18	02	01.0	02	01.0	.	.	09	01.1	01	01.0	06	01.0	.	.	12	02.1	41	
GOD.	-	11.0	18.1	13.0	13.8	18.6	07.8	37.6	le VII -07.0	00.1	23	02.1	10.2	01.5	47	C2.1	75	01.2	30	01.1	73	01.4	08	02.0	266	01.5	411	
$\varphi = 41^{\circ}45'N \lambda = 22^{\circ}11'E$ Gr. $\Delta G = + 1h 29 min.$																												

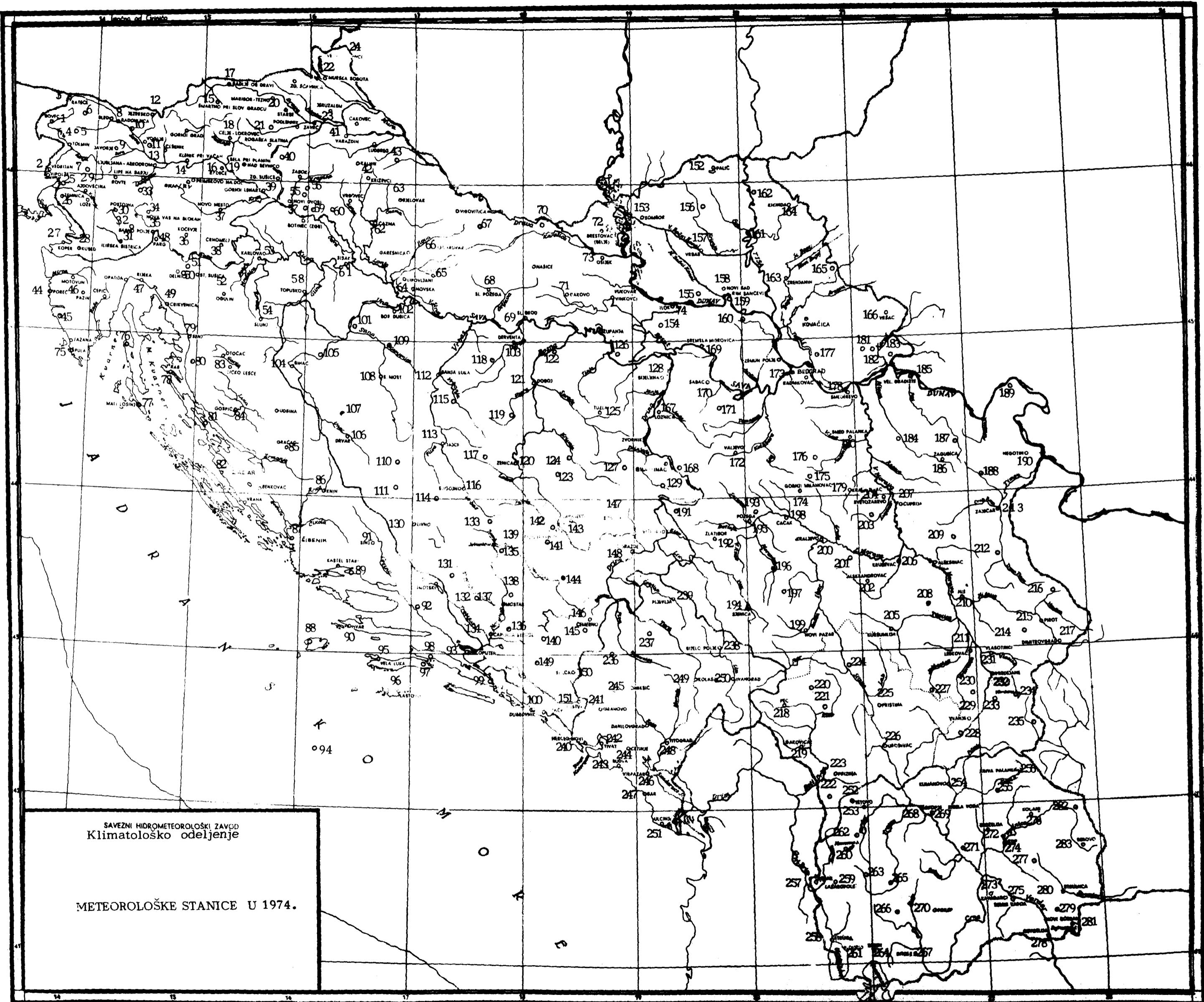


Mesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, fm (0-12)																				
		Tm				Dat.				N			NE		E		SE		S		SW		W		NW		C			
		7	14	21	Sred. (dies)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\varphi = 41^{\circ}55'N \lambda = 22^{\circ}25'E$ Gr. AG = + 1h 30 min.																														
I	-	00.5	05.9	02.6	02.9	06.3	-06.6	10.0	03	-06.8	16	26	C2.7	C3	02.0	.	.	.	12	02.2	07	02.1	.	.	.	.	.	.	45	
II	-	03.3	10.1	05.9	06.3	11.0	01.8	15.5	18	-03.5	02	17	C2.7	C3	03.0	C1	02.0	.	.	C4.2	01	02.0	.	.	.	.	.	.	33	
III	-	05.3	13.3	09.3	09.3	14.0	03.6	24.0	21	-02.0	02	24	C2.5	C7	02.4	.	.	.	C4.7	02	02.0	02	02.0	.	.	.	.	.	36	
IV	-	07.2	15.1	10.5	10.8	15.5	04.5	23.5	30	06.6	20	29	C2.9	C1	03.1	.	.	.	19	03.1	.	.	.	.	.	.	.	.	32	
V	-	12.6	19.4	14.9	15.5	20.4	09.6	27.2	31	04.5	11	28	C2.6	C6	02.5	.	.	.	15	02.9	02	02.5	.	.	.	.	.	.	42	
VI	-	16.9	24.9	19.1	20.0	25.6	13.7	31.2	27	07.6	13	24	C3.0	C3	02.0	.	.	.	16	C2.2	*	.	.	.	.	.	.	.	39	
VII	-	18.3	26.4	22.2	22.8	29.0	14.3	35.5	16	09.0	10	16	C2.9	C1	07.0	.	.	.	17	01.2	02	02.0	.	.	.	.	.	57		
VIII	-	19.2	29.7	25.2	25.8	30.2	16.4	34.5	08.0	11.5	31	16	C2.2	C5	02.8	.	.	02	03.5	14	02.3	01	03.0	.	.	01	03.0	54		
IX	-	13.5	25.2	18.5	18.9	26.0	11.6	32.0	04	02.5	28	24	C2.7	C1	03.0	.	.	.	14	02.4	01	02.0	.	.	.	.	.	50		
X	-	10.4	19.2	14.4	14.6	20.1	08.1	24.8	23	-03.2	28	26	C2.6	C1	03.0	.	.	.	C4.2	0.8	01	C2.0	.	.	.	.	.	44		
XI	-	03.6	11.4	06.8	07.1	12.0	02.2	17.0	06	-02.0	03	13	C2.2	C4	02.7	.	.	.	07	02.6	01	02.0	.	.	.	.	.	66		
XII	-	-00.3	06.3	01.9	02.5	06.9	-01.8	12.5	26	20	C2.6	C3	02.0	.	.	.	.	C5	02.0	02	03.5	01	02.0	.	.	.	62			
GOD.	-	09.2	17.4	12.4	12.9	18.1	07.0	35.5	KGW	-06.8	KGW	271	C2.7	C6	02.6	C1	02.0	02	03.5	191	02.6	20	02.3	03	02.0	01	03.0	560		
$\varphi = 41^{\circ}38'N \lambda = 22^{\circ}27'E$ Gr. AG = + 1h 30 min.																														
I	-	00.8	05.0	01.9	02.4	05.7	00.0	05.5	30	-06.5	16	12	C6.2	C1	03.0	28	C1.6	C3	01.7	C1	03.0	.	.	19	02.1	14	C4.3	15		
II	-	03.4	05.1	05.0	05.7	09.7	02.0	15.0	16	-03.0	28	04	C4.0	.	.	20	C2.2	C8	03.1	C4	02.0	.	.	22	02.4	06	C4.3	20		
III	-	05.1	12.1	07.5	06.1	13.0	04.1	24.0	23	-02.5	02	10	C4.4	.	.	24	C4.0	10	02.0	10	02.7	01	01.0	14	02.4	06	C3.0	19		
IV	-	07.1	13.9	09.1	09.6	15.1	05.1	21.5	30	01.9	20	09	C5.1	.	.	25	C2.2	11	C3.1	C7	C3.3	01	02.0	12	C4.4	14	04.9	11		
V	-	12.3	18.7	13.6	14.6	20.3	05.5	25.5	31	05.2	06	08	C4.5	C2	03.0	17	C1.1	C8	03.0	C3	02.0	04	03.2	19	02.1	16	C4.6	16		
VI	-	17.0	23.9	17.9	19.2	25.7	13.5	31.5	29	07.1	13	09	C5.1	C1	03.0	10	C2.0	C6	03.2	C2	02.5	25	03.3	21	04.3	12				
VII	-	19.4	28.5	21.0	22.5	29.7	15.1	37.5	17	09.7	10	16	C4.1	C1	03.0	14	C4.8	C6	03.0	C1	03.0	23	03.1	14	C5.1	29				
VIII	-	19.9	24.9	21.9	23.1	30.2	16.7	36.0	05	12.2	31	15	C3.1	C1	03.0	14	C2.8	C5	03.7	C5	03.8	03	03.7	16	03.2	09	04.8	27		
IX	-	14.8	24.8	17.4	18.6	25.6	12.5	31.5	03	06.0	28	05	C2.6	C2	01.0	13	C2.2	C3	04.6	C4	02.5	07	03.3	20	02.8	03	05.7	33		
X	-	10.5	15.7	12.9	13.6	19.1	08.8	24.4	15	-01.7	28	07	C0.4	03	02.3	23	C0.0	C8	03.4	C3	03.0	.	.	10	01.9	08	02.5	21		
XI	-	04.7	11.2	06.2	07.1	11.9	03.4	15.4	06	-06.0	03	10	C3.4	.	.	17	C1.7	C3	02.3	C4	04	04.0	.	.	22	02.2	10	03.6	24	
XII	-	01.0	05.8	02.1	02.8	07.0	-06.6	12.1	04	-05.5	18	25	C0.4	.	.	05	C1.4	C1	01.0	05	C0.2	01	01.0	.	.	27	03.0	15	C3.6	19
GOD.	-	09.7	16.6	11.4	12.3	17.8	07.5	37.5	KGW	-06.5	KGW	170	C0.4	11	C2.6	110	C1.4	C5	C2.4	80	C2.2	79	C2.3	37	C2.4	02	04.0	325	04.4	245
$\varphi = 41^{\circ}09'N \lambda = 22^{\circ}30'E$ Gr. AG = + 1h 30 min.																														
GEVGELIJA																														
BR. ST.278																														
I	-	02.2	07.8	03.7	04.3	08.6	00.5	12.3	28.20	-05.6	15	16	C2.8	C2	01.5	C3	01.5	C7	04.3	C8	01.5	04	02.0	.	.	.	19	C4.5	37	
II	-	04.2	10.6	06.3	06.8	11.0	02.6	16.8	11	-06.4	02	09	C3.4	.	.	C1	03.0	19	C1.5	C3	01.7	08	01.5	01	02.0	18	C3.6	25		
III	-	05.3	13.3	08.6	09.6	14.1	03.4	24.0	21	-04.4	02	07	C0.9	02	01.5	C1.0	01.0	35	C1.6	07	01.9	06	01.0	04	04.8	09	C3.3	27		
IV	-	08.6	15.4	10.6	11.2	16.6	05.6	22.4	27	-06.3	10	09	C2.6	C1	01.0	06	01.0	38	C1.7	06	01.0	03	02.0	01	01.0	.	11	C3.9	16	
V	-	14.9	21.8	15.5	16.9	23.0	10.6	27.4	14	03.5	06	10	C2.1	C4	01.2	C5	01.0	16	C1.6	C6	01.4	01	02.0	02	02.5	19	C1.7	22		
VI	-	19.6	26.6	20.2	21.6	27.6	14.0	34.0	29	09.5	15	20	C3.1	C2	03.4	C5	01.2	21	C1.8	C2	01.5	C2	02.5	02	C1.0	20	C1.8	10		
VII	-	21.6	30.8	23.0	24.6	31.7	16.3	37.9	17	17.16	12	13	C3.4	C5	01.8	C7	01.1	18	C1.4	C3	01.0	05	01.0	05	01.2	07	01.0	22	C0.0	22
VIII	-	21.0	31.4	23.9	25.0	32.0	17.1	37.4	14	14.4	11	13	C2.5	C2	01.5	C9	01.4	25	C0.5	C1.0	06	01.5	06	01.0	02	01.0	18	C0.3	13	
IX	-	16.2	26.8	18.1	19.8	27.5	12.7	32.1	03	03.6	29	06	C2.7	C4	02.6	C5	01.6	24	C1.6	C3	02.3	.	.	.</						

Mesec	Obnovljenost Nm (0-10)				Vlažnost vazduha %	Padavine R mm				Broj dana na snazi:																										
										Tr	Tx	In	Ix	Ts	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	≡	☒								
	7	14	21	Sred. (dani) Temeplat (sati)	em mm	7	14	21	Seč. mm	Min.	Σ	xx %	nat.	0,00,0	0,025,0	0,020,0	6	8	2,0	8,0	0,1	1,00,0,0														
<b>KCCANI</b>																																				
BR. ST.276																																				
I	6.6	6.3	6.0	6.3	-	05,1	91	84	90	PF	62	042	017,0	02	-	-	17	-	-	-	-	05	13	10	05	01	04	-	-	-	-	04				
II	6.4	5.8	5.4	6.1	-	06,1	86	76	86	PF	51	051	015,4	06	-	-	09	-	-	-	-	01	05	13	06	04	04	-	-	-	-	01				
III	6.5	5.8	6.0	6.1	-	05,5	84	63	74	74	35	032	020,0	07	-	-	02	-	-	-	-	05	12	07	05	01	04	-	-	-	-	01				
IV	5.7	6.1	6.4	6.3	-	07,0	84	60	72	72	43	030	011,5	15	-	-	09	-	-	-	-	01	01	16	08	06	01	08	-	-	-	-	01			
V	5.6	5.5	5.5	5.8	-	05,6	83	81	74	73	37	095	030,5	16	-	-	02	-	-	-	-	02	03	06	12	02	15	-	-	-	-	01				
VI	4,1	5,0	5,2	4,8	-	12,2	80	55	73	69	40	058	014,5	08	-	-	21	03	-	-	-	01	02	02	06	07	02	06	-	-	-	-	01			
VII	2,4	2,1	2,3	2,6	-	12,6	81	44	65	63	24	013	007,5	01	-	-	25	16	01	02	02	16	02	06	05	06	06	-	-	-	-	01				
VIII	2,7	3,0	3,4	3,0	-	11,2	73	33	56	56	16	044	004,4	24	-	-	29	16	02	-	-	09	05	04	05	04	05	-	-	-	-	04				
IX	2,8	4,3	3,2	3,5	-	11,1	85	48	77	70	28	0,04	014,5	27	-	-	21	04	-	01	-	13	02	04	04	01	06	-	-	-	-	03				
X	5,4	5,5	4,6	5,2	-	05,7	84	64	83	77	35	052	026,2	22	-	-	01	-	-	-	-	01	05	04	14	28	02	12	-	-	-	-	01			
XI	5,5	5,9	6,0	6,3	-	06,7	89	81	86	85	62	026	015,7	01	-	-	05	-	-	-	-	05	12	08	04	01	07	-	-	-	-	04				
XII	5,7	6,0	5,5	5,7	-	04,4	90	60	79	76	55	043	013,7	15	-	-	21	-	-	-	-	07	06	08	03	01	07	02	-	-	-	03	01			
GOD.	5,0	5,2	5,1	5,1	-	08,6	84	62	77	74	16	491	030,5	1,00	-	-	55	98	36	03	05	02	76	88	96	80	16	91	06	-	-	-	01	10	07	05
<b>RACOVIS</b>																																				
BR. ST.277																																				
I	6,7	6,5	5,4	6,2	-	04,6	85	76	87	84	55	042	014,6	02	-	-	15	-	-	-	-	05	07	05	11	12	10	01	01	02	-	-	03	02		
II	6,7	6,4	5,4	6,2	-	05,4	66	65	79	77	42	067	022,0	20	-	-	07	-	-	-	-	01	02	07	12	07	06	04	07	-	-	-	01			
III	6,6	5,5	5,8	6,2	-	05,0	80	60	78	74	28	043	019,5	07	-	-	02	-	-	-	-	08	12	09	08	01	06	02	01	-	-	01				
IV	5,4	7,1	4,7	5,7	-	06,2	78	54	72	68	34	042	014,6	15	-	-	04	-	-	-	-	03	03	09	10	06	01	10	-	-	-	03				
V	5,6	6,4	5,0	5,6	-	08,5	71	58	75	71	33	061	016,8	19	-	-	01	-	-	-	-	04	02	03	06	15	11	02	15	-	-	-	06			
VI	3,7	4,0	4,6	4,3	-	10,9	75	51	70	65	30	054	010,4	17	-	-	20	02	-	-	-	05	01	11	08	02	11	-	-	-	-	10				
VII	1,3	2,2	1,3	1,6	-	10,9	64	37	58	53	22	003	018,8	02	-	-	26	16	01	07	07	22	02	02	02	02	02	-	-	-	-	04				
VIII	2,7	2,7	2,3	2,6	-	11,8	69	40	61	57	24	004	002,0	29	-	-	26	17	01	04	04	13	05	02	05	-	-	-	-	05						
IX	2,6	3,7	1,6	2,7	-	10,3	80	44	72	65	23	038	016,3	26	-	-	20	02	-	03	01	15	01	06	06	01	06	-	-	-	05					
X	5,4	5,7	3,4	4,9	-	08,6	85	57	75	72	19	051	034,4	27	-	-	01	-	-	-	-	02	04	06	11	10	01	11	-	-	-	04				
XI	5,0	6,2	4,2	4,5	-	06,2	90	69	84	81	42	044	020,9	09	-	-	02	-	-	-	-	02	08	07	06	02	05	-	-	-	04					
XII	4,7	3,9	3,5	4,0	-	04,5	65	69	81	78	46	036	008,6	14	-	-	20	-	-	-	-	05	05	08	06	07	02	-	-	-	05					
GOD.	4,7	4,9	4,0	4,5	-	07,8	80	57	74	70	16	487	032,4	22,0	-	-	47	95	37	04	44	03	102	76	105	63	35	101	10	05	-	-	42	10	03	
<b>GEVGELIJA</b>																																				
BR. ST.278																																				
I	6,4	6,2	5,6	6,1	-	05,4	89	79	85	84	54	092	024,1	02	-	-	17	-	-	-	-	07	-	-	-	-	-	-	-	-	-	01				
II	6,9	6,5	6,5	6,6	-	05,5	85	71	79	65	45	104	035,2	20	-	-	07	-	-	-	-	02	-	-	-	-	-	-	-	-	-	02				
III	6,3	6,3	5,9	5,3	-	07,2	91	73	86	83	43	086	017,2	05	-	-	07	-	-	-	-	06	14	10	09	04	10	-	-	-	-	01				
IV	5,2	6,2	5,4	5,8	-	07,7	64	64	81	76	38	105	034,6	15	-	-	01	-	-	-	-	01	07	12	08	03	12	-	-	-	-	01				
V	3,9	5,7	4,5	4,7	-	09,6	73	51	74	66	23	061	014,5	30	-	-	11	08	-	-	-	02	03	03	14	04	02	14	-	-	-	04				
VII	3,5	4,8	4,2	4,2	-	11,8	68	49	63	60	32	033	013,1	17	-	-	25	07	01	03	-	06	22	07	02	01	07	-	-	-	06					
VIII	2,9	3,6	3,0	3,2	-	13,2	68	40	62	56	21	001	000,6	21	-	-	31	24	07	01	-	04	-	01	-	-	-	-	-	05						
IX	3,0	4,2	2,6	3,3	-	11,0	79	48	79	66	22	022	012,5	08	-	-	25	10	01	01	-	15	02	06	04	01	04	-	-	-	02					
X	4,9	5,4	4,2	4,9	-	05,4	87	52	80	73	32	080	046,5	22	-	-	02	09	-	-	-	01	05	05	09	07	02	05	-	-	01					
XI	6,6	6,8	4,9	5,2	-	06,6	88	66	85	80	40	083	046,0	08	-	-	07	07	-	-	-	08	06	10	02	10	09	-	-	-	02					
XII	5,7	4,9	4,9	5,2	-	05,1	65	63	46	77	41	056	039,2	14	-	-	19	-	-	-	-	05	08	05	05	01	02	02	-	-	01					
GOD.	4,5	5,2	4,4	4,7	-	08,9	78	53	67	66	22	600	037,0	20,0	-	-	21	129	65	08	13	114	87	72	69	19	10	02	-	-	02	22	10			
<b>VALANDOVC</b>																																				
BR. ST.279																																				
I	6,4	6,1	4,7	5,7	-	04,8	82	64	79	75	35	052	014,5	02	-	-	09	-	-	-	-	02	-	-	08	12	04	01	06	-	-	-	01			
II	6,9	6,6	6,0	6,5	-	05,8	81	61	77	73	29	098	033,2	20	-	-	05	05	-	-	-	01	07	15	08	07	04	04	-	-	-	01				
III	6,5	6,5	5,8	6,3	-	06,2	85	57	70	71	27	043	014,5	07	-	-	02	-	-	-	-	06	14	10	08	06	01	08	-	-	-	01				
IV	6,3	7,7	5,4	6,5	-	07,1	80	57	70	69	33	070	033,2	15	-	-	01	-	-	-	-	07	01	12	10	09	01	14	-	-	-	02				
V</																																				

Mesec	Vazdušni pritisak: P <sub>0</sub> : 1013 hPa	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	R	BL	E	SE	S	SW	W	NW	C									
		7	14	21																								
$\Delta G = +1h\ 31\text{ min.}$																												
I	-	02.7	06.1	03.4	03.9	06.4	01.2	22	-04.0	15	+	05.5	.	.	15	02.9	.	.	.	.	.	25	04.4	53				
II	-	05.2	09.3	04.3	06.8	10.2	03.8	15.0	16.11	-01.5	02	00	05.5	.	.	16	02.6	.	.	.	.	.	17	04.7	49			
III	-	06.4	11.6	07.9	08.4	14.6	05.1	22.0	23.21	-01.2	02	.	.	.	19	02.8	.	.	.	.	.	.	08	02.4	66			
IV	-	09.3	14.3	09.6	10.7	15.6	06.9	21.0	13	04.0	10	03	04.3	.	.	11	04.3	.	.	.	.	.	18	03.5	50			
V	-	14.6	20.7	14.8	16.2	21.9	11.8	26.7	31	07.4	06	.	.	.	14	03.5	.	.	.	.	.	.	36	03.7	67			
VI	-	19.7	25.8	19.4	21.1	27.2	16.3	34.0	29	05.6	13	.	.	.	08	02.1	.	.	03	01.3	.	.	27	03.7	52			
VII	-	22.0	29.8	22.7	24.2	31.2	17.3	39.4	16	14.0	09	.	.	.	01	07.0	.	.	03	01.7	.	.	35	04.1	54			
VIII	-	24.1	30.5	23.1	24.7	31.8	19.4	36.1	20.03	17.6	22.13	.	.	.	10	07.5	.	.	05	01.8	.	.	01	03.0	23			
IX	-	17.6	25.4	18.3	19.9	24.4	15.4	32.0	C3	05.5	29	.	.	.	C2	02.0	.	.	C4	01.0	.	.	17	03.3	67			
X	-	13.5	19.9	14.7	15.7	20.7	11.9	26.5	24	04.2	31	.	.	.	17	03.2	.	.	C9	02.9	.	.	15	02.9	52			
XI	-	07.4	12.5	06.2	C9.1	13.1	06.2	16.0	14.06	02.5	04	01	03.0	.	.	12	03.5	.	.	01	02.5	04	02.2	34				
XII	-	03.7	08.6	05.0	05.6	C9.6	01.9	14.0	04	-02.0	11	.	.	.	C1	01.0	.	.	01	02.0	57	C3.8	34					
GOD.	-	12.0	17.9	12.8	13.9	18.9	09.9	39.4	4.01	-04.0	C1.1	66	04.5	.	.	116	03.1	.	.	38	02.4	.	.	02	02.5	297		
$\Delta G = 41^{\circ}38'N \times 22^{\circ}46'E$ Gr. +1h 31 min.																												
I	-	-01.0	04.2	00.2	06.9	04.8	-03.0	08.6	23	-12.0	16	18	01.8	C3	01.7	C7	C1.0	C1	02.0	C5	C1.0	02	C2.5	56				
II	-	00.4	06.3	02.2	03.4	C8.8	-01.9	15.0	16	-06.0	02	15	C2.2	07	04.7	.	08	04.2	01	08.0	06	C2.2	08	01.6	02	C1.5	36	
III	-	01.8	11.3	06.4	04.5	12.1	00.4	24.5	22	-08.5	02	20	C1.8	03	02.3	C9	C1.3	04	01.8	09	01.3	02	02.5	08	01.2	04	C2.2	34
IV	-	03.9	12.9	07.7	08.1	13.5	01.5	21.5	10	-03.0	04	13	C2.2	08	01.7	10	C1.2	10	03.6	C6	02.7	03	03.7	10	02.4	08	C2.7	28
V	-	10.3	17.5	12.5	13.2	18.2	04.2	23.5	26.12	01.5	26.16	07	C2.6	02	01.5	C9	C1.4	C5	03.7	08	C1.8	03	01.7	10	02.5	C3	C2.0	43
VI	-	15.1	22.3	16.3	17.5	22.6	09.5	24.0	28	03.0	17	06	C2.5	03	03.0	C4	C1.3	08	02.6	06	01.7	12	02.3	11	02.3	09	C2.3	34
VII	-	17.0	24.6	17.6	15.8	27.1	16.6	35.5	18	04.0	10	15	C2.4	05	01.0	C4	C1.0	02	02.0	06	C1.5	03	02.4	05	C3.0	43		
VIII	-	16.7	27.7	19.9	21.0	28.1	11.3	35.0	06	04.5	11	11	C2.7	08	01.9	06	C2.0	04	03.0	07	C1.7	04	02.2	07	02.0	C5	C2.4	41
IX	-	12.1	23.6	15.0	16.5	24.0	00.2	31.0	04	-01.5	28	06	C2.3	04	04.0	C5	C1.6	06	02.0	18	C1.6	10	02.9	07	02.6	C6	C1.7	30
X	-	07.7	16.7	10.7	11.4	17.6	04.4	22.5	05	-04.5	28	01	C2.0	01	03.0	C5	C1.2	06	04.8	21	03.0	04	02.8	18	02.0	02	C2.5	24
XI	-	01.4	10.8	03.8	04.9	11.2	-02.3	14.6	20	-05.5	17.16	07	C2.7	03	04.0	C6	C1.8	C3	04.0	09	02.3	*	*	15	07.5	04	C3.0	43
XII	-	-02.5	05.5	-00.5	06.5	05.9	-04.2	10.5	13	-10.5	25	17	C2.2	03	04.0	C4	C1.0	02	02.5	10	C1.5	*	*	06	01.7	04	C4.5	47
GOD.	-	06.9	15.6	09.4	10.3	16.2	03.4	35.5	35.6	-12.0	C1.1	119	02.2	44	03.2	C3	C1.4	59	03.2	104	02.0	54	02.7	109	02.1	50	C2.5	41
$\Delta G = 41^{\circ}13'N \times 22^{\circ}51'E$ Gr. +1h 31 min.																												
I	682.6	-02.6	02.6	-C1.1	-00.5	03.5	-04.3	09.0	03	-12.7	16	17	C1.8	C3	C1.3	*	*	C3	C1.2	C4	01.8	C2	02.0	*	*	07	01.0	56
II	688.2	-00.8	06.5	01.0	01.9	C7.6	-02.5	13.2	12	-08.6	01	17	C1.6	C7	C1.5	*	*	15	02.9	C2	02.5	03	01.7	01	02.0	01	C1.0	43
III	690.1	01.4	C9.6	04.6	10.9	-00.5	22.0	21	-08.2	02	11	C1.3	C2	C1.5	*	*	14	01.8	C5	01.4	10	01.5	02	01.5	04	C1.5	45	
IV	684.4	03.8	10.7	C5.2	06.2	12.1	00.3	15.8	10	-05.0	03	16	C1.7	04	02.0	*	*	14	02.6	C2	02.5	09	02.1	02	02.5	05	C2.0	40
V	687.5	09.3	15.1	09.8	11.0	17.1	04.8	23.0	31	-00.7	06	15	C1.6	C2	C1.0	*	*	C4	02.0	C8	C2.6	C3	03.0	*	*	07	C1.7	54
VI	688.6	13.3	20.3	15.7	15.2	22.0	06.8	27.6	29	01.3	13	19	C1.9	C7	02.0	*	*	01	02.0	10	01.8	07	02.6	02	03.0	05	C2.0	48
VII	690.7	14.4	24.3	15.9	17.7	25.3	09.3	32.4	17	03.4	10	22	C1.6	C2	C1.5	C3	C1.0	01	02.0	01	02.0	06	02.2	14	02.0	43		
VIII	691.2	14.9	24.6	16.6	18.2	26.4	10.2	31.6	06	06.5	12	20	C1.7	04	02.0	*	*	C3	02.0	C4	02.0	02	02.0	01	02.0	07	C2.0	57
IX	691.0	05.8	21.5	12.5	14.3	22.9	06.8	26.7	04	-02.0	28	09	C1.0	*	*	*	C5	01.8	C7	C2.4	04	02.2	01	01.0	08	C2.1	61	
X	687.6	06.1	15.5	08.4	09.8	16.7	03.7	21.8	15	-06.6	28	03	C2.0	01	01.0	01	01.0	10	02.1	24	02.4	08	02.1	*	*	02	C1.5	44
XI	691.1	00.2	09.4	02.1	03.6	10.6	-01.2	16.8	18	-05.6	16.16	08	C1.6	C2	C1.5	C3	C1.0	01	02.0	07	01.9	01	02.0	07	01.4	56		
XII	690.5	-04.1	04.1	-02.5	-01.3	05.3	-06.3	16.8	11	-12.8	18	17	C1.9	C3	C1.3	*	*	C2	02.5	C1	03.0	*	*	*	*	03	C1.3	67
GOD.	685.6	05.5	13.7	07.2	08.4	15.0	02.4	32.4	32.4	-12.8	61	169	C1.7	25	C1.6	C2	C1.0	75	02.2	74	02.2	61	02.1</td					

Mjesec	Oblačnost Nm (0-10)			Insolacija Troj sati	Vlažnost vazduha						Padavine R/mm		Broj dana na sat																		
	7	14	21		mm	7	14	21	Sred.	Ned.	Σ	Max	Dan.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	▲	R	T	≡
<b>NEVI DEJMAN</b>																															
BR. ST. 281																															
I 6.8 6.0 5.0 5.9	-	05.5	91 85 85 88 55	C70 028.0	02	.	.	06	*	*	*	03	*	09	14	08	08	C2	08	01	01	*	*	*	*	*	*	*	*	03	
II 6.6 6.0 5.6 6.1	-	06.4	90 78 86 85 60	C70 C24.0	20	.	.	04	*	*	*	03	*	06	13	06	06	04	06	*	*	*	*	*	*	*	*	*	*	*	
III 6.7 6.3 6.0 6.3	-	07.6	92 81 91 88 66	070 027.0	07	.	.	01	*	*	*	03	*	08	17	09	09	02	09	*	*	*	*	*	*	*	*	*	*	01	
IV 6.0 6.5 4.2 5.6	-	08.5	88 79 88 85 52	C66 C31.0	15	.	.	*	*	*	*	05	*	05	09	09	09	02	09	*	*	*	*	*	*	*	*	*	*	04	
V 4.1 4.0 4.3 5.4	-	11.3	82 71 84 79 49	065 014.3	30	.	.	06	*	*	*	05	*	05	09	08	08	03	08	*	*	*	*	*	*	*	*	*	05	*	
VI 4.2 4.6 4.6 4.4	-	15.1	81 71 80 77 51	C34 C13.0	17	.	.	22	C7	02	04	09	05	07	07	01	07	*	*	*	*	*	*	*	*	*	*	01	07		
VII 1.1 1.5 1.7 1.5	-	16.2	73 61 69 68 42	011 006.3	01	.	.	26	20	06	04	23	C1	07	02	*	02	*	*	*	*	*	*	*	*	*	*	01	*		
VIII 3.0 2.6 3.6 3.1	-	16.3	74 58 72 68 41	001 001.0	21	.	.	31	21	10	02	15	03	01	01	*	01	*	*	*	*	*	*	*	*	*	*	03	*		
IX 3.6 3.6 1.4 2.9	-	13.9	82 67 83 77 40	049 031.0	08	.	.	21	04	*	01	15	C1	04	04	02	04	*	*	*	*	*	*	*	*	*	02	*			
X 6.4 5.5 3.5 5.1	-	10.9	83 70 84 79 35	C36 C21.0	22	.	.	03	*	*	*	08	C1	04	04	01	04	*	*	*	*	*	*	*	*	*	*	01	*		
XI 5.5 4.3 4.6 4.8	-	07.8	91 63 90 88 58	110 037.0	06	.	.	05	*	*	*	09	05	08	08	04	08	*	*	*	*	*	*	*	*	*	*	04			
XII 4.5 4.2 4.0 4.2	-	05.6	86 76 62 61 61	C14 C11.0	31	.	.	05	*	*	*	05	*	12	06	04	02	01	04	*	*	*	*	*	*	*	*	*	*		
GOD. 5.0 4.8 4.0 4.6	-	10.4	84 73 83 80 35	59K 037.0	18.0	.	.	16	111	52	18	34	*	124	95	70	68	22	70	01	01	*	*	*	*	*	01	24	07		
<b>DELČEVC</b>																															
BR. ST. 282																															
I 7.5 5.4 5.2 6.0	-	04.1	80 76 85 80 51	C44 C15.0	18	02	.	24	*	*	*	08	13	13	11	03	06	C5	01	*	*	*	*	*	*	*	*	*	07		
II 6.1 4.9 4.5 5.2	-	04.5	83 60 84 76 34	050 014.5	08	.	.	19	*	*	*	05	02	09	10	05	04	02	05	*	*	*	*	*	*	*	*	*	01	01	
III 7.2 5.2 6.2 6.2	-	05.3	87 75 77 74 25	050 C18.5	29	.	.	10	*	*	*	08	14	09	08	02	09	05	04	*	*	*	*	*	*	*	*	*	01		
IV 5.5 5.7 3.8 5.0	-	6.1	78 65 75 71 79	021 C06.0	17	.	.	09	*	*	*	01	01	07	07	06	04	*	06	*	*	*	*	*	*	*	*	01			
V 5.7 4.6 5.0 5.9	-	06.3	84 57 76 72 33	101 022.0	06	.	.	*	*	*	*	01	04	06	14	13	04	14	*	*	*	*	*	*	*	*	*	07			
VI 4.6 4.4 4.1 4.5	-	10.6	78 55 77 70 33	070 012.0	02	.	.	11	*	*	*	02	01	06	02	12	11	03	12	*	*	*	*	*	*	*	*	04	01		
VII 3.3 3.1 2.2 2.5	-	12.2	74 54 75 68 31	C24 012.0	01	.	.	21	11	*	*	15	03	05	05	01	05	*	*	*	*	*	*	*	*	*	01	*			
VIII 2.3 2.4 2.0 2.9	-	11.7	77 46 68 63 15	C43 014.6	25	.	.	25	09	*	05	13	*	07	05	02	07	*	*	*	*	*	*	*	*	*	05				
IX 2.5 3.6 2.2 2.8	-	10.2	86 51 79 72 28	034 016.8	06	.	.	02	16	01	*	02	*	14	01	06	04	01	06	*	*	*	*	*	*	*	05	01			
X 5.1 4.9 4.2 4.7	-	08.1	88 64 80 77 27	076 040.0	22	.	.	05	*	*	*	04	01	03	03	14	10	01	14	*	*	*	*	*	*	*	01	01			
XI 7.3 4.6 3.8 5.3	-	05.6	90 69 89 93 40	060 015.6	01	.	.	17	*	*	*	03	*	05	08	06	06	03	06	*	*	*	*	*	*	*	*	09			
XII 5.7 5.0 4.7 5.1	-	04.2	84 78 91 84 49	C35 030.2	15	01	.	28	*	*	*	01	*	08	07	05	02	01	04	01	*	*	*	*	*	*	*	04	12		
GOD. 5.2 4.7 4.1 4.6	-	07.5	83 60 80 74 16	634 040.0	22.0	03	.	114	73	21	*	22	06	100	74	102	83	23	94	15	05	*	*	*	*	*	17	19	20		
<b>BERGVC</b>																															
BR. ST. 283																															
I 7.7 7.3 6.0 7.0	-	089.4	03.8 92 70 88 36	048 020.2	02	03	02	26	*	*	*	06	17	12	08	01	04	C1	01	*	*	*	*	*	*	*	*	*	11		
II 7.1 6.8 4.5 6.1	-	112.7	04.4 92 64 87 81	30 055 017.7	08	.	.	23	*	*	*	05	10	08	05	03	07	04	02	*	*	*	*	*	*	*	*	*	01		
III 7.3 6.5 4.6 6.2	-	138.6	04.9 93 57 84 78	19 047 019.6	07	.	.	18	*	*	*	04	14	10	07	01	06	06	02	*	*	*	*	*	*	*	*	02			
IV 6.4 6.3 5.1 6.6	-	162.5	05.5 92 57 82 77	32 058 021.6	15	.	.	13	*	*	*	01	01	11	14	09	02	14	01	*	*	*	*	*	*	*	*	03			
V 6.6 7.9 5.1 6.5	-	212.9	07.7 89 58 85 77	28 082 019.0	19	.	.	01	*	*	*	07	00	18	13	07	18	*	*	*	*	*	*	*	*	*	14				
VI 5.6 7.3 4.6 5.8	-	278.6	09.7 66 53 85 74	35 150 036.6	19	.	.	04	*	*	*	01	*	03	06	15	11	05	15	*	*	*	*	*	*	*	*	07			
VII 2.3 5.3 1.5 3.0	-	368.0	10.0 84 42 75 67	28 023 C11.0	21	.	.	21	C1	*	*	12	*	05	02	01	05	*	*	*	*	*	*	*	*	*	03				
VIII 3.1 5.8 2.5 3.8	-	311.4	10.1 83 43 72 66	27 027 014.2	25	.	.	11	06	*	*	07	02	08	05	01	08	*	*	*	*	*	*	*	*	*	10				
IX 3.1 5.4 1.9 3.5	-	260.0	08.5 91 43 82 72	14 011 004.7	26	.	.	01	08	*	*	08	01	06	03	*	06	*	*	*	*	*	*	*	*	03					
X 6.1 7.8 3.9 5.9	-	180.4	06.0 91 72 81 75	29 075 C25.7	22	.	.	09	*	*	*	10	15	10	03	15	*	*	*	*	*	*	*	*	*	01					
XI 6.1 5.5 4.0 5.7	-	147.3	04.8 94 58 90 81	30 036 C12.7	01	.	.	17	*	*	*	08	10	07	05	01	07	*	*	*	*	*	*	*	*	01					
XII 5.7 5.9 3.1 4.1	-	110.7	03.6 93 67 91 84	24 040 018.4	15	05	.	30	*	*	*	05	06	10	05	01	06	07	01	*	*	*	*	*	*	*	*	17			
GOD. 5.6 6.7 3.9 5.4	-	2372.5	06.4 90 55 83 78	19 647 036.6	110	08	02	138	53	11	*	02	*	61	96	128	84	21	111	27	06	*	*	*	*	*	33	03			



SAVEZNI HIDROMETEOROLOŠKI ZAVOD  
Klimatološko odeljenje

## METEOROLOŠKE STANICE U 1974